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EVALUATION OF FLARED APPROACH GUARDRAIL TRANSITIONS: TEST NO. FLAGT-1

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Submitted to

MIDWEST POOLED FUND PROGRAM

Nebraska Department of Transportation 1500 Nebraska Highway 2 Lincoln, Nebraska 68502

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16. Abstract

Approach guardrail transitions (AGTs) are used to safely connect guardrail to rigid parapets, such as bridge rails. Ideally, AGTs are installed tangent to the roadway and the bridge rail. However, there was a desire to install AGTs flared away from the roadway to satisfy geometry constraints or to shorten system lengths. Phase I of this study used LS-DYNA simulation to explore the performance of AGTs flared away from the roadway. Ultimately, a 15:1 flare rate was identified as the critical maximum flare rate for AGTs that would remain crashworthy.

Phase II of this project consisted of full-scale crash testing in accordance with Test Level 3 (TL-3) criteria of the American Association of State and Highway and Transportation Officials' (AASHTO) *Manual for Assessing Safety Hardware* (MASH). In test no. FLAGT-1, the 2270P vehicle impacted the system at an angle 25.4 degrees relative to the roadway and a speed of 63.3 mph. The 2270P pickup truck was contained and redirected by the flared AGT. However, the vehicle snagged on the system at the upstream edge of the concrete buttress, which resulted in excessive occupant compartment deformations to the toe pan and wheel well, as well as an excessive longitudinal acceleration of -24.2 g's. Thus, test no. FLAGT-1 failed to satisfy the safety performance criteria of MASH test designation no. 3-11.

17. Key Words		18. Distribution Statement		
Highway Safety, Crash Test, Roadside Appurtenances, Compliance Test, MASH 2016, Test Level 3, Approach Guardrail Transition, AGT, Flare, Flared Guardrail		No restrictions. This document is available through the National Technical Information Service. 5285 Port Royal Road Springfield, VA 22161		
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DISCLAIMER STATEMENT

This material is based upon work supported by the Federal Highway Administration, U.S. Department of Transportation and the Midwest Pooled Fund Program under TPF-5(430) Supplement #3. The contents of this report reflect the views and opinions of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the University of Nebraska-Lincoln, state highway departments participating in the Midwest Pooled Fund Program nor the Federal Highway Administration, U.S. Department of Transportation. This report does not constitute a standard, specification, or regulation. Trade or manufacturers' names, which may appear in this report, are cited only because they are considered essential to the objectives of the report. The United States (U.S.) government and the State of Nebraska do not endorse products or manufacturers.

UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

A2LA ACCREDITATION

The test reported herein is within the scope of MwRSF's A2LA Accreditation. MwRSF's accreditation documentation can be found in Appendix A.

INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority for the data contained herein was Dr. Andrew Loken, Research Assistant Professor.

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		N METRIC) CONVE			
APPROXIMATE CONVERSIONS TO SI UNITS					
Symbol	When You Know	Multiply By	To Find	Symbol	
		LENGTH			
in.	inches	25.4	millimeters	mm	
ft	feet	0.305	meters	m	
yd	yards	0.914	meters	m	
mi	miles	1.61	kilometers	km	
		AREA			
in ²	square inches	645.2	square millimeters	mm^2	
ft ²	square feet	0.093	square meters	m^2	
d^2	square yard	0.836	square meters	m^2	
ıc	acres	0.405	hectares	ha	
ni ²	square miles	2.59	square kilometers	km ²	
		VOLUME			
l oz	fluid ounces	29.57	milliliters	mL	
gal	gallons	3.785	liters	L	
ft ³	cubic feet	0.028	cubic meters	m^3	
d^3	cubic yards	0.765	cubic meters	m^3	
	NOTE:	volumes greater than 1,000 L shall	be shown in m ³		
		MASS			
oz	ounces	28.35	grams	g	
b	pounds	0.454	kilograms	kg	
Γ	short ton (2,000 lb)	0.907	megagrams (or "metric ton")	Mg (or "t")	
		TEMPERATURE (exact de	egrees)		
_		5(F-32)/9			
°F	Fahrenheit	or (F-32)/1.8	Celsius	°C	
		ILLUMINATION			
îc .	foot-candles	10.76	lux	lx	
1	foot-Lamberts	3.426	candela per square meter	cd/m ²	
		ORCE & PRESSURE or S		CG/III	
lbf		4.45	newtons	N	
lbf/in ²	poundforce per square inch	6.89		kPa	
101/111			kilopascals	KPa	
		MATE CONVERSIONS			
Symbol	When You Know	Multiply By	To Find	Symbol	
		LENGTH			
nm	millimeters	0.039	inches	in.	
n	meters	3.28	feet	ft	
n	meters	1.09	yards	yd	
cm	kilometers	0.621	miles	mi	
		AREA			
nm^2	square millimeters	0.0016	square inches	in^2	
n^2	square meters			ft ²	
		10.764	square reer		
n^2	•	10.764 1.195	square feet square vard		
	square meters	1.195	square yard	yd^2	
ıa	square meters hectares	1.195 2.47			
ıa	square meters	1.195 2.47 0.386	square yard acres	yd² ac	
m ² na km ²	square meters hectares square kilometers	1.195 2.47 0.386 VOLUME	square yard acres square miles	yd² ac mi²	
na km² nL	square meters hectares square kilometers milliliter	1.195 2.47 0.386 VOLUME 0.034	square yard acres square miles fluid ounces	yd² ac mi² fl oz	
na cm² mL	square meters hectares square kilometers milliliter liters	1.195 2.47 0.386 VOLUME 0.034 0.264	square yard acres square miles fluid ounces gallons	yd ² ac mi ² fl oz gal	
na km² mL m³	square meters hectares square kilometers milliliter liters cubic meters	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314	square yard acres square miles fluid ounces gallons cubic feet	yd ² ac mi ² fl oz gal ft ³	
na km² mL m³	square meters hectares square kilometers milliliter liters	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307	square yard acres square miles fluid ounces gallons	yd ² ac mi ² fl oz gal	
na km² mL c_ m³ m³	square meters hectares square kilometers milliliter liters cubic meters cubic meters	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS	square yard acres square miles fluid ounces gallons cubic feet cubic yards	yd² ac mi² fl oz gal ft³ yd³	
na m ² nL n ³ n ³	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces	yd² ac mi² fl oz gal ft³ yd³	
na nnL n ³ n ³	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds	yd² ac mi² fl oz gal ft³ yd³ oz lb	
a m ² nL n ³ n ³	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton")	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb)	yd² ac mi² fl oz gal ft³ yd³	
na cm² nL n³ n³ gg Mg (or "t")	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton")	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103 TEMPERATURE (exact de	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb) egrees)	yd² ac mi² fl oz gal ft³ yd³ oz lb T	
na cm² nL n³ n³ gg Mg (or "t")	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton")	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103 TEMPERATURE (exact de 1.8C+32	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb)	yd² ac mi² fl oz gal ft³ yd³ oz lb	
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na cm² nL n³ n³ gg/gg (or "t")	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton")	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103 TEMPERATURE (exact de 1.8C+32 ILLUMINATION 0.0929	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb) egrees) Fahrenheit foot-candles	yd² ac mi² fl oz gal ft³ yd³ oz lb T	
na cm² mL n³ n³ s g Mg (or "t")	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton") Celsius	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103 TEMPERATURE (exact de 1.8C+32 ILLUMINATION	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb) egrees) Fahrenheit	yd² ac mi² fl oz gal ft³ yd³ oz lb T	
na cm² mL n³ n³ s g Mg (or "t")	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton") Celsius lux candela per square meter	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103 TEMPERATURE (exact de 1.8C+32 ILLUMINATION 0.0929	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb) egrees) Fahrenheit foot-candles foot-Lamberts	yd² ac mi² fl oz gal ft³ yd³ oz lb T	
na cm² mL m³ m³ gg Mg (or "t")	square meters hectares square kilometers milliliter liters cubic meters cubic meters grams kilograms megagrams (or "metric ton") Celsius lux candela per square meter	1.195 2.47 0.386 VOLUME 0.034 0.264 35.314 1.307 MASS 0.035 2.202 1.103 TEMPERATURE (exact de 1.8C+32 ILLUMINATION 0.0929 0.2919	square yard acres square miles fluid ounces gallons cubic feet cubic yards ounces pounds short ton (2,000 lb) egrees) Fahrenheit foot-candles foot-Lamberts	yd² ac mi² fl oz gal ft³ yd³ oz lb T	

^{*}SI is the symbol for the International System of Units. Appropriate rounding should be made to comply with Section 4 of ASTM E380.

TABLE OF CONTENTS

DISCLAIMER STATEMENT	ii
UNCERTAINTY OF MEASUREMENT STATEMENT	ii
A2LA ACCREDITATION	ii
INDEPENDENT APPROVING AUTHORITY	ii
ACKNOWLEDGEMENTS	ii
LIST OF FIGURES	vii
LIST OF TABLES	X
1 INTRODUCTION	1
1.1 Background	
1.2 Objective	
1.3 Scope	
1.5 Scope	
2 FLARED AGT CONNECTION OPTIONS	3
2.1 Option 1: Flared Concrete Buttress	
2.2 Option 2: Tapered Concrete Buttress	
2.3 Option 3: Angled Connector Plate Assembly	
2.4 Option 4: Radiused Thrie-Beam Guardrail	
2.5 Discussion	
2.6 Vertical Slotted Terminal Connector	
3 TEST REQUIREMENTS AND EVALUATION CRITERIA	9
3.1 Test Requirements	
3.2 Evaluation Criteria	
3.3 Soil Strength Requirements	
4 DESIGN DETAILS	11
5 TEST CONDITIONS	42
5.1 Test Facility	42
5.2 Vehicle Tow and Guidance System	42
5.3 Test Vehicle	42
5.4 Simulated Occupant	47
5.5 Data Acquisition Systems	47
5.5.1 Accelerometers	47
5.5.2 Rate Transducers	47
5.5.3 Retroreflective Optic Speed Trap	47
5.5.4 Digital Photography	
6 FULL-SCALE CRASH TEST NO. FLAGT-1	50
6.1 Static Soil Test	50

50
50
58
65
68
69
71
74
76
79
80
83
120
122
125
AGT-1 131

LIST OF FIGURES

Figure 1. AGT Installation [1]	1
Figure 2. Option 1 – Flared Concrete Buttress	3
Figure 3. Option 2 – Tapered Concrete Buttress	4
Figure 4. Option 3 – Angled Connector Plate Assembly	4
Figure 5. Option 3 – Angled Connector Plate Assembly, Enlarged	
Figure 6. Option 4 – Radiused Thrie-Beam	5
Figure 7. 12.5-ft Long Radiused Thrie-Beam Section	5
Figure 8. Comparison of Guardrail Offset from Buttress Lower Chamfer	7
Figure 9. Vertical Slotted Terminal Connector	8
Figure 10. Test Installation Layout, Test No. FLAGT-1	
Figure 11. System Details, Test No. FLAGT-1	14
Figure 12. Thrie-beam End Connector and Buttress Details, Test No. FLAGT-1	
Figure 13. Post Nos. 3-10 Details, Test No. FLAGT-1	
Figure 14. Post Nos. 11-21 Details, Test No. FLAGT-1	17
Figure 15. Splice Detail, Test No. FLAGT-1	18
Figure 16. End Section Detail, Test No. FLAGT-1	19
Figure 17. BCT Anchor Details, Test No. FLAGT-1	
Figure 18. Buttress Details, Test No. FLAGT-1	21
Figure 19. Rebar Detail, Test No. FLAGT-1	
Figure 20. Rebar Detail Sections, Test No. FLAGT-1	23
Figure 21. Vertical Rebar Details, Test No. FLAGT-1	24
Figure 22. Horizontal Rebar Details, Test No. FLAGT-1	25
Figure 23. Post Nos. 3 through 9 Components, Test No. FLAGT-1	26
Figure 24. Post Nos. 10 through 15 Components, Test No. FLAGT-1	
Figure 25. Post Nos. 16 through 21 Components, Test No. FLAGT-1	
Figure 26. BCT Timber Post and Foundation Tube Details, Test No. FLAGT-1	
Figure 27. Ground Strut Details, Test No. FLAGT-1	
Figure 28. BCT Anchor Cable, Test No. FLAGT-1	
Figure 29. AGT Connector Plate Assembly, Test No. FLAGT-1	
Figure 30. AGT Connector Plate Assembly Face Plate Details, Test No. FLAGT-1	
Figure 31. AGT Connector Assembly Components, Test No. FLAGT-1	
Figure 32. Guardrail Section Details, Test No. FLAGT-1	
Figure 33. Rail Transition and Component Details, Test No. FLAGT-1	
Figure 34. Hardware, Test No. FLAGT-1	
Figure 35. Bill of Materials, Test No. FLAGT-1	
Figure 36. Bill of Materials, Cont., Test No. FLAGT-1	
Figure 37. Test Installation Photographs	
Figure 38. Test Installation Photographs	
Figure 39. Test Vehicle, Test No. FLAGT-1	
Figure 40. Test Vehicle's Interior Floorboards and Undercarriage, Test No. FLAGT-1	
Figure 41. Vehicle Dimensions, Test No. FLAGT-1	
Figure 42. Target Geometry, Test No. FLAGT-1	
Figure 43. Camera Locations, Speeds, and Lens Settings, Test No. FLAGT-1	49
Figure 44. Impact Location, Test No. FLAGT-1	
Figure 45. Sequential Photographs, Test No. FLAGT-1	53

Figure 46. Additional Sequential Photographs, Test No. FLAGT-1	54
Figure 47. Additional Documentary Photographs, Test No. FLAGT-1	55
Figure 48. Additional Documentary Photographs, Test No. FLAGT-1	56
Figure 49. Vehicle Final Position and Trajectory Marks, Test No. FLAGT-1	
Figure 50. System Damage, Test No. FLAGT-1	59
Figure 51. System Damage, Test No. FLAGT-1	60
Figure 52. Post Nos. 18 through 21 Damage, Test No. FLAGT-1	61
Figure 53. Post Nos. 15 through 17 Damage, Test No. FLAGT-1	
Figure 54. Soil Gaps, Test No. FLAGT-1	
Figure 55. Permanent Set Deflection, Dynamic Deflection, and Working Width, Test No.	
FLAGT-1	
Figure 56. Vehicle Damage, Test No. FLAGT-1	66
Figure 57. Vehicle Damage, Undercarriage and Occupant Compartment, Test No.	
FLAGT-1	67
Figure 58. Summary of Test Results and Sequential Photographs, Test No. FLAGT-1	70
Figure 59. Comparison of Longitudinal CFC 180 10-msec Extracted Average Accelerations	71
Figure 60. Overhead View of Test No. FLAGT-1, 95 ms after Impact	72
Figure A-1. Midwest Roadside Safety Facility A2LA Accreditation Certificate No. 2937.01	81
Figure A-2. Midwest Roadside Safety Facility Scope of Accreditation to ISO/IEC 17025	
Figure B-1. 12.5-ft Thrie Beam Guardrail, Test No. FLAGT-1 (Item No. a1)	87
Figure B-2. 6.25-ft Thrie Beam Guardrail, Test No. FLAGT-1 (Item No. a2)	87
Figure B-3. 10-ga. W-to-Thrie Transition Segment, Test No. FLAGT-1 (Item No. a3)	88
Figure B-4. 12.5-ft W-beam Guardrail, Test No. FLAGT-1 (Item No. a4)	
Figure B-5. 12.5-ft W-beam End Section, Test No. FLAGT-1 (Item No. a5)	89
Figure B-6. 10-ga Thrie Beam Terminal Connector, Test No. FLAGT-1 (Item No. a6)	90
Figure B-7. Buttress Concrete, Test No. FLAGT-1 (Item No. b1)	
Figure B-8. BCT Timber Posts, Test No. FLAGT-1 (Item No. c1)	92
Figure B-9. BCT Foundation Tube, Test No. FLAGT-1 (Item No. c2)	
Figure B-10. Strut and Yoke Assembly, Test No. FLAGT-1 (Item No. c3)	
Figure B-11. BCT Anchor Cable Assembly, Test No. FLAGT-1 (Item No. c4)	
Figure B-12. Anchor Bracket, Test No. FLAGT-1 (Item No. c5)	
Figure B-13. Anchor Bearing Plate, Test No. FLAGT-1 (Item No. c6)	95
Figure B-14. BCT Post Sleeve, Test No. FLAGT-1 (Item No. c7)	96
Figure B-15. 6-ft W6x8.5 Posts, Test No. FLAGT-1 (Item Nos. d1 and d2)	97
Figure B-16. 6.5-ft W6x8.5 Posts, Test No. FLAGT-1 (Item No. d3)	97
Figure B-17. 6-in. x 12-in. x 14-in. Timber Blockout, Test No. FLAGT-1 (Item No. d4)	98
Figure B-18. 6-in. x 12-in. x 19-in. Timber Blockout, Test No. FLAGT-1 (Item No. d5)	
Figure B-19. HSS4x7x ³ / ₁₆ Steel Blockout, Test No. FLAGT-1 (Item No. d6)	.100
Figure B-20. 16D Nail, Test No. FLAGT-1 (Item No. d7)	.101
Figure B-21. #4 Rebar, Test No. FLAGT-1 (Item Nos. e1 through e10)	.101
Figure B-22. 5%-in. x 14-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f1)	.102
Figure B-23. 5%-in. x 10-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f2)	.103
Figure B-24. 5/8-in. x 2-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f3)	
Figure B-25. 5/8-in. x 11/4-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f4)	
Figure B-26. 7/8-in. x 151/2-in. Heavy Hex Bolt, Test No. FLAGT-1 (Item No. f5)	
Figure B-27. 7/8-in. x 8-in. Hex Bolt, Test No. FLAGT-1 (Item No. f6)	.107
Figure R-28 %-in x 10-in Hex Rolt Test No. FLAGT-1 (Item No. f7)	108

Figure B-29. %-in. x 1½-in. Hex Bolt, Test No. FLAGT-1 (Item No. f8)	109
Figure B-30. 7%-in. Round Washer, Test No. FLAGT-1 (Item No. g1)	
Figure B-31. %-in. Round Washer, Test No. FLAGT-1 (Item No. g2)	111
Figure B-32. Square Washer Plate, Test No. FLAGT-1 (Item No. g3)	112
Figure B-33. 1-in. Round Washer, Test No. FLAGT-1 (Item No. g4)	112
Figure B-34. %-in. Heavy Hex Nut, Test No. FLAGT-1 (Item No. h1)	113
Figure B-35. %-in. Hex Nut, Test No. FLAGT-1 (Item No. h2)	114
Figure B-36. %-in. Heavy Hex Nut, Test No. FLAGT-1 (Item No. h3)	115
Figure B-37. %-in. Hex Nut, Test No. FLAGT-1 (Item No. h4)	116
Figure B-38. 1-in. Heavy Hex Nut, Test No. FLAGT-1 (Item No. h5)	117
Figure B-39. ³ / ₁₆ -in. AGT Connector Face Plate, Test No. FLAGT-1 (Item No. i1)	118
Figure B-40. 1/4-in. AGT Connector Gusset Plates, Test No. FLAGT-1 (Item Nos. i2	
through i7)	119
Figure C-1. Vehicle Mass Distribution, Test No. FLAGT-1	121
Figure D-1. Soil Strength, Initial Calibration Tests, Test No. FLAGT-1	123
Figure D-2. Static Soil Test, Test No. FLAGT-1	
Figure E-1. Floor Pan Deformation Data – Set 2, Test No. FLAGT-1	126
Figure E-2. Occupant Compartment Deformation Data - Set 2, Test No. FLAGT-1	127
Figure E-3. Maximum Occupant Compartment Deformations by Location, Test No.	
FLAGT-1	128
Figure E-4. Exterior Vehicle Crush (NASS) - Front, Test No. FLAGT-1	129
Figure E-5. Exterior Vehicle Crush (NASS) - Side, Test No. FLAGT-1	130
Figure F-1. 10-ms Average Longitudinal Deceleration (SLICE-1), Test No. FLAGT-1	132
Figure F-2. Longitudinal Occupant Impact Velocity (SLICE-1), Test No. FLAGT-1	132
Figure F-3. Longitudinal Occupant Displacement (SLICE-1), Test No. FLAGT-1	133
Figure F-4. 10-ms Average Lateral Deceleration (SLICE-1), Test No. FLAGT-1	133
Figure F-5. Lateral Occupant Impact Velocity (SLICE-1), Test No. FLAGT-1	134
Figure F-6. Lateral Occupant Displacement (SLICE-1), Test No. FLAGT-1	134
Figure F-7. Vehicle Angular Displacements (SLICE-1), Test No. FLAGT-1	135
Figure F-8. Acceleration Severity Index (SLICE-1), Test No. FLAGT-1	135
Figure F-9. 10-ms Average Longitudinal Deceleration (SLICE-2), Test No. FLAGT-1	136
Figure F-10. Longitudinal Occupant Impact Velocity (SLICE-2), Test No. FLAGT-1	136
Figure F-11. Longitudinal Occupant Displacement (SLICE-2), Test No. FLAGT-1	137
Figure F-12. 10-ms Average Lateral Deceleration (SLICE-2), Test No. FLAGT-1	137
Figure F-13. Lateral Occupant Impact Velocity (SLICE-2), Test No. FLAGT-1	138
Figure F-14. Lateral Occupant Displacement (SLICE-2), Test No. FLAGT-1	138
Figure F-15. Vehicle Angular Displacements (SLICE-2), Test No. FLAGT-1	
Figure F-16. Acceleration Severity Index (SLICE-2), Test No. FLAGT-1	

LIST OF TABLES

Table 1. MASH TL-3 Crash Test Matrix for AGT	9
Table 2. MASH Evaluation Criteria for Longitudinal Barrier	10
Table 3. Weather Conditions, Test No. FLAGT-1	50
Table 4. Sequential Description of Impact Events, Test No. FLAGT-1	52
Table 5. Maximum Occupant Compartment Intrusion by Location, Test No. FLAGT-1	68
Table 6. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. FLAGT-1	69
Table 7. Maximum Lateral Dynamic Deflections in AGT Posts	73
Table 8. Permanent Set Comparison, Test No. FLAGT-1, Simulation, and Test No.	
AGTB-2	73
Table 9. Summary of Safety Performance Evaluation	75
Table B-1. Bill of Materials, Test No. FLAGT-1	84
Table B-2. Bill of Materials, Test No. FLAGT-1, Cont.	85
Table B-3. Bill of Materials, Test No. FLAGT-1, Cont.	86

1 INTRODUCTION

1.1 Background

Approach guardrail transitions (AGTs) are commonly used to safeguard rigid hazards, including bridge railings and concrete parapets. A typical AGT is shown in Figure 1 [1]. AGT installations provide a gradual transition in lateral stiffness between semi-rigid guardrail and rigid bridge rail in order to prevent vehicle snag and pocketing within the barrier. Often, intersecting roadways or other roadside obstacles create space constraints that limit the ability to install an AGT within the desired area. Thus, a need exists to minimize the length of AGTs tangent to the roadway.



Figure 1. AGT Installation [1]

Installing an AGT with a flare away from the roadway would reduce the system length along the primary roadway, as the guardrail would intercept the vehicle runout path closer to the hazard, when compared to a tangent installation. Additionally, the flared AGT configuration would result in a greater lateral offset between the guardrail and the traveled roadway. Thus, the flared AGT configuration would move the hazard posed by impacts with the guardrail farther away from the traveled road and increase the area for the drivers to regain control of the vehicle. As a result, flared AGT installations would reduce both accident frequency and the overall installation maintenance and material costs.

Previously, guidance for flaring the Midwest Guardrail System (MGS) away from the roadway [2] was established in accordance with NCHRP Report 350 Test Level 3 (TL-3) criteria [3]. Due to the need to reduce the length of the guardrail adjacent to the rigid parapet, initiating the flare in the transition region rather than the upstream MGS is more desirable as it would provide a greater reduction in barrier length along the primary road than flaring the W-beam section of guardrail at the upstream end of the transition. Unfortunately, minimal research and full-scale crash testing have been conducted on flared AGTs.

Several concerns have arisen about flaring AGTs resulting from previous flare rate studies. Flaring a guardrail system away from the roadway increases the vehicle impact angle with the barrier installation, which increases the chance for pocketing and vehicle snag. The increased impact angle also results in larger loads imparted to the barrier system, which could lead to component failure or rail rupture. Thus, a need exists to evaluate and establish guidance for flaring AGT installations under the American Association of State and Highway and Transportation Officials' (AASHTO) *Manual for Assessing Safety Hardware* (MASH) safety performance criteria [4].

Phase I of this research effort was conducted to identify the critical flare rate for a thrie-beam AGT, which would provide the greatest reduction in length of need (LON) while ensuring the system remained crashworthy to MASH Test Level 3 (TL-3) [5-6]. Phase I efforts included a literature review of existing AGTs and flared guardrail installations, validation of a tangent AGT LS-DYNA model, and determination of the critical flare rate for an AGT installation using the validated LS-DYNA model. Computer simulations identified a 15:1 flare rate (3.81 degrees from the roadway) as the maximum critical flare rate for full-scale testing, as steeper flare rates showed increased risks of snag and vehicle instabilities.

Phase I of the study concluded with computer simulations to identify critical impact points (CIPs) for both MASH test designation nos. 3-20 and 3-21 impacting the 15:1 flared AGT [5]. However, no funding was allocated for the full-scale crash testing and evaluation of the flared AGT installation during the Phase I research effort. Thus, a need existed to full-scale crash test and evaluate flared AGTs according to the MASH TL-3 safety performance criteria.

1.2 Objective

The objective of the research study was to identify the critical flare rate for flaring AGTs away from the primary roadway. Research focused on determining the maximum allowable flare rate that could safely be applied to 31-in. tall thrie-beam AGTs without curbs below the guardrail. Additionally, the standardized buttress was targeted for use at the downstream end of the AGT because it included chamfers intended to mitigate tire snag.

The objective of Phase II of the research project was to evaluate the safety performance of AGTs flared away from the roadway using full-scale crash testing according to the TL-3 criteria of MASH. Both MASH test designation nos. 3-20 and 3-21 were to be conducted on both the upstream and downstream ends of the AGT. Test no. FLAGT-1, documented herein, was conducted with the 2270P pickup truck impacting the downstream end of the flared AGT to evaluate the potential for vehicle snag on the rigid buttress.

1.3 Scope

The research objective was achieved through the completion of several tasks. First, a sponsor survey was conducted to identify the preferred connection method to facilitate the 15:1 flare away from the roadway. CAD details for the 15:1 flared AGT were developed, and the test installation was constructed. One full-scale crash test was conducted on the 15:1 flared AGT according to MASH test designation no. 3-21. The crash test results were analyzed, evaluated, and documented. Conclusions and recommendations were then made pertaining to the safety performance of the 15:1 flared AGT.

2 FLARED AGT CONNECTION OPTIONS

A special connection design was necessary to attach an AGT with a 15:1 flare rate to a rigid buttress installed tangent to the roadway. Four options for connecting the flared AGT to the rigid buttress were explored:

- Option 1: Flared Concrete Buttress
- Option 2: Tapered Concrete Buttress
- Option 3: Angled Connector Plate Assembly
- Option 4: Radiused Thrie-Beam Guardrail

The four options are discussed in the following sections.

2.1 Option 1: Flared Concrete Buttress

The first option was to modify the geometry of the upstream end of the concrete buttress to match the flare rate of the AGT. As shown in Figure 2, the upstream 3 ft of the buttress was flared back at 3.8 degrees (matching the 15:1 flare rate) through the entire thickness of the standardized buttress. While this option would require alteration of the standardized buttress and a new standard detail, it would achieve the desired flare rate without requiring additional connection hardware and would utilize standard (unbent) thrie-beam guardrail.

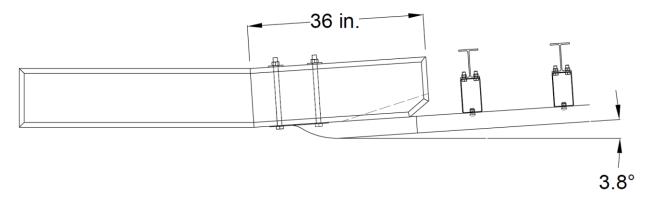


Figure 2. Option 1 – Flared Concrete Buttress

2.2 Option 2: Tapered Concrete Buttress

Option 2 was similar to Option 1, but only the front face of the concrete buttress was tapered at 3.8 degrees to match the 15:1 flare rate. The back side of the buttress would remain tangent to the roadway, as shown in Figure 3. Thus, the upstream end of the standardized buttress would be tapered to facilitate the 15:1 flare. Option 2 would require alteration of the standardized buttress geometry and a new standard detail, but like Option 1, would not require additional components and would utilize standard (unbent) thrie-beam guardrail to achieve the 15:1 flare rate.

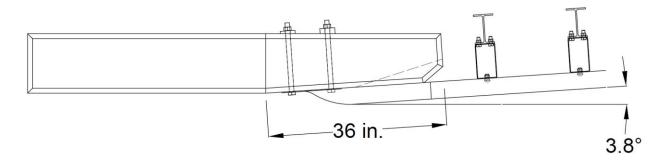


Figure 3. Option 2 – Tapered Concrete Buttress

2.3 Option 3: Angled Connector Plate Assembly

Option 3 included a wedge-shaped connector plate installed between the thrie-beam terminal connector and the standardized concrete buttress, as shown in Figures 4 and 5. Similar connection plates have been used to connect vertical thrie beam to the sloped faces of safety shape and single slope parapets [7-8]. However, this angled connector plate assembly would be used to fill the gap between the angled thrie beam and the vertical buttress face.

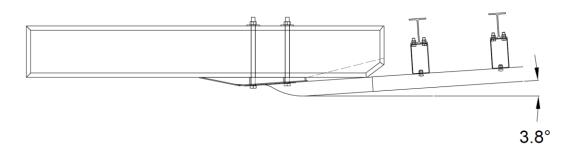


Figure 4. Option 3 – Angled Connector Plate Assembly

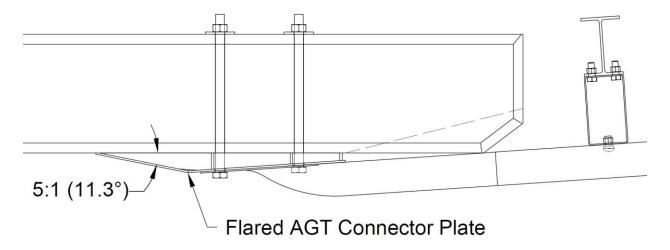


Figure 5. Option 3 – Angled Connector Plate Assembly, Enlarged

Use of an angled connector plate assembly would enable the use of standard AGT components (i.e., the standardized transition buttress and unbent thrie beam segments). However, the connector plate assembly would be an additional required component and the plate would extend 2 in. from the face of the buttress into the traveled way, which could result in a snag hazard in the reverse direction. To mitigate the snag hazard, the downstream end of the connector plate would transition back to the traffic-side face of the standardized concrete buttress with a 5:1 taper. Steel connection plates with a 5:1 taper/slope have demonstrated acceptable safety performance in previous MASH TL-3 crash testing [9].

2.4 Option 4: Radiused Thrie-Beam Guardrail

Option 4 would utilize bent, or radiused, guardrail to achieve the 15:1 flare away from the roadway, as shown in Figures 6 and 7. The bend in the thrie beams would initiate 13½ in. from the downstream end of the thrie-beam segments, which would coincide with the upstream end of the thrie-beam terminal connector. Rather than bending the guardrail at a single point, the radiused guardrail would achieve the 15:1 flare rate over a 16-in. long bend with a 240-in. radius. Only the first post immediately upstream from the standardized buttress would be located within the radiused section. This option would require the fabrication of radiused thrie-beam guardrail sections, but the thrie-beam terminal connector would be mounted flush with the traffic-side face of the buttress and the standardized transition buttress geometry would be unchanged. Fabrication of a radiused thrie beam guardrail has previously been done for other guardrail systems, such as the bullnose crash cushion [10]. However, nesting of bent guardrail sections may prove to be difficult as the bent sections may not perfectly line up to fit together.

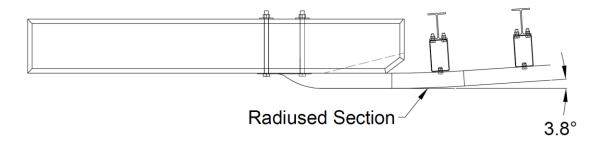


Figure 6. Option 4 – Radiused Thrie-Beam

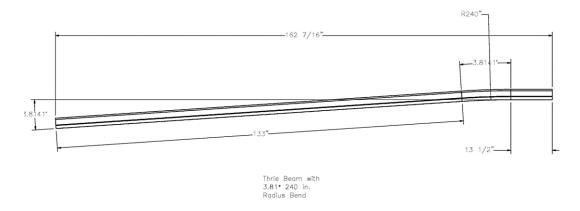
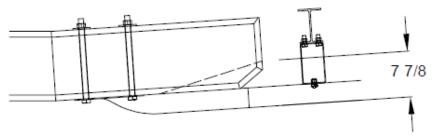


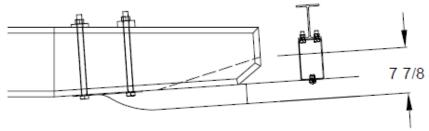
Figure 7. 12.5-ft Long Radiused Thrie-Beam Section

2.5 Discussion

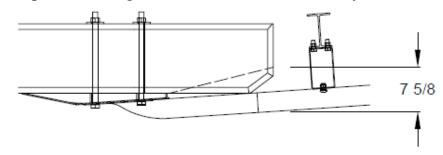
Each of the connection concepts were considered viable options for connecting a flared AGT to a tangent buttress. Further, all four options were expected to perform similarly and provide MASH crashworthy solutions, but the angled connector plate (Option 3) may have a slightly higher risk for snag underneath the thrie-beam guardrail. As shown in Figure 8, the flared AGT connector plate geometry results in a ¼-in. reduction in the offset distance from the front face of the guardrail to the edge of the lower chamfer on the buttress. In each of the other three options (Options 1, 2, and 4) the thrie-beam terminal connector would be bolted flush with the face of the buttress, so the guardrail immediately upstream from the buttress would have the same offset as the tangent AGT installation. Thus, Option 3 was selected as the critical connection design for full-scale crash testing. If the angled connector plate configuration was found to perform acceptably during crash testing, the other three connection options would also be considered crashworthy.



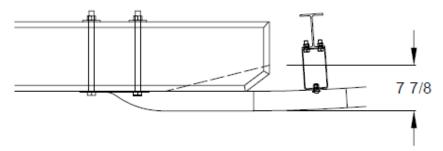
Option 2 – Tapered Concrete Buttress



Option 3 – Angled Connector Plate Assembly



Option 4 – Radiused Thrie-Beam Guardrail



Tangent AGT

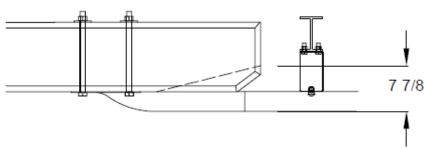


Figure 8. Comparison of Guardrail Offset from Buttress Lower Chamfer

2.6 Vertical Slotted Terminal Connector

Thrie-beam terminal connectors are used at the downstream end of a thrie-beam AGT to connect the thrie-beam guardrail to a rigid bridge rail, buttress, or concrete parapet. Alignment issues often occur at the splice between the terminal connection and the nested thrie beam segments that result in difficulties installing the splice bolts.

In 2017, the Texas A&M Transportation Institute (TTI) evaluated existing thrie-beam terminal connector designs and developed design improvements to improve constructability and reduce or eliminate the need for rail modifications in the field [11]. The research study recommended the use of splice slots oriented in the vertical direction, as this splice slot orientation demonstrated adequate strength during component testing and improved the constructability of the nested connection. Thus, a thrie-beam terminal connector with 1-in. wide by 1½-in. tall splice slots oriented in the vertical direction was selected for use during the evaluation of the flared AGT and would be recommended for use with any of the four connection options. The vertical slotted terminal connector is shown in Figure 9.

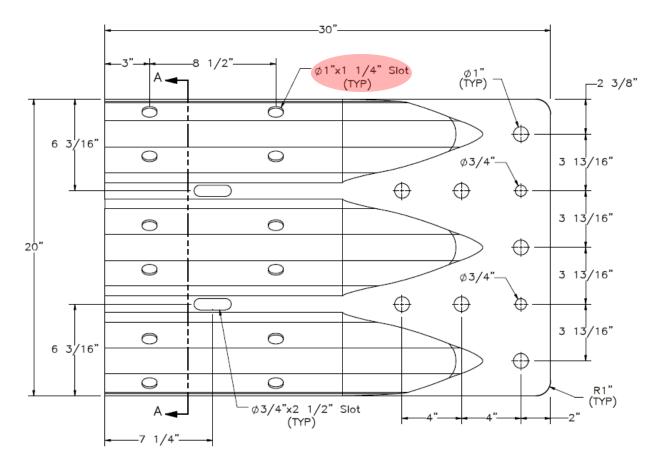


Figure 9. Vertical Slotted Terminal Connector

3 TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 Test Requirements

Longitudinal barriers, such as AGTs, must satisfy impact safety standards in order to be declared eligible for federal reimbursement by the Federal Highway Administration (FHWA) for use on the National Highway System. For new hardware, these safety standards consist of the guidelines and procedures published in the 2016 edition of MASH [4]. Note, for longitudinal barriers, there is no difference between the 2009 edition of MASH [12] and the current 2016 edition except that additional occupant compartment deformation measurements, photographs, and documentation are required. According to TL-3 of MASH, longitudinal barrier systems must be subjected to two full-scale vehicle crash tests, MASH test designation no. 3-20 with the 1100C small car and MASH test designation no. 3-21 with the 2270P pickup truck. However, recent testing has demonstrated that there are two CIPs for an AGT: (1) near the downstream end of the AGT to maximize snagging on the buttress and (2) near the upstream end to maximize snagging and pocketing at the W-to-thrie transition section. Thus, four crash tests were required to evaluate the flared AGT, as summarized in Table 1.

Table 1. MASH TL-3 Crash Test Matrix for AGT

Test	Test	Test	Vehicle	-	pact itions	Evaluation	Immo at Daint	
Article	Designation No.	Vehicle	Weight lb	Speed mph	Angle deg.	Criteria ¹	Impact Point	
	3-20	1100C	2,420	62	25	A,D,F,H,I	Downstream AGT	
Longitudinal	3-21	2270P	5,000	62	25	A,D,F,H,I	Downstream AGT	
Barrier	3-20	1100C	2,420	62	25	A,D,F,H,I	Upstream AGT	
	3-21	2270P	5,000	62	25	A,D,F,H,I	Upstream AGT	

¹ Evaluation criteria explained in Table 2.

3.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the flared AGT to contain and redirect impacting vehicles. In addition, controlled lateral deflection of the test article is acceptable. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are summarized in Table 2 and defined in greater detail in MASH [4]. Each full-scale vehicle crash test was conducted and reported in accordance with the procedures provided in MASH.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported. Additional discussion on PHD, THIV and ASI is provided in MASH [4].

Table 2. MASH Evaluation Criteria for Longitudinal Barrier

Structural Adequacy	A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.				
	D.	should not penetrate or show compartment, or present an un or personnel in a work zone. I occupant compartment should	Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH.			
	F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.				
Occupant Risk	H.	Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH for calculation procedure) should satisfy the following limits:				
KISK		Occupant In	npact Velocity Limit	ts		
		Component	Preferred	Maximum		
		Longitudinal and Lateral	30 ft/s	40 ft/s		
	I.	The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.2.2 of MASH for calculation procedure) should satisfy the following limits:				
		Occupant Ridedown Acceleration Limits				
		Component	Preferred	Maximum		
		Longitudinal and Lateral	15.0 g's	20.49 g's		

3.3 Soil Strength Requirements

In accordance with Chapter 3 and Appendix B of MASH, foundation soil strength must be verified before any full-scale crash testing can occur. During the installation of a soil dependent system, W6x16 posts are installed near the impact region utilizing the same installation procedures as the system itself. Prior to full-scale testing, a dynamic impact test must be conducted to verify a minimum dynamic soil resistance of 7.5 kips at post deflections between 5 and 20 in. measured at a height of 25 in. If dynamic testing near the system is not desired, MASH permits a static test to be conducted instead and compared against the results of a previously established baseline test. In this situation, the soil must provide a resistance of at least 90% of the static baseline test at deflections of 5, 10, and 15 in. Further details can be found in Appendix B of MASH [4].

4 DESIGN DETAILS

The flared AGT test installation was approximately 81 ft – 6 in. long and consisted of five main components: (1) a concrete buttress, (2) a thrie-beam AGT, (3) standard MGS, (4) a guardrail anchorage system, and (5) the flared AGT connector plate. Design details for test no. FLAGT-1 are shown in Figures 10 through 36. Photographs of the test installation are shown in Figures 37 and 38. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix B.

The downstream end of the installation consisted of a concrete parapet with dimensions matching those of the standardized concrete buttress [1]. The buttress was 84 in. long and 36 in. tall. To prevent vehicle snag on the buttress above the thrie-beam rail, the upstream end of the buttress was 32 in. tall and incorporated a 24-in. long slope to bring the barrier height up to 36 in. The upstream end of the standardized buttress utilized a dual tapered design, or dual chamfer, as shown in Figure 18. The lower tire chamfer was 18 in. long by 4½ in. wide by 14 in. tall and was designed to reduce the propensity for wheel snag on the buttress. The upper chamfer measured 4 in. long by 3 in. wide and extended vertically 18 in. along the remaining height of the buttress. The upper chamfer was designed to limit vehicle snag on the buttress, prevent the guardrail from bending around a rigid corner, and to limit the unsupported span length of the rail upstream from the buttress. The buttress was reinforced with Grade 60 rebar, as detailed in Figures 19 through 22, and the vertical steel in the buttress was anchored to the tarmac using an epoxy adhesive, as detailed in Figure 19.

The AGT consisted of a 12½-ft section of nested 12-gauge thrie-beam, a 6¼-ft section of 12-gauge thrie-beam, a 6¼-ft long 10-gauge W-to-thrie transition section, and a 12½-ft section of nested 12-gauge W-beam guardrail. Upstream from the AGT was 37½ ft of 12-gauge W-beam guardrail, which included the MGS and a guardrail anchor. All guardrail sections were mounted with a top guardrail height of 31 in. and were supported by W6x8.5 ASTM A992 steel guardrail posts. Posts. 3 through 15 were 72 in. long and embedded 40 in. into the soil, while the six posts adjacent to the buttress, post nos. 16 through 21, were 78 in. long and embedded at a depth of 49 in. As shown in Figure 11, post nos. 1 through 8 were spaced at 75 in., post nos. 8 through 12 were spaced at 37½ in., and post nos. 12 through 21 were spaced at 18¾ in.

The nested thrie beam AGT utilized herein was previously shown to be MASH TL-3 crashworthy via full-scale crash testing [1, 13]. The AGT configuration was selected for use in this flared AGT study because it was a common AGT configuration that had a lower lateral stiffness than other crashworthy AGTs (i.e., it allowed higher system displacements than other MASH TL-3 AGTs). Thus, this AGT configuration represented a critical configuration to evaluate vehicle snag on the buttress.

The upstream stiffness transition, or the W-beam to nested thrie beam transition, was also previously full-scale crash tested to MASH TL-3 [14]. Nested W-beam was placed adjacent to the W-to-thrie transition segment to strengthen the AGT and prevent rupture of the W-beam, as was previously done to strength the upstream stiffness transition installed behind a curb [15].

All guardrail segments were installed with a 15:1 flare rate relative to the face of the concrete buttress. An angled connector plate assembly was placed between the thrie-beam terminal connector and the buttress to connect the guardrail at a 15:1 flare rate, as shown in Figure 12 and

detailed in Figures 29 through 31. The angled connector plate assembly was constructed with a $^{3}/_{16}$ -in. thick steel face plate and $^{1}/_{4}$ -in. thick steel gussets. The plate extended 2 in. laterally from the traffic-side face of the buttress and the downstream end of the plate tapered flush with the face of the buttress via a 5:1 slope to mitigate snag in the reverse direction. As shown in Figure 33, the 10-gauge thrie-beam terminal connector had $1^{1}/_{4}$ -in. tall by 1-in. wide splice slots oriented in the vertical direction to improve constructability of the nested thrie-beam splice connection. Five $^{7}/_{8}$ -in. diameter ASTM F3125, Grade 120 heavy hex head bolts were used to connect the guardrail and connector assembly to the buttress.

The upstream end of the guardrail installation was configured with a non-proprietary guardrail anchorage system. The anchorage system consisted of timber posts, foundation tubes, anchor cables, bearing plates, rail brackets, and channel struts. The guardrail anchorage system had a strength comparable to other crashworthy end terminals. This anchorage system was successfully crash tested to MASH TL-3 as a downstream, trailing-end, guardrail terminal [16-19].

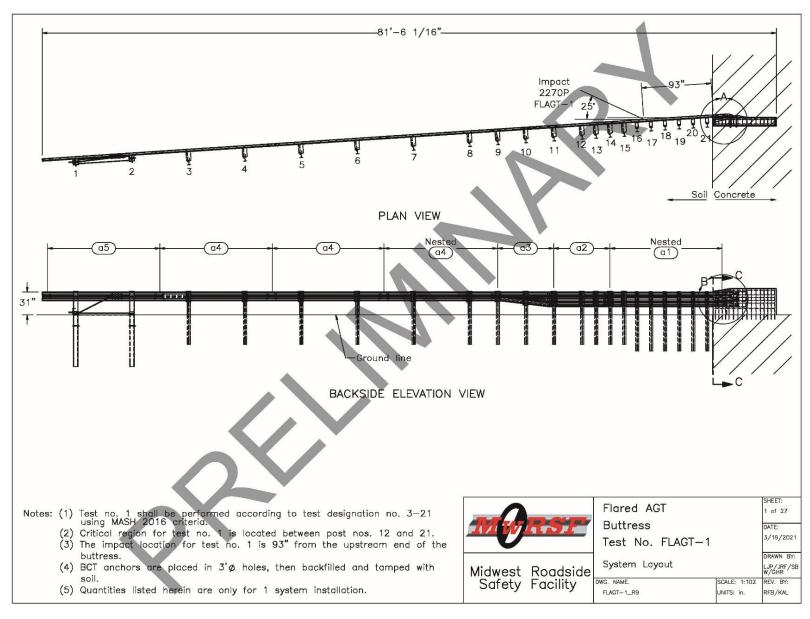


Figure 10. Test Installation Layout, Test No. FLAGT-1

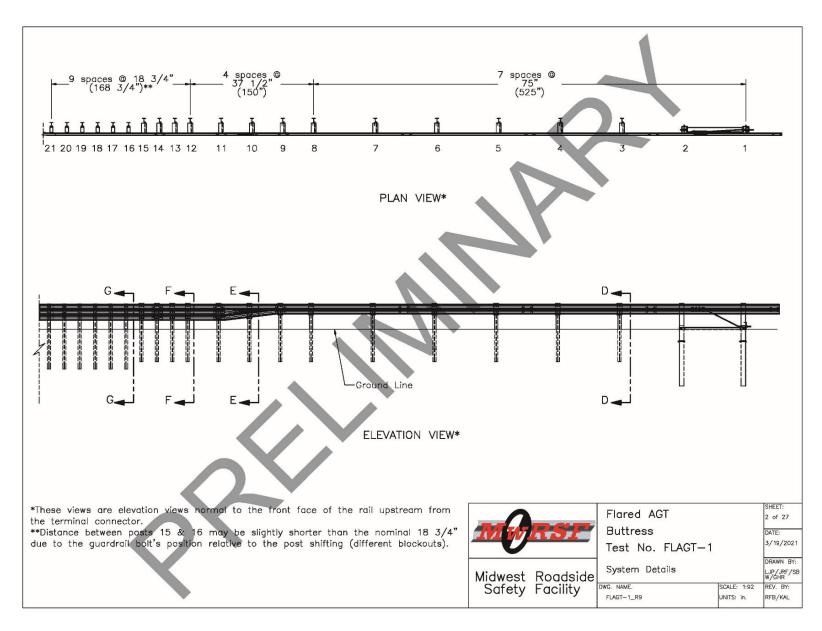


Figure 11. System Details, Test No. FLAGT-1

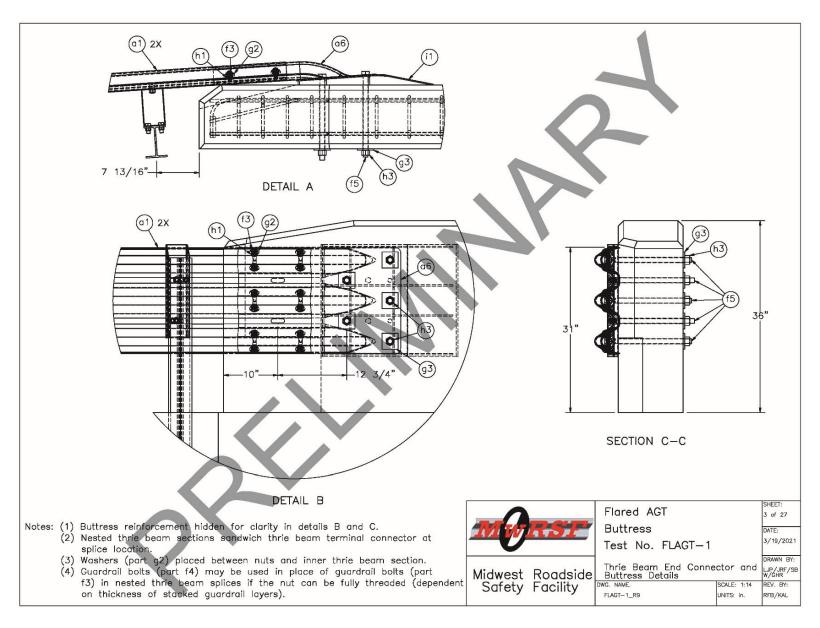


Figure 12. Thrie-beam End Connector and Buttress Details, Test No. FLAGT-1

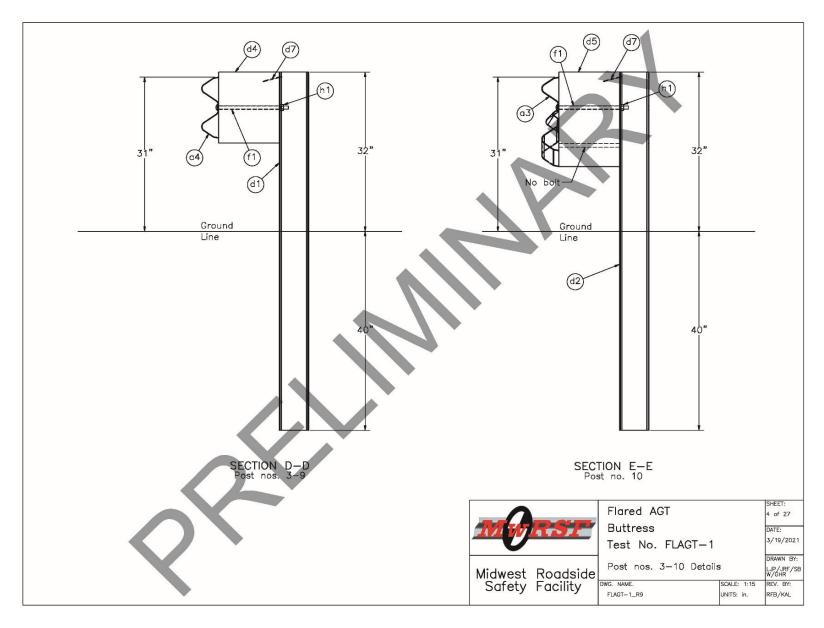


Figure 13. Post Nos. 3-10 Details, Test No. FLAGT-1

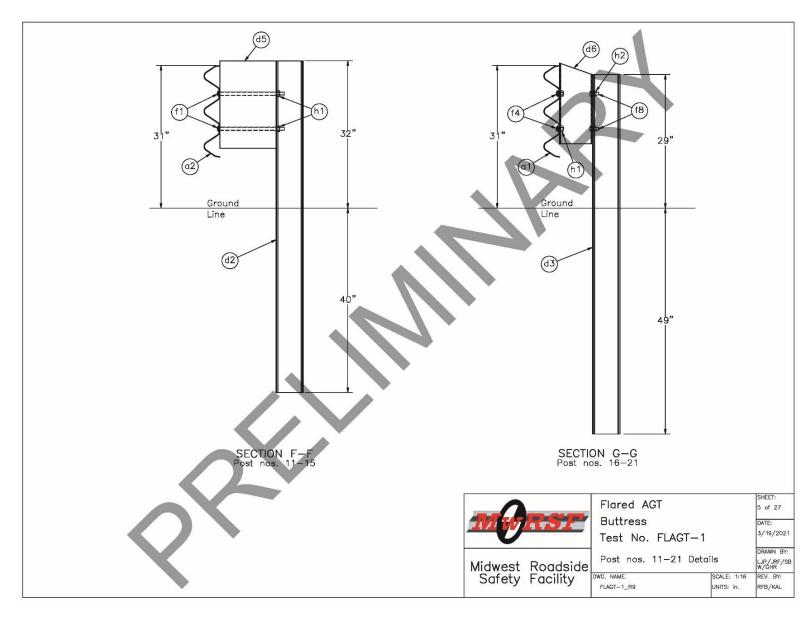


Figure 14. Post Nos. 11-21 Details, Test No. FLAGT-1

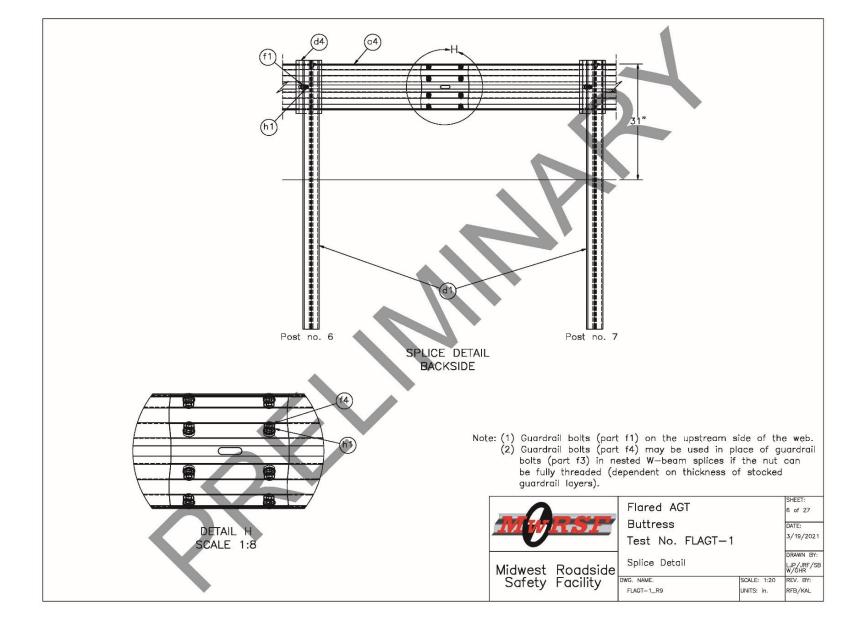


Figure 15. Splice Detail, Test No. FLAGT-1

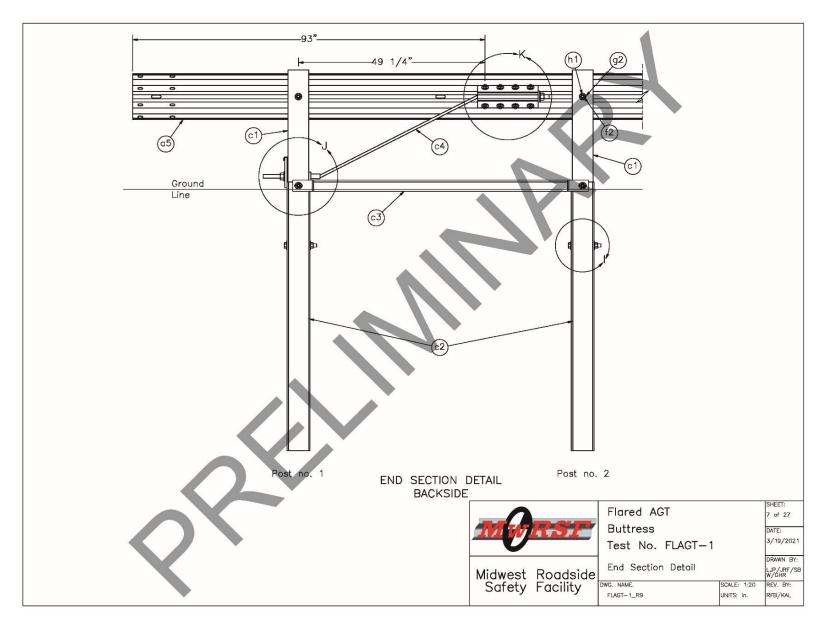


Figure 16. End Section Detail, Test No. FLAGT-1

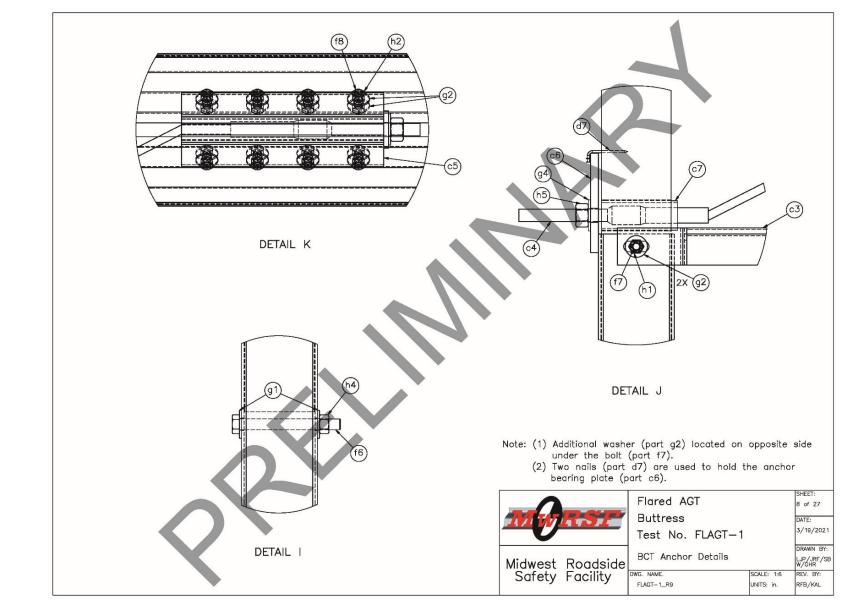


Figure 17. BCT Anchor Details, Test No. FLAGT-1

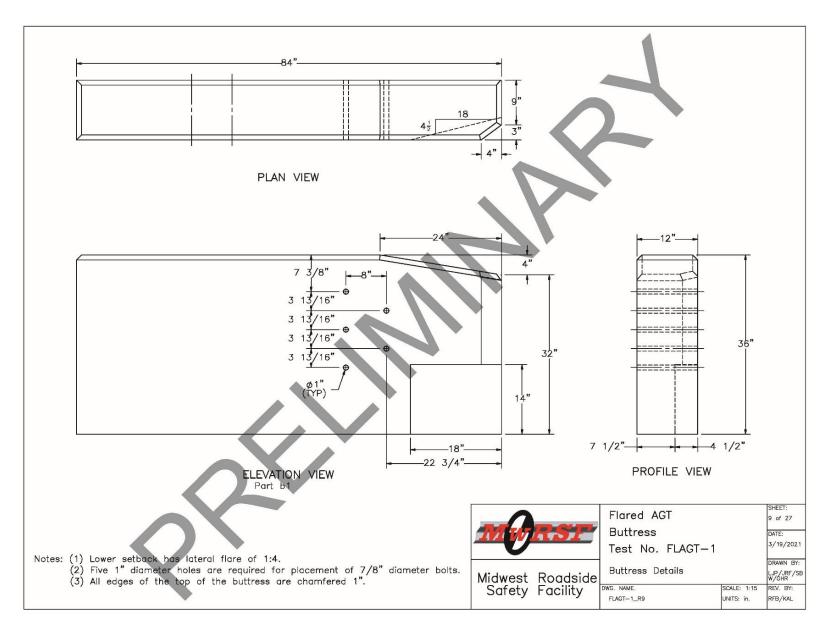


Figure 18. Buttress Details, Test No. FLAGT-1

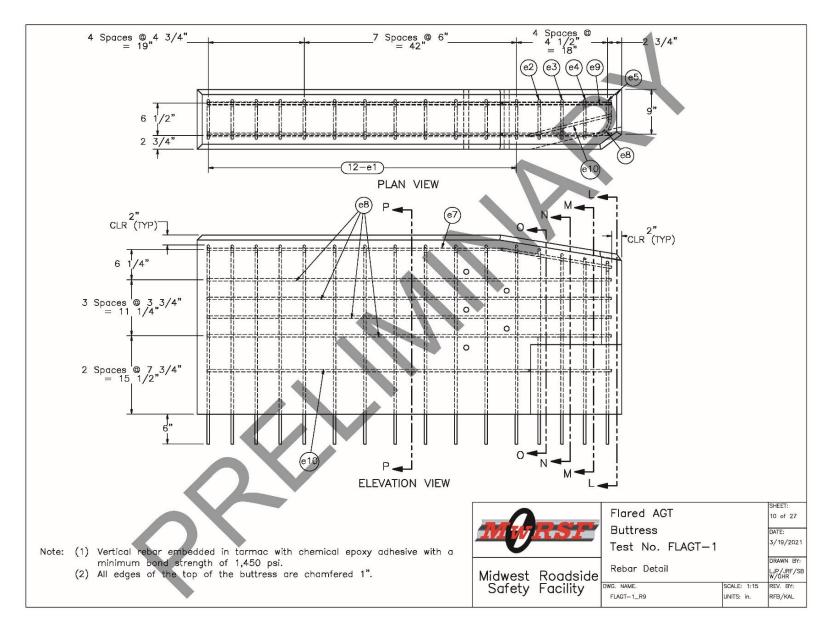


Figure 19. Rebar Detail, Test No. FLAGT-1

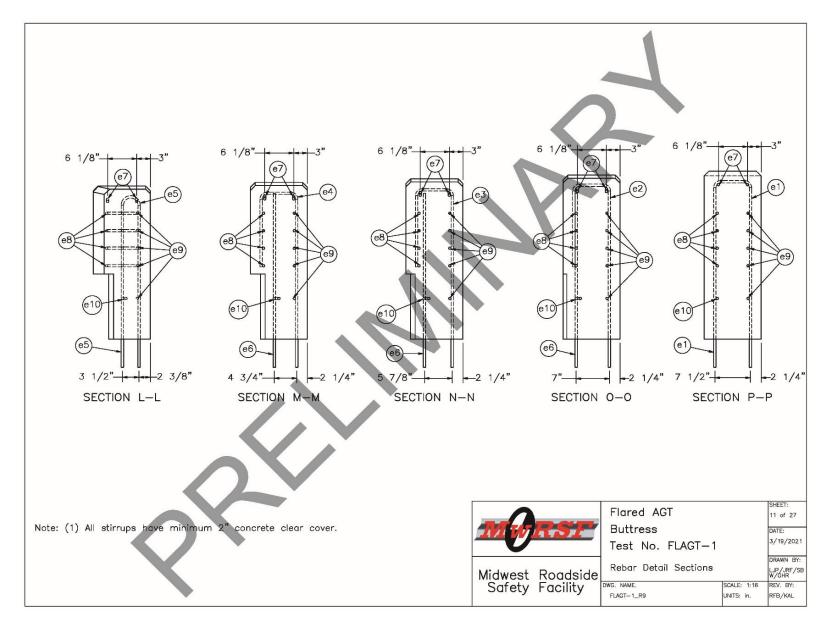


Figure 20. Rebar Detail Sections, Test No. FLAGT-1

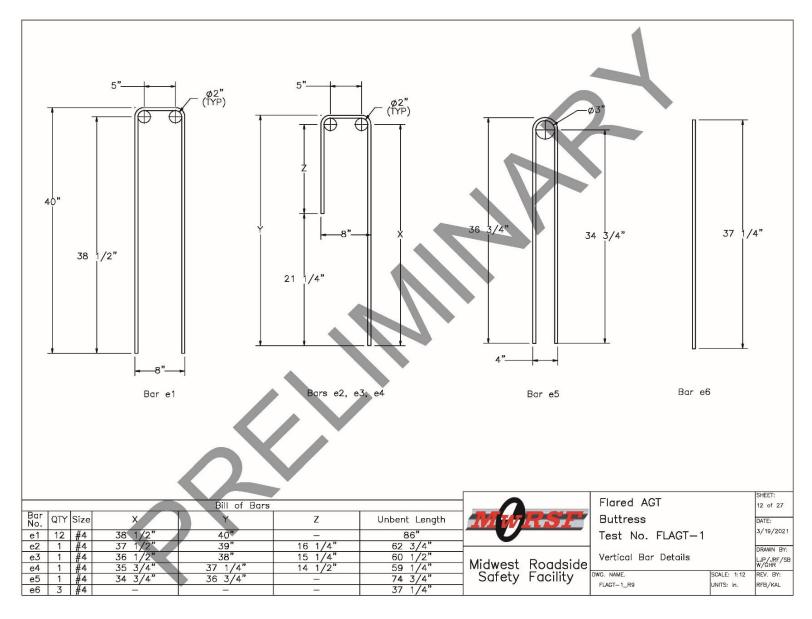


Figure 21. Vertical Rebar Details, Test No. FLAGT-1

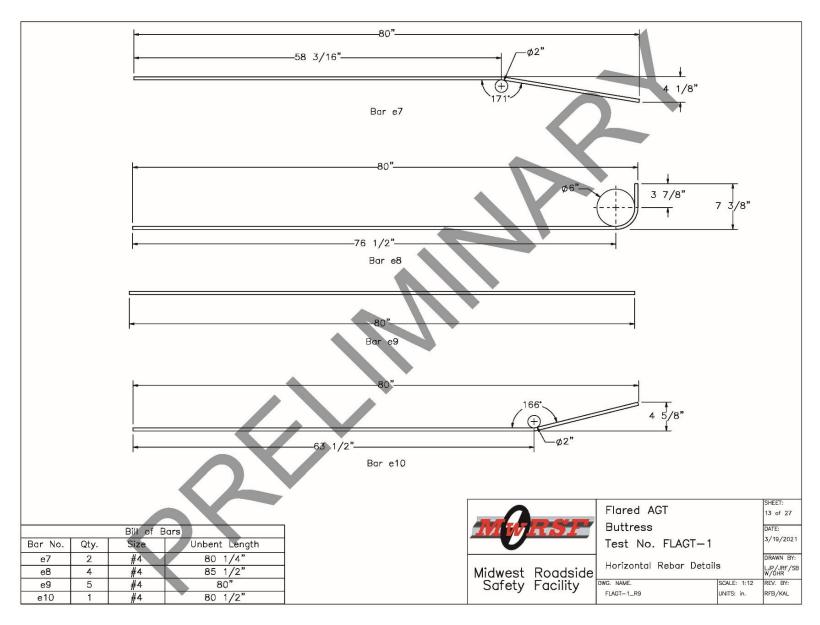


Figure 22. Horizontal Rebar Details, Test No. FLAGT-1

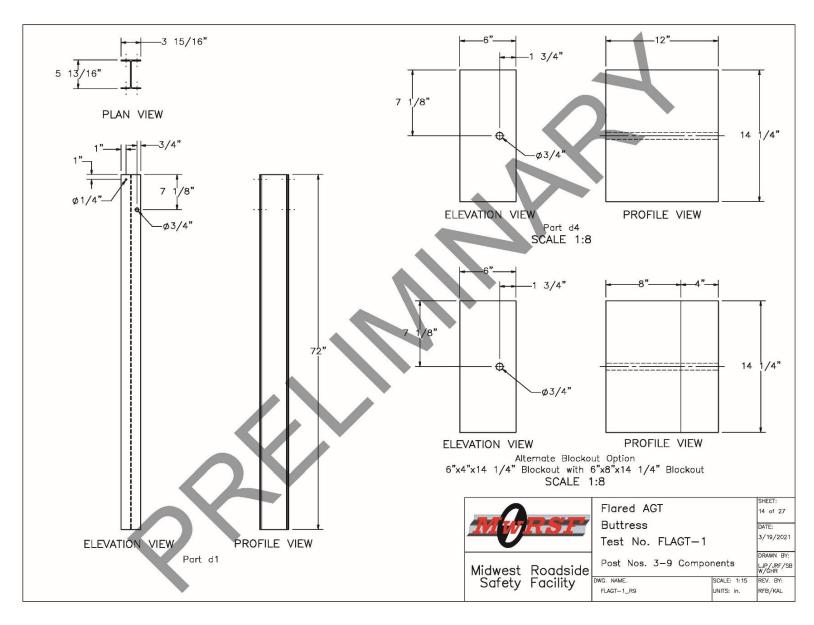


Figure 23. Post Nos. 3 through 9 Components, Test No. FLAGT-1

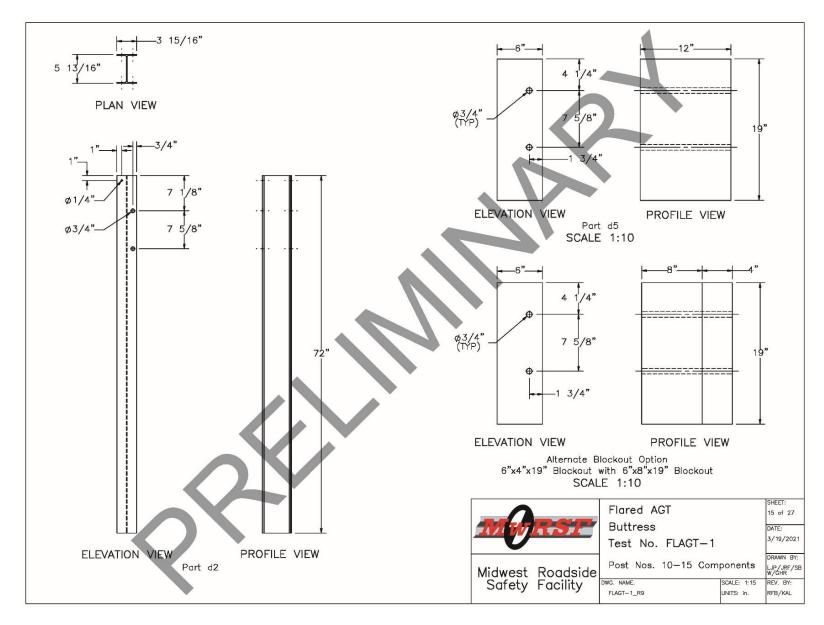


Figure 24. Post Nos. 10 through 15 Components, Test No. FLAGT-1

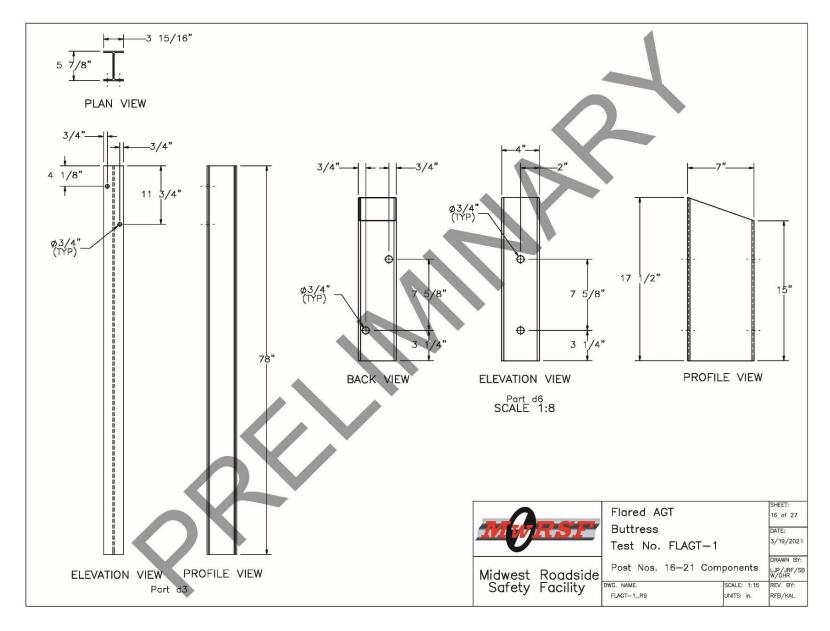


Figure 25. Post Nos. 16 through 21 Components, Test No. FLAGT-1

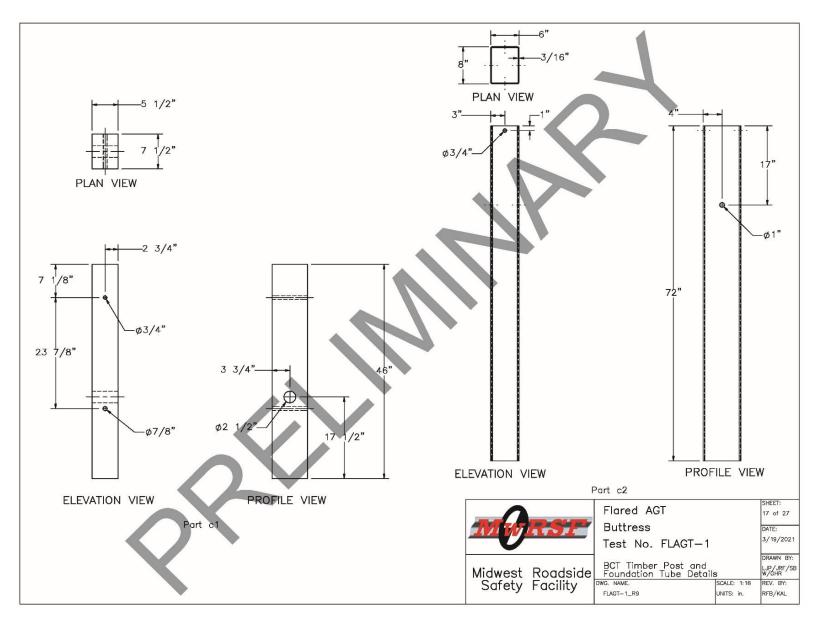


Figure 26. BCT Timber Post and Foundation Tube Details, Test No. FLAGT-1

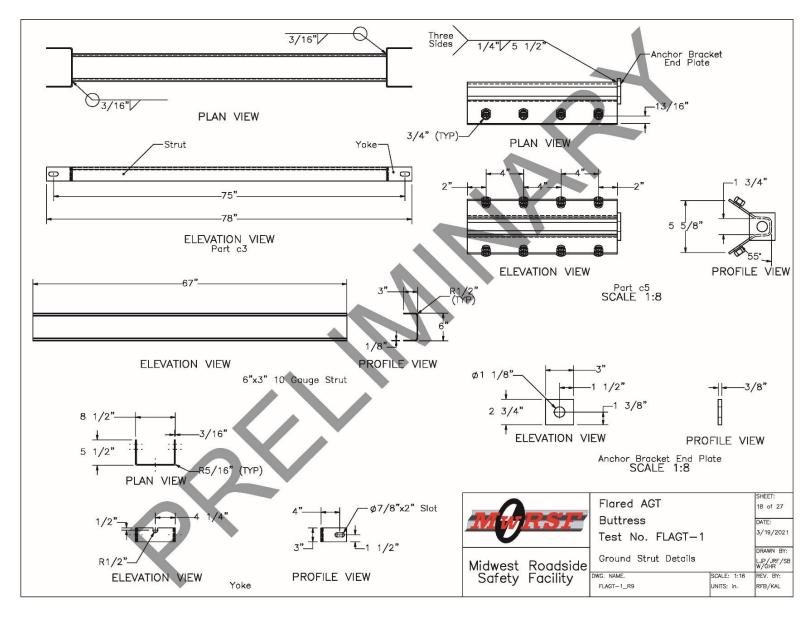


Figure 27. Ground Strut Details, Test No. FLAGT-1

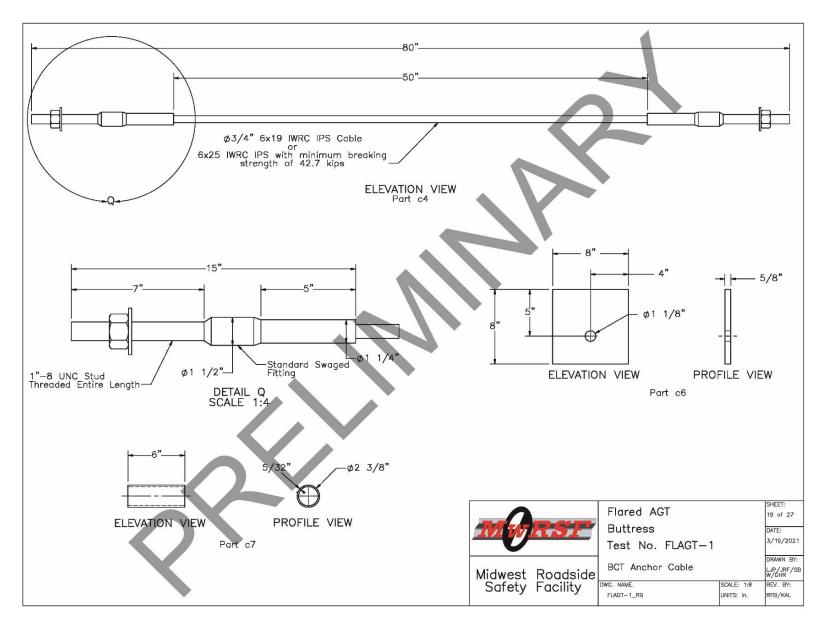


Figure 28. BCT Anchor Cable, Test No. FLAGT-1

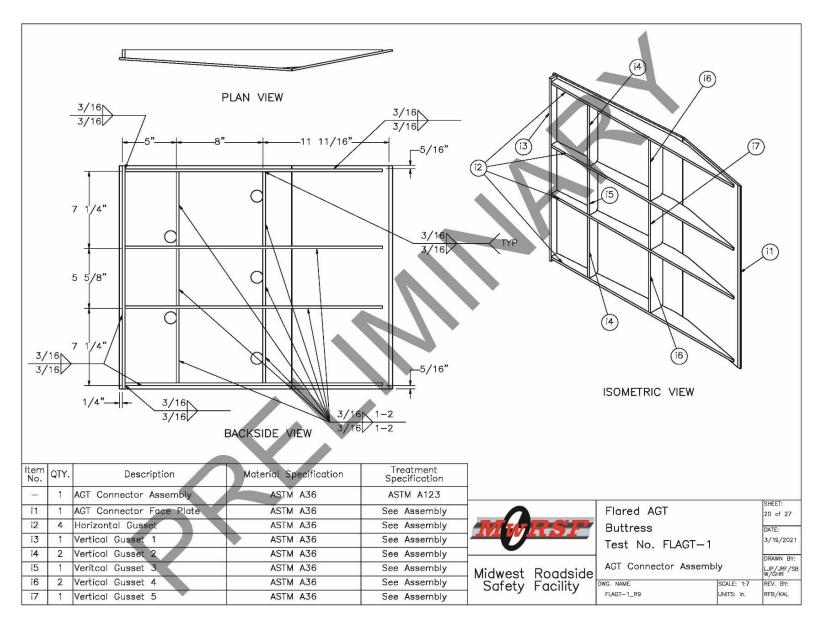


Figure 29. AGT Connector Plate Assembly, Test No. FLAGT-1

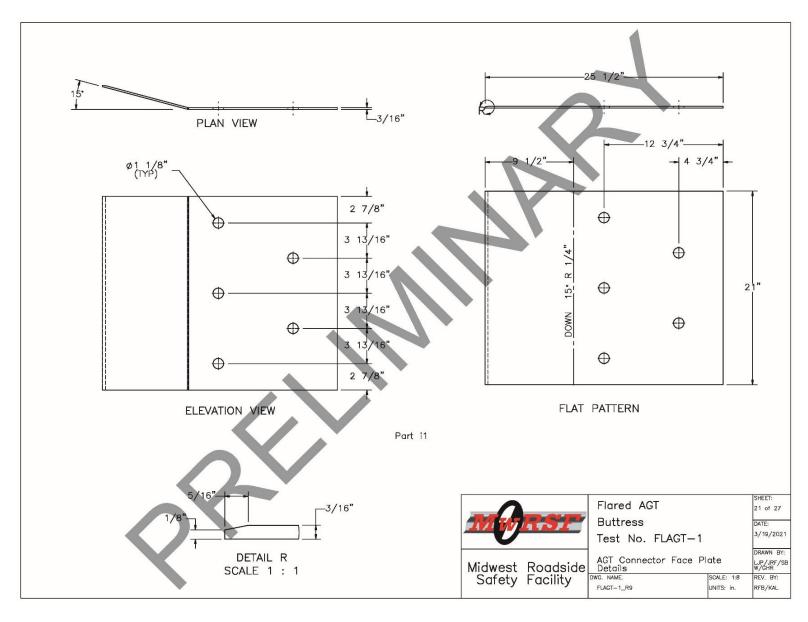


Figure 30. AGT Connector Plate Assembly Face Plate Details, Test No. FLAGT-1

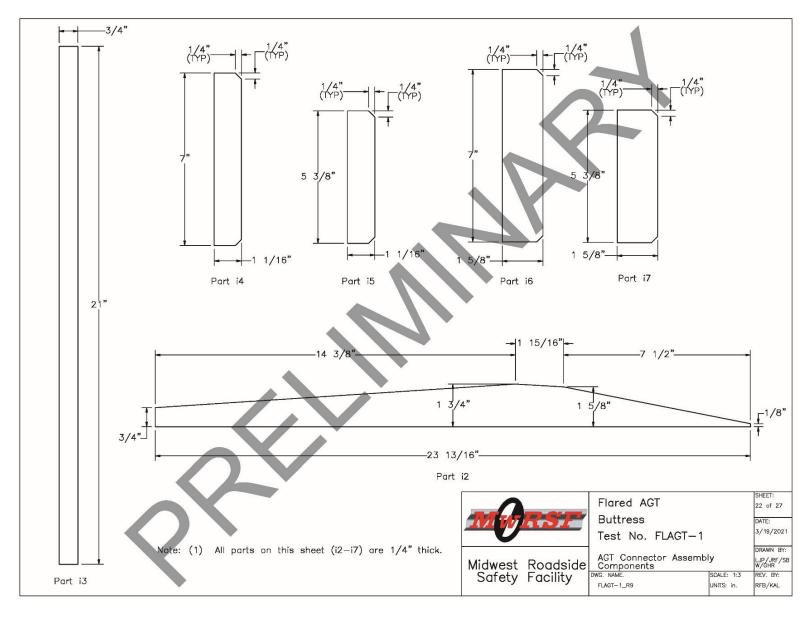


Figure 31. AGT Connector Assembly Components, Test No. FLAGT-1

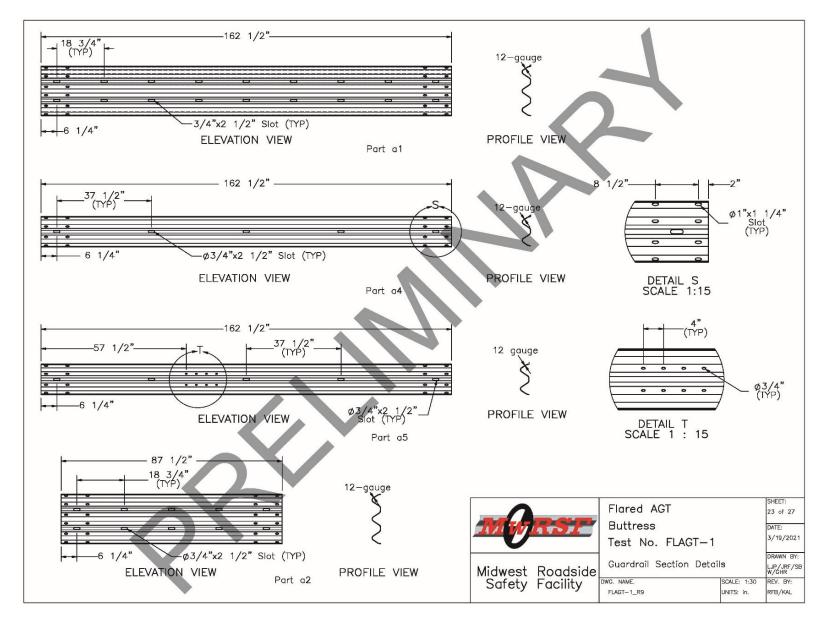


Figure 32. Guardrail Section Details, Test No. FLAGT-1

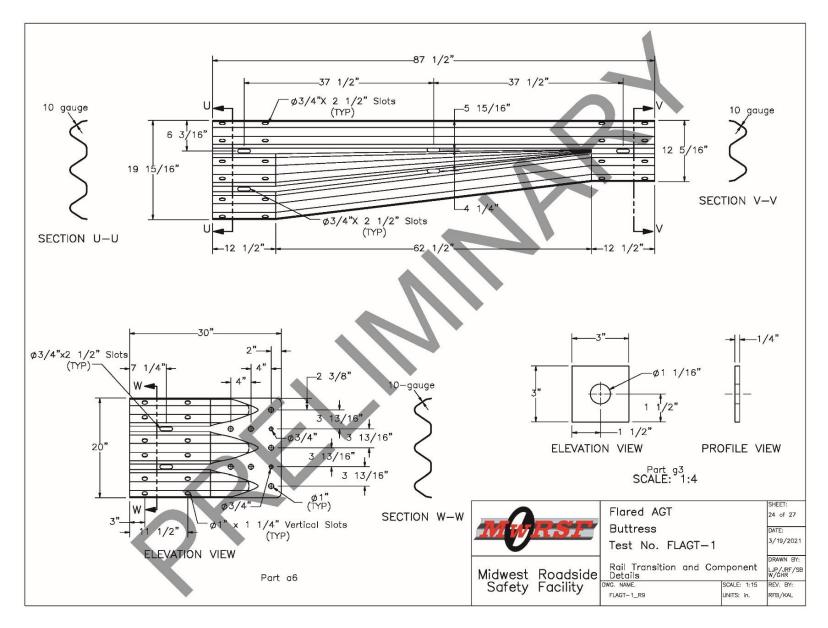


Figure 33. Rail Transition and Component Details, Test No. FLAGT-1

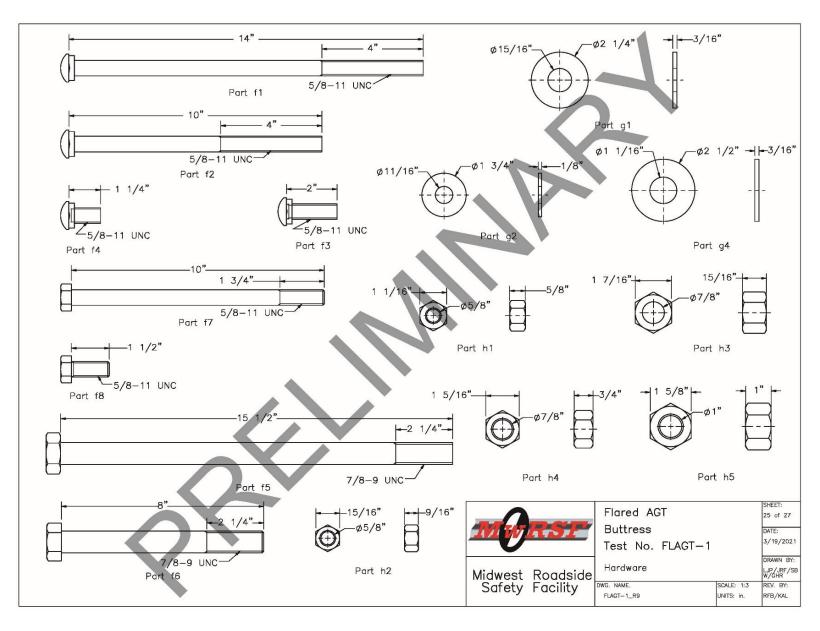


Figure 34. Hardware, Test No. FLAGT-1

Item No.	QTY.	Description	Material Specification	Treatment Specification	Hardware Guide
a1	2	12'-6" 12-gauge Thrie Beam Section	AASHTO M180	ASTM A123 or A653	RTM08a
a2		6'-3" 12-gauge Thrie Beam Section	AASHTO M180	ASTM A123 or A653	RTM19a
a3	1	6°-3" 10-gauge W-Beam to Thrie-Beam Asymetric Transition Section	AASHTO M180	ASTM A123 or A653	RWT02
a4	4	12'-6" 12-gauge W-Beam MGS Section	AASHTO M180	ASTM A123 or A653	RWM04a
a5	1	12'-6" 12-gauge W-Beam MGS End Section	AASHTO M180	ASTM A123 or A653	RWM14a
a6	1	10—gauge Thrie Beam Terminal Connector	AASHTO M180 Gr. 50 Min. yield strength = 50 ksi Min. ultimate strength = 70 ksi	ASTM A123 or A653	-
ь1	1	Concrete — 21.9 cubic ft	Min. f'c = 4,000 psi	-	-
c1	2	BCT Timber Post — MGS Height	SYP Grade No. 1 or better (No knots +/- 18" from ground on tension face)	M -	PDF01
c2	2	72" Long Foundation Tube	ASTM A500 Gr. B	*ASTM A123	PTE06
сЗ	1	Ground Strut Assembly	ASTM A36	*ASTM A123	PFP02
с4	1	BCT Cable Anchor Assembly	-	-	FCA01
с5	1	Anchor Bracket Assembly	ASTM A36	*ASTM A123	FPA01
с6	1	8"x8"x5/8" Anchor Bearing Plate	ASTM A36	*ASTM A123	FPB01
c7	1	2 3/8" O.D. x 6" Long BCT Post Sleeve	ASTM A53 Gr. B Schedule 40	*ASTM A123	FMM02
d1		W6x8.5 or W6x9, 72" Long Steel Post	ASTM A992	*ASTM A123	PWE06
d2	6	W6x8.5 or W6x9, 72" Long Steel Post	ASTM A992	*ASTM A123	PWE06
d3	6	W6x8.5 or W6x9, 78" Long Steel Post	ASTM A992	*ASTM A123	-
d4	7	6"x12"x14 1/4" Timber Blockout	SYP Grade No.1 or better	<u>₩</u>	PDB10d
d5	6	6"x12"x19" Timber Blockout	SYP Grade No.1 or better	=,	_
d6	6	17 1/2" Long, 7"x4"x3/16" lowa Steel Blockout	ASTM A500 Gr. B	*ASTM A123	-
d7	9	16D Double Head Naîl	_	-	(-)
e1	12	86" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
e2	1	62 3/4" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
еЗ	1	60 1/2" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
e4	1	59 1/4" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	_
e5	1	74 3/4" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	_
e6	3	37 1/4" Long #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
e7	2	80 1/4" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	_
e8	4	85 1/2" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
		ent does not need to be galvanized for testing pur does not need to be epoxy—coated for testing purp		Flared AGT Buttress Test No. FLAGT-1	SHEET: 26 of DATE: 3/19/

M	RSF	Flared AGT Buttress Test No. FLAGT-1		SHEET: 26 of 27 DATE: 3/19/2021
Midwest	Roadside	Bill of Materials		DRAWN BY: LJP/JRF/SB W/GHR
		DWG. NAME. FLAGT-1_R9	SCALE: None UNITS: in.	REV. BY: RFB/KAL

Figure 35. Bill of Materials, Test No. FLAGT-1

Note: (1) Quantities listed herein are only for 1 system installation.
(2) For testing purposes part b1 used NE Mix 47B1S/1PF4000HW.

No.	QTY.	Description	Material Specification	Treatment Specification	Hardwar Guide
e9	5	80" Long #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
e10	1	80 1/2" Unbent Length #4 Rebar	ASTM A615 Gr. 60	**Epoxy Coated (ASTM A775 or A934)	-
f1	18	5/8" Dia. UNC, 14" Long Guardrail Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	FBB06
f2	2	5/8" Dia. UNC, 10" Long Guardrail Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	FBB03
f3	24	5/8" Dia. UNC, 2" Long Guardrail Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	FBB02
f4	56	5/8" Dia. UNC, 1 1/4" Long Guardrail Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	FBB01
f5	5	7/8 Dia. UNC, 15 1/2" Long Heavy Hex Head Bolt	ASTM F3125 Gr. 120 (A325) or A354 Gr. BC	ASTM A153 or B695 Class 55 or F1136 Gr. 3 or F2329 or F2833 Gr. 1	FBX22I
f6		7/8" Dia. UNC, 8" Long Hex Head Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	_
f7	2	5/8" Dia. UNC, 10" Long Hex Head Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	FBX16
f8	20	5/8" Dia. UNC, 1 1/2" Long Hex Head Bolt	ASTM A307 Gr. A	ASTM A153 or B695 Class 55 or F2329	FBX16
g1	4	7/8" Dia. Plain Round Washer	ASTM F844	ASTM A123 or A153 or F2329	::
g2		5/8" Dia. Plain Round Washer	ASTM F844	ASTM A123 or A153 or F2329	FWC16
g3	5	3"x3"x1/4" or 3 1/2"x3 1/2"x1/4" Square Washer Plate	ASTM A572 Gr. 50	*ASTM A123	1 - 1
g4	2	1" Dia. Plain Round Washer	ASTM F844	ASTM A153 (AASHTO M232) for Class D or ASTM B695 (AASHTO M298) for Class 50	FWC24
h1	102	5/8" Dia. Heavy Hex Nut	ASTM A563A	ASTM A153 (AASHTO M232) for Class C or ASTM B695 (AASHTO M298) for Class 50	1-2
h2		5/8" Dia. Hex Nut	ASTM A563A	ASTM A153 (AASHTO M232) for Class C or ASTM B695 (AASHTO M298) for Class 50	-
h3	5	7/8" Dia. UNC Heavy Hex Nut	ASTM A563DH or A194 Gr. 2H	-	_
h4	2	7/8" Dia. Hex Nut	ASTM A307	ASTM A153 (AASHTO M232) for Class C or ASTM B695 (AASHTO M298) for Class 50	-
n5	2	1"-8 UNC Heavy Hex Nut	ASTM A563DH or equivalent	ASTM A153 or B695 Class 55 or F2329	FNX24
i1	1	AGT Connector Face Plate	ASTM A36	See Assembly	_
2	4	Horizontal Gusset	ASTM A36	See Assembly	_
i3	1	Vertical Gusset 1	ASTM A36	See Assembly	=
i4	2	Vertical Gusset 2	ASTM A36	See Assembly	1-3
i5	1	Veritcal Gusset 3	ASTM A36	See Assembly	
i6	2	Vertical Gusset 4	ASTM A36	See Assembly	
i7	1	Vertical Gusset 5	ASTM A36	See Assembly	-

^{**} Rebar does not need to be epoxy-coated for testing purposes.

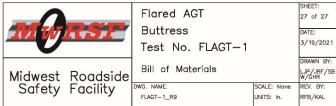


Figure 36. Bill of Materials, Cont., Test No. FLAGT-1





Figure 37. Test Installation Photographs







Figure 38. Test Installation Photographs

5 TEST CONDITIONS

5.1 Test Facility

The Outdoor Test Site is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles northwest of the University of Nebraska-Lincoln.

5.2 Vehicle Tow and Guidance System

A reverse-cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [20] was used to steer the test vehicle. A guide flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the barrier system. The 3/8-in. diameter guide cable was tensioned to approximately 3,500 lb and supported both laterally and vertically every 100 ft by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

5.3 Test Vehicle

For test no. FLAGT-1, a 2016 Ram 1500 quad cab pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 4,910 lb, 5,003 lb, and 5,163 lb, respectively. The test vehicle is shown in Figures 39 and 40, and vehicle dimensions are shown in Figure 41. The rear track width of the vehicle (69 in.) was 0.5 in. greater than the maximum value specified in MASH (67 in. \pm 1.5 in.).

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The Suspension Method [21] was used to determine the vertical component of the c.g. for the pickup truck. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The location of the final c.g. is shown in Figures 41 and 42. Data used to calculate the location of the c.g. and ballast information are shown in Appendix C.

Square, black- and white-checkered targets were placed on the vehicle for reference to be viewed from the high-speed digital video cameras and aid in the video analysis, as shown in Figure 42. Round, checkered targets were placed at the c.g. on the left-side door, the right-side door, and the roof of the vehicle.

The front wheels of the test vehicle were aligned to vehicle standards except the toe-in value was adjusted to zero such that the vehicles would track properly along the guide cable. A 5B flash bulb was mounted under the vehicle's right-side windshield wiper and was fired by a pressure tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial

impact with the test article to create a visual indicator of the precise time of impact on the high-speed digital videos. A radio-controlled brake system was installed in the test vehicle so the vehicle could be brought safely to a stop after the test.







Figure 39. Test Vehicle, Test No. FLAGT-1









Figure 40. Test Vehicle's Interior Floorboards and Undercarriage, Test No. FLAGT-1

eport No. TRP-03-439b-

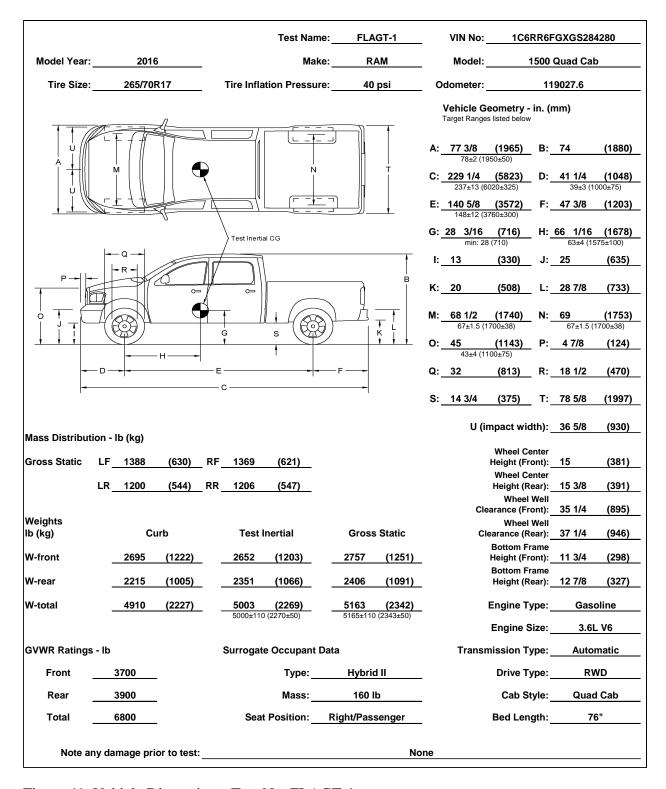


Figure 41. Vehicle Dimensions, Test No. FLAGT-1

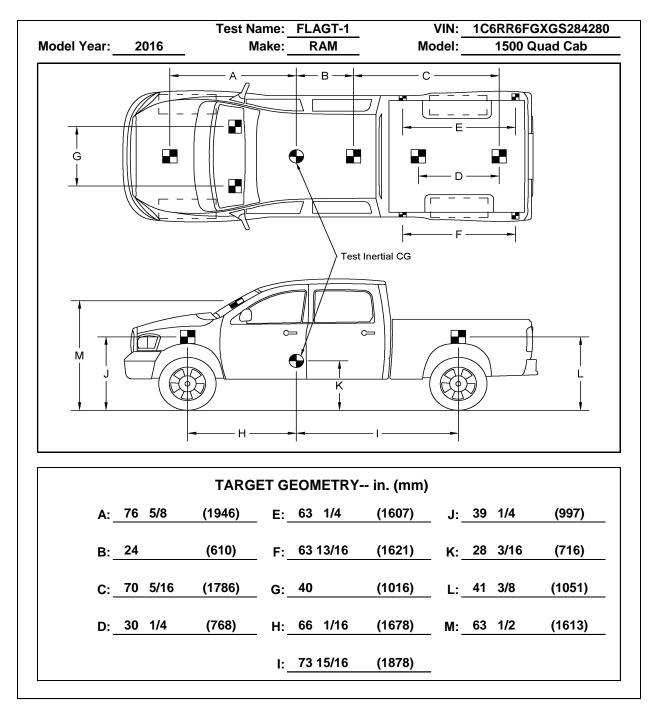


Figure 42. Target Geometry, Test No. FLAGT-1

5.4 Simulated Occupant

For test no. FLAGT-1, a Hybrid II 50th-Percentile, Adult Male Dummy equipped with footwear was placed in the right-front seat of the test vehicle with the seat belt fastened. The simulated occupant had a final weight of 160 lb. As recommended by MASH, the simulated occupant weight was not included in calculating the c.g. location.

5.5 Data Acquisition Systems

5.5.1 Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. Both accelerometer systems were mounted near the c.g. of the test vehicle. The electronic accelerometer data obtained in dynamic testing was filtered using the SAE Class 60 and the SAE Class 180 Butterworth filter conforming to the SAE J211/1 specifications [22].

The two systems, the SLICE-1 and SLICE-2 units, were modular data acquisition systems manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. The SLICE-2 unit was designated as the primary system. The acceleration sensors were mounted inside the bodies of custom-built, SLICE 6DX event data recorders and recorded data at 10,000 Hz to the onboard microprocessor. Each SLICE 6DX was configured with 7 GB of non-volatile flash memory, a range of ± 500 g's, a sample rate of 10,000 Hz, and a 1,650 Hz (CFC 1000) anti-aliasing filter. The "SLICEWare" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

5.5.2 Rate Transducers

Two identical angular rate sensor systems mounted inside the bodies of the SLICE-1 and SLICE-2 event data recorders were used to measure the rates of rotation of the test vehicle. Each SLICE MICRO Triax ARS had a range of 1,500 degrees/sec in each of the three directions (roll, pitch, and yaw) and recorded data at 10,000 Hz to the onboard microprocessors. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The "SLICEWare" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

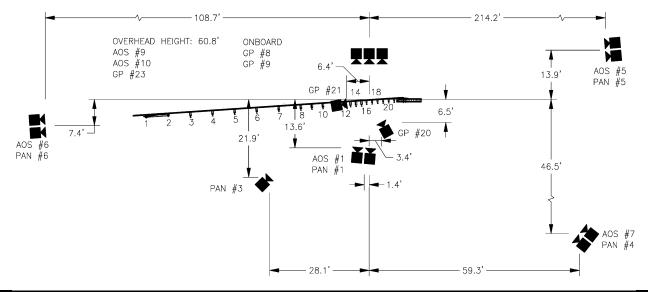
5.5.3 Retroreflective Optic Speed Trap

The retroreflective optic speed trap was used to determine the speed of the test vehicle before impact. Five retroreflective targets, spaced at approximately 18-in. intervals, were applied to the side of the vehicle. When the emitted beam of light was reflected by the targets and returned to the Emitter/Receiver, a signal was sent to the data acquisition computer, recording at 10,000 Hz, as well as the external LED box activating the LED flashes. The speed was then calculated using the spacing between the retroreflective targets and the time between the signals. LED lights and high-speed digital video analysis are only used as a backup in the event that vehicle speeds cannot be determined from the electronic data.

5.5.4 Digital Photography

Six AOS high-speed digital video cameras, five GoPro digital video cameras, and five Panasonic digital video cameras were utilized to film test no. FLAGT-1. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 43. A digital still camera was also used to document pre- and post-test conditions.

The high-speed videos were analyzed using TEMA Motion and Redlake MotionScope software programs. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed videos.



No.	Туре	Operating Speed (frames/sec)	Lens	Lens Setting
AOS-1	AOS Vitcam	500	Kowa 25mm	-
AOS-5	AOS X-PRI Gigabit	500	100 mm	-
AOS-6	AOS X-PRI Gigabit	500	Fujinon 50mm	-
AOS-7	AOS X-PRI Gigabit	500	Fujinon 50mm	-
AOS-9	AOS TRI-VIT 2236	1000	Kowa 12mm	-
AOS-10	AOS TRI-VIT 2236	1000	Kowa 16mm	-
GP-8	GoPro Hero 4	120		
GP-9	GoPro Hero 4	120		
GP-20	GoPro Hero 6	240		
GP-21	GoPro Hero 6	240		
GP-23	GoPro Hero 7	240		
PAN-1	Panasonic HC-V770	120		
PAN-3	Panasonic HC-V770	120		
PAN-4	Panasonic HC-V770	120		
PAN-5	Panasonic HC-VX981	120		
PAN-6	Panasonic HC-VX981	120		

Figure 43. Camera Locations, Speeds, and Lens Settings, Test No. FLAGT-1

6 FULL-SCALE CRASH TEST NO. FLAGT-1

6.1 Static Soil Test

Before full-scale crash test no. FLAGT-1 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The static test results, as shown in Appendix D, demonstrated a soil resistance above the baseline test limits. Thus, the soil provided adequate strength, and full-scale crash testing could be conducted on the barrier system.

6.2 Weather Conditions

Test no. FLAGT-1 was conducted on March 31, 2021 at approximately 2:15 p.m. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/KLNK) were reported and are shown in Table 3.

Table 3.	Weather	Conditions,	Test No.	FLAGT-1

Temperature	51° F
Humidity	17 %
Wind Speed	20 mph
Wind Direction	300° from True North
Sky Conditions	Scattered Clouds
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0.00 in.
Previous 7-Day Precipitation	0.00 in.

6.3 Test Description

Initial vehicle impact was to occur 93 in. upstream from the upstream edge of the concrete buttress, as shown in Figure 44, which was selected during Phase I of this project using computer simulations to maximize the probability of vehicle snag [5]. The 5,003-lb quad cab pickup truck impacted the 15:1 flared AGT at a speed of 63.2 mph and at an angle of 25.4 degrees relative to the roadway, which corresponded to 29.2 degrees relative to the flared guardrail. The actual point of impact was 90 in. upstream from the edge of the concrete buttress.

The vehicle was contained and redirected by the flared AGT, and the vehicle remained stable throughout the impact event. However, the increased effective impact severity associated with the flared installation resulted in increased system deflections as compared to other MASH TL-3 AGTs. The nested thrie beam kinked at the end of the concrete buttress, and the vehicle snagged on the kink and the buttress as it was being redirected, causing high magnitude decelerations to the vehicle. After exiting the system, the brakes were applied remotely, and the vehicle came to rest approximately 76.6 ft downstream from the upstream end of the concrete buttress and 3.6 ft in front of the system. A detailed description of the sequential impact events is contained in Table 4. Sequential photographs are shown in Figures 45 and 46. Documentary photographs of the crash test are shown in Figures 47 and 48. The vehicle trajectory and final position are shown in Figure 49.

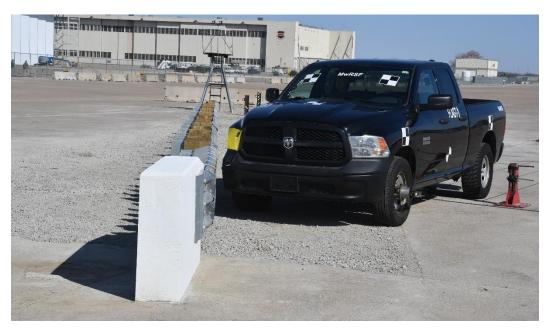






Figure 44. Impact Location, Test No. FLAGT-1

Table 4. Sequential Description of Impact Events, Test No. FLAGT-1

TIME (sec)	EVENT		
0.000	Vehicle's front bumper contacted rail 3 in. downstream from target impact location.		
0.010			
0.016	Vehicle's right fender contacted rail.		
0.020	Vehicle's grille contacted rail.		
0.030	Vehicle's hood deformed.		
0.036	Post nos. 14 through 18 deflected backward and vehicle yawed away from system.		
0.056	Vehicle's right headlight shattered and grille disengaged.		
0.060	Post no. 19 deflected backward.		
0.066	Vehicle's left fender deformed.		
0.070	Vehicle's right-front door contacted rail.		
0.078	Post no. 20 deflected backward, vehicle's right-front corner contacted upstream end of concrete buttress.		
0.088	Vehicle rolled toward system.		
0.098	Post no. 21 deflected backward.		
0.118	Vehicle's right-front door deformed. Top of door became ajar. Vehicle's left headlight disengaged.		
0.136	Vehicle's windshield cracked and roof deformed.		
0.140	Vehicle's right-front door window shattered.		
0.144	Vehicle's left-front tire became airborne.		
0.152	Vehicle's left-rear tire became airborne.		
0.168	Occupant's head contacted right-front door.		
0.192	Vehicle pitched upward.		
0.240	Vehicle was parallel to system at a speed of 33.0 mph.		
0.317	Vehicle's right quarter panel contacted concrete buttress.		
0.432	Vehicle pitched downward, vehicle yawed toward system, and vehicle exited system at a speed of 28.6 mph and an angle of -11 degrees.		
0.458	Vehicle's left-front tire regained contact with ground.		
3.124	Vehicle came to rest.		

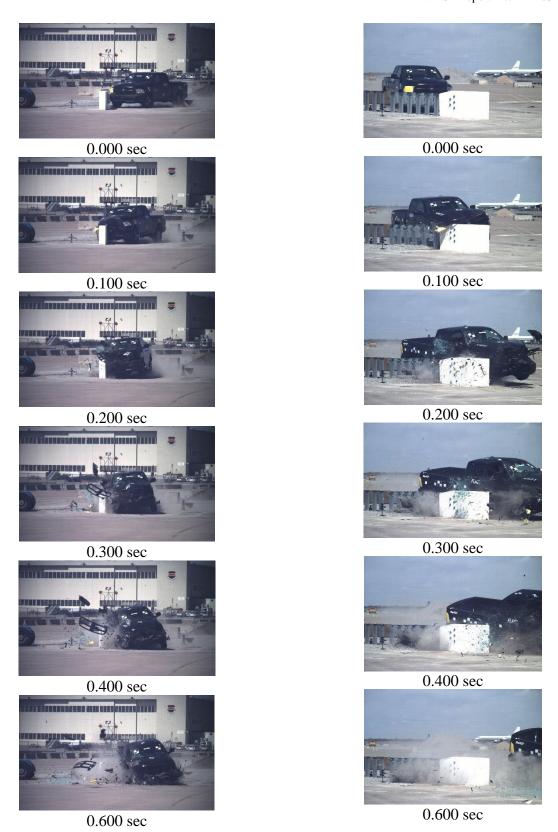


Figure 45. Sequential Photographs, Test No. FLAGT-1

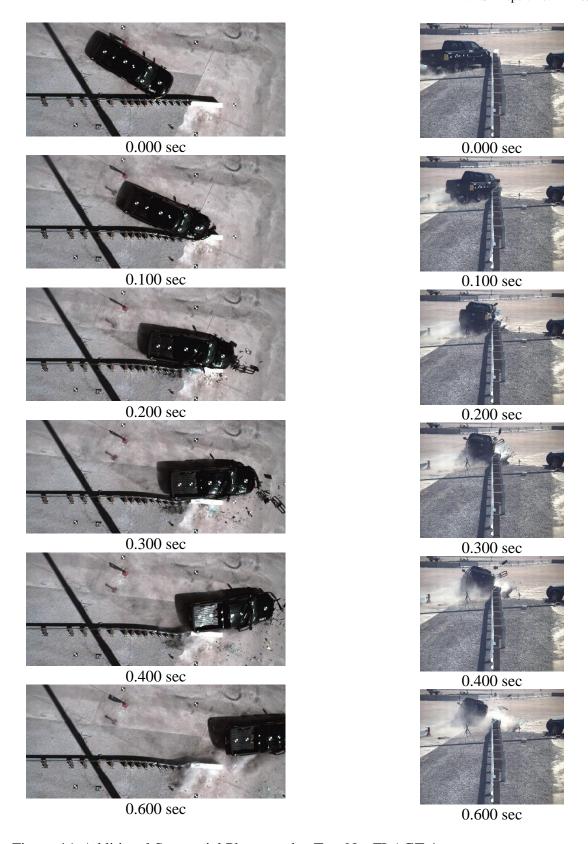


Figure 46. Additional Sequential Photographs, Test No. FLAGT-1



















Figure 47. Additional Documentary Photographs, Test No. FLAGT-1



Figure 48. Additional Documentary Photographs, Test No. FLAGT-1





Figure 49. Vehicle Final Position and Trajectory Marks, Test No. FLAGT-1

6.4 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 50 through 54. The overall length of vehicle contact along the barrier was approximately 12 ft - 3 in. and began 10 in. upstream from the center line of post no. 17. Contact marks in this region were found along the face of the thriebeam rail, the sloped top surface of the concrete buttress, and along the front of the buttress. Additionally, tire marks were observed on the lower taper of the buttress and extended $1\frac{1}{2}$ in. laterally onto the upstream face of the buttress.

Damage to the rail segments consisted of various dents, kinks, gouges, and flattening of the nested thrie beam rails. The majority of the dents and gouges were on the middle corrugation, while the bottom corrugation of the guardrail was flattened beginning at post no. 17. Small kinks were present on the top and bottom corrugations of the guardrail near post nos. 14 through 20. A large kink through the entire cross section of the thrie beam was found at the edge of the concrete buttress.

Post nos. 1 through 15 all twisted slightly to face downstream (toward impact). Post nos. 14 through 21 rotated backward, and a large soil crack had formed along the front flanges of post nos. 17 though 20. The soil crack had a depth of at least 15 in. and maximum width of 4 in. near post no. 19. Various contact marks were observed on the blockouts of post nos. 18 through 20, and localized buckling and deformations were found on the front flanges of post nos. 19 and 20.





Figure 50. System Damage, Test No. FLAGT-1





Figure 51. System Damage, Test No. FLAGT-1









Figure 52. Post Nos. 18 through 21 Damage, Test No. FLAGT-1









Figure 53. Post Nos. 15 through 17 Damage, Test No. FLAGT-1





Figure 54. Soil Gaps, Test No. FLAGT-1

May 16, 2025 MwRSF Report No. TRP-03-439b-25

The maximum lateral permanent set of the barrier system was 10.8 in., which occurred in the guardrail between post nos. 19 and 20, as measured in the field. The maximum lateral dynamic barrier deflection was 16.8 in. located at post no. 19, as determined from high-speed digital video analysis. The working width of the system was found to be 36.5 in., determined from high-speed digital video analysis. A schematic of the permanent set deflection, dynamic deflection, and working width is shown in Figure 55.

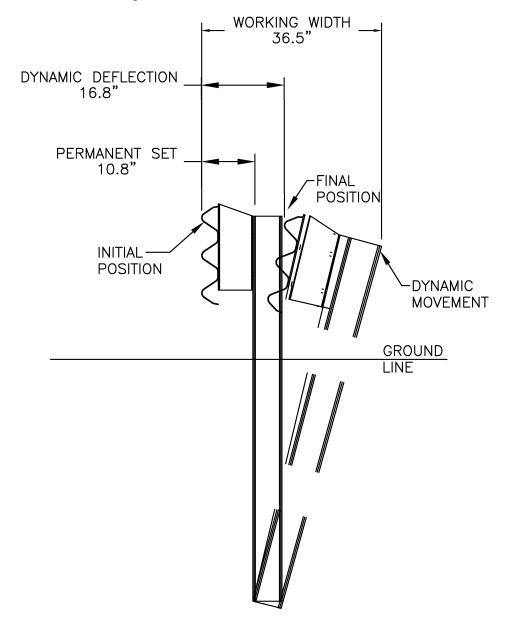


Figure 55. Permanent Set Deflection, Dynamic Deflection, and Working Width, Test No. FLAGT-1

6.5 Vehicle Damage

The damage to the vehicle was severe, as shown in Figures 56 and 57. Majority of the exterior damage was concentrated on the right-front area of the vehicle where the impact had occurred. The right-front corner of the vehicle and the right-front door were both crushed inward. The grille was disengaged, the right side of the front bumper was crushed inward, and the left side of the bumper was pushed out slightly. The right-front fender panel was completely crushed inward. There were scrapes, dents and gouges present along the entire right side of the vehicle, but they were concentrated on the bottom half of the right-side doors. Both right-side wheels were deflated.

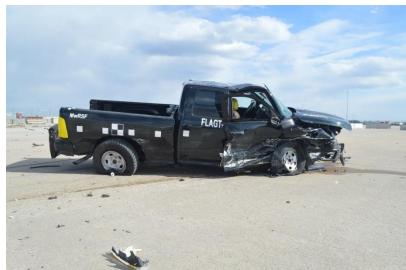
The front right and left front shocks and springs were bent rearward, and the front-right bump stop disengaged. The rear right spring was also disengaged. The sway bar shifted and the right-front steering knuckle was scraped. The right lower control arm disconnected from the cross member, the right tie rod was bent, and the gearbox was cracked. The right side axle tube was bent severely and the engine mounts completely disengaged. The oil pan was punctured and crushed on the right side, and the casting was fractured on the pan.

The chassis of the vehicle was severely deformed around the contact area. The right-side engine cross members were bent backward, and scrapes were found along the right side of the transmission cross member. The right frame horn was completely crushed inward and the left frame horn was facing slightly outward. The windshield was severely cracked due to loading and displacement of the A-pillar, but the windshield remained in place. The front-right window was shattered and disengaged from the vehicle due to contact with the simulated occupant.

The maximum occupant compartment intrusions are listed in Table 5, along with the intrusion limits established in MASH for various areas of the occupant compartment. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix E. MASH defines intrusion or deformation as the occupant compartment being deformed and reduced in size with no observed penetration. Outward deformations, which are denoted as negative numbers in Appendix E, are not considered crush toward the occupant, and are not evaluated by MASH criteria. The maximum occupant compartment deformation was 12.0 in. in the wheel well and toe pan, which exceeded MASH limits. Significant deformations were also observed to the side front panel and the right-side A-pillar, though these deformations did not violate MASH limits.











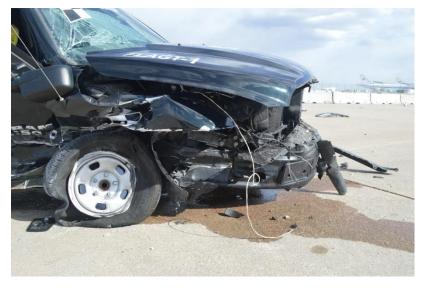




Figure 57. Vehicle Damage, Undercarriage and Occupant Compartment, Test No. FLAGT-1

Table 5. Maximum Occupant Compartment Intrusion by Location, Test No. FLAGT-1

Location	Maximum Intrusion In.	MASH Allowable Intrusion in.
Wheel Well & Toe Pan	12.0	≤ 9
Floor Pan & Transmission Tunnel	7.8	≤ 12
A-Pillar	4.1	≤ 5
A-Pillar (Lateral)	1.5	≤ 3
B-Pillar	1.8	≤ 5
B-Pillar (Lateral)	1.0	≤ 3
Side Front Panel (in Front of A-Pillar)	8.6	≤ 12
Side Door (Above Seat)	0.0*	≤ 9
Side Door (Below Seat)	2.6	≤ 12
Roof	2.1	≤ 4
Windshield	**	≤ 3
Side Window	Shattered due to contact with simulated occupant's head	No shattering resulting from contact with structural member of test article
Dash	6.0	N/A

^{*}Negative value reported as 0.0. See Appendix E for further information.

6.6 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec average occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions, as determined from the accelerometer data, are shown in Table 6. Note that the longitudinal ORA measured by the primary accelerometer exceeded MASH limits. The calculated THIV, PHD, and ASI values are also shown in Table 6. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix F.

^{**}The windshield was cracked and deformed but no intrusion into the cab was present. The right-side A-pillar's inward movement caused the windshield to crush and bow outward. Therefore, no measurements were taken. N/A – No MASH criteria exist for this location.

Table 6. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. FLAGT-1

			ducer	MACH
Evaluation Criteria		SLICE-1 (backup)	SLICE-2 (primary)	MASH Limits
OIV	Longitudinal	-35.62	-29.06	±40
ft/s	Lateral	-23.30	-24.12	±40
ORA	Longitudinal	-17.22	-24.23	±20.49
g's	Lateral	-7.68	-12.46	±20.49
Maximum	Roll	20.9	19.4	±75
Angular Displacement	Pitch	-10.2	-11.6	±75
deg.	Yaw	-40.4	-39.6	not required
THIV – ft/s		36.52	36.20	not required
PHD – g's		25.27	30.05	not required
ASI		1.61	1.68	not required

6.7 Discussion

The analysis of test no. FLAGT-1 showed that the system adequately contained and redirected the 2270P vehicle. A summary of the test results and sequential photographs are shown in Figure 58. The test vehicle remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix F, were deemed acceptable. Detached elements, fragments, or other debris from the test article did not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or work-zone personnel. After impact, the vehicle exited the barrier at an angle of -11 degrees, and its trajectory did not violate the bounds of the exit box. Note, exit box criteria is difficult to apply to any longitudinal barrier system that changes direction within the impact region as the face of the system would have multiple tangent lines. However, in Figure 58 the exit box is drawn relative to the flared AGT since the majority of contact was with the AGT.

However, increased system deflections lead to a large kink forming the nested thrie beam at the upstream end of the concrete buttress, and the test vehicle snagged on the kink as it was being redirected. This snag caused excessive vehicle deformation and decelerations. The maximum occupant compartment intrusion measurement at the wheel well and toe pan location of 12.0 in. exceeded the MASH limit of 9 in., and the longitudinal ORA value of -24.23 g's exceeded the MASH limit of \pm 20.49 g's. Thus, due to the excessive occupant compartment deformation and longitudinal ORA value, test no. FLAGT-1 was determined to be unacceptable according to the MASH safety performance criteria for test designation no. 3-21.

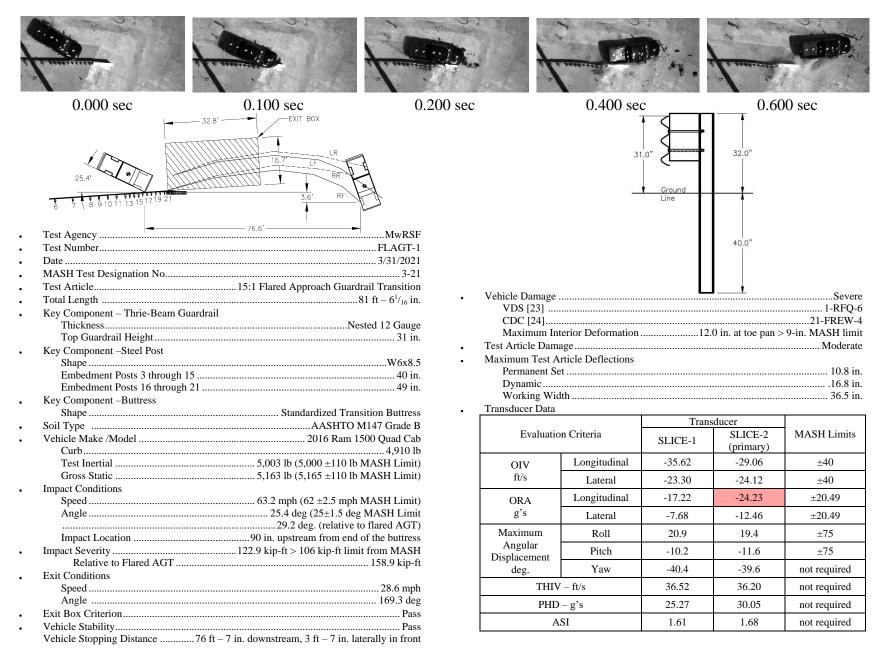


Figure 58. Summary of Test Results and Sequential Photographs, Test No. FLAGT-1

7 TEST NO. FLAGT-1 FAILURE ANALYSIS

Test no. FLAGT-1 was determined to be unacceptable according to the safety performance criteria for MASH test designation no. 3-21 for two reasons: (1) the longitudinal ORA of -24.23 g's exceeded the MASH limit of ± 20.49 g's, and (2) the 12.0-in. intrusion into the toe pan area of the occupant compartment exceeded the MASH limit of 9 in. After examining all available data for this test, it became evident that both the excessive decelerations and excessive occupant compartment crush were the result of the vehicle snagging on the system during redirection. Recall, a large kink formed in the rail at the upstream end of the concrete buttress. This kink and the rigid buttress located directly behind it were responsible for causing the vehicle snag.

A review of the longitudinal acceleration data showed a high-magnitude spike centered about 95 ms after initial impact. As shown in Figure 59, this spike was well above the accelerations observed during the rest of the impact and a departure from the acceleration observed in previous MASH evaluations of AGTs. Shown in Figure 59, the "AGTB-2" [1] data represents a MASH test designation no. 3-21 impact into the same AGT tested herein, only installed tangent to the roadway (i.e., without a flare), and the "15:1 Simulation" data was taken from the simulation analysis conducted on the 15:1 flared AGT during Phase I of this project [5]. Neither of these previous analyses showed vehicle snagging nor had test curves with high acceleration spikes. At 95 ms into test no. FLAGT-1, the vehicle was in direct contact with the guardrail kink and the upstream end of the concrete buttress, as shown in Figure 60.

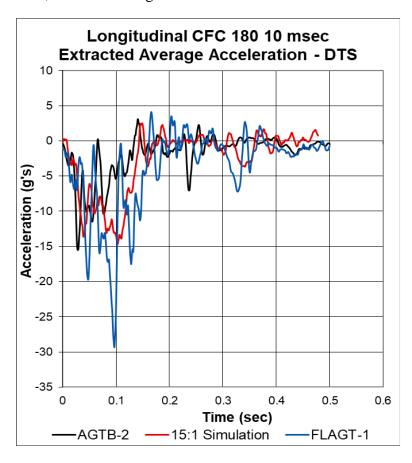


Figure 59. Comparison of Longitudinal CFC 180 10-msec Extracted Average Accelerations



Figure 60. Overhead View of Test No. FLAGT-1, 95 ms after Impact

As noted previously in Section 6.4, tire contact marks were found on the lower taper and upstream end of the concrete buttress. However, this is not uncommon for MASH tests on AGTs with the standardized transition buttress. The amount of lateral overlap of the tire on the buttress in test no. FLAGT-1 was estimated to be 6 in., as measured from the front face of the buttress. This tire overlap fell between two other MASH test designation no. 3-21 tests on tangent AGTs with the standardized transition buttress. Test no. AGTB-2 [1] had 5 in. of tire overlap, while test no. 34AGT-1 [25] had 6.5 in. of tire overlap. This indicated that the wheel snag on the buttress was similar to previous successful MASH tests. Thus, the excessive decelerations and occupant compartment crush were not the result of wheel snag, but instead were caused by the vehicle snagging on the kink and the concrete buttress behind the guardrail.

The large kink that formed in the nested thrie beam was a damage characteristic not observed in previous MASH testing of AGTs. It is believed that excessive guardrail deflections within the nested thrie beam region of the AGT led to the formation of this kink. System deflections were expected to be higher than previous MASH AGTs due to the increase in impact severity associated with the flared guardrail. However, the lateral deflections of the flared AGT in test no. FLAGT-1 were significantly higher than predicted.

The maximum dynamic deflections for each post in the impact region from test no. FLAGT-1 are listed in Table 7 and compared to the deflections in the simulated crash test for the 15:1 flared AGT [5] and test no. AGTB-2 [1], which evaluated a tangent installation of the AGT evaluated herein. The simulation analysis predicted deflection increases of about 1.5 to 2 times the observed post deflections from test no. AGTB-2. However, the dynamic deflections from test no. FLAGT-1 were over 3 times that of the tangent system and over 50 percent higher than the simulation results. Specifically, the maximum dynamic deflection was 3.7 times higher in test no. FLAGT-1 as compared to test no. AGTB-2. These trends were also observed in the permanent set displacements of the AGTs, shown in Table 8.

The unusually high deflections within the AGT posts were also evident by the large soil crack that opened up along the front flanges of the transition posts. This was another damage characteristic not observed in previous successful MASH testing of AGTs. The posts themselves did not plastically bend during the impact, rather, the soil behind the posts shifted and allowed the posts to rotate back to achieve high system deflections. Design changes to increase the post-soil strength and reduce the system deflections may be necessary to create a crashworthy AGT flared at a 15:1 rate. These design changes will be explored in the next phase of the project.

Table 7. Maximum Lateral Dynamic Deflections in AGT Posts

-				Dynamic Deflection (in.)		
Test	Post No. 21	Post No. 20	Post No. 19	Post No. 18	Post No. 17	Post No. 16
FLAGT-1 15:1 Flare	4.6	13.1	16.8	10.4	7.2	4.3
Simulation 15:1 Flare	2.4	8.1	10.7	8.8	4.9	2.0
AGTB-2 Tangent	1.4	3.9	4.5	3.9	2.8	1.9

Table 8. Permanent Set Comparison, Test No. FLAGT-1, Simulation, and Test No. AGTB-2

T	Permanent Set (in.)					
Test	Post No. 21	Post No. 20	Post No. 19	Post No. 18	Post No. 17	Post No.
FLAGT-1	4.1	9.3	10.4	8.4	5.1	3.3
Simulation	2.0	7.2	9.2	7.6	4.2	1.6
AGTB-2	1.0	1.6	2.3	2.5	1.9	1.1

8 SUMMARY AND CONCLUSIONS

The main research objective for this project was to develop guidelines for flaring approach guardrail transitions. A critical AGT design, the critical flare rate of 15:1, and critical impact points were identified during Phase I of this project. The research documented in this report focused on the full-scale crash testing and evaluation of the 15:1 flared AGT according to MASH TL-3 criteria. A summary of the test evaluation is shown in Table 9.

In test no. FLAGT-1, the 5,003-lb pickup truck impacted the AGT at a 25.4-degree angle relative to the roadway (29.2 degrees relative to the guardrail) and at a speed of 63.2 mph, resulting in an impact severity of 122.9 kip-ft (158.9 kip-ft relative to the guardrail). The actual impact location was 90 in. upstream from the end of the concrete buttress. The pickup truck was captured and redirected in a stable manner and came to rest 76.6 ft downstream from the buttress after brakes were applied. Permanent set, dynamic deflection, and working width were measured at 10.8 in., 16.8 in., and 36.5 in., respectively.

However, the vehicle toe pan area was crushed inward 12 in., which exceeded the MASH limit of 9 in. for this region of the occupant compartment. Additionally, the longitudinal ORA value of -24.23 g's exceeded the MASH limit of ± 20.49 g's. Because of these two factors, test no. FLAGT-1 was deemed unsuccessful according to the safety criteria of MASH.

Detailed evaluation of test no. FLAGT-1 revealed that excessive guardrail deflections resulted in a large kink forming in the nested thrie beam rails at the upstream end of the concrete buttress. The pickup truck snagged on this guardrail kink and the rigid buttress directly behind it, which caused excessive occupant compartment intrusion and decelerations. The flared AGT will need to be redesigned to limit system deflections and create a crashworthy barrier.

Table 9. Summary of Safety Performance Evaluation

Evaluation Factors		Evaluation Criteria			Test No. FLAGT-1
Structural Adequacy	A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.			S
	D.	1. Detached elements, fragme should not penetrate or show compartment, or present an un or personnel in a work zone.	potential for penetrating t	he occupant	S
		2. Deformations of, or intrus should not exceed limits set for MASH.			U
	F.		The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.		
Occupant Risk	H.		Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH for calculation procedure) should satisfy the following limits:		
		Occupant Ir	npact Velocity Limits		S
		Component	Preferred	Maximum	
		Longitudinal and Lateral	30 ft/s	40 ft/s	
	I. The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.2.2 of MASH for calculation procedure) should satisfy the following limits:			U	
	Occupant Ridedown Acceleration Limits				U
		Component	Preferred	Maximum	
		Longitudinal and Lateral			
Longitudinal and Lateral 15.0 g's 20.49 g's MASH Test Designation No.				3-21	
Final Evaluation (Pass or Fail)			Fail		

 $S-Satisfactory \quad \ \ U-Unsatisfactory \quad NA-Not \ Applicable$

9 REFERENCES

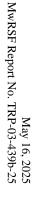
- 1. Rosenbaugh, S.K., Faller, R.K., Asselin, N., and Hartwell, J.A., *Development of a Standardized End Buttress for Approach Guardrail Transitions*, Report No. TRP-03-369-20, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, November 10, 2020.
- 2. Stolle, C.S., Polivka, K.A., Reid, J.D., Faller, R.K., Sicking, D.L., Bielenberg, R.W., and Rohde, J.R., *Evaluation of Critical Flare Rates for the Midwest Guardrail System (MGS)*, Report No. TRP-03-191-08, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, July 15, 2008.
- 3. Ross, H.E., Sicking, D.L., Zimmer, R.A., and Michie, J.D., *Recommended Procedures for the Safety Performance Evaluation of Highway Features*, National Cooperative Highway Research Program (NCHRP) Report 350, Transportation Research Board, Washington, D.C., 1993.
- 4. *Manual for Assessing Safety Hardware (MASH)*, Second Edition, American Association of State Highway and Transportation Officials (AASHTO), Washington, D.C., 2016.
- 5. Bickhaus, R.F., Rasmussen, J.D., Bielenberg, R.W., Rosenbaugh, S.K., Faller, R.K., and Reid, J.D., *Evaluation of Flare Rates for Approach Guardrail Transitions Phase I*, Report No. TRP-03-439a-22, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, November 22, 2022.
- 6. Bickhaus, R.F., Rasmussen, J.D., Reid, J.D., *Development and Validation of a Thrie-Beam AGT LS-DYNA Model*, Report No. TRP-03-441-22, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, May 13, 2022.
- 7. Polivka, K.A., Faller, R.K., Sicking, D.L., Rohde, J.R., Bielenberg, R.W., Reid, J.D., and Coon, B.A., *Performance Evaluation of the Guardrail to Concrete Barrier Transition Update to NCRP 350 Test No. 3-21 with 28" C.G. Height (2214T-1)*, Report No. TRP-03-175-06, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, October 12, 2006.
- 8. Soyland, K., Faller, R.K., Sicking, D.L., and Holloway, J.C., *Development and Testing of an Approach Guardrail Transition to a Single Slope Concrete Median Barrier*, Report No. TRP-03-47-95, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, November 1995.
- 9. Bielenberg, R.W., Lingenfelter, J.L., Kohts, J.E., Faller, R.K., and Reid, J.D., *Testing and Evaluation of MASH TL-3 Transition between Guardrail and Portable Concrete Barriers*, Report No. TRP-03-335-17, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, May 2, 2017.

- 10. Bielenberg, R.W., Ahlers, T.J., Faller, R.K., and Holloway, J.C., *MASH Testing of Bullnose with Breakaway Steel Posts (Test Nos. MSPBN-4 through MSPBN-8)*, Report No. TRP-03-418-20, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, September 1 2020.
- 11. Abu-Odeh, A.Y., Smith, C., Menges, W.L., and Kuhn, D.L., *Optimization of Thrie Beam Terminal End Shoe Connection*, Report No. 9-1002-15-6, Texas A&M Transportation Institute, Texas A&M University System, College Station, Texas, April, 2017.
- 12. *Manual for Assessing Safety Hardware (MASH)*, American Association of State Highway and Transportation Officials (AASHTO), Washington, D.C., 2009.
- 13. Polivka, K.A., Faller, R.K., Sicking, D.L., Rohde, J.R., Bielenberg, R.W., Reid, J.D., and Coon, B.A., *Performance Evaluation of the Guardrail to Concrete Barrier Transition Update to NCHRP 350 Test No. 3-21 with 28 in. C.G. Height (2214T-1)*, Report No. TRP03-175-06, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, NE, October 12, 2006.
- 14. Rosenbaugh, S.K., Lechtenberg, K.A., Faller, R.K., Sicking, D.L., Bielenberg, R.W., and Reid, J.D., *Development of the MGS Approach Guardrail Transition Using Standardized Steel Posts*, Report No. TRP-03-210-10, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, December 21, 2010.
- 15. Winkelbauer, B.J., Putjenter, J.G., Rosenbaugh, S.K., Lechtenberg, K.A., Bielenberg, R.W., Faller, R.K., and Reid, J.D., *Dynamic Evaluation of MGS Stiffness Transition with Curb*, Report No. TRP-03-291-14, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, June 30, 2014.
- Mongiardini, M., Faller, R.K., Reid, J.D., Sicking, D.L., Stolle, C.S., and Lechtenberg, K.A., *Downstream Anchoring Requirements for the Midwest Guardrail System*, Report No. TRP- 03-279-13, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, October 28, 2013.
- 17. Mongiardini, M., Faller, R.K., Reid, J.D., and Sicking, D.L., *Dynamic Evaluation and Implementation Guidelines for a Non-Proprietary W-Beam Guardrail Trailing-End Terminal*, Paper No. 13-5277, Transportation Research Record No. 2377, Journal of the Transportation Research Board, TRB AFB20 Committee on Roadside Safety Design, Transportation Research Board, Washington D.C., January 2013, pages 61-73.
- 18. Stolle, C.S., Reid, J.D., Faller, R.K., and Mongiardini, M., *Dynamic Strength of a Modified W-Beam BCT Trailing-End Termination*, Paper No. IJCR 886R1, Manuscript ID 1009308, International Journal of Crashworthiness, Taylor & Francis, Vol. 20, Issue 3, Published online February 23, 2015, pages 301-315.
- 19. Griffith, M.S., Federal Highway Administration (FHWA), *Eligibility Letter HSST/B-256 for: Trailing-End Anchorage for 31" Tall Guardrail*, December 18, 2015.

- 20. Hinch, J., Yang, T.L., and Owings, R., *Guidance Systems for Vehicle Testing*, ENSCO, Inc., Springfield, Virginia, 1986.
- 21. Center of Gravity Test Code SAE J874 March 1981, SAE Handbook Vol. 4, Society of Automotive Engineers, Inc., Warrendale, Pennsylvania, 1986.
- 22. Society of Automotive Engineers (SAE), *Instrumentation for Impact Test Part 1 Electronic Instrumentation*, SAE J211/1 MAR95, New York City, New York, July, 2007.
- 23. *Vehicle Damage Scale for Traffic Investigators*, Second Edition, Technical Bulletin No. 1, Traffic Accident Data (TAD) Project, National Safety Council, Chicago, Illinois, 1971.
- 24. Collision Deformation Classification Recommended Practice J224 March 1980, Handbook Volume 4, Society of Automotive Engineers (SAE), Warrendale, Pennsylvania, 1985.
- 25. Rosenbaugh, S.K., Fallet, W.G., Faller, R.K., Bielenberg, R.W., and Schmidt, J.D., *34-in. Tall Thrie Beam Transition to Concrete Buttress*, Report No. TRP-03-367-19, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, March 27, 2019.

10 APPENDICES

Appendix A. A2LA Accreditation Certificates





Accredited Laboratory

A2LA has accredited

MIDWEST ROADSIDE SAFETY FACILITY (MWRSF)

Lincoln, NE

for technical competence in the field of

Mechanical Testing

This laboratory is accredited in accordance with the recognized International Standard ISO/IEC 17025:2017

General requirements for the competence of testing and calibration laboratories. This accreditation demonstrates technical competence for a defined scope and the operation of a laboratory quality management system

(refer to joint ISO-ILAC-IAF Communiqué dated April 2017).



Presented this 12th day of February 2020.

Vice President, Accreditation Services For the Accreditation Council Certificate Number 2937.01 Valid to November 30, 2021

For the tests to which this accreditation applies, please refer to the laboratory's Mechanical Scope of Accreditation.

Figure A-1. Midwest Roadside Safety Facility A2LA Accreditation Certificate No. 2937.01



SCOPE OF ACCREDITATION TO ISO/IEC 17025:2017

MIDWEST ROADSIDE SAFETY FACILITY (MwRSF)1 University of Nebraska-Lincoln 4630 NW 36th Street Lincoln, NE 68524 Ms. Karla Lechtenberg Phone: 402 472 9070

MECHANICAL

Valid To: November 30, 2021 Certificate Number: 2937.01

In recognition of the successful completion of the A2LA evaluation process, accreditation is granted to this laboratory to perform the following tests:

<u>Tests</u>	Test Methods ²
Full-Scale Vehicle Crash Tests of Highway Safety Features	NCHRP Report 350; MASH; EN 1317
Full-Scale Vehicle Crash Tests of Perimeter Protection Systems and Access Control Devices	ASTM F2656; SD-STD-02.01 Revision A
Bogie Dynamic Tests of Highway Safety Features	Non-Standard Test Method: Dynamic Testing of Steel Post and Rigid Foundation; Non-Standard Test Method: Dynamic Testing of Post in Soil; Non-Standard Test Method: Dynamic Testing of Spacer Blocks
Crushable Nose Bogie Testing for Breakaway Supports	Non-Standard Test Method: Dynamic Testing of Breakaway Supports; AASHTO Breakaway Poles and Supports; NCHRP Report 350

On the following types of products, materials, and/or structures:

Metal, Wood, Concrete and Plastic Structures, Components of Structures, Fasteners, and Roadway Pavements.

(A2LA Cert. No. 2937.01) 02/12/2020

5202 Presidents Court, Suite 220 | Frederick, MD 21703-8515 | Phone: 301 644 3248 | Fax: 240 454 9449 | www.A2LA.org

Figure A-2. Midwest Roadside Safety Facility Scope of Accreditation to ISO/IEC 17025

¹ Administrative office located at: 2200 Vine Street, 130 Whittier Building, Lincoln, NE 68583-0853.

² This laboratory meets A2LA R104 - General Requirements: Accreditation of Field Testing and Field Calibration Laboratories for these tests.

Appendix B. Material Specifications

Table B-1. Bill of Materials, Test No. FLAGT-1

Item No.	Description	Material Specification	Reference
a1	12'-6" 12-gauge Thrie-Beam Section	AASHTO M180	H#L33120
a2	6'-3" 12-gauge Thrie-Beam Section	AASHTO M180	H#L33720
a3	6'-3" 10-gauge W-Beam to Thrie- Beam Asymmetric Transition Section	AASHTO M180	H#250344
a4	12'-6" 12-gauge W-Beam MGS Section	AASHTO M180	H#C85187
a5	12'-6" 12-gauge W-Beam MGS End Section	AASHTO M180	H#9411949
a6	10-gauge Thrie-Beam Terminal Connector	AASHTO M180 Gr. 50 Min. yield strength=50 ksi Min. ultimate strength=70 ksi	H#833M66260
b1	Concrete - 21.9 cubic ft	Min. f'c = 4,000 psi	Sample #011 Set # FLAGT1,FLAGT2
c1	BCT Timber Post - MGS Height	SYP Grade No. 1 or better (No knots +/- 18" from ground on tension face)	C#2538 P#GS6846
c2	72" Long Foundation Tube	ASTM A500 Gr. B	H#821T08220
c3	Ground Strut Assembly	ASTM A36	H#163375
c4	BCT Cable Anchor Assembly	-	PO#40299 ASPI#122160
c5	Anchor Bracket Assembly	ASTM A36	H#V911470
с6	5/8"x8"x8" Anchor Bearing Plate	ASTM A36	H#4181496
c7	2 ³ / ₈ " O.D. x 6" Long BCT Post Sleeve	ASTM A53 Gr. B Schedule 40	H#8712810
d1	W6x8.5, 72" Long Steel Post	ASTM A992	H#55066501/03
d2	W6x8.5, 72" Long Steel Post	ASTM A992	H#55066501/03
d3	W6x8.5, 78" Long Steel Post	ASTM A992	H#55068023/02
d4	6"x12"x14" Timber Blockout	SYP Grade No.1 or better	C#1695 P#GR61214
d5	6"x12"x19" Timber Blockout	SYP Grade No.1 or better	C#2580 P#GR61219
d6	17 ½" Long, 7"x4"x ³ / ₁₆ " Iowa Steel Blockout	ASTM A500 Gr. B	H#Y0521/Y0523

Table B-2. Bill of Materials, Test No. FLAGT-1, Cont.

Item No.	Description	Material Specification	Reference
d7	16D Double Head Nail	-	PO#E000548963 P#97812A109
e1	86" Unbent Length, #4 Rebar ASTM A615 Gr. 60		H#3600014740
e2	62 ¾" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e3	60 ½" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e4	59 ¼" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e5	74 ¾" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e6	37 ¼" Long, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e7	80 1/4" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e8	85 ½" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e9	80" Long, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
e10	80 ½" Unbent Length, #4 Rebar	ASTM A615 Gr. 60	H#3600014740
f1	%" Dia. UNC, 14" Long Guardrail Bolt	ASTM A307 Gr. A	H#100897520
f2	%" Dia. UNC, 10" Long Guardrail Bolt	ASTM A307 Gr. A	H#1721198
f3	%" Dia. UNC, 2" Long Guardrail Bolt	ASTM A307 Gr. A	H#20303430
f4	%" Dia. UNC, 1 ¼" Long Guardrail Bolt	ASTM A307 Gr. A	H#10634210
f5	%" Dia. UNC, 15 ½" Long Heavy Hex Head Bolt	ASTM F3125 Gr. 120 (A325) or A354 Gr. BC	H#3093334
f6	%" Dia. UNC, 8" Long Hex Head Bolt	ASTM A307 Gr. A	FASTENAL COC 04/12/2018
f7	%" Dia. UNC, 10" Long Hex Head Bolt	ASTM A307 Gr. A	H#JK18104124
f8	5/8" Dia. UNC, 11/2" Long Hex Head Bolt	ASTM A307 Gr. A	H#5-01571
g1	7/8" Dia. Plain Round Washer	ASTM F844	L#1844804 PO#170089822
g2	5/8" Dia. Plain Round Washer	ASTM F844	L#20200515 C#000825
g3	3"x3"x ¹ / ₄ " or 3 ¹ / ₂ "x ³ / ₂ "x ¹ / ₄ " Square Washer Plate	ASTM A572 Gr. 50	H#B9L648

Table B-3. Bill of Materials, Test No. FLAGT-1, Cont.

Item No.	Description	Material Specification	Reference
g4	1" Dia. Plain Round Washer	nd Washer ASTM F844 PO#2	
h1	5/8" Dia. Heavy Hex Nut	ASTM A563A	H#10640980
h2	5/8" Dia. Hex Nut	ASTM A563A	H#331608011
h3	7/8" Dia. UNC Heavy Hex Nut	ASTM A563DH or A194 Gr. 2H	H#190841
h4	7/8" Dia. Hex Nut	ASTM A563A	H#331704677
h5	1" Dia. Heavy Hex Nut	ASTM A563A	FASTENAL COC 11/29/2018
i1	AGT Connector Face Plate	ASTM A36	H#Y6325
i2	Horizontal Gusset	ASTM A36	H#813L65970
i3	Vertical Gusset 1	ASTM A36	H#813L65970
i4	Vertical Gusset 2	ASTM A36	H#813L65970
i5	Vertical Gusset 3	ASTM A36	H#813L65970
i6	Vertical Gusset 4	ASTM A36	H#813L65970
i7	Vertical Gusset 5	ASTM A36	H#813L65970

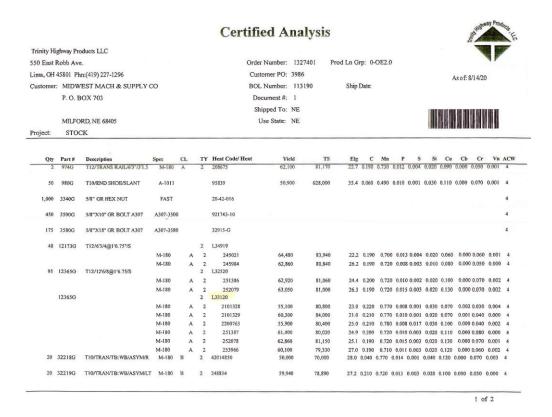


Figure B-1. 12.5-ft Thrie Beam Guardrail, Test No. FLAGT-1 (Item No. a1)

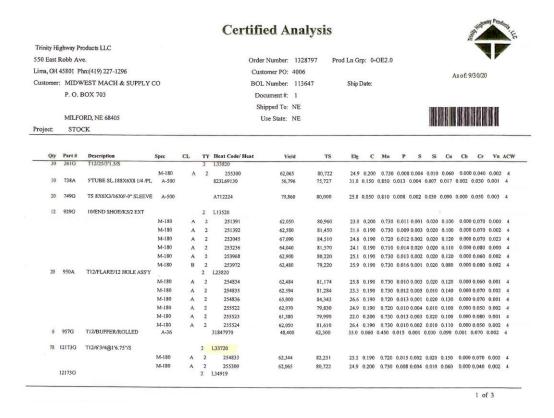


Figure B-2. 6.25-ft Thrie Beam Guardrail, Test No. FLAGT-1 (Item No. a2)



PO Box 699 - Pleasant Grove, UT 84062 Phone (801) 785-0505 www.uisutah.com

Customer PO Number: FLAGT

Material Certificate Of Compliance

Date: 12/08/20

Page 1/1

Customer: Ship To:

University of Nebraska Lincoln
PO Box 880439
University of Nebraska Lincoln
Midwest Roadside Safety Facility
4630 NW 36 ST
Lincoln
NE 685880439
Lincoln
NE 68524

Project ID:

Transitions

Project Description: (GR) Nebraska

Order Number: 78327

Line #	QTY	Units	Description
1	4	EACH	10 / 6'-3 / 3'-1 1/2" Transition A Sym. Left (IMH # RWT-ALbB-Leading)

This is to certify that the materials shipped meet the requirements of the above Contract Specifications and Special Provisions. Guardrail meets the requirements of AASHTO M-180, Type I, II, III, or IV as stamped. Steel Posts meet the requirements of AASHTO M-270 / M-183, ASTM A992-06a: A36 and are Galvanized per ASTM A-123 OR Steel Posts meet the requirements of ASTM A588 (if required per Contract Specifications). Anchor Cable meets the requirements of ASTM 741-11, AASHTO M30. Hardware meets the requirement of AASHTO M-180, ASTM A-307 and/or A-325 or A449 per contract requirements. Galvanized per ASTM A-153. All Structural Steel conforms to AASHTO M-270 / M-183 and the Buy America Act 23 CFR 635.410. All other Galvanized Materials conform to ASTM A-123 or ASTM A-153. The materials covered by this certification conform to the requirements specified in the contract documents. The individual signing has the legal authority to bind the manufacturer or supplier of material.

STATE OF UTAH, COUNTY OF UTAH

Sworn and Subscribed before me

Universal Industrial Sales, Inc.

ROBERT JON McDONALD BY
NOTARY PUBLIC STATE OF UTAH
COMMISSION# 713304
COMM. EXP. 08-06-2024

Sign Structures, Bridge Rail, Steel Fabrication, Anchor Bolts, Highway Construction Products

Figure B-3. 10-ga. W-to-Thrie Transition Segment, Test No. FLAGT-1 (Item No. a3)

Description

12GA 12FT6IN/3FT1 1/2IN WB T2

GREGORY HIGHWAY PRODUCTS, INC. 4100 13th St. SW Canton, Ohio 44710

Test Report Ship Date: Customer P O: 1/26/2018 UNIVERSITY OF NEBRASKA-LINCOLN 401 CANFIELD ADMIN BLDG P O BOX 880439 LINCOLN,NE,68588-0439 36263 UNIVERSITY OF NEBRASKA-LINCOLN Shipped to: 319AA Elong. Yield HT#code Heat # 150 80433 59371 0.48 0.008 0.003

Bolts comply with ASTM A-307 specifications and are galvanized in accordance with ASTM A-153, unless otherwise stated.
Nuts comply with ASTM A-563 specifications and are galvanized in accordance with ASTM A-153, unless otherwise stated.
All other galvanized material conforms with ASTM-123 & ASTM-653
All Calvanizing has occurred in the United States
All Salvanizing has occurred in the United States
All Stell used in the manufacture is of Domestic Origin, "Made and Melted in the United States"
All Stell used meets Title 23CFR 63.6.10 E. By America
All Guardrait and Terminal Sections meets AASHTO M-180, All structural steel meets AASHTO M-183 & M270
All Bolts and Nuts are of Domestic Origin.
All material fabricated in accordance with Nebraska Department of Transportation
All controlled oxidized/corrosion resistant Guardrail and terminal sections meet ASTM A609, Type 4.

C85187

1207

Jeffry & Gracuer

James P Dehnke Notary Public - State of Ohio My Commission Expires October 19, 2019

STATE OF OHIO: COUNTY OF STARK Sworn to and subscribed before me, a Not Jeffery Grover this 29 day of January 2011

Figure B-4. 12.5-ft W-beam Guardrail, Test No. FLAGT-1 (Item No. a4)

GREGORY HIGHWAY PRODUCTS, INC. 4100 13th St. SW Canton, Ohio 44710

UNIVERSITY OF NEBRASKA-LINCOLN 401 CANFIELD ADMIN BLDG P O BOX 880439 LINCOLN,NE,68588-0439 183306 Yield 56527 56527 56527 Description 12GA 25FT WB TZ MGS ANCHOR PANEL 12GA 12FT6IN/3FT1 1/2IN WB T2 12GA 25FT0IN 3FT1 1/2IN WB T2 8534 8534 8534

g inas occurrer on the United States in the America and Melted in the United States" meets Title 23CFR 635.410 - Buy America in the Title 23CFR 635.410 - Buy America in and Terminal Sections meets AASHTO M-180, All structural steel meets AASHTO M-183 & M270 title and O'Demarks Origin

s of Domesiic Unigin I in accordance with Nebraska Department of Transportation I/Corrosion resistant Guardrail and terminal sections meet ASTM A606, Type 4

DAWN R. BATTON NOTARY PUBLIC STATE OF OHIO COMM. Expires March 03, 2018 Recorded in Portage County

Figure B-5. 12.5-ft W-beam End Section, Test No. FLAGT-1 (Item No. a5)

ROALWAY 511 WES	Tisuzes) CONSTRUCTION PRODUCTS THAIN STREET N KY 42726	SH F TA ROADWAY CORFTRUE SIJ WEST MAIN TH CIZRKEOF 1, 177	3- K	11
Tel: 57	0-365-4875 Pax: 270-242-9288			
	CERTIFICATE of ANALYSIS as	ad TESTS	rt No.)	7.055.50
Part No Glood Hot Roll She	46BS			187130
10GA1270 1	Min X 51.0000" X 92.0000"		Pcs	Met
YIELD=50,000 TENSILE= 70,0 P= .02 MAX SI= .04 MAX C= .26 MAX S= .05 MAX DRY MATERIAL	PSI MIN 000 PSI MIN SUITABLE FOR GALVANIZING		264	&7,420
Heat Number	Tag No			
833M66260	506876		Pcs 28	Wgt: 5,030
833M66260	YLD=<66600>/TEN=<74800 506877		28	
833M66260	YLD=<66600>/TEN=<74800		28	5,030
833M66260	YLD=<66600>/TEN=<74800: 506879			5,030
833M66260	YLD=<66600>/TEN=<74800:		28	5,030
833M66260	YLD=<66600>/TEN=<74800>	·/ELG=<29>	28	5,030
833M66260	YLD=<66600>/TEN=<74800>	/ELG=<29>	28	5,030
833M66260	YLD=<66600>/TEN=<74800>	/ELG=<29>	28	5,030
833M66260	YLD=<66600>/TEN=<74800>	/ELG=<29>	28	5,030
833M66260	YLD=<66600>/TEN=<74800>		25	4,490
000,000,000	506885 YLD=<66600>/TEN=<74800>		15	2,690
Heat Number Arcelor Mittal 833M66260	*** Chomical 2	*** =<.005> Si=<.029> Al:	=<.034> Cu Ni=<.01>	l=<.019>
PROCESSED IN U	SA			

Figure B-6. 10-ga Thrie Beam Terminal Connector, Test No. FLAGT-1 (Item No. a6)



Page 1 of 1

Concrete Sample Test Report Cylinder Compressive Strength

Project Name:	Midwest Roadside Safety - Misc Testing
Project Number:	00110546.00
Client:	Midwest Roadside Safety Facility
Location:	MNPD
Sample:	011
Description:	FLAGT

Field Data (ASTM C172, C143, C173/C231, C138, C1064)

Supplier:		Property	Test Result
Mix Name:		Slump (in):	
Ticket Number:		Air Content (%):	
Truck Number:		Unit Weight (lb/ft³):	
Load Volume (yd³):		Air Temp (°F):	
Mold Date:	12/16/2020	Mix Temp (°F):	
Molded By:		Min Temp (°F):	
Initial Cure Method:		MaxTemp (°F):	

Laboratory Test Data (ASTM C39)

https://forneytools.forneyvault.com/Report?id=abb450a3-e139-43b0-af03-6755a5f2fe83

Sample Number:	011	011		
Set Number:	FLAGT1	FLAGT2		
Specimen Number:	1	1		
Age:	20	20		
Length (in):	8	12		
Diameter (in):	3.99	5.98		
Area (in²):	12.50	28.09		
Test Date:	01/05/2021	01/05/2021		
Break Type:	3	5		
Max Load (lbf):	72,045	142,222		
Strength (psi):	5,760	5,060		
Spec Strength (psi):				

Remarks: Average 20-	-day Compres	sive Strengt	th (psi):	5,410)	Date received: 01/05/2021 Curing: ☑ Standard ☐ Field ASTM C511
						Submitted by: Mall Roculer
\times	X X	1				Distribution:
Type 1	Type 2	Type 3	Type 4	Type 5	Type 6	Report Date: 1/5/21

This report shall not be reproduced, except in full, without prior approval of Alfred Benesch & Company. Results relate only to items tested.

825 M Street Suite 100 Lincoln, NE 68508

Alfred Benesch & Company

Figure B-7. Buttress Concrete, Test No. FLAGT-1 (Item No. b1)



1098 East Maple St Sutton, NE 68979 Phone: 402.773.4319

Email: nick@nebraskawood.com

CERTIFICATE OF COMPLIANCE

Shipped To: Midwest Machinery and Supply

BOL# N32346

Customer PO# 3988

Preservative: CCA - C 0.60D pcf AWPA UC4B

Part #	Physical Description	# Pieces	Charge #	Retention
GS6846 PST	5.5x7.5-46" BCT	42	2538	.716
GR6819 BLK	6x8-19" Block	84	2580	.632

I certify the above referenced material has been produced, treated and tested in accordance with and conforms to AASHTO M133 & M168 standards.

VA: Iowa Wood Preservers certifies that the treated wood products listed above have been treated in accordance with AWPA standards, Section 236 of the VDOT Road & Bridge Specifications and meets the applicable minimum penetration and retention requirements.

Nick Sowl, General Counsel

GENERAL NOTARY-State of Nebraska LINDA L. SCHROETLIN My Comm. Exp. May 20, 2024

Figure B-8. BCT Timber Posts, Test No. FLAGT-1 (Item No. c1)

Canton, Ohio 44710 MIDWEST MACHINERY & SUPPLY CO. P. O. BOX 703 Ship Date: 10/26/2017 Customer P.O.: Shipped to: 3501 MIDWEST MACHINERY & SUPPLY CO. MILFORD,NE,68405 PROJECT 7044AA HT CODE 0.93 0.81 0.83 0.81 32 32 28.6 3/16 X 6IN X 8IN X 5FT0IN TUBE SLEEVE 616137 0.21 73148 58210 0.013 0.006 0.006 57275 3/16IN X 6IN X 8IN X 6FT0IN TUBE SLEEVE 10GA MGS TB TRAN APPROACH END-RIGH

GREGORY HIGHWAY PRODUCTS, INC. 4100 13th St. SW

Bolts comply with ASTM A-307 specifications and are galvanized in accordance with ASTM A-153, unless otherwise sta Bolts comply with ASTM A-193 specifications and are galvanized in accordance with ASTM A-193, unless otherwise stated Nuts comply with ASTM A-693 specifications and are galvanized in accordance with ASTM A-193, unless otherwise stated. All other galvanized material conforms with ASTM-123 & ASTM-693 All Galvanizing has occurred in the United States All state used in the manufacture is of Domestic Origin, "Made and Melted in the United States" All State used meets Title 23CRF 693.610 e19 Warnerica All Guardrail and Terminal Sections meets AASHTO M-180, All structural steel meets AASHTO M-183 & M270 All Bolts and Nuts are of Domestic Origin.

All Guardrail and Terminal Sections meets AASHTO M-180, All structural steel meets AASHTO M-180, all All Botts and Nuts are of Domestic Origin
All material fabricated in accordance with Nebraska Department of Transportation
All material fabricated in accordance with Nebraska Department of Transportation
All sheet, zinc-costed or zinc-iron alloy-coasted by the hot dip process that meets ASTM Specifications A653

Jeffry & Concrea

Figure B-9. BCT Foundation Tube, Test No. FLAGT-1 (Item No. c2)



Figure B-10. Strut and Yoke Assembly, Test No. FLAGT-1 (Item No. c3)



PH 216.676.5600 FX 216.676.6761 www.assemblyspecialty.com

ISO 9001:2008

14700 Brookpark Rd Cleveland, OH 44135-5166 customerservice@assemblyspecialty.com

Certificate of Conformance

Date: September 24, 2018

To: Gregory Industries, Inc.

Gregory Galv. & Metal Processing

4100 13th St. SW Canton, OH 44710

We certify that our system and procedures for the control of quality assures that all items furnished on the order will meet applicable tests, requirements and inspection requirements as required by the purchase order and applicable specifications and drawings.

PURCHASE ORDER #: 40299

DATE SHIPPED: 09/24/18

ASPI SALES ORDER #: 122160

MANUFACTURER: ASSEMBLY SPECIALTY PRODUCTS, INC.

QTY	CUST P/N	ASPI P/N	ASPI LOT#	DESCRIPTION
250	3012G	C-2028	89315	6' 6" BCT Cable Assembly
250	3012G	C-2028	89316	6' 6" BCT Cable Assembly
250	3012G	C-2028	89318	6' 6" BCT Cable Assembly
250	3012G	C-2028	89864	6' 6" BCT Cable Assembly
250	3012G	C-2028	89865	6' 6" BCT Cable Assembly
250	. 3012G	C-2028	89866	6' 6" BCT Cable Assembly
250	3012G	C-2028	89929	6' 6" BCT Cable Assembly
250	3012G	C-2028	89930	6' 6" BCT Cable Assembly
250	3012G	C-2028	89931	6' 6" BCT Cable Assembly
250	3012G	C-2028	89932	6' 6" BCT Cable Assembly

REMARKS: NOMINAL BREAKING STRENGTH: 46,000 lbs

WIRE ROPE MANUFACTURED IN ACCORDANCE WITH AASHTO DESIGNATION: M30-02 and ASTM A741 TYPE 2, CLASS A FITTINGS GALVANIZED IN ACCORDANCE WITH ASTM A-153 CLASS C.

STEEL USED TO MANUFACTURE THESE ITEMS WAS MELTED AND MANUFACTURED IN THE U.S.A.
ALL MANUFACTURING PROCESSES SUPPLIED OR PERFORMED BY ASSEMBLY SPECIALTY PRODUCTS, INC. TOOK PLACE IN THE U.S.A.

Signature:

Certification and Compliance Manager

Figure B-11. BCT Anchor Cable Assembly, Test No. FLAGT-1 (Item No. c4)

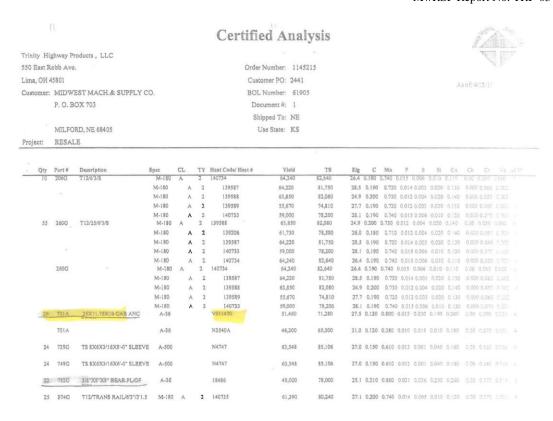


Figure B-12. Anchor Bracket, Test No. FLAGT-1 (Item No. c5)

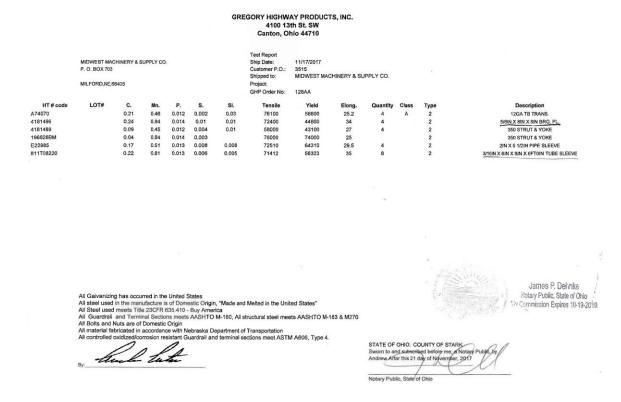


Figure B-13. Anchor Bearing Plate, Test No. FLAGT-1 (Item No. c6)

Atlas Tube (Alabama), Inc. 171 Cleage Dr Birmiagham; Alabama, USA 35217 Tel: Fax:



Ref.B/L: 80791452 Date: 11.10.2017 Customer: 179

MATERIAL TEST REPORT

Sold to

Steel & Pipe Supply Compan PO Box 1688 MANHATTAN KS 66505 USA

Shipped to

Steel & Pipe Supply Compan 401 New Century Parkway NEW CENTURY KS 66031 USA

		3x40'0"0(5	κ4).				o: 0300					Made in Melted	in: USA		
Sales order:		1000000					Order: 4			Cust Ma			0018840		
Heat No	C	Mn	Р	S	Si	Al	Cu	СЬ	Mo	Ni	Cr	v	Ti	В	N
B704212	0.200	0.450	0.010	0.004	0.020	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Bundle No	PCs	Yield	Ter	nsile	Eln.				Се	rtification			C	E: 0.2	В
40867002	20	064649 P	si 08	7652 Psi	24 %			A	STM A5	00-13 GR	ADE B&	C			
Material Note Sales Or.Note															
Material: 2.3	75x154x	42'0"0(34x	:1).		М	aterial N	o: R023	7515442	200			Made in			
Sales order:	122697	6			Pu	ırchase (Order: 4	5002966	556	Cust Ma	terial #:	642004	in: USA 042		
Heat No	С	Mn	P	s	Si	AI	Cu	Ср	Мо	Ni	Cr	v	Ti	В	N
B712810	0.210	0.460	0.012	0.002	0.020	0.024	0.100	0.002	0.020	0.030	0.060	0.004	0.002	0.000	0.008
Bundle No	PCs	Yield	Төг	sile	Eln.		Rb		Се	rtification			С	E: 0.3	2
MC00006947	34	063688 P	si 08	3220 Psi	25 %	91			STM A5	00-13 GR	ADE B&	C			
Material Note Sales Or.Note															
Material: 2.3	75x154x	42'0"0(34x	1).		М	aterial N	o: R023	7515442	200			Made in			
		6			Pt	rchase (Order: 4	5002966	556	Cust Ma	terial #:	642004			
Sales order:	122697				Si	AI	Cu	СЬ	Мо	Ni	Cr	v	Ti	В	N
	122697 C	Mn	P	S	٠.						**********	************			
Sales order: Heat No 17037261	1004000		P 0.005	0.004	0.020	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Heat No	С		0.005				0.000	0.000		0.000	0.000	0.000		0.000 E: 0.3	-

Authorized by Quality Assurance:
The results reported on this report represent the actual attributes of the material furnished and indicate full compliance with all applicable specification and contract requirements.

Consider the property of the material furnished and indicate full compliance with all applicable specification and contract requirements.

Page 2 00

Figure B-14. BCT Post Sleeve, Test No. FLAGT-1 (Item No. c7)

(2 S) (3 S) (3 S) (4 S)			CERTIFIED MA	ATERIAL TEST R	EPORT .					Page 1 / I
	CUSTOMER SHI		CUSTOMER	BILL TO		GRADE		APE / SIZE		DOCUMENT ID:
(c) GERDAU	GO GERDAU HIGHWAY SAFETY CORP			SAFETY CORP	A992/A709-36	13.0	Wide Flange Beam / 6 X 8.5# / 150 > 000032023			
	MARION, OH 4		GLASTONE	BURY,CT 06033-03	58		PCS	WEIGHT	HEAT/BATCH	
US-ML-CARTERSVILLE	USA		USA			42'00"	105	37,485 LB		55066501/03
384 OLD GRASSDALE ROAD NE CARTERSVILLE, GA 30121	SALES ORDE	2	CUSTON	MER MATERIAL N	*	SPECIFICATION / DAT	E or REVI	ISION		
USA	8525742/00006					ASTM A6-17			IR-RO	0600800 1176
CUSTOMER PURCHASE ORDER NUMBER		BILL OF LADING		DATE		ASTM A709-17 ASTM A992-11 (2015)			7.0	
1832		1323-0000156951		05/08/2020		CSA G40.21-13 345WM			1832	176
CHEMICAL COMPOSITION										
C Mn P	§ 0.027	0.21 0.	Žu 1	% G 17 0.18		(o Sn 048 0.008	0.002	₩ 0.009		
	0.027	0.21 0.	29 U.	17 0.12	0.0	740 0.006	0.002	0.009		
MECHANICAL PROPERTIES YS 0.2% PSI	TS SI	MPa		UTS MPa		Y/T rati	1	Elong.		
62200 77	000	429		531		0.810		23.40		
61000 78	400	421		541		0.780		24.40		
COMMENTS / NOTES										
1										

The above figures are certified chemical and physical test records as contained in the permanent records of compar specified requirements. Weld repair has not been performed on this material. This material, including the billets, w 10204-3.1.	
Mackey BILASKAR YALAMANCHILI	YAN WANG QUALITY ASSURANCE MOR.
Phone: (409) 267-1071 Email: Bbasker.Yalamanchili@gerdan.com	Phone: (770) 387 5718 Email: yan.wang@gerdan.com

Figure B-15. 6-ft W6x8.5 Posts, Test No. FLAGT-1 (Item Nos. d1 and d2)

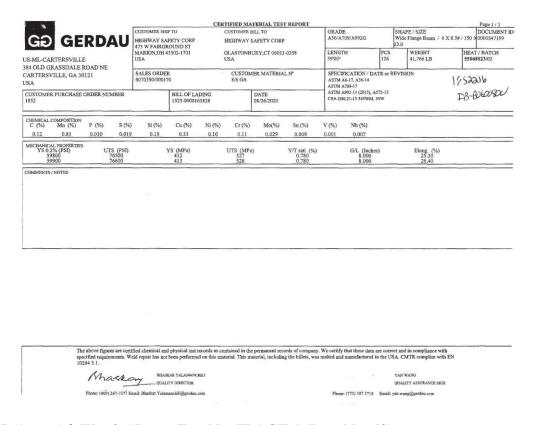


Figure B-16. 6.5-ft W6x8.5 Posts, Test No. FLAGT-1 (Item No. d3)



1098 East Maple St Sutton, NE 68979 Phone: 402.773.4319 Email: nick@nebraskawood.com

CERTIFICATE OF COMPLIANCE

Shipped To: Midwest Machinery and Supply

BOL# <u>N26219</u> Customer PO# <u>3930</u>

Preservative: CCA - C 0.60D pcf AWPA UC4B

Part #	Physical Description	# Pieces	Charge #	Retention
6117b	6x8-6.5' CRT	35	1413	.626
GR6814 BLK	6x8-14" OCD Block	126	1696	.621
GR61214 BLK	6x12-14" OCD Block	168	1695	.625
GR61222 BLK	6x12-22" OCD Block	168	1695	.625
				* *

I certify the above referenced material has been produced, treated and tested in accordance with and conforms to AASHTO M133 & M168 standards.

VA: Iowa Wood Preservers certifies that the treated wood products listed above have been treated in accordance with AWPA standards, Section 236 of the VDOT Road & Bridge Specifications and meets the applicable minimum penetration and retention requirements.

Nick Sowl, General Counsel

4/1/20 Date

Figure B-17. 6-in. x 12-in. x 14-in. Timber Blockout, Test No. FLAGT-1 (Item No. d4)



1098 East Maple St Sutton, NE 68979 Phone: 402.773.4319

Email: nick@nebraskawood.com

CERTIFICATE OF COMPLIANCE

Shipped To: Midwest Machinery and Supply

BOL# N32346

Customer PO# 3988

Preservative: CCA - C 0.60D pcf AWPA UC4B

(A)		Charge #	Retention
5.5x7.5-46" BCT	42	2538	.716
6x8-19" Block	84	2580	.632

I certify the above referenced material has been produced, treated and tested in accordance with and conforms to AASHTO M133 & M168 standards.

VA: Iowa Wood Preservers certifies that the treated wood products listed above have been treated in accordance with AWPA standards, Section 236 of the VDOT Road & Bridge Specifications and meets the applicable minimum penetration and retention requirements.

Nick Sowl, General Counsel

GENERAL NOTARY-State of Nebraska LINDA L. SCHROETLIN My Comm. Exp. May 20, 2024

Figure B-18. 6-in. x 12-in. x 19-in. Timber Blockout, Test No. FLAGT-1 (Item No. d5)



CERTIFICATE OF TEST

Page 01 of 02

Certification Date 8-MAY-2020

CUSTOMER ORDER NUMBER

50375

EARLE M. JORGENSEN COMPANY 1800 N UNIVERSAL AVENUE KANSAS CITY MO 64120

Invoice Number S719292

CUSTOMER PART NUMBER

0001

121076

SOLD TO:

RIVERS METAL PRODUCTS

SHIP TO:

RIVERS METAL PRODUCTS

3100 N 38TH

LINCOLN NE 68504

3100 NORTH 38TH LINCOLN NE 68504

4 X 7 X	188 WALI	GTM A500 GR J X 24'		1076	Line Tota	l: 48 FT	THOLOGIADER
Specifi ASTM A5	cations:	C	.6				THE CANADA
			CHEMICA	L ANALYSIS	 3		
C 0.19	MN 0.64	P 0.012	S 0.01	SI 0.02	AL 0.039	CU 0.13	CB 0.001
0.01 C	0.04 MN	P	0.002 S 0.01	0.002 ST	AT.	0.0029	CB 0.001
MO 0.01	NI 0.05	CR 0.08	V 0.002	TI 0.002	N 0.006	CA 0.003	CE 0.33
	R858184 ATLAS TUB	 E		COUNTRY	OF ORIGIN	: USA	
			MECHANI	CAL PROPER	TIES		
DESCRIP	TION	YLD STR PSI 57688.0 54794.0	PSI 74730.0	IN 02 IN	%RED IN AREA		

The above data were transcribed from the manufacturer's Certificate of Test after verification for completeness and specification requirements of the information on the certificate. All test results remain on file subject to examination.

We hereby certify that the material covered by this report will meet the applicable requirements described herein, including any specification forming a part of the description.

The willful recording of false, fictitious, or fraudulent statements in connection with test results may be punishable as a felony under federal statutes.

Material did not come in contact with mercury while in our possession.

LARRY BUSICK

Manager, Quality Assurance

Figure B-19. HSS4x7x³/₁₆ Steel Blockout, Test No. FLAGT-1 (Item No. d6)



Certificate of Compliance

600 N County Line Rd Elmhurst IL 60126-2081 630-600-3600 chi.sales@mcmaster.com University of Nebraska
Midwest Roadside Safety Facility
M W R S F
4630 Nw 36TH St
Lincoln NE 68524-1802
Attention: Shaun M Tighe
Midwest Roadside Safety Facility

Purchase Order E000548963 Order Placed By Shaun M Tighe McMaster-Carr Number

7204107-01

Page 1 of 1 08/02/2018

Line Product Ordered Shipped

1 97812A109 Raised-Head Removable Nails, 16D Penny Size, 3" Long, Packs of 5

Packs

Certificate of compliance

This is to certify that the above items were supplied in accordance with the description and as illustrated in the catalog. Your order is subject only to our terms and conditions, available at www.mcmaster.com or from our Sales Department.

Sarah Weinberg Compliance Manager

Figure B-20. 16D Nail, Test No. FLAGT-1 (Item No. d7)

NUCOR°

Mill Certification

MTR#:458890-2 Lot #:360001474020 ONE NUCOR WAY BOURBONNAIS, IL 60914 US 815 937-3131 Fax: 815 939-5599

Sold To: SIMCOTE INC 1645 RED ROCK RD ST PAUL, MN 55119 US Ship To: SIMCOTE INC 1645 RED ROCK RD ST PAUL, MN 55119 US

Customer PO	MN-3748	Sales Order #	36013225 - 1.31
Product Group	Rebar	Product #	2110206
Grade	A615 Gr 60/AASHTO M31	Lot #	360001474020
Size	#4	Heat #	3600014740
BOL#	BOL-567414	Load #	458890
Description	Rebar #4/13mm A615 Gr 60/AASHTO M31 60' 0" [720"] 6001- 10000 lbs	Customer Part #	
Production Date	08/12/2020	Qty Shipped LBS	22725
Product Country Of Origin	United States	Qty Shipped EA	567
Original Item Description		Original Item Number	

I hereby corify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements Melt Country of Origin: United States Melting Date: 08/07/2020 Si (%) Ni (%) Cr (%) Mo (%) Cu (%) V (%) Nb (%) C (%) Mn (%) P (%) S (%) 0.34 0.90 0.015 0.043 0.198 0.18 0.23 0.06 0.40 0.012 0.002

 Other Test Results

 Yield (PSI): 66100
 Tensile (PSI): 99200
 Average Deformation Height (IN): 0.036

 Elongation in 8" (%): 14.5
 Bend Test: Pass
 Weight Percent Variance (%): -4.00

Comments:

All manufacturing processes of the steel materials in this product, including melting, have occurred within the United States. Products produced are weld free. Mercury, in any form, has not been used in the production or testing of this material.

CERTIFICATE OF COMPLIANCE

ROCKFORD BOLT & STEEL CO. 126 MILL STREET ROCKFORD, IL 61101 815-968-0514 FAX# 815-968-3111

CUSTOMER NAME:

TRINITY INDUSTRIES

CUSTOMER PO:

200208

SHIPPER #: 067063 DATE SHIPPED: 08/21/2019

LOT#:

32086-B

SPECIFICATION:

ASTM A307, GRADE A MILD CARBON STEEL BOLTS

TENSILE:

SPEC:

60,000 psi*min

RESULTS:

74,700

74,000 89.20

HARDNESS: 100 max

88.60

*Pounds Per Square Inch.

COATING:

ASTM SPECIFICATION F-2329 HOT DIP GALVANIZE

AZZ GALVANIZING:

32086-B

CHEMICAL COMPOSITION

MILL	GRADE	HEAT#	- С	Mn	P	S	Si
NUCOR	1010	100897520	.11	.51	.012	.007	.18

10,650

PCS 5/8" X 14" GUARD RAIL BOLT

WE HEREBY CERTIFY THE ABOVE BOLTS HAVE BEEN MANUFACTURED BY ROCKFORD BOLT AND STEEL AT OUR FACILITY IN ROCKFORD, ILLINOIS, USA. THE MATERIAL USED WAS MELTED AND MANUFACTURED IN THE USA. WE FURTHER CERIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIALS SUPPLIER, AND THAT OUR PROCEDURES FOR THE CONTROL OF PRODUCT QUALITY ASSURE THAT ALL ITEMS FURNISHED ON THIS ORDER MEET OR EXCEED ALL APPLICABLE TESTS, PROCESS, AND INSPECTION REQUIREMENT PER ABOVE SPECIFICATION.

STATE OF ILLINOIS

COUNTY OF WINNEBAGO

Official Seal

Merry F Shane
Notary Public State of Illinois
My Commission Expires 10/03/2022

Diside Milomas

DATE

Figure B-22. %-in. x 14-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f1)

CERTIFICATE OF COMPLIANCE

ROCKFORD BOLT & STEEL CO. 126 MILL STREET ROCKFORD, IL 61101 815-968-0514 FAX# 815-968-3111

CUSTOMER NAME:

GREGORY INDUSTRIES

CUSTOMER PO:

39864

SHIPPER #: 063466

DATE SHIPPED: 05/24/2018

LOT#:

30920-B

SPECIFICATION:

ASTM A307, GRADE A MILD CARBON STEEL BOLTS

TENSILE:

SPEC:

60,000 psi*min

RESULTS:

79,300

HARDNESS:

100 max

76,800 90.00

90.80

*Pounds Per Square Inch.

COATING: ASTM AZZ GALVANIZING:

ASTM SPECIFICATION F-2329 HOT DIP GALVANIZE

30920-B

CHEMICAL COMPOSITION

MILL	GRADE	HEAT#	С	Mn	Р	S	Si
MID AMERICAN STEEL & WIRE	1012	1721198	.13	.51	.016	.027	.19

20,700

PCS 5/8" X 10" GUARD RAIL BOLT P/N 1010G

WE HEREBY CERTIFY THE ABOVE BOLTS HAVE BEEN MANUFACTURED BY ROCKFORD BOLT AND STEEL AT OUR FACILITY IN ROCKFORD, ILLINOIS, USA. THE MATERIAL USED WAS MELTED AND MANUFACTURED IN THE USA. WE FURTHER CERIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIALS SUPPLIER, AND THAT OUR PROCEDURES FOR THE CONTROL OF PRODUCT QUALITY ASSURE THAT ALL ITEMS FURNISHED ON THIS ORDER MEET OR EXCEED ALL APPLICABLE TESTS, PROCESS, AND INSPECTION REQUIREMENT PER ABOVE SPECIFICATION.

STATE OF ILLINOIS
COUNTY OF WINNEBAGO

SIGNED BEFORE ME ON THIS

ADD

STOREGO SIGNATORY

DATE

OFFICIAL SEAL
MERRY F. SHANE

NOTARY PUBLIC - STATE OF ILLINOIS MY COMMISSION EXPIRES OCTOBER 3, 2018

Figure B-23. %-in. x 10-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f2)

*		5	/8"x	2" S	plic	е Во	lt									
		P	GT E	Buttr	ess											
		F	#16-	0009	L#1	4081	2B H	#203	0343	0				2	3400	56-
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Cust	omer:		Stock	(Date:	Nove	mber 2	0,2014	100)	7	
							Invoi	ce Nu	mber:				MA	- V 1- V 19	+ 6	AUN
							L	ot Nu	mber:		40812	2B		OPPHILI	ו או כבי	J388V4
Part Number: 3400G		3				Qua	antity:		118,82	21	L					
Descri	otion:	5/8	"x 2"	G.R.			Heat	Numb	er(s):	2	03034	30	-	118	8821	
	Bolt										,					
Specification: ASTM A307-A / A153 / F2329																
						MATI	ERIAL	CHE	MIST	RY						
Heat	С	MN	Р	S	SI	NI	CR	MO	CU	SN	V	AL	N	В	TI	NB
20303430	.08	.34	.007	.002	.06	.04	.05	.02	.08	.005	.001	.032	.009	.0001	.001	.001
							*									
				P	LATI	NG OI	R PRO	TECT	TVE C	COATI	NG					
HOT	IP GAL	VANIZ	ED (Lo	t Ave.T	hickne	ss / Mil	s)		2.	55	(2.0 Mils	Minimu	m)			
	**	AAMITTE	nnon	TIOT II	140341	MITTEL	CTUDE	n ter or	TTIS TIME	TED C	PATER	OE AN	EDICA	***		
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Figure B-24. 5%-in. x 2-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f3)

CERTIFICATE OF COMPLIANCE

ROCKFORD BOLT & STEEL CO. **126 MILL STREET** ROCKFORD, IL 61101 815-968-0514 FAX# 815-968-3111

CUSTOMER NAME:

TRINITY INDUSTRIES

CUSTOMER PO:

203160

SHIPPER #: 068184 DATE SHIPPED: 02/06/2020

LOT#:

32539-P

SPECIFICATION:

ASTM A307, GRADE A MILD CARBON STEEL BOLTS

TENSILE:

SPEC:

60,000 pai*min

RESULTS:

69,000 69,300

HARDNESS:

100 max

68.80 68,30

"Pounds Per Square Inch.

COATING: ASTM SPECIFICATION F-2329 HOT DIP GALVANIZE

AZZ GALVANIZING:

32539-P

CHEMICAL COMPOSITION

MILL	GRADE	HEAT#	С	Mn	Р	S	Si
CHARTER STEEL	1010	10634210	.10	.52	.008	.009	.08

QUANTITY AND DESCRIPTION:

12,000

PCS 5/8" X 1.25" GUARD RAIL BOLT

P/N 3360G

WE HEREBY CERTIFY THE ABOVE BOLTS HAVE BEEN MANUFACTURED BY ROCKFORD BOLT AND STEEL AT OUR FACILITY IN ROCKFORD, ILLINOIS, USA, THE MATERIAL USED WAS MELTED AND MANUFACTURED IN THE USA. WE FURTHER CERIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIALS SUPPLIER, AND THAT OUR PROCEDURES FOR THE CONTROL OF PRODUCT QUALITY ASSURE THAT ALL ITEMS FURNISHED ON THIS ORDER MEET OR EXCEED ALL APPLICABLE TESTS, PROCESS, AND INSPECTION REQUIREMENT PER ABOVE SPECIFICATION.

STATE OF ILLINOIS

COUNTY OF WINNEBAGO SIGNED BEFORE ME ON THIS

Official Seal Merry F Shane Notary Public State of Illinois My Commission Expires 10/03/2022

Figure B-25. %-in. x 11/4-in. Guardrail Bolt, Test No. FLAGT-1 (Item No. f4)



Phone: 800-547-6758 | Fax: 503-227-4634 3441 NW Guam Street, Portland, OR 97210 Web: www.portlandbolt.com | Email: sales@portlandbolt.com | CERTIFICATE OF CONFORMANCE |

For: MIDWEST ROADSIDE SAFETY FACIL

PB Invoice#: 136724

Cust PO#: FL AGT ITEM#F5/H

Date: 11/13/2020 Shipped: 11/16/2020

We certify that the following items were manufactured and tested in accordance with the chemical, mechanical, dimensional and thread fit requirements of the specifications referenced.

Description: 7/8 X 15-1/2 GALV ASTM F3125 GRADE A325 HEAVY HEX BOLT **Heat#:** 3093334 Base Steel: 4140 **Diam:** 7/8 +-----Source: COMMERCIAL METALS CO Proof Load: 39,250 LBF **P** : .016 **C**: .400 Mn: .810 Hardness: 293 HBN Si: .240 Ni: .190 **S**: .019 Tensile: 67,180 LBF RA: .00% 0 Cr: .870 Mo: .208 Cu: .320 Yield: Elon: .00% Sample Length: **Pb:** .000 **V**: .024 **Cb:** .000 N: .000 **CE:** .6329 CVN Temp: Charpy: LOT#19878

Nuts:

ASTM A563DH HVY HX

Coatings:

ITEMS HOT DIP GALVANIZED PER ASTM F2329/A153C

Figure B-26. %-in. x 151/2-in. Heavy Hex Bolt, Test No. FLAGT-1 (Item No. f5)

Apr. 12. 2018 4:32PM Fastenal-NELI

No. 4682 P. 3

Certificate of Compliance

Sold To:	Purchase Order	
UNL TRANSPORTATION	Job:	TL-2 and Bullnose
	Invoice Date:	03/27/2018
THIS IS TO CERTIFY THAT WE THESE PARTS WERE PUR	HAVE SUPPLIED YOU WITH THE CHASED TO THE FOLLOWING SP	FOLLOWING PARTS. ECIFICATIONS.
5 PCS 7/8"-9 x 8" ASTM A307 Grade A Hot Dipped G UNDER PART NUMBER 92005	alvanized Hex Bolt SUPPLIED UNDE	R OUR TRACE NUMBER line35042 AND
20 PCS 7/8"-9 Hot Dip Galvanized Finish Grade A Fini UNDER PART NUMBER 36717	shed Hex Nut SUPPLIED UNDER OU	JR TRACE NUMBER 110254885 AND
5 PCS 7/8"-9 x 8" ASTM A307 Grade A Hot Dipped Gr UNDER PART NUMBER 92005	alvanized Hex Bolt SUPPLIED UNDE	R OUR TRACE NUMBER ilne35042 AND
5 PCS 7/8"-9 x 8" ASTM A307 Grade A Hot Dipped Gr UNDER PART NUMBER 92005	alvanized Hex Bolt SUPPLIED UNDE	R OUR TRACE NUMBER line35042 AND
5 PCS 7/8"-9 x 8" ASTM A307 Grade A Hot Dipped Go UNDER PART NUMBER 92005	alvanized Hex Bolt SUPPLIED UNDE	R OUR TRACE NUMBER IIne35042 AND
		,
This is to certify that the above document is true and accurate to the best of my knowledge.	Please check current r	evision to avoid using obsolete copies.
Said MM	This document was pr time.	rinted on 04/12/2018 and was current at that
Fastenal Account Representative Signature	Fastenal Store Locat	tion/Address
1 1. 1. 1.	3201 N. 23rd Street S.	TE I
Printed Name	LINCOLN, NE 68521	
rimed Maille	Phone #: (402)476-79	200
4/12/18	Fax #: 402/476-7958	
	Page 1 of 1	

Figure B-27. 1/8-in. x 8-in. Hex Bolt, Test No. FLAGT-1 (Item No. f6)

Certificate of Compliance
Birmingham Fastener Manufacturing
PO Box 10323 Birmingham, AL 35202 (205) 595-3512

Customer _	Midwest M	fachinery & Supply			Date Shipp	ed	11/28/2018	
Customer Orde	er Number _	36	664		BFM Order	Number	1553751	
			Item	Descrip	otion			
Description_			5/8"-11 x 10	"Hex Bolt			Qty	298
Lot#	81342	Sp	ecification	ASTM A30	17-14 Gr A	Finish	ASTM	F2329
			Raw Ma	terial A	nalysis			
Heat#	JK	(18104124	1)					
Chemical Cor C 0.18	mposition (w Mn 1.19	/t% Heat / P 0.012	Analysis) By S 0.034	/ Material S Si 0.20	Supplier Cu 0.29	Ni 0.13	Cr 0.11	Mo 0.04
			Mechan	ical Pro	perties			
Sample # 1 2 3 4 5	Hardness 93 HRBW		Tensile Str 22,)	Tensile Str 99,4)
This information customer order All steel melte	r. The samp	les tested	conform to t				stated	
Authorized Signature: _		ian Hugh			Date:	11/29	/2018	

Figure B-28. 5%-in. x 10-in. Hex Bolt, Test No. FLAGT-1 (Item No. f7)

CERTIFIED MATERIAL TEST REPORT TO DIN EN 10204-2005 3.1 FOR ASTM A307, GRADE A - MACHINE BOLTS

FACTORY: IFI & MORGAN LTD. REPORT DATE:2019/4/9

ADDRESS: No.583-28, Chang'an North Road, Wuyuan Town, Haiyan,

Zhejiang, China MANUFACTURE DATE:2019/3/28

CUSTOMER: FASTENAL MFG LOT NUMBER:M-2019HT200-9

SAMPE SIZE: ACC. TO ASME B18.18 CATEGORY 2-2011; ASTM F1470-12 TABLE 3

MANU QTY: 28130PCS SHIPPED QTY:28080PCS

SIZE: 5/8-11X1 1/2 HDG

HEADMARKS: 307A PLUS NY
PO NUMBER:180170611
PART NO:91919

STEEL PROPERTIES:

MATERIAL TYPE:Q195C HEAT NUMBER:5-01571

CHEMISTRY SPEC: Grade A ASTM A307-12 TEST:

C %*100	Mn%*100	P %*1000	S %*1000
0.29max	1.20 max	0.04max	0.15max
0.08	0.33	0.016	0.024

DIMENSIONAL INSPECT	TIONS Unit:inch		SPECIFICATION: ASM	ME B18.2.1	- 2012
CHARACTERISTICS	SPECIFIE	D	ACTUAL RESULT	ACC.	REJ.
*******	******	******	*******	*****	*****
VISUAL	ASTM F788-20	013	PASSED	29	0
THREAD	ASME B1.1-20	003, 3A GO, 2A NO GO	PASSED	15	0
WIDTH A/F	H A/F 0.906-0.938			4	0
WIDTH A/C	1.033-1	1.048-1.057	4	0	
HEAD HEIGHT	0.378-0	.444	0.395-0.411	4	0
THREAD LENGTH	1.420-1	.560	1.434-1.486	15	0
LENGTH	1.420-1	.560	1.434-1.486	15	0
MECHANICAL PROPERT	ΓΙΕS:	SPECIFICAT	ΓΙΟΝ: ASTM A307 - 14e	l GR.A	
CHARACTERISTICS	TEST METHOD	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
******	******	******	******	*****	*****
CORE HARDNESS:	ASTM F606/F606M-2016	69-100 HRB	76-80 HRB	4	0
WEDGE TENSILE:	ASTM F606/F606M-2016	Min 60 KSI	65-69 KSI	4	0
CHARACTERISTICS	TEST METHOD	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
COATINGS OF ZINC:		SPECIFIATION: ASTM I	F2329/F2329M-15		
HOT DIP GAL VANIZED .	ASTM B568-98(2014)	Min 0.0020"	0.0021" -0.0022"	4	0

We hereby certify that above products supplied are in compliance with all the requirements of the order.

We here by certify that this MTR is in compliance to DIN EN 10204 3.1 content.

ALL TESTS IN ACCORDANCE WITH THE METHODS PRESCRIBED IN THE APPLICABLE ASTM SPECIFICATION. WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND CURRENT IN GLABORATORY.

Maker's ISO 9001:2015 SGS Certificate # HK04/0105

(SIGNATURE ON O.A. LAB MER.) (NAME OF MANUFACTURER)

Figure B-29. %-in. x 1½-in. Hex Bolt, Test No. FLAGT-1 (Item No. f8)

CERTIFIED MATERIAL TEST REPORT FOR USS FLAT WASHERS HDG

FACTORY: IFI & Morgan Ltd REPORT DATE: 23/4/2019

ADDRESS: Chang'an North Road, Wuyuan Town, Haiyan, Zhejiang, China

MFG LOT NUMBER: 1844804

SAMPLING PLAN PER ASME B18.18-11 PO NUMBER: 170089822

SIZE: USS 7/8 HDG QNTY(Lot size):

HEADMARKS: NO MARK PART NO: 33187

DIMENSIONAL INSPECT	ΓΙΟΝS	SPECIFIC	CATION: ASTM B1	8.21.1-2011		
CHARACTERISTICS	SPECI	FIED	ACTUAL RESU	LT ACC.	REJ.	
*******	**********	******	******	**: ******	*****	
APPEARANCE	ASTM F8	344	PASSED	100	0	
OUTSIDE DIA	2.243-2.28	0	2.246-2.254	10	0	
INSIDE DIA	0.931-0.96	8	0.956-0.965	10	0	
THICKNESS	0.136-0.19	2	0.136-0.157			
CHARACTERISTICS	TEST METHOD	SPECIFIED	ACTUAL RESUI	LT ACC.	REJ.	
********	******	******	* *********	*** ******	******	
HOT DIP GALVANIZED	ASTM F2329-13	Min 0.0017"	0.0017-0.0020	in 8	0	

7200PCS

ALL TESTS IN ACCORDANCE WITH THE METHODS PRESCRIBED IN THE APPLICABLE ASTM SPECIFICATION. WE CERTIFY THAT THIS DAIA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND COURT TESTING LABORATORY.

ISO 9001:2015 SGS Certificate # HK04/0105

NATURE OF QA. LAB MGR.

Figure B-30. %-in. Round Washer, Test No. FLAGT-1 (Item No. g1)

SSF INDUSTRIAL CO., LIMITED

MILL TEST CERTIFICATION

Certification Conforms to EN1024 3.1B

Supplier: SSF INDUSTRIAL CO.,LIMITED **Certificate No.:** 000825

Buyer: FASTENAL COMPANY PURCHASING Invoice No.: FASTCO2020051501

Product Description: 5/8 USS F/W GALV

 Product Size:
 5/8
 Shipped Q'ty:
 12 MPCS

 Quality Acceptance:
 ISO 3269
 Lot No.:
 20200515

RAW MATERIAL scrap

Element C Si Mn S P Ni Cr Cu

SURFACE

Test Item	Spec.	Standard	Remark
Appearance	Flawless	1	ок

DIMENSION MEASUREMENT(L According to: USS

Test Item	Standa	rd (mm)	Campling	Remark	Test Result	
rest item	Min	Max	Sampling	Remark	rest Result	
INNER DIAMETER (d1)	17.3	18.23	80	ок		
OUTTER DIAMETER (d2)	44.28	45.21	80	ок		
THICKNESS (h)	2.75	4.06	80	ок		

MACHANICAL PROPERTIES According to: ISO 6507

Test Item	Spec.	Sampling	Remark	Test Result
HARDNESS (HRC/HV)	HV10 140 ~ HV10 250	10	ок	HV10 145 ~ HV10 150

COATING According to: ISO 4042

Test Item	Spec.	Sampling	Remark	Test Result
Plating thickness	min.3 µm	5	ок	4.573 μm - 5.328 μm
ISST	2 hours no white corrosion and 12 hours no red rust	5	ок	ок

We hereby certify that all the above material were manufactured, sampled, tested, and inspected in accordance with the relevant specification and any supplementary requirements or other requirements designated in the purchase order and was found to meet those requirements.

Inspector: QC Chen Inspec. Date: 2020.11.16



Figure B-31. 5%-in. Round Washer, Test No. FLAGT-1 (Item No. g2)

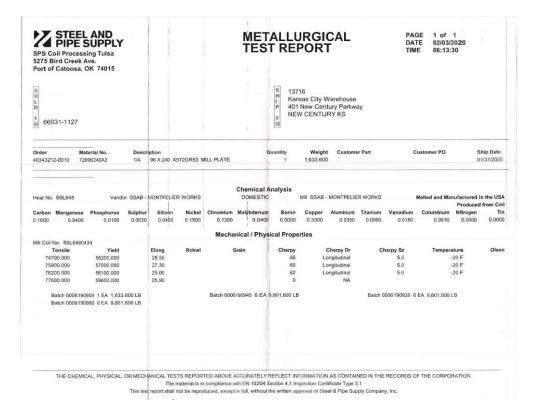


Figure B-32. Square Washer Plate, Test No. FLAGT-1 (Item No. g3)

FOR USS FLAT WASHERS HDG FACTORY: IFI & Morgan Ltd 22/10/2018 ADDRESS: Chang'an North Road, Wuyuan Town, Haiyan, Zhejiang, China SAMPLING PLAN PER ASME B18.18-11 PO NUMBER: 210151571 SIZE: USS 1 HDG QNTY(Lot size): 3240PCS HEADMARKS: NO MARK PART NO: DIMENSIONAL INSPECTIONS SPECIFICATION: ASTM B18.21.1-2011 CHARACTERISTICS SPECIFIED ACTUAL RESULT ACC. REJ. ********** ************* ************ ****** APPEARANCE ASTM F844 PASSED 100 0 OUTSIDE DIA 2.492-2.529 2.496-2.504 10 0 1.055-1.092 1.080-1.089 INSIDE DIA 10 0 0.135-0.192 0.135-0.157 THICKNESS 10 0 CHARACTERISTICS TEST METHOD SPECIFIED ACTUAL RESULT ACC. REI ************* ********* ****** ******* Min 0.0017" HOT DIP GALVANIZED ASTM F2329-13 0.0017-0.0020 ALL TESTS IN ACCORDANCE WITH THE METHODS PRESCRIBED IN THE APPLICABLE ASTM SPECIFICATION. WE CERTIFY THAT THIS DAIA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER TESTING LABORATORY. ISO 9001:2015 SGS Certificate # HK04/0105 检验专用章 . LAB MGR.)

CERTIFIED MATERIAL TEST REPORT

Figure B-33. 1-in. Round Washer, Test No. FLAGT-1 (Item No. g4)



DECKER MANUFACTURING CORPORATION 703 N. Clark Street Alpian, Michigan 49224 P: 517.629.3955 > F: 517.629.7535

LABORATORY AND TESTING FACILITY

Reaffirmed to be in compliance to current Rev Level. Form 8.0
ORIGINAL LABORATORY AND/OR INSPECTION REPORT
THIS IS A LEGAL DOCUMENT

NAME AND ADDRESS OF CLIENT:	
DAGE 1 DE 3	TO A STORE OF THE A STATE OF THE STATE OF TH
PAGE _ L OF _ 2 LAB FILE ID NUMBER/LOT NUMBER: 20 - 42-00	DATE OF MANUFACTURE: 3-5-2020
	The second state of the second state of the second
DMC PART NUMBER #: 035-1031-26 ITEM DESCRIPTION: 5/8 X 11 +.031 2B GUARD RAIL NUT	
GRADE ID MARK AND INSIGNIA: DMC	The state of the s
NAME (S) OF PERSON (S) SAMPLING M. OCT 2 /J. CO.	sampling
PROCEDURES ARE UNDER THE SUPERVISION OF DECKER	
OUALITY DEPARTMENT.	territor activities conformation 3
PRODUCTION LOT SIZE: Q00M SUITABILITY/CONDIT	ION OF TEST SPECIMENS: ACCEPTABLE
TOTAL NO. OF SAMPLES INSPECTED AND/OR TESTED (
INSPECTIONS AND/O	OR TESTS:
INSPECTION/TEST DATE (S): 3-6-2020	3-19-2020
DESCRIPTION (S): ROCKWELL HRB	PROOFLOAD
SPECIFICATION (S): ASTM E18	ASTM F606
REQUIREMENTS: ASTM-A563 GRADE P. G. HRB 69 MIN &HRC 32 MAX	I ASTM AS63 GRADE B Zn @ 20.340 LBF.
EQUIPMENT ID: # FH10000120120012	I# 184280
	/ TEST RESULTS:
UNIT OF MEASUREMENT: HRB W	UNIT OF MEASUREMENT: LBF
(1) 88.2 (5) 85.55	(1) 21,300 (5) 21,300
(2) 88.7 (6) 87.0	(2) 21 300 (6) ZI 100
(3) 8805 (7) 88.2	(3) 21,200 (7) 21,300
(4) 85.8 (8) 86.3	(4) 21 200 (8) 21,300
RESULTS OBTAINED FROM: WRENCH FLATS	(1)
SPECIFICATION OR MATERIAL GRADE AS EVIDENCED:	C-1010 Non- 10140980
REMARKS OR DEVIATIONS: MEET AND EXCEED ASTM AS	63 (09) GRADE A REQUIREMENTS
PER ASTM F606 SECTION 4 THE HARDNESS OF EACH SAMPL	E IS THE AVERAGE OF TWO READINGS.
HEAT TREAT, SURFACE TREATMENT, COATING, ETC.,:	PROOFLOAD SAMPLES WERE GALVANIZED.
TO THE SPECIFICATIONS ABOVE, THE SAME	LES INSPECTED AND/OR TESTED
	201102 0012201
CONFORM: X ARE RESULTS ONLY:	DO NOT CONFORM:
APPROVED SIGNATORY	Commence III
QUALITY MANAGER	INSPECTED AND/OR TESPED BY:
Russell L. Wilson	And and X A. Trade labor
Russell L. Wilson	Authorized Lab Technician
I CERTIFY THAT THE ABOVE TEST(S) WERE CONDUCTED IN ACCORDANCE	WITH THE ABOVE STATED SPECIFICATION(8) AND THAT THE
RESULTS ARE CORRECT AS SHIPPRED. THE ABOVE RESULTS ONLY PERTAIN TO	D THE SAMPLE ITEMS TESTED, SEE THE QUALITY MANUAL FOR
MANDATORY REPORT CONTENT. THIS DOCUMENT SHALL NOT BE REP	MODUCED IN FULL WINDOWS INE APPROVAL OF DELACA
MANUFACTURING CORPORATION. DO NOT ERASE OR ALTER ANY ERRORS DR	An a straight line through and initial, see reverse of
THIS DOCUMENT FOR THE TERMS AND CONDITIONS OF THIS TEST REPORT. THI	e decision nole is simple exceptance.
	And Cally
	TESTING CERT #0499-01
	PERFORM FERFARANCE

Figure B-34. %-in. Heavy Hex Nut, Test No. FLAGT-1 (Item No. h1)



GEM-YEAR TESTING LABORATORY CERTIFICATE OF INSPECTION

MANUFACTURER: GEM-YEAR INDUSTRIAL CO., LTD.

ADDRESS: NO.8 GEM-YEAR

ROAD, E.D.Z., JIASHAN, ZHEJIANG, P.R. CHINA

PURCHASER: FASTENAL COMPANY PURCHASING

PO. NUMBER: 110216407

COMMODITY: FINISHED HEX NUT GR-A SIZE: 5/8-11 NC 0/T 0.51MM

LOT NO: 1N1680027

SHIP QUANTITY: 23, 400 PCS LOT QUANTITY 170, 278 PCS

HEADMARKS:

MANUFACTURE DATE: 2016/08/26

COUNTRY OF ORIGIN: CHINA

Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567

DATE: 2017/03/23

PACKING NO: GEM160919007
INVOICE NO: GEM/FNL-160929WI

PART NO: 36713 SAMPLING PLAN:

ASME B18.18-2011 (Category.2) / ASTM F1470-2012

HEAT NO: **331608011**MATERIAL: ML08

FINISH: HOT DIP GALVANIZED PER ASTM A153-

2009/ASTM F2329-2013

R#17-507 H#331608011

BCT Cable Bracket Nuts

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO ASTM A563-2007

Chemistry	AL%	C%	MN%	P%	S%	SI%
Spec. : MIN.						
MAX.		0.5800		0.1300	0. 2300	
Test Value	0. 0350	0. 0700	0. 4100	0.0160	0. 0060	0. 0500

DIMENSIONAL INSPECTIONS :ACCORDING TO ASME B18. 2. 2-2010

SAMPLED BY: DWTING

INSPECTIONS ITEM	SAMPLE	SP	ECIFIED	ACTUAL RESULT	ACC.	REJ.
WIDTH ACROSS CORNERS	6 PCS		1.0510-1.0830 inch	1.0560-1.0690 inch	6	0
FIM	15 PCS	ASME B18. 2. 2-2010	Max. 0.0210 inch	0.0020-0.0040 inch	15	0
THICKNESS	6 PCS		0.5350-0.5590 inch	0.5390-0.5570 inch	6	0
WIDTH ACROSS FLATS	6 PCS		0.9220-0.9380 inch	0.9240-0.9340 inch	6	0
SURFACE DISCONTINUITIES	29 PCS		ASTM F812-2012	PASSED	29	0
THREAD	15 PCS		GAGING SYSTEM 21	PASSED	15	0

MECHANICAL PROPERTIES: ACCORDING TO ASTM A563-2007

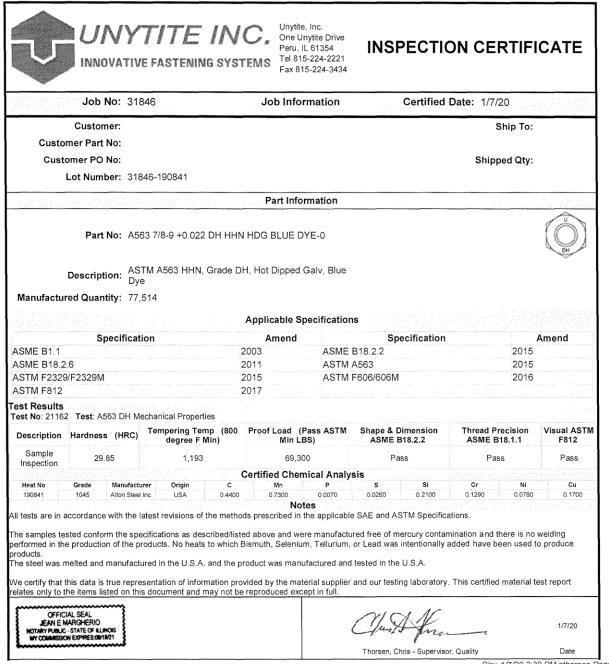
SAMPLED BY: GDAN LIAN

INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
CORE HARDNESS	15 PCS	ASTM F606-2014		68-107 HRB	79-81 HRB	15	0
PROOF LOAD	4 PCS	ASTM F606-2014		Min. 90 KSI	ОК	4	0
PLATING THICKNESS (µ m)	5 PCS	ASTM B568-1998		>=53	70. 02-75. 81	5	0

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER:3358.01)
WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER

Quality Supervisor:

Figure B-35. %-in. Hex Nut, Test No. FLAGT-1 (Item No. h2)



Plex 1/7/20 2:39 PM cthorsen Page 1

Figure B-36. %-in. Heavy Hex Nut, Test No. FLAGT-1 (Item No. h3)



GEM-YEAR TESTING LABORATORY CERTIFICATE OF INSPECTION

 ${\bf MANUFACTURER:} \textbf{GEM-YEAR INDUSTRIAL CO., LTD.}$

ADDRESS: NO.8 GEM-YEAR

ROAD, E.D.Z., JIASHAN, ZHEJIANG, P.R.CHINA

PURCHASER: FASTENAL COMPANY PURCHASING

PO. NUMBER: 110254885

COMMODITY: FINISHED HEX NUT GR-A SIZE: 7/8-9 NC 0/T 0.56MM

LOT NO: 1N1810005

SHIP QUANTITY: 9,000 PCS LOT QUANTITY 55,748 PCS

HEADMARKS:

MANUFACTURE DATE: 2018/01/05
COUNTRY OF ORIGIN: CHINA

Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567

DATE: 2018/03/28

PACKING NO: GEM180115010
INVOICE NO: GEM/FNL-180201WI-1

PART NO: 36717 SAMPLING PLAN:

ASME B18.18-2011(Category.2)/ASTM F1470-2012

HEAT NO: 331704677 MATERIAL: XGML08

FINISH: HOT DIP GALVANIZED PER ASTM A153-

2009/ASTM F2329-2013

SAMPLED BY: TANCHAO

19 riv

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO ASTM A563-2015

Chemistry	AL%	C%	MN%	P%	S%	SI%
Spec. : MIN.					-	
MAX.		0.5800		0.1300	0. 2300	
Test Value	0. 0360	0.0600	0. 4500	0.0140	0.0030	0.0300

DIMENSIONAL INSPECTIONS :ACCORDING TO ASME B18. 2. 2-2015

		S	AMPLED	BY: WDANDAN		
INSPECTIONS ITEM	SAMPLE	SPECIFIED		ACTUAL RESULT	ACC.	REJ.
WIDTH ACROSS CORNERS	5 PCS	1. 4470-1. 5160	inch	1.4850-1.4930 inch	5	0
FIM	15 PCS	ASME B18. 2. 2-2015 Max. 0. 0250	inch	0.0110-0.0200 inch	15	0
THICKNESS	5 PCS	0. 7240-0. 7760	inch	0.7460-0.7570 inch	5	0
WIDTH ACROSS FLATS	5 PCS	1. 2690-1. 3120	inch	1.2930-1.2980 inch	5	0
SURFACE DISCONTINUITIES	29 PCS	ASTM F812-2012		PASSED	29	0
THREAD	15 PCS	GAGING SYSTE	M 21	PASSED	15	0

MECHANICAL PROPERTIES: ACCORDING TO ASTM A563-2015

					TILIOILIO			
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ.	
CORE HARDNESS	15 PCS	ASTM F606-2014		68-107 HRB	86-90 HRB	15	0	
PROOF LOAD	5 PCS	ASTM F606-2014		Min. 31,416 LBF	OK	5	0	
PLATING THICKNESS (µ m)	29 PCS	ASTM B568-1998		>=53	62. 38-62. 57	29	0	

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER:3358.01)
WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER

Quality Supervisor:

Figure B-37. 1/8-in. Hex Nut, Test No. FLAGT-1 (Item No. h4)

Nov. 26. 2018 3:47PM Fastenal-NELIN

No. 5947 P. 2

Certificate of Compliance

Sold To: Purchase Order: STBR UNL TRANSPORTATION Item# f3, h1 and i1 Job: Invoice Date: 11/8/2018 THIS IS TO CERTIFY THAT WE HAVE SUPPLIED YOU WITH THE FOLLOWING PARTS. THESE PARTS WERE PURCHASED TO THE FOLLOWING SPECIFICATIONS. 80 PCS 1"-8 Hot Dipped Galvanized A563 Grade DH Heavy Hex Nut Made In USA SUPPLIED UNDER OUR TRACE NUMBER 210157128 AND UNDER PART NUMBER 38210 450 PCS·3/4"-10 Hot Dipped Galvanized A563 Grade DH Heavy Hex Nut Made In USA SUPPLIED UNDER OUR TRACE NUMBER 210169774 AND UNDER PART NUMBER 38208. 80 PCS 1"-8 Hot Dipped Galvanized A563 Grade DH Heavy Hex Nut Made In USA SUPPLIED UNDER OUR TRACE NUMBER 210157128 AND UNDER PART NUMBER 38210 This is to certify that the above document is true Please check current revision to avoid using obsolete copies. and accurate to the best of my knowledge. This document was printed on 11/26/2018 and was current at that Fastenal Account Representative Signature Fastenal Store Location/Address 3201 N. 23rd Street STE 1 LINCOLN, NE 68521 Phone #: (402)476-7900 Fax #: 402/476-7958 Page 1 of 1

Figure B-38. 1-in. Heavy Hex Nut, Test No. FLAGT-1 (Item No. h5)



Norfolk Iron & Metal Co.

3001 North Victory Road Norfolk, NE 68701 PH: (402) 371-1810

Document: 01131005

Sold To: RIVERS METAL PRODUCTS 3100 N 38TH ST LINCOLN, NE 68504

Sales Order: 01414254

Ship To: RIVERS METAL PRODUCTS 3100 N 38TH ST LINCOLN, NE 68504

Customer PO: /po 51265

Product Information

30185 - PLATE 3/16 A36 COLD REDUCED

Thickness: .1875 Width: 48.0000

Length: 96.0000

Mill Coil: 5301939 NLMK IN

Heat: Y6325 Supplier: NLMK INDIANA

Specification(s): ASTM A36 PLATE-19, ASME SA36-2019

Chemistry Data

Mechanical Data

	Yield (PSI)	Tensile (PSI)	Elongation	Reduction Of Area
1	48873	64548	44.63 2"	72.5300
2	48389	64315	40.39 2"	62.7900

Sample Taken From Head

Center

Produced From Coil

The Mechanical Data for the product described above reflect the results of tests made by us in accordance with applicable ASTM or ASME standards and our testing procedures, and we certify that the information included in this Test Certificate with respect to such Mechanical Data is accurate to the best of our knowledge.

The Chemistry Data shown above was reported to us by NLMK INDIANA Test Certificate solely for your information. and have been included in this

Figure B-39. ³/₁₆-in. AGT Connector Face Plate, Test No. FLAGT-1 (Item No. i1)



Norfolk Iron & Metal Co.

3001 North Victory Road Norfolk, NE 68701 PH: (402) 371-1810

Document: 01130910

Sold To: RIVERS METAL PRODUCTS 3100 N 38TH ST LINCOLN, NE 68504

Sales Order: 01378617

Ship To: RIVERS METAL PRODUCTS 3100 N 38TH ST LINCOLN, NE 68504

Customer PO: /po 50335

Product Information

25872 - PLATE 1/4 A36 COLD REDUCED

Thickness: .2500 Width: 48.0000

Length: 96.0000

Mill Coil: 363757 ARC BH

Heat: 813L65970 Supplier: ARCELORMITTAL

Specification(s):
ASTM A36 PLATE-19, ASME SA36-2019

Chem	is	trv	Da	ta

.16	MN .87	P .011	S .004	.009	AL .039	CB .002	.001	.014	CR .02
NI	MO	SN	TI	N	B	ZR	PB . 00	MG	ZN
.01	.002	.003	.002	.004	.0002	.00		.00	.00

Mechanical Data

	Yield (PSI)	Tensile (PSI)	Elongation	Reduction Of Area	Sample Taken From
1	41580	64129	40.15 2"	53.4500	Head
2	42270	62242	42.52 2"	59.7600	Center

Produced From Coil

Melted In: UNITED STATES, Manufacured In: UNITED STATES

The Mechanical Data for the product described above reflect the results of tests made by us in accordance with applicable ASTM or ASME standards and our testing procedures, and we certify that the information included in this Test Certificate with respect to such Mechanical Data is accurate to the best of our knowledge.

The Chemistry Data shown above was reported to us by ARCELORMITTAL Test Certificate solely for your information. and have been included in this

Figure B-40. ¼-in. AGT Connector Gusset Plates, Test No. FLAGT-1 (Item Nos. i2 through i7)

Appendix C. Vehicle Center of Gravity Determination

		Test Name:		_ VIN:		R6FGXGS28	
Model Year: 2	2016	Make:_	RAM	Model:	1:	500 Quad Ca	ıb
Vehicle CG Deter	minatio	1					
Vehicle Equipment				Weight (lb)	Vertical CG (in.)	Vertical M (lb-in.)	
		Fruck (Curb)		4910	28.536214	140112.81	
+ Hub		rack (Garz)		19	15	285	
(C) E-(C)(V)		ion cylinder &	frame	7	29 7/8	209.125	
		nk (Nitrogen)	Hamo	22	27 4/7	606.375	
	be/Brake			5	26	130	
		er/Wires		5	53	265	
		uding DAQ		30	29	870	
- Batte		a.ag 27, .a.		-44	42 1/4	-1859	
- Oil	70.J.			-12	19	-228	
- Inter	ior			-91	36	-3276	
- Fuel	20000000			-143	19	-2717	
- Cool				-12	32 1/2	-390	
	sher fluid			-8	32 1/2	-260	
		t (In Fuel Tanl	()	228	19	4332	
		plemental Bat		5	26	130	
	l Plate	F1-111-111-11		67	33 5/8	2252.875	
				10.00	17.5 .51.5	0	
LAND MY AND MY IN THE STATE OF							
Note: (+) is added equip		Estimated Tota	al Weight (lb)	4988]	140463.19	
	I	Estimated Total Vertical CG	al Weight (lb) Location (in.)	4988		355023	
Note: (+) is added equip Vehicle Dimension Wheel Base: 14	ns for C	Estimated Total Vertical CG	al Weight (lb) Location (in.)	4988	•	355023	
Vehicle Dimensio	ns for C	Estimated Tota Vertical CG G. Calculation	al Weight (lb) Location (in.) ons Front Tr	4988 28.1602	68.5	140463.19	
Vehicle Dimensio Wheel Base: 14	ns for C	Estimated Tota Vertical CG . G. Calculatic n.	al Weight (lb) Location (in.) ons Front Tr Rear Tr	4988 28.1602 ack Width:	68.5 69	140463.19 in. in.	Difference
Vehicle Dimension Wheel Base: 14	ns for C . 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS	al Weight (lb) Location (in.) ons Front Tr Rear Tr	4988 28.1602 ack Width:	68.5 69 Test Inertial	140463.19 in. in.	
Vehicle Dimension Wheel Base: 14	ns for C . 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000:	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110	4988 28.1602 ack Width:	68.5 69 Test Inertial 5003	140463.19 in. in.	3.0
Vehicle Dimension Wheel Base: 14	ns for C . 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110	4988 28.1602 ack Width:	68.5 69 Test Inertial	140463.19 in. in.	3.0 3.08223
Vehicle Dimension Wheel Base: 14 Center of Gravity Test Inertial Weight Longitudinal CG (in Lateral CG (in.)	ns for C . 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA	al Weight (lb) Location (in.) ons Front Tr Rear Tr 6H Targets ± 110 ± 4	4988 28.1602 ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442	140463.19 in. in.	3.0 3.08223 NA
Vehicle Dimension Wheel Base:146 Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.)	ns for C 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28:0	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater	4988 28.1602 ack Width:	68.5 69 Test Inertial 5003 66.082226	140463.19 in. in.	3.0 3.08223 NA
Vehicle Dimension Wheel Base: 14 Center of Gravity Test Inertial Weight Longitudinal CG (in Lateral CG (in.)	ns for C 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28:0 front axle of test	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16	140463.19 in. in.	Difference 3.0 3.08223 NA 0.16022
Vehicle Dimension Wheel Base: 149 Center of Gravity Test Inertial Weight Longitudinal CG (in.) Lateral CG (in.) Vertical CG (in.) Note: Long. CG is mea	ns for C 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28:0 front axle of test	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16	140463.19 in. in.	3.08223 NA 0.16022
Vehicle Dimension Wheel Base: 146 Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.) Vertical CG (in.) Note: Long. CG is mea Note: Lateral CG meas CURB WEIGHT (Ib	ns for C. 0.625 i t (lb) n.)	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28: front axle of test centerline - positi	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16	in. in.	3.08223 NA 0.16022 T (lb.)
Vehicle Dimension Wheel Base: 146 Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.) Vertical CG (in.) Note: Long. CG is mea Note: Lateral CG meas CURB WEIGHT (Ib	ns for C. 0.625 i t (lb) n.) sured from c.)	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28:0 front axle of test centerline - positi	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16 TEST INER	in. in. tin. Left	3.08223 NA 0.16022 T (lb.)
Vehicle Dimension Wheel Base:14i Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.) Vertical CG (in.) Note: Long. CG is mea Note: Lateral CG meas CURB WEIGHT (III Front 1	ns for C. 0.625 i t (lb) n.) sured from o.) Left	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28:0 front axle of test centerline - positi Right 1319	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16 TEST INER	in. in. Left 1373	3.08223 NA 0.16022 T (lb.) Right 1279
Vehicle Dimension Wheel Base:14i Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.) Vertical CG (in.) Note: Long. CG is mea Note: Lateral CG meas CURB WEIGHT (III Front 1	ns for C. 0.625 i t (lb) n.) sured from c.)	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28:0 front axle of test centerline - positi	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16 TEST INER	in. in. tin. Left	3.08223 NA 0.16022 T (lb.)
Vehicle Dimension Wheel Base:14l Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.) Note: Long. CG is mea Note: Lateral CG meas CURB WEIGHT (III Front1 Rear1	ns for C 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28: front axle of test centerline - positi Right 1319 1086	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16 TEST INER	in. in. in. Left 1373 1181	3.08223 NA 0.16022 T (lb.) Right 1279 1170
Vehicle Dimension Wheel Base:14 Center of Gravity Test Inertial Weight Longitudinal CG (in.) Vertical CG (in.) Vertical CG (in.) Note: Long. CG is mea Note: Lateral CG meas CURB WEIGHT (Ib: Front1 Rear1 FRONT2	ns for C 0.625 i	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28: front axle of test centerline - positi Right 1319 1086 b	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16 TEST INER Front Rear FRONT	in. in. in. Left 1373 1181	3.08223 NA 0.16022 T (lb.) Right 1279 1170
Vehicle Dimension Wheel Base:	ns for C 0.625 i t (lb) n.) sured from b.) Left 376 129 2695 2215	Estimated Total Vertical CG G. Calculation 2270P MAS 5000: 63: NA 28: front axle of test centerline - positi Right 1319 1086	al Weight (lb) Location (in.) ons Front Tr Rear Tr SH Targets ± 110 ± 4 or greater vehicle	4988 28.1602 ack Width: ack Width:	68.5 69 Test Inertial 5003 66.082226 -0.721442 28.16 TEST INER	in. in. in. Left 1373 1181 2652 2351	3.08223 NA 0.16022 T (lb.) Right 1279 1170

Figure C-1. Vehicle Mass Distribution, Test No. FLAGT-1

Appendix D. Static Soil Tests

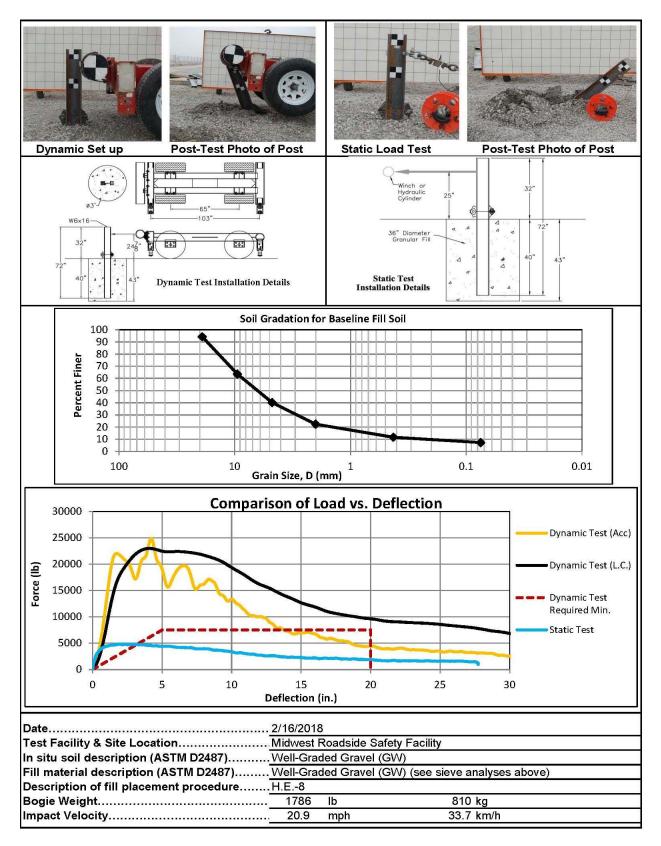


Figure D-1. Soil Strength, Initial Calibration Tests, Test No. FLAGT-1

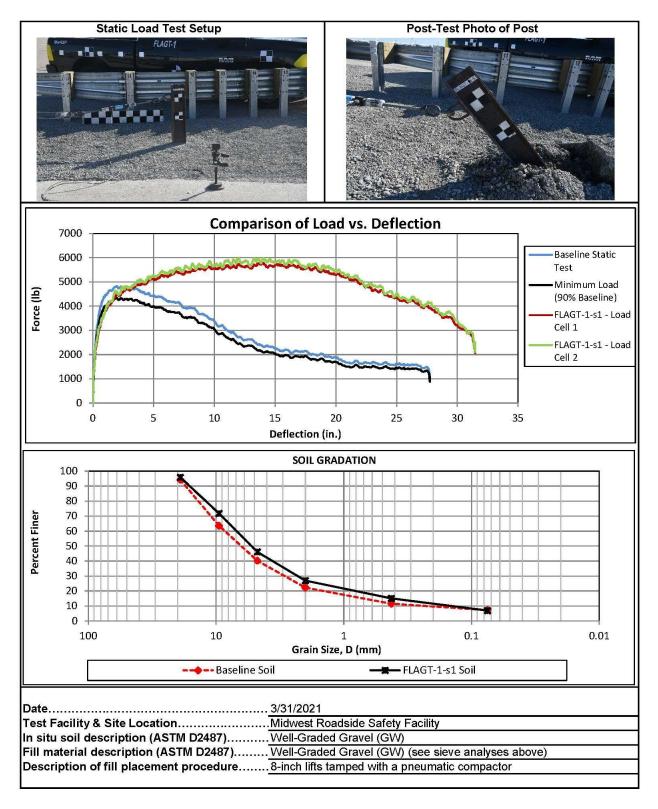


Figure D-2. Static Soil Test, Test No. FLAGT-1

Appendix E. Vehicle Deformation Records

The following figures and tables describe all occupant compartment measurements taken on the test vehicles used in full-scale crash testing herein. MASH defines intrusion as the occupant compartment being deformed and reduced in size with no penetration. Outward deformations, which are denoted as negative numbers within this appendix, are not considered as crush toward the occupant, and are not subject to evaluation by MASH criteria.

odel Year.	20	116	6		Test Name: Make:		GT-1 AM			VIN: Model:		R6FGXGS: 500 Quad C		
	VEHICLE DEFORMATION PASSENGER SIDE FLOOR PAN - SET 2													
	POINT	Pretest X (in.)	Pretest Y (in.)	Pretest Z (in.)	Posttest X (in.)	Posttest Y (in.)	Posttest Z (in.)	ΔΧ ^A (in.)	ΔΥ ^A (in.)	ΔZ ^A (in.)	Total ∆ (in.)	Crush ⁸ (in.)	Direction for Crush ^C	
	1	52.5478	32.6316	-7.1908	N/a	N/a	N/a	#VALUE!	#VALUE!	#VALUE!	NA	NA	#VALUE	
	2	53.6385	36.5714	-5.1093	47.8097	35.4114	-9.5232	5.8288	1.1600	4.4139	7.4029	7.3115	X, Z	
	3	54.7467	41.5102	-1.6958	47.9035	36.9411	-4.6330	6.8432	4.5691	2.9372	8.7369	7.4469	X, Z	
TOE PAN - WHEEL WELL (X, Z)	4	55.3417	46.8894	-2.2714	44.4622	39.9821	-7.4000	10.8795	6.9073	5.1286	13.8700	12.0277	X,Z	
PAN LWE	.5	54.7380	50.7480	-1.9434	45.7057	42.6574	-5.9780	9.0323	8.0906	4.0346	12.7796	9.8924	X,Z	
計画人	6	49.3102	30.3283	-6.4779	N/a	N/a	N/a	#VALUE!	#VALUE!	#VALUE!	NA	NA	#VALUI	
TOE HEEL	7	50.2384	35.0131	-3.9381	44.2854	33.9749	-10.1793	5.9530	1.0382	6.2412	8.6873	8.6250	X,Z	
3	8	51.5779	40.5391	0.0543	44.9338	36.7037	-3.6019	6.6441	3.8354	3.6562	8.4984	7.5837	X, Z	
200	9	51.6064	46.0474	0.0166	43.5474	40.2226	-2.8338	8.0590	5.8248	2.8504	10.3441	8.5482	X, Z	
	10	51.4276	50.5666	0.1318	43.3624	43.1802	-2.9840	8.0652	7.3864	3.1158	11.3717	8.6461	X,Z	
	11	45,7751	29.6318	-5.2667	42.8688	28.3552	-8.0436	2.9063	1.2766	2.7769	4.2175	2.7769	Z	
8	12	46.9725	34.1169	-1.5718	40.2057	33.0980	-9.3245	6.7668	1.0189	7.7527	10.3408	7.7527	Z	
	13	48.0209	40.1839	1.3141	41.2095	37.2978	-3.6025	6.8114	2.8861	4.9166	8.8824	4.9166	Z	
	14	48.0937	45.7289	1.3275	42.2586	40.8073	0.3628	5.8351	4.9216	0.9647	7.6942	0.9647	Z	
	15	47.9001	50.3799	1.3407	41.9406	44.5043	-0.5223	5.9595	5.8756	1.8630	8.5737	1.8630	Z	
	16	42.3108	29.8014	-3.7243	40.2300	29.2059	-5.5110	2.0808	0.5955	1.7867	2.8065	1.7867	Z	
	17	43.6580	33.4900	1.1486	38.4309	34.0034	-6.2914	5.2271	-0.5134	7.4400	9.1071	7.4400	Z	
<u> 22</u> 2	18	44.0169	39.7450	1.2965	37.5569	38.0640	-3.8515	6.4600	1.6810	5.1480	8.4297	5.1480	Z	
₹	19	44.1033	46.4285	1.3124	38.6434	42.8407	0.5514	5.4599	3.5878	0.7610	6.5774	0.7610	Z	
7.KZ	20	44.0693	50.4249	1.3250	38.7357	45.4254	0.9497	5.3336	4.9995	0.3753	7.3201	0.3753	Z	
Ď.	21	38.0583	30.0018	-3.5626	36.3453	29.1957	-3.7137	1.7130	0.8061	0.1511	1.8992	0.1511	Z	
FLOOR PAN (Z)	22	39.6803	33.3762	1.0421	37.0015	34.2955	-2.7025	2.6788	-0.9193	3.7446	4.6950	3.7446	Z	
ш	23	39.6934	40.0794	1.0204	33.8438	39.8391	-4.4534	5.8496	0.2403	5.4738	8.0149	5.4738	Z	
	24	39.5391	45.8373	1.0331	35.1194	44.2515	-0.8228	4,4197	1.5858	1.8559	5.0490	1.8559	Z	
	25	39.5235	50.0241	1.0496	35.1853	47.0588	2.1557	4.3382	2.9653	-1.1061	5.3700	-1.1061	Z	
	26	34.2159	30.0742	-2.5885	32.9958	30.0847	-1.9923	1.2201	-0.0105	-0.5962	1.3580	-0.5962	Z	
	27	34.3557	33.1591	0.8753	33.7174	34.1056	0.8128	0.6383	-0.9465	0.0625	1.1433	0.0625	Z	
	28	34.2595	39.6990	0.8578	33.0026	40.5266	0.6149	1.2569	-0.8276	0.2429	1.5244	0.2429	Z	
	29	34.2291	45.6846	0.8924	31.0290	45.9300	-0.0707	3.2001	-0.2454	0.9631	3.3509	0.9631	Z	
	30	34.2888	49.8939	0.9822	N/a	N/a	N/a	#VALUE!	#VALUE!	#VALUE!	NA	NA	Z	

A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

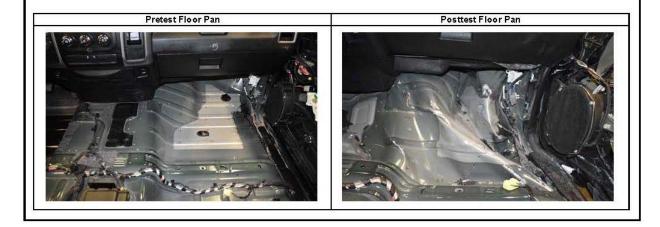


Figure E-1. Floor Pan Deformation Data – Set 2, Test No. FLAGT-1

Comparation in the calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

City Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

/lodel Year:	20	116	e e		Test Name: Make:		GT-1 AM			VIN: Model:		R6FGXGS: 500 Quad C	
					VE	UICLE DE	CODMATI	ON			Č.		
				PA			FORMATI		T 2				
	8	Pretest X	Pretest Y	Pretest Z			Posttest Z	ΔX ^A	ΔY ^A	ΔZ ^A	Total ∆	Crush ^B	Directio for
	POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	Crush
	1	46.2479	50.2141	-30.7012	41.9370	48.0129	-32.9524	4.3109	2.2012	-2.2512	5.3383	5.3383	X, Y, 2
τÑ	2	44.0204	37.5314	-30.1476	40.6783	35.2630	-32.5884	3.3421	2.2684	-2.4408	4.7194	4.7194	X, Y, Z
DASH (X, Y, Z)	3 4	41.1750 40.9373	20.5048 50.8392	-30.7039 -19.7193	38.8772 36.2363	17.8674 48.0538	-32.9284 -22.2961	2.2978 4.7010	2.6374 2.7854	-2.2245 -2.5768	4.1454 6.0413	4.1454 6.0413	X, Y, Z X, Y, Z
_ ≥	5	40.1948	38.6811	-20.0835	36.3364	35.8747	-22.6852	3.8584	2.8064	-2.6017	5.4343	5.4343	X, Y, Z
	6	38.0422	20.4905	-20.4788	35.3816	17.8537	-22.9086	2.6606	2.6368	-2.4298	4.4649	4.4649	X, Y, 2
ᄪᆒ	7	49.9066	53.3107	-6.0084	42.9208	45.8149	-8.0659	6.9858	7.4958	-2.0575	10.4509	7.4958	Y
SIDE PANEL	8	50.1667	53.3149	-9.8343	43.1509	46.3736	-12.0212	7.0158	6.9413	-2.1869	10.1087	6.9413	Y
	9	53.5214	53.2351	-5.6343	46.2280	44.6561	-8.1285	7.2934	8.5790	-2.4942	11.5332	8.5790	Y
씽	10 11	16.5802	55.1470 54.9409	-23.6893	12.0382	60.1802	-21.2792	4.5420 5.2858	-5.0332	2.4101 0.5350	7.1952 6.9405	-5.0332	Y
N K -	12	29.4850 41.1025	55.1701	-23.6816 -23.2067	24.1992 34.8253	59.4069 55.4122	-23.1466 -24.2086	6.2772	-4.4660 -0.2421	-1.0019	6.3613	-4.4660 -0.2421	Y
386	13	16.7220	55.1792	-7.1085	N/a	N/a	N/a	#VALUE!	#VALUE!	#VALUE!	NA	NA	Y
IMPACT SIDE DOOR (Y)	14	25.2677	55.9609	-8.1587	19.0089	56.7599	-8.3018	6.2588	-0.7990	-0.1431	6.3112	-0.7990	Y
=	15	36.9107	55.7373	-6.9771	30.3820	53.1157	-7.8754	6.5287	2.6216	-0.8983	7.0925	2.6216	Υ
	16	33.5150	43.0529	-46.3404	33.6745	41.5732	-50.3429	-0.1595	1.4797	-4.0025	4.2702	-4.0025	Z
	17	36.1385	33.1055	-46.6144	36.2455	31.5709	-49.7271	-0.1070	1.5346	-3.1127	3.4721	-3.1127	Z
	18 19	37.3060 27.4083	20.9809 42.9246	-46.8191 -49.0587	37.1526 27.3379	19.4842 41.3084	-48.9948 -51.7789	0.1534 0.0704	1.4967 1.6162	-2.1757 -2.7202	2.6452 3.1649	-2.1757 -2.7202	Z Z
	20	30.3254	32.3000	-49.3595	30.2431	30.6744	-51.6596	0.0704	1.6256	-2.7202	2.8178	-2.7202	Z
_	21	31.2878	20.8878	-49.4910	31.1842	19.3019	-51.5382	0.1036	1.5859	-2.0472	2.5917	-2.0472	Z
Z) -	22	21.3382	42.5442	-49.9646	21.4347	40.9596	-50.2895	-0.0965	1.5846	-0.3249	1.6204	-0.3249	Z
ROOF - (Z)	23	22.8164	32.6754	-50.4381	23.1220	30.9588	-49.5590	-0.3056	1.7166	0.8791	1.9527	0.8791	Z
» l	24	23.8092	21.2270	-50.6818	23.8288	19.7992	-51.7753	-0.0196	1.4278	-1.0935	1.7985	-1.0935	Z
_	25	14.7631	42.1954	-50.4204	15.1863	40.6154	-48.2829	-0.4232	1.5800	2.1375	2.6915	2.1375	Z
	26 27	16.6528 17.3962	32.5732 21.9850	-50.9241 -51.1325	16.9620 17.4641	31.2041 20.7896	-50.7479 -50.6301	-0.3092 -0.0679	1.3691 1.1954	0.1762 0.5024	1.4146 1.2985	0.1762 0.5024	Z
*	28	10.2152	41.7249	-50.6783	10.6871	40.5127	-49.7209	-0.4719	1.2122	0.9574	1.6152	0.9574	Z
	29	10.3178	32.4585	-51.2254	10.5885	31.3605	-50.1958	-0.2707	1.0980	1.0296	1.5294	1.0296	Z
	30	10.4432	22.4787	-51.4470	10.6304	21.2987	-50.4622	-0.1872	1.1800	0.9848	1.5483	0.9848	Z
50	31	49.8368	52.0262	-32.3206	46.0375	50.5464	-33.6997	3.7993	1.4798	-1.3791	4.3042	4.0773	X, Y
A-PILLAR Maximum (X, Y, Z)	32	47.0144	51.3208	-34.3679	43.9347	49.9353	-36.5195	3.0797	1.3855	-2.1516	4.0042	3.3770	X, Y
⋣ ₹ \	33 34	43.0848	50.5493	-38.2487 -40.8526	41.5095	49.1214	-41.4440 -45.0671	1.5753 0.5372	1.4279	-3.1953	3.8380 4.4526	2.1261	X, Y
₽ ĝ ×	35	39.4660 35.8978	49.7038 48.8791	-43.1443	38.9288 36.2421	48.3714 47.5782	-48.3074	-0.3443	1.3324 1.3009	-4.2145 -5.1631	5.3356	1.4366 1.3009	X, Y
Carrier 1	36	32.4710	47.7751	-44.6398	33.1849	46.4064	-49.2252	-0.7139	1.3687	-4.5854	4.8383	1.3687	Ÿ
	31	49.8368	52.0262	-32.3206	46.0375	50.5464	-33.6997	3.7993	1.4798	-1.3791	4.3042	1.4798	Y
A-PILLAR Lateral (Y)	32	47.0144	51.3208	-34.3679	43.9347	49.9353	-36.5195	3.0797	1.3855	-2.1516	4.0042	1.3855	Y
_ = E	33	43.0848	50.5493	-38.2487	41.5095	49.1214	-41.4440	1.5753	1.4279	-3.1953	3.8380	1.4279	Y
ate at	34	39.4660	49.7038	-40.8526	38.9288	48.3714	-45.0671	0.5372	1.3324	-4.2145	4.4526	1.3324	Y
47	35 36	35.8978 32.4710	48.8791 47.7751	-43.1443 -44.6398	36.2421 33.1849	47.5782 46.4064	-48.3074 -49.2252	-0.3443 -0.7139	1.3009 1.3687	-5.1631 -4.5854	5.3356 4.8383	1.3009 1.3687	Y
۳ E -	37	9.4304	47.7731	-46.4760	9.9402	46.3537	-44.9099	-0.5098	0.9665	1.5661	1.9096	1.8403	Y, Z
B-PILLAR Maximum (X, Y, Z)	38	8.3713	48.3468	-43.3440	8.8529	47.4326	-41.8299	-0.4816	0.9142	1.5141	1.8331	1.7687	Y, Z
	39	6.5271	49.7915	-39.0853	6.7443	48.8641	-37.6194	-0.2172	0.9274	1.4659	1.7482	1.7346	Y, Z
	40	9.4939	51.6467	-33.7235	9.4780	50.8447	-32.1685	0.0159	0.8020	1.5550	1.7497	1.7497	X, Y, 2
38	37	9.4304	47.3202	-46.4760	9.9402	46.3537	-44.9099	-0.5098	0.9665	1.5661	1.9096	0.9665	Y
-PILLAR ateral (Y)	38	8.3713	48.3468	-43.3440	8.8529	47.4326	-41.8299	-0.4816	0.9142	1.5141	1.8331	0.9142	Y
B-PILL Lateral	39	6.5271	49.7915	-39.0853	6.7443	48.8641	-37.6194	-0.2172	0.9274	1.4659	1.7482	0.9274	Y
A Positive v	40	9.4939	51.6467	-33.7235	9.4780	50.8447	-32.1685	0.0159	0.8020	1.5550	1.7497	0.8020	T

Figure E-2. Occupant Compartment Deformation Data – Set 2, Test No. FLAGT-1

CDirection for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

MwRSF Report N	
MwRSF Report No. TRP-03-439b-25	141ay 10, 2020

Model Year:	2016		Test Name: Make:	FLAGT-1 RAM	VIN: Model:		
		F	Passenger Side M	Maximum Deformation			
	Reference Set				Reference Se	t 2	
Location Roof	Maximum Deformation ^{A,B} (in.) 0.0	MASH Allowable Deformation (in.) ≤ 4	Directions of Deformation ^C	Location Roof	Maximum Deformation ^{A,B} (in.) 2.1	MASH Allowable Deformation (in.) ≤ 4	Directions of Deformation ^C
Windshield ^D	0.0	≤ 3	X, Z	Windshield ^D	NA	≤ 3	X, Z
A-Pillar Maximum	0.0	≤ 5	NA	A-Pillar Maximum	4.1	≤ 5	X, Y
A-Pillar Lateral	0.0	≤3	Υ	A-Pillar Lateral	1.5	≤3	Υ
B-Pillar Maximum	0.0	≤ 5	NA	B-Pillar Maximum	1.8	≤ 5	Y, Z
B-Pillar Lateral	0.0	≤3	Υ	B-Pillar Lateral	1.0	≤3	Υ
Toe Pan - Wheel Well	0.0	≤ 9	NA	Toe Pan - Wheel Well	12.0	≤ 9	X, Z
Side Front Panel	0.0	≤ 12	Υ	Side Front Panel	8.6	≤ 12	Υ
Side Door (above seat)	0.0	≤ 9	Υ	Side Door (above seat)	-5.0	≤ 9	Υ
Side Door (below seat)	0.0	≤ 12	Υ	Side Door (below seat)	2.6	≤ 12	Υ
Floor Pan	0.0	≤ 12	Z	Floor Pan	7.8	≤ 12	Z
Dash - no MASH requirement	0.0	NA	X, Y, Z	Dash - no MASH requirement	6.0	NA	X, Y, Z
[©] For Toe Pan - Wheel Well the didirections. The direction of deforr occupant compartment. If direction	ion as inward towar rection of defromati nation for Toe Pan on of deformation is	d the occupant compion may include X an -Wheel Well, A-Pillar "NA" then no intrusio	nd Z direction. For A Maximum, and B-F on is recorded and c	values denote deformations outward av -Pillar Maximum and B-Pillar Maximum Pillar Maximum only include component deformation will be 0. I posttest with an examplar vehicle, the	the direction of de s where the deform	formation may include ation is positive and	intruding into the
Notes on vehicle interior cru	sh:						

Figure E-3. Maximum Occupant Compartment Deformations by Location, Test No. FLAGT-1

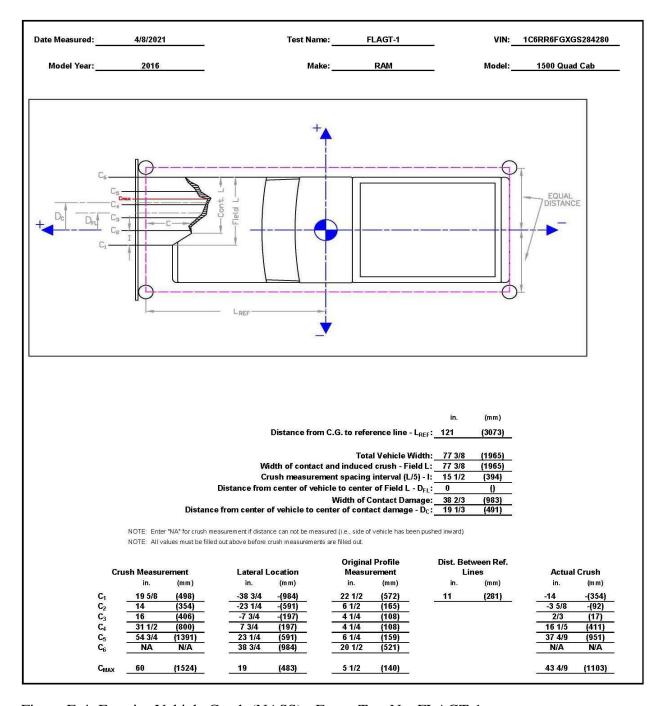


Figure E-4. Exterior Vehicle Crush (NASS) - Front, Test No. FLAGT-1

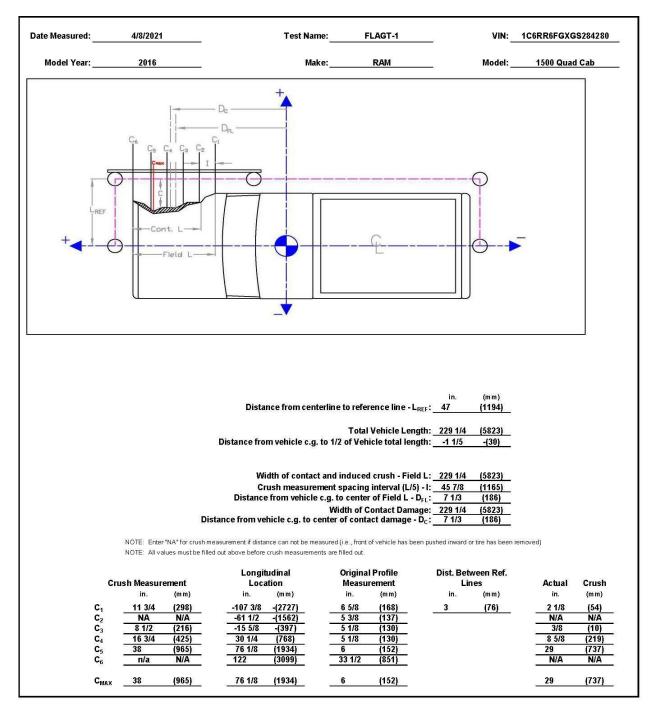


Figure E-5. Exterior Vehicle Crush (NASS) - Side, Test No. FLAGT-1

Appendix F. Accelerometer and Rate Transducer Data Plots, Test No. FLAGT-1

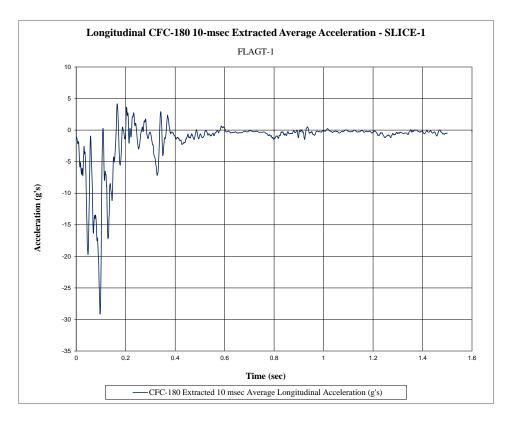


Figure F-1. 10-ms Average Longitudinal Deceleration (SLICE-1), Test No. FLAGT-1

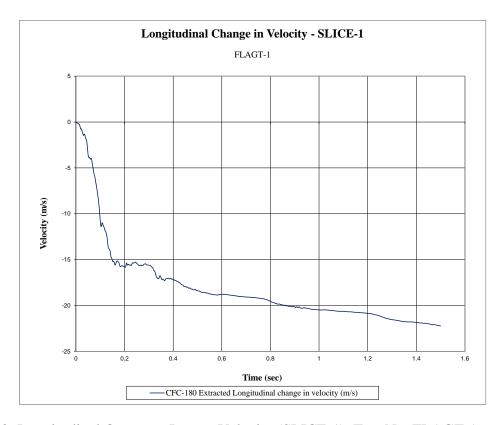


Figure F-2. Longitudinal Occupant Impact Velocity (SLICE-1), Test No. FLAGT-1

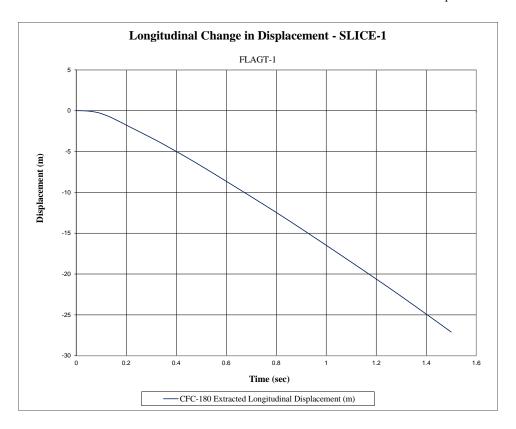


Figure F-3. Longitudinal Occupant Displacement (SLICE-1), Test No. FLAGT-1

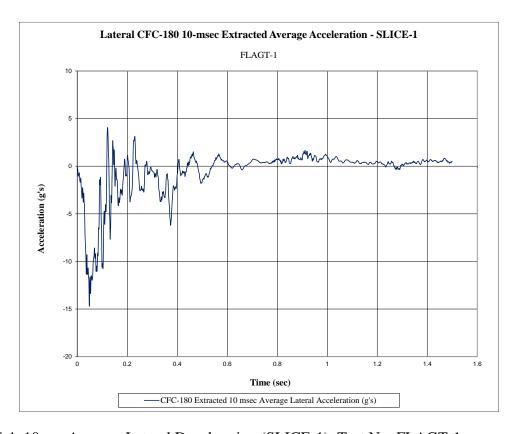


Figure F-4. 10-ms Average Lateral Deceleration (SLICE-1), Test No. FLAGT-1

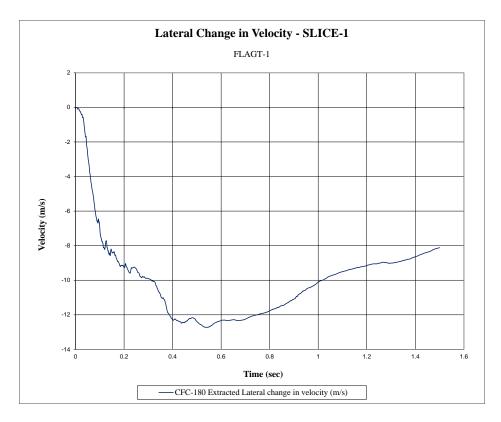


Figure F-5. Lateral Occupant Impact Velocity (SLICE-1), Test No. FLAGT-1

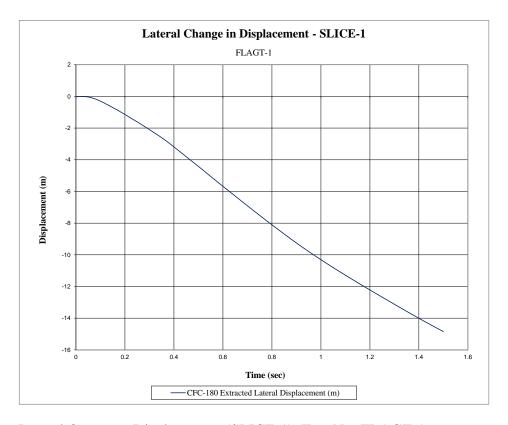


Figure F-6. Lateral Occupant Displacement (SLICE-1), Test No. FLAGT-1

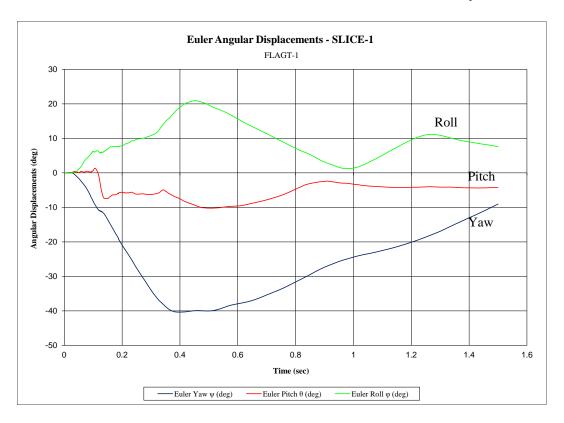


Figure F-7. Vehicle Angular Displacements (SLICE-1), Test No. FLAGT-1

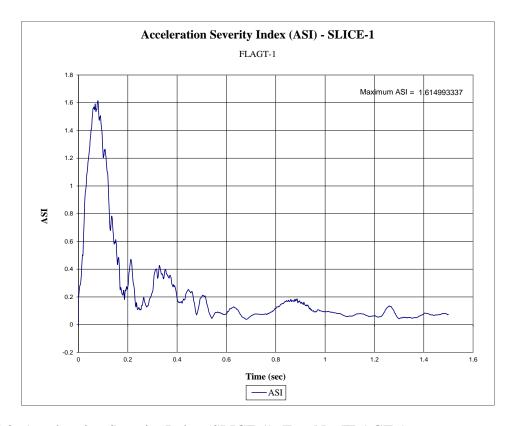


Figure F-8. Acceleration Severity Index (SLICE-1), Test No. FLAGT-1

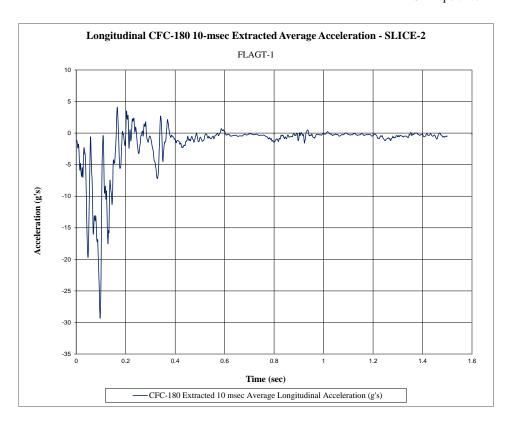


Figure F-9. 10-ms Average Longitudinal Deceleration (SLICE-2), Test No. FLAGT-1

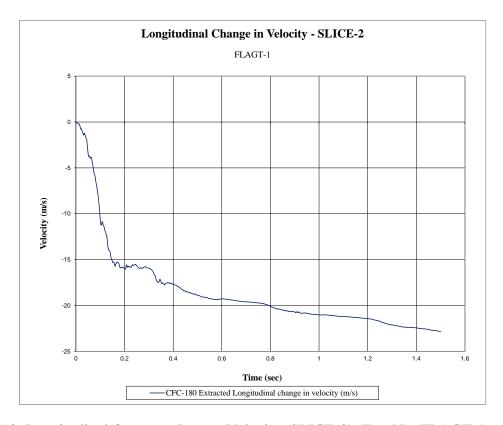


Figure F-10. Longitudinal Occupant Impact Velocity (SLICE-2), Test No. FLAGT-1

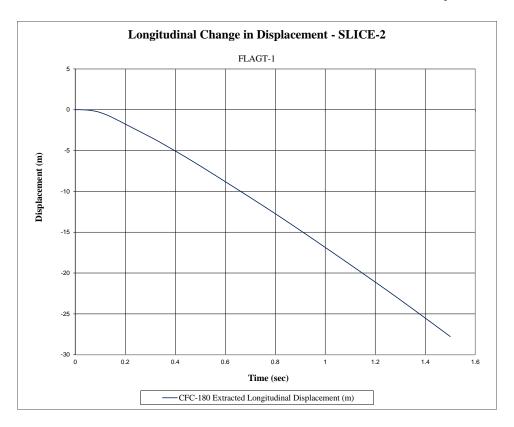


Figure F-11. Longitudinal Occupant Displacement (SLICE-2), Test No. FLAGT-1

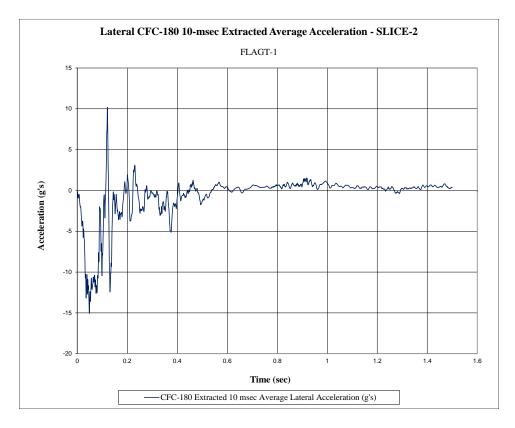


Figure F-12. 10-ms Average Lateral Deceleration (SLICE-2), Test No. FLAGT-1

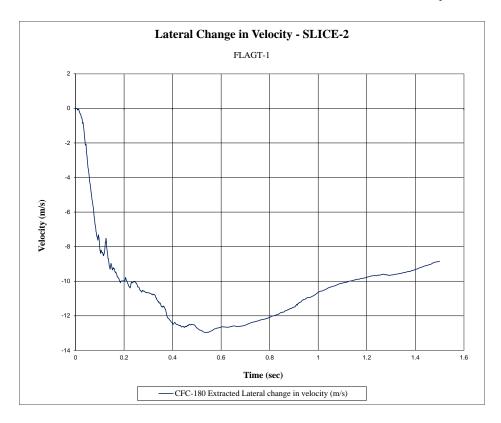


Figure F-13. Lateral Occupant Impact Velocity (SLICE-2), Test No. FLAGT-1

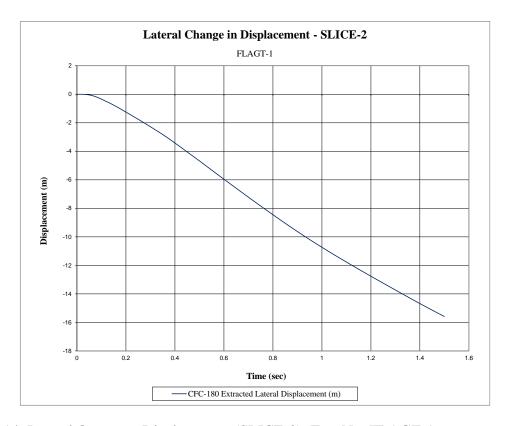


Figure F-14. Lateral Occupant Displacement (SLICE-2), Test No. FLAGT-1

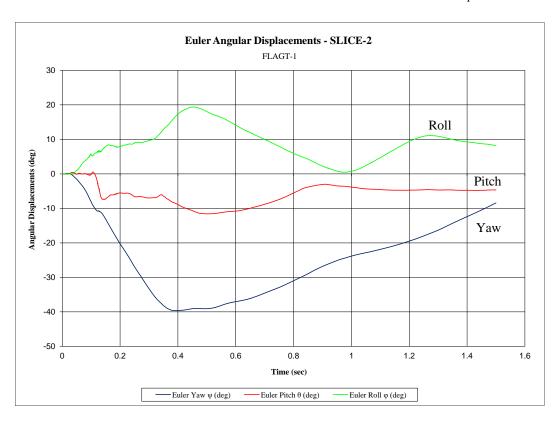


Figure F-15. Vehicle Angular Displacements (SLICE-2), Test No. FLAGT-1

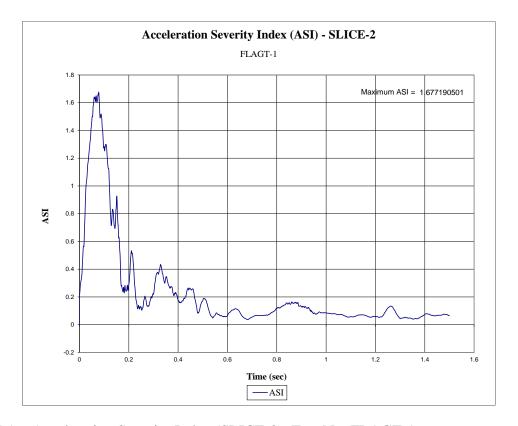


Figure F-16. Acceleration Severity Index (SLICE-2), Test No. FLAGT-1

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