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EVALUATION OF THE HAWAII MODIFIED NATCHEZ TRACE BRIDGE RAIL: MASH TEST DESIGNATION NO. 3-11



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| 16. Abstract <p>The Hawaii Department of Transportation (HDOT) utilizes the Hawaii Modified Natchez Trace Bridge Rail to safely redirect vehicles on bridges. However, the crashworthiness of this bridge rail has not been investigated under current impact safety standards. This report documents one full-scale crash test conducted to evaluate the safety performance of HDOT's Hawaii Modified Natchez Trace Bridge Rail. The system had a mounting height of 36 in. and varied in width from 18¼ in. at the top to 24 in. at the bottom. The bridge rail design utilized 12-in. long by 12-in. wide posts that were spaced 90 in. apart on centerlines and mounted on top of a 10-in. high curb. The test installation had an overall length of 70 ft – 7 in. and incorporated three railing segments with ½-in. expansion joints placed at the end of each rail segment. Test no. HNTBR-1 was conducted according to the <i>Manual for Assessing Safety Hardware</i> (MASH) test designation no. 3-11.</p> <p>In test no. HNTBR-1, a 2270P vehicle impacted the Hawaii Modified Natchez Trace Bridge Rail at a speed of 62.3 mph and an angle of 25.0 degrees. The vehicle was safely contained and redirected with minimal damage to the bridge rail. However, the occupant compartment intrusion at the wheel well and toe pan measured 12.7 in., which exceeded the MASH limit of 9 in. Thus, test no. HNTBR-1 failed to satisfy the safety standards of MASH. The system will need to be redesigned and re-tested in future research efforts.</p> | | | | | |
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DISCLAIMER STATEMENT

This material is based upon work supported by the Federal Highway Administration, U.S. Department of Transportation, and the Hawaii Department of Transportation under Research Contract No. 69876. The contents of this report reflect the views and opinions of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the University of Nebraska-Lincoln, Hawaii Department of Transportation nor the Federal Highway Administration, U.S. Department of Transportation. This report does not constitute a standard, specification, or regulation. Trade or manufacturers' names, which may appear in this report, are cited only because they are considered essential to the objectives of the report. The United States (U.S.) government and the States of Nebraska and Hawaii do not endorse products or manufacturers.

UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority for the data contained herein was Dr. Andrew Loken, Research Assistant Professor.

A2LA ACCREDITATION

The tests reported herein are within the scope of MwRSF's A2LA Accreditation. MwRSF's accreditation documentation can be found in Appendix A.

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| SI* (MODERN METRIC) CONVERSION FACTORS | | | | |
|---|-----------------------------|----------------------------|-----------------------------|---------------------|
| APPROXIMATE CONVERSIONS TO SI UNITS | | | | |
| Symbol | When You Know | Multiply By | To Find | Symbol |
| LENGTH | | | | |
| in. | inches | 25.4 | millimeters | mm |
| ft | feet | 0.305 | meters | m |
| yd | yards | 0.914 | meters | m |
| mi | miles | 1.61 | kilometers | km |
| AREA | | | | |
| in ² | square inches | 645.2 | square millimeters | mm ² |
| ft ² | square feet | 0.093 | square meters | m ² |
| yd ² | square yard | 0.836 | square meters | m ² |
| ac | acres | 0.405 | hectares | ha |
| mi ² | square miles | 2.59 | square kilometers | km ² |
| VOLUME | | | | |
| fl oz | fluid ounces | 29.57 | milliliters | mL |
| gal | gallons | 3.785 | liters | L |
| ft ³ | cubic feet | 0.028 | cubic meters | m ³ |
| yd ³ | cubic yards | 0.765 | cubic meters | m ³ |
| NOTE: volumes greater than 1,000 L shall be shown in m ³ | | | | |
| MASS | | | | |
| oz | ounces | 28.35 | grams | g |
| lb | pounds | 0.454 | kilograms | kg |
| T | short ton (2,000 lb) | 0.907 | megagrams (or "metric ton") | Mg (or "t") |
| TEMPERATURE (exact degrees) | | | | |
| °F | Fahrenheit | 5(F-32)/9 or (F-32)/1.8 | Celsius | °C |
| ILLUMINATION | | | | |
| fc | foot-candles | 10.76 | lux | lx |
| fl | foot-Lamberts | 3.426 | candela per square meter | cd/m ² |
| FORCE & PRESSURE or STRESS | | | | |
| lbf | poundforce | 4.45 | newtons | N |
| lbf/in ² | poundforce per square inch | 6.89 | kilopascals | kPa |
| APPROXIMATE CONVERSIONS FROM SI UNITS | | | | |
| Symbol | When You Know | Multiply By | To Find | Symbol |
| LENGTH | | | | |
| mm | millimeters | 0.039 | inches | in. |
| m | meters | 3.28 | feet | ft |
| m | meters | 1.09 | yards | yd |
| km | kilometers | 0.621 | miles | mi |
| AREA | | | | |
| mm ² | square millimeters | 0.0016 | square inches | in ² |
| m ² | square meters | 10.764 | square feet | ft ² |
| m ² | square meters | 1.195 | square yard | yd ² |
| ha | hectares | 2.47 | acres | ac |
| km ² | square kilometers | 0.386 | square miles | mi ² |
| VOLUME | | | | |
| mL | milliliter | 0.034 | fluid ounces | fl oz |
| L | liters | 0.264 | gallons | gal |
| m ³ | cubic meters | 35.314 | cubic feet | ft ³ |
| m ³ | cubic meters | 1.307 | cubic yards | yd ³ |
| MASS | | | | |
| g | grams | 0.035 | ounces | oz |
| kg | kilograms | 2.202 | pounds | lb |
| Mg (or "t") | megagrams (or "metric ton") | 1.103 | short ton (2,000 lb) | T |
| TEMPERATURE (exact degrees) | | | | |
| °C | Celsius | 1.8C+32 | Fahrenheit | °F |
| ILLUMINATION | | | | |
| lx | lux | 0.0929 | foot-candles | fc |
| cd/m ² | candela per square meter | 0.2919 | foot-Lamberts | fl |
| FORCE & PRESSURE or STRESS | | | | |
| N | newtons | 0.225 | poundforce | lbf |
| kPa | kilopascals | 0.145 | poundforce per square inch | lbf/in ² |

*SI is the symbol for the International System of Units. Appropriate rounding should be made to comply with Section 4 of ASTM E380.

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1 INTRODUCTION

1.1 Background

The Hawaii Department of Transportation (HDOT) utilizes the Hawaii Modified Natchez Trace Bridge Rail to safely redirect vehicles on bridges. However, the crashworthiness of this bridge rail has not been investigated under current impact safety standards. This report documents full-scale crash testing conducted to evaluate the safety performance of the Hawaii Modified Natchez Trace Bridge Rail according to the Test Level 3 (TL-3) criteria of the *Manual for Assessing Safety Hardware* (MASH) [1].

In 1992, the original Natchez Trace Parkway Bridge Rail [2] was evaluated to Performance Level 1 (PL-1) criteria according to the *AASHTO Guide Specifications for Bridge Railings* [3] at the Midwest Roadside Safety Facility (MwRSF). The Natchez Trace Bridge Rail was an open concrete bridge rail positioned atop a 10-in. tall curb, as shown in Figure 1. The railing incorporated a 13-in. tall by 12-in. wide concrete rail supported by 9-in. x 18-in. concrete posts spaced 7 ft – 6¾ in. apart. The face of the curb extended approximately 4½ in. out from the face of the concrete railing.

In test no. NTBR-1, a 1984 Chevrolet Custom Deluxe 20 pickup truck impacted the bridge rail at 45.2 mph and an angle of 22.4 degrees. Upon impact, the test vehicle was smoothly redirected. There was no intrusion or deformation of the occupant compartment, and the bridge rail received only superficial damage. Therefore, test no. NTBR-1 was deemed acceptable according to the NCHRP Report 230 safety performance criteria for test designation PL-1. In test no. NTBR-2, a 1984 Renault Encore small car impacted the bridge rail at 51.5 mph and an angle of 19.5 degrees. Similarly, the vehicle was smoothly redirected with minimal bridge rail damage. Thus, the Natchez Trace Bridge Rail successfully passed all requirements for AASHTO PL-1.

In 2001, researchers at the Texas A&M Transportation Institute (TTI) conducted crash tests to evaluate the Natchez Trace Bridge Rail in accordance with NCHRP Report 350 [4, 5]. The test installation, shown in Figure 2, was identical to the system crash tested at MwRSF except for minor variations in reinforcement.

In test no. 405181-11, a 1997 Geo Metro small car impacted the Natchez Trace Bridge Rail at 62.1 mph and an impact angle of 19.8 degrees. The bridge rail safely contained and redirected the passenger car, resulting in the test successfully passing NCHRP 350 test designation no. 3-10 safety requirements. In test no. 405181-12, a 1997 Chevrolet 2500 pickup truck impacted the Natchez Trace Bridge Rail at 61.1 mph and an impact angle of 26.1 degrees. The bridge rail safely contained and redirected the pickup truck, and the test successfully met NCHRP 350 test designation no. 3-11 evaluation criteria.

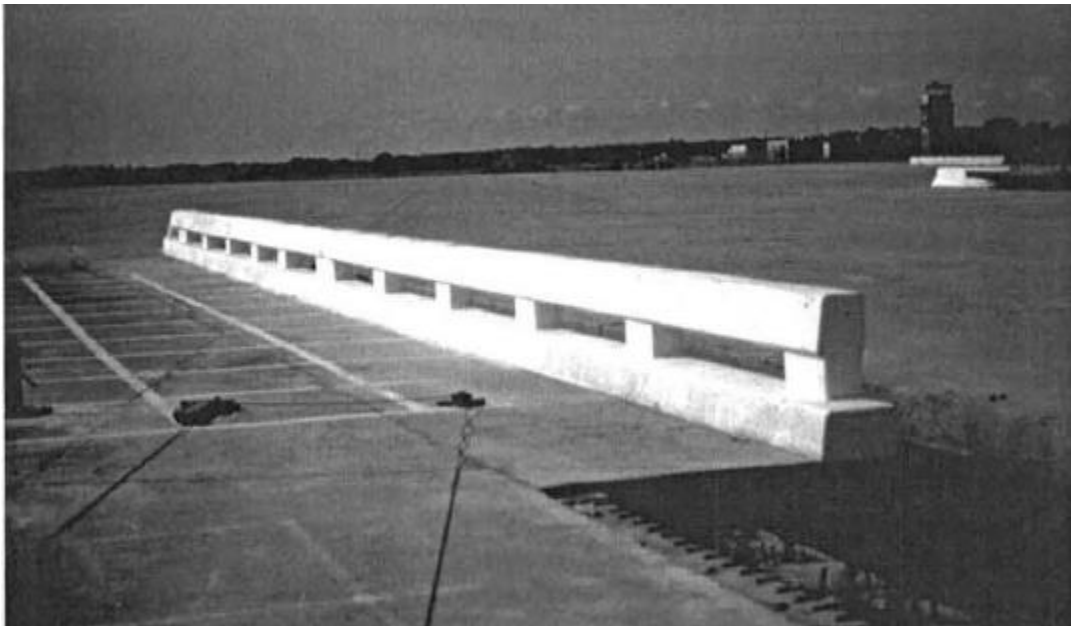
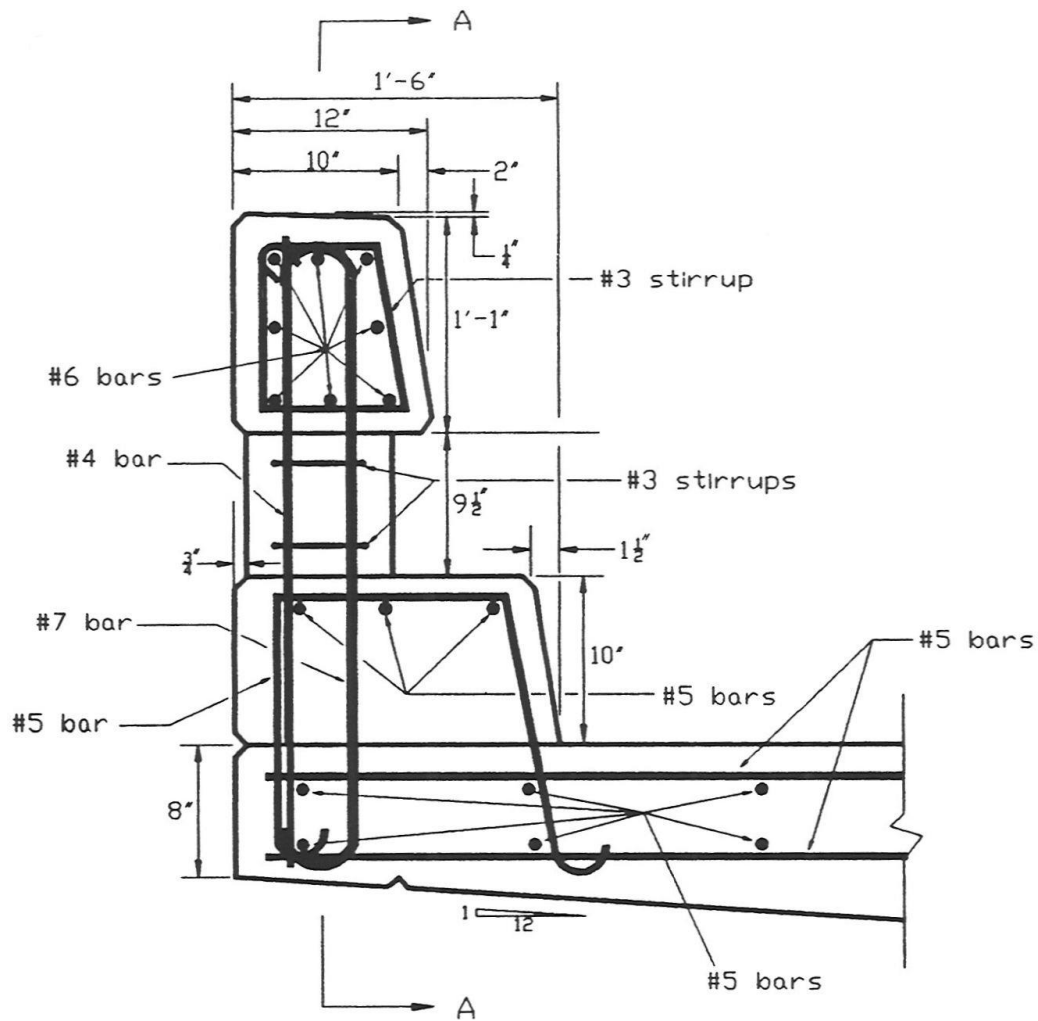


Figure 1. Natchez Trace Bridge Rail Design Details, Test No. NTBR-1 [2]

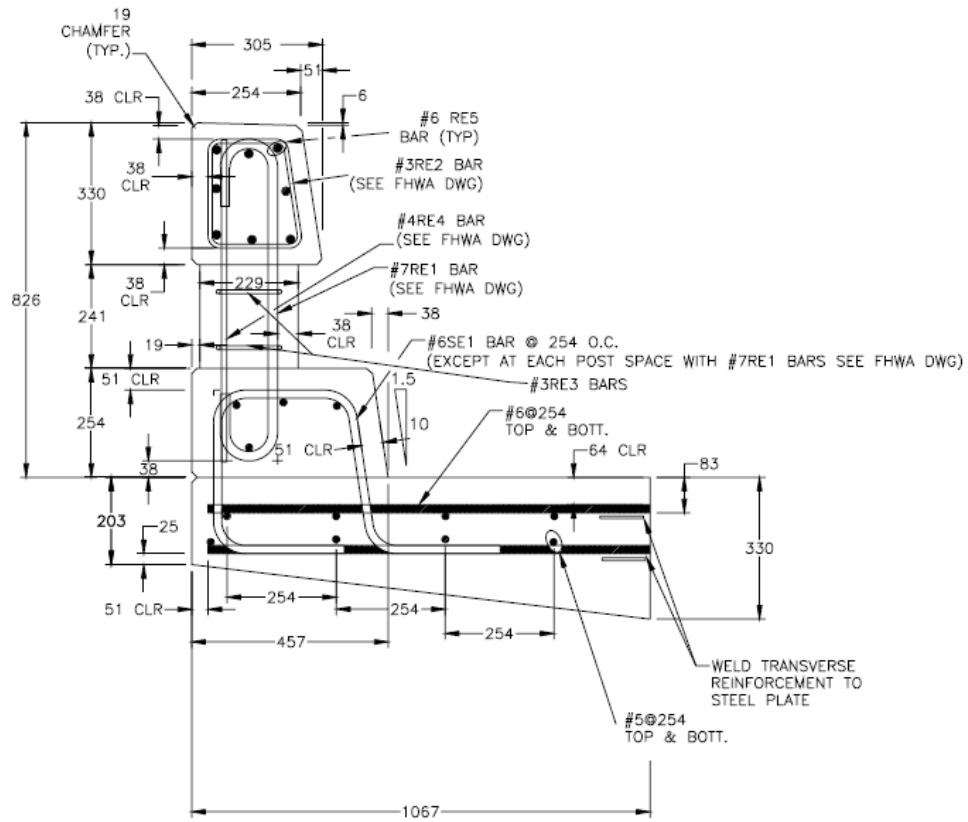


Figure 2. Natchez Trace Bridge Rail Design Details, Test Nos. 405181-11 and 405181-12 (dimensions in mm) [4]

Recently, HDOT desired to have its modified version of the Natchez Trace Bridge Rail evaluated according to MASH TL-3 criteria [1]. The Hawaii-modified version of the Natchez Trace Bridge Rail had several differences compared to the original design previously crash tested at MwRSF [2] and TTI [5]. The height of the Hawaii modified design increased from 32½ in. to 36 in., and the width of the railing also increased significantly. The original Natchez Trace Bridge Rail had a top width of 10 in., a base width of 18 in., and a 4½-in offset between the bottom corner of the rail and the top corner of the curb. The Hawaii modified design had a top width of 18¼ in., a base width of 24 in., and a 1½-in. offset between the bottom corner of the rail and the top corner of the curb. Note, this offset effectively gave the Hawaii modified design a single slope profile when combining the rail and the curb. The Hawaii modified design used smaller, 12-in. long by 12-in. wide posts to support the rail. Finally, the Hawaii design incorporated a steel tube, pedestrian handrail mounted to the back side of the concrete rail. Details for the Hawaii Modified Natchez Trace Bridge Railing are shown in Figure 3.

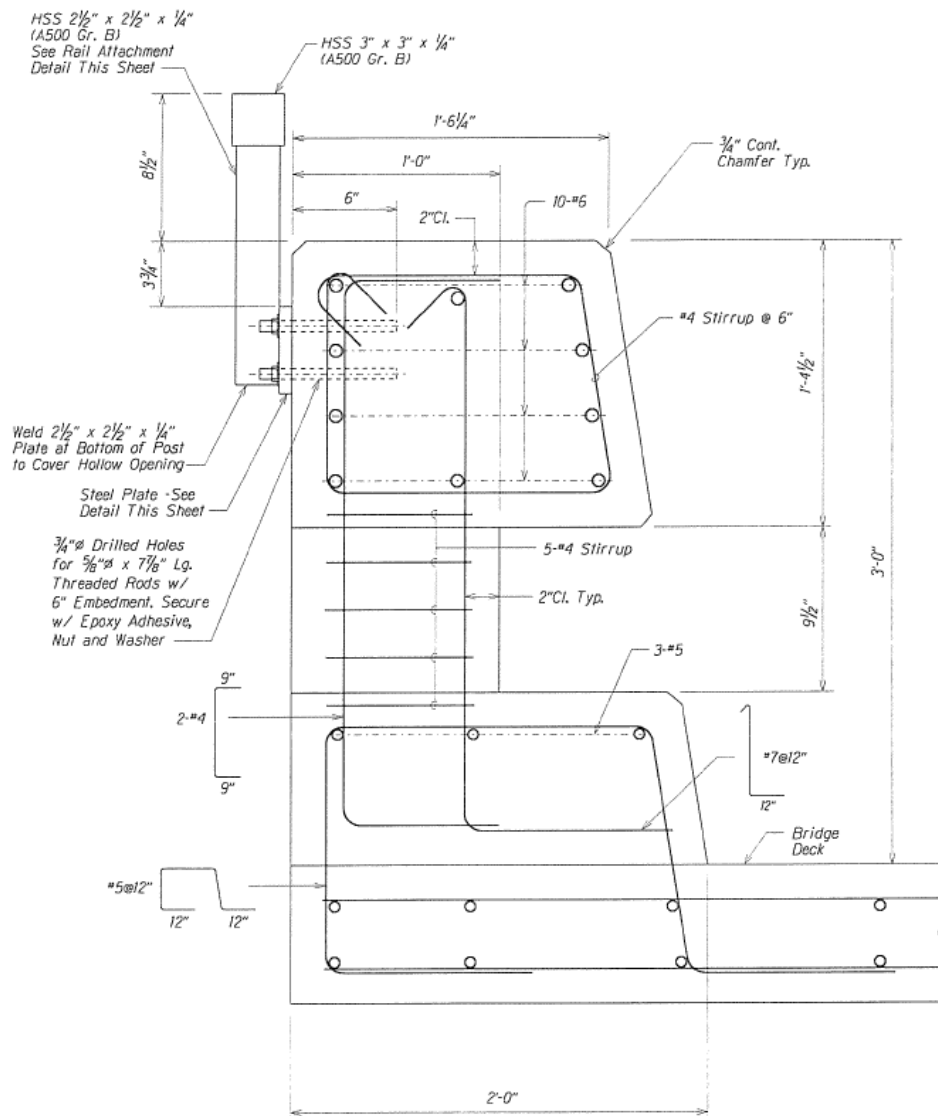


Figure 3. Hawaii Modified Natchez Trace Bridge Rail Design Details

1.2 Objective

The objective of this project was to evaluate the safety performance of the Hawaii Modified Natchez Trace Bridge Rail according to the TL-3 criteria of MASH [1].

1.3 Scope

The research objective was achieved through the completion of several tasks. The first task included a review of HDOT's existing standard plans for the Hawaii Modified Natchez Trace Bridge Rail, identification of potential safety issues, and recommendation of system modifications to improve the crashworthiness of the bridge rail. Next, one full-scale crash test was conducted on the Hawaii Modified Natchez Trace Bridge Rail according to MASH test designation no. 3-11. The full-scale vehicle crash test results were analyzed, evaluated, and documented. Conclusions and recommendations were then made pertaining to the safety performance of the bridge rail and future research.

2 DESIGN DETAILS

The Hawaii Modified Natchez Bridge Railing consisted of a curb-mounted, open concrete bridge railing with a single slope front profile, as shown in Figures 4 through 14. Photographs of the test installation are shown in Figures 15 and 16.

The test installation had an overall length of 70 ft – 7 in. and incorporated three railing segments with ½-in. expansion joints placed between adjacent rail segments. The design featured a 16½-in. tall by 20⅞-in. wide concrete rail with a top height of 36 in. The width of the bridge rail varied from 18¼ in. at the top to 24 in. at the bottom. The back side of the railing was vertical, and the front face maintained a continuous slope from top to bottom, including the curb. The design used 12-in. long by 12-in. wide concrete posts spaced 7 ft – 6 in. apart. The open concrete bridge railing was positioned on a 10-in. tall concrete curb.

The rail, posts, and curb were reinforced with a combination of transverse and longitudinal rebar. Reinforcement in the rail consisted of ten #6 bars located inside #4 enclosed stirrups. There were four #6 bars on each face of the rail and two additional #6 bars on the top and bottom of the rail. Vertical reinforcement in the posts consisted of four #7 hooked bars on the traffic face of the posts with four #4 bars on the non-traffic side. The vertical bars in the posts were enclosed by five #4 stirrups that were evenly spaced at 2¾ in. between the top of the curb and the bottom of the rail. Longitudinal reinforcement in the curb consisted of three longitudinal #5 bars located inside #5 transverse U-bars. The U-bars were epoxied into the concrete tarmac to a depth of 6 in. using Hilti HIT RE-500 epoxy to develop their full tensile strength.

The pedestrian handrail installed on the back side of the bridge rail had a top mounting height of 42½ in. The handrail assembly consisted of HSS3x3x¼ steel tubes supported by 13¾-in. long HSS2½x2½x¼ tube posts. The tube posts were welded to 8-in. x 5-in. x ¾-in. thick mounting plates, which were attached to the back-side of the concrete railing using four ⅝-in. diameter threaded rods epoxied into the railing. The handrail segments were spliced together using 7-in. long HSS2x2x¼ tubes with ⅜-in. thick shims. One end of the splice tube was inserted 2 in. and welded to the downstream end of the handrail tube, while the other end extended into the upstream end of the adjacent handrail tube.

The concrete mix for the bridge railing required a minimum 28-day compressive strength of 4,000 psi. The cylinder break strength 1 week prior to testing was 4,060 psi. All reinforcement was epoxy-coated ASTM A615 Grade 60 bars. The handrail was assembled from ASTM A500 Grade B tubes and ASTM A16 steel plates. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix B.

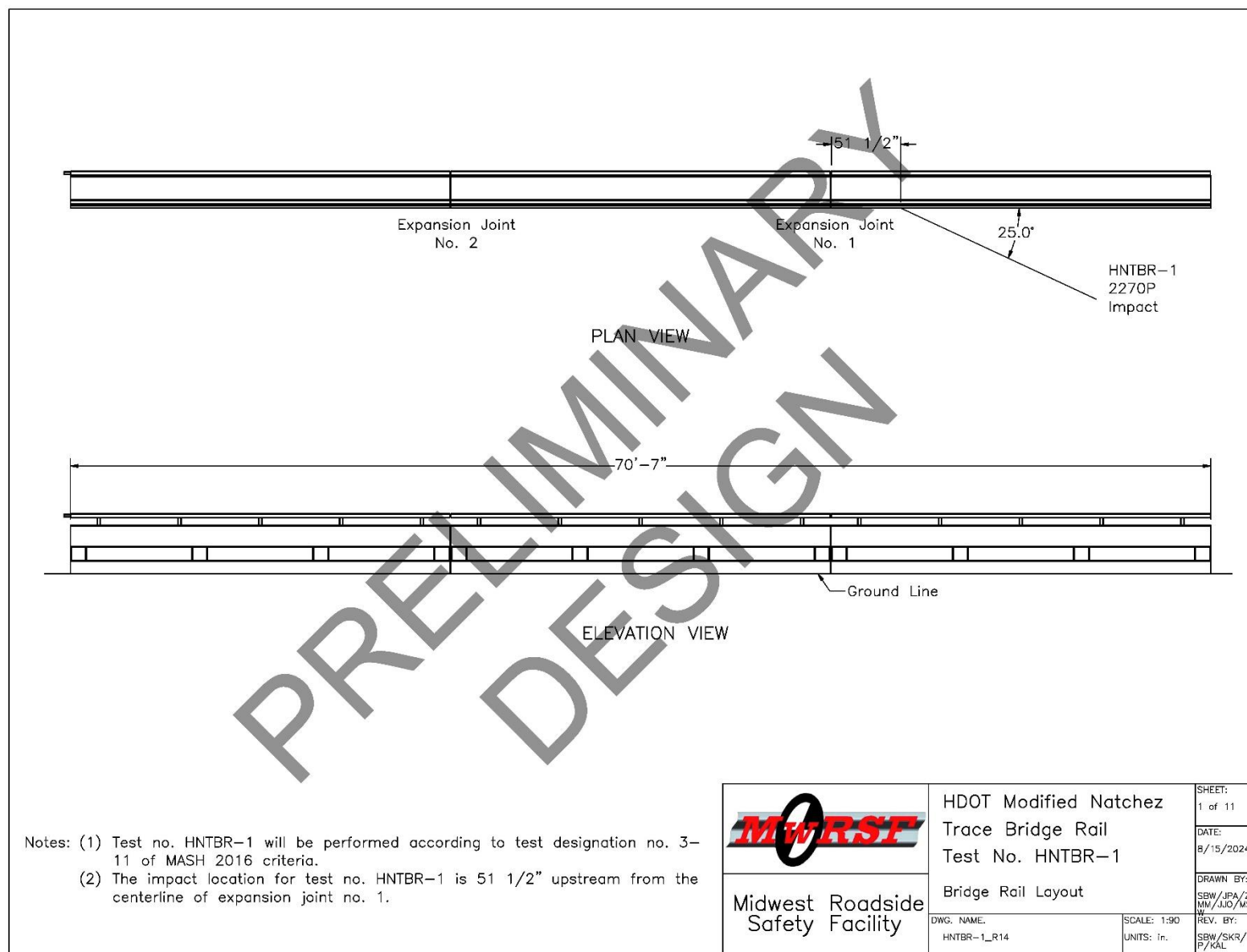


Figure 4. Test Installation Layout, Test No. HNTBR-1

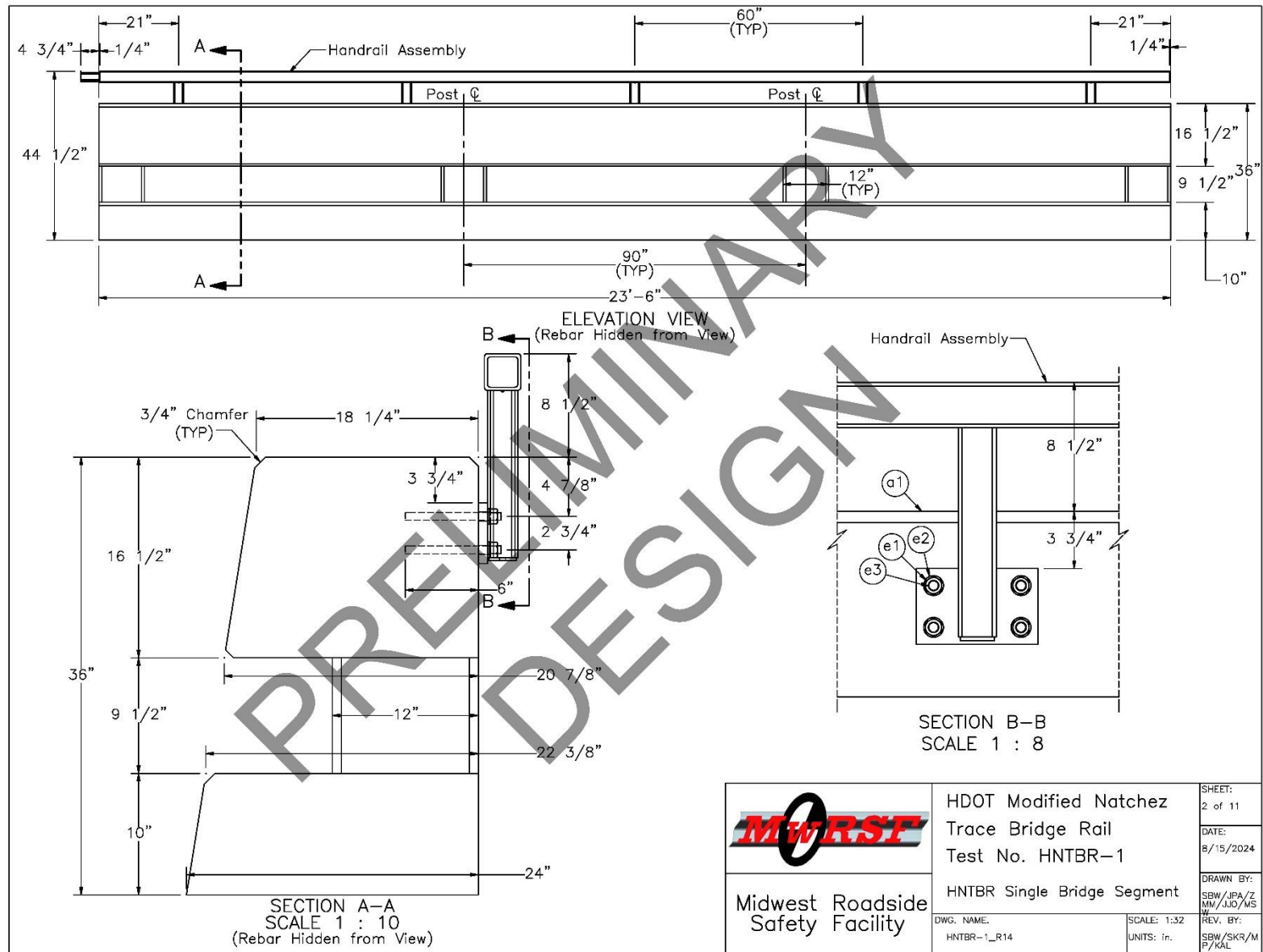


Figure 5. Bridge Rail Layout, Test No. HNTBR-1

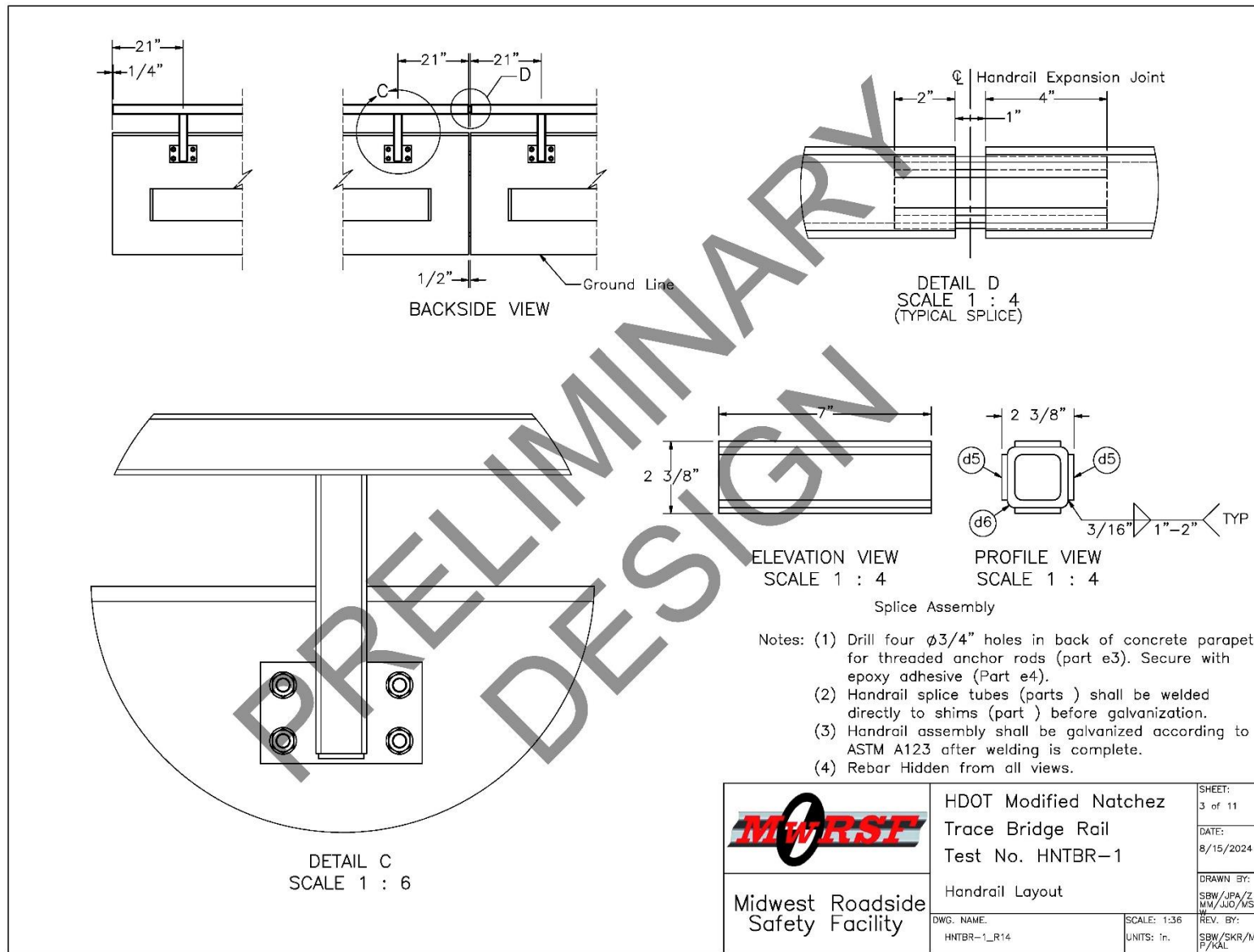


Figure 6. Handrail Detail, Test No. HNTBR-1

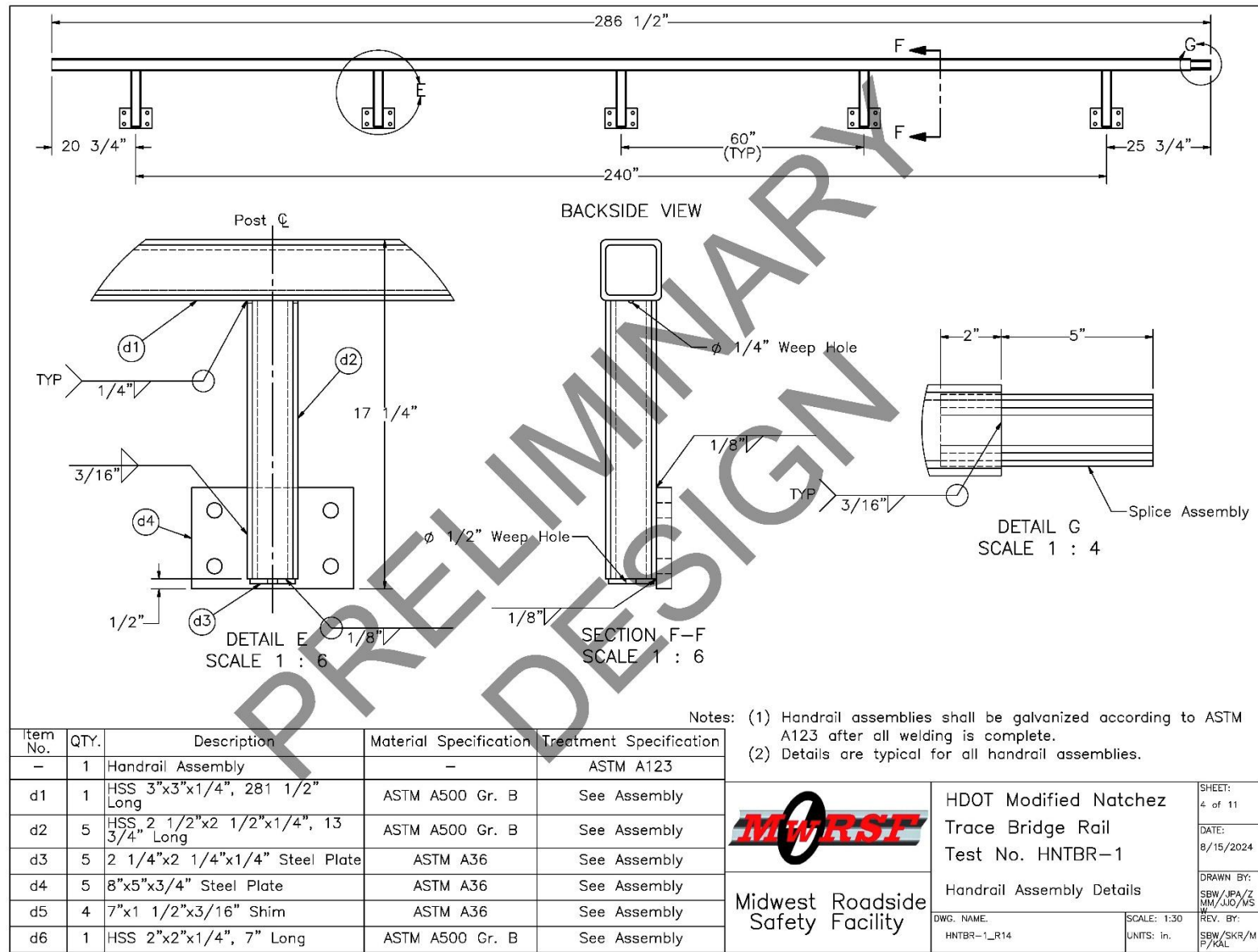


Figure 7. Handrail Detail, Test No. HNTBR-1

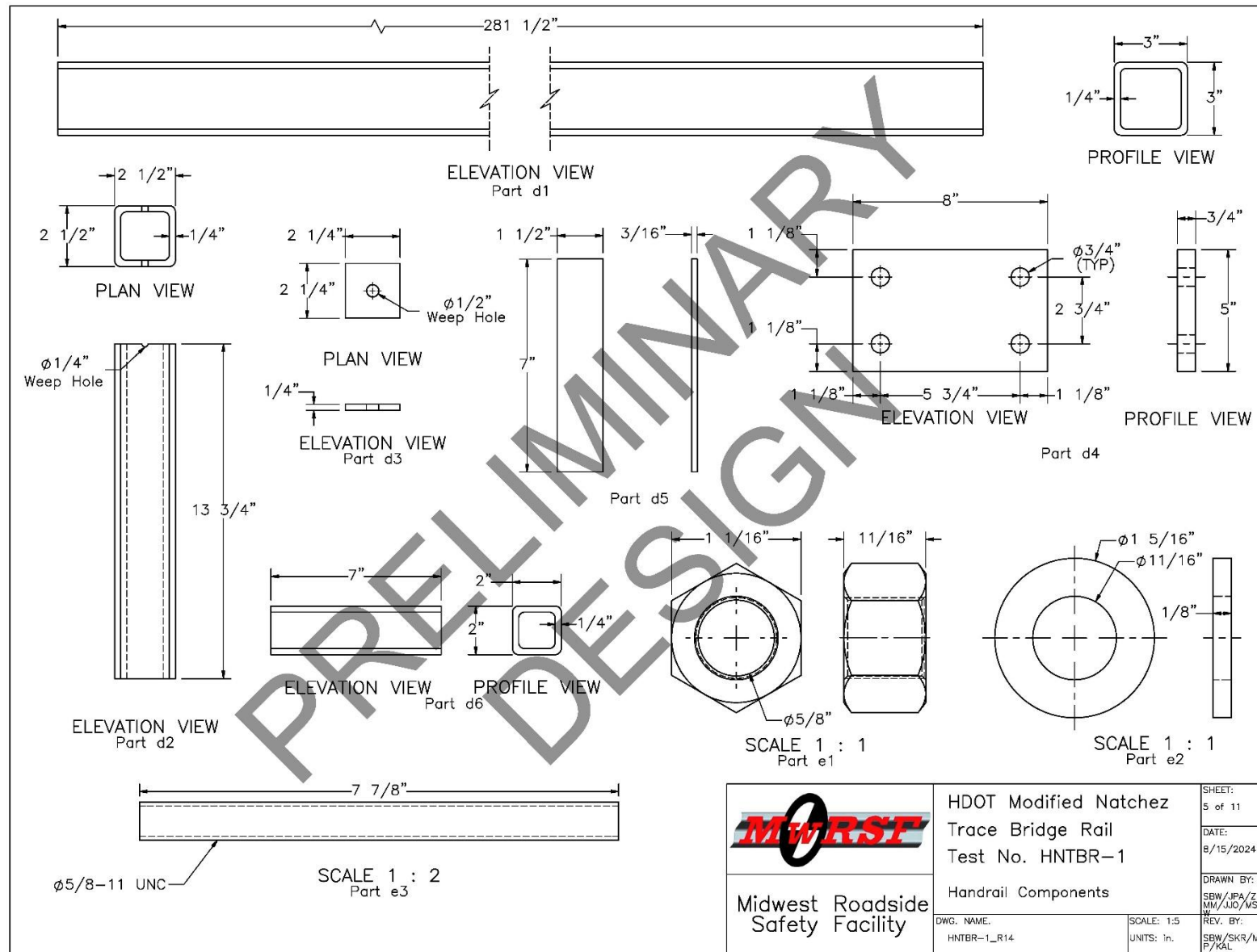


Figure 8. Handrail Assembly Components, Test No. HNTBR-1

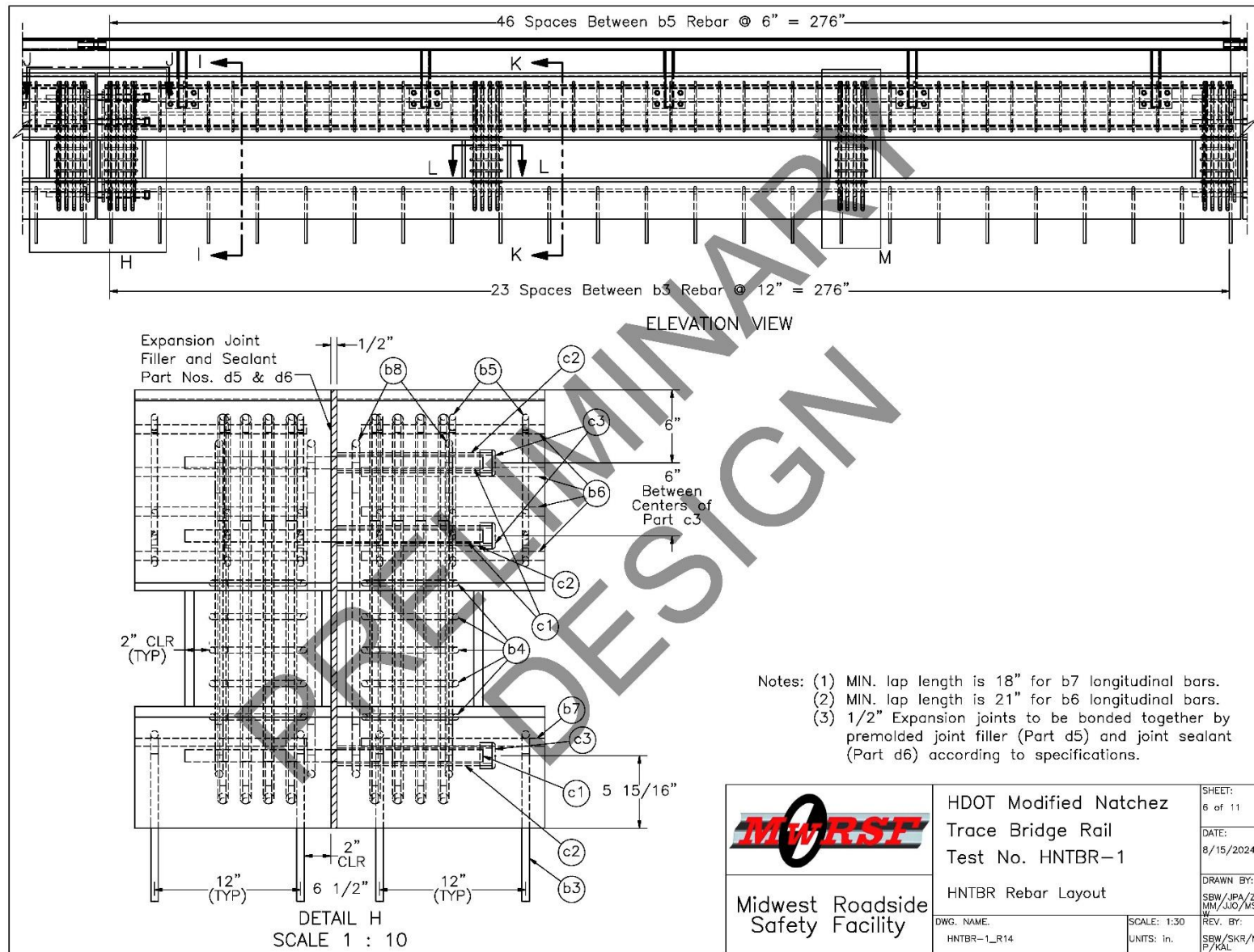


Figure 9. Rails Rebar Detail, Test No. HNTBR-1

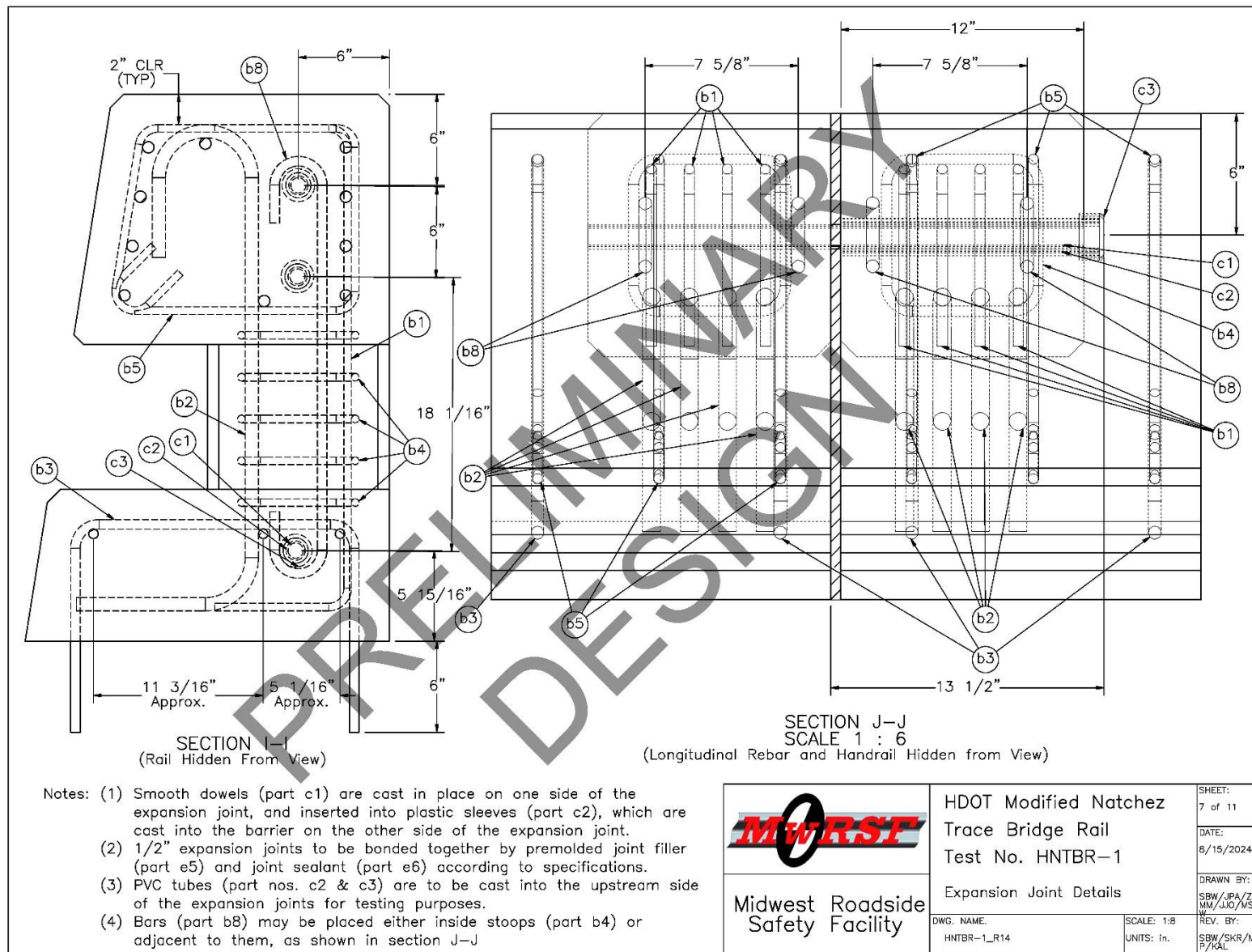


Figure 10. Post-Rail Rebar Arrangement, Test No. HNTBR-1

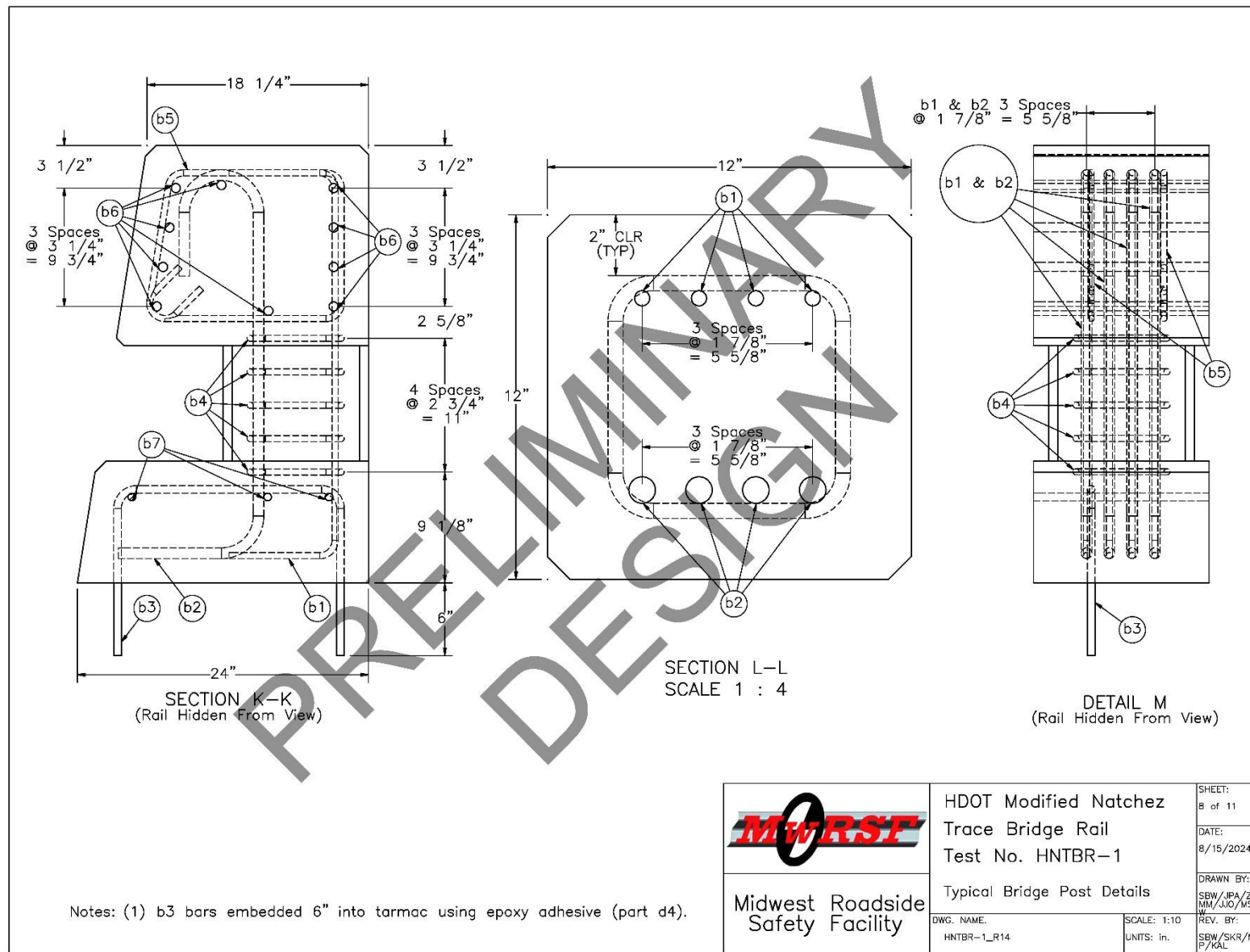


Figure 11. Post-Rail Rebar Arrangement, Test No. HNTBR-1

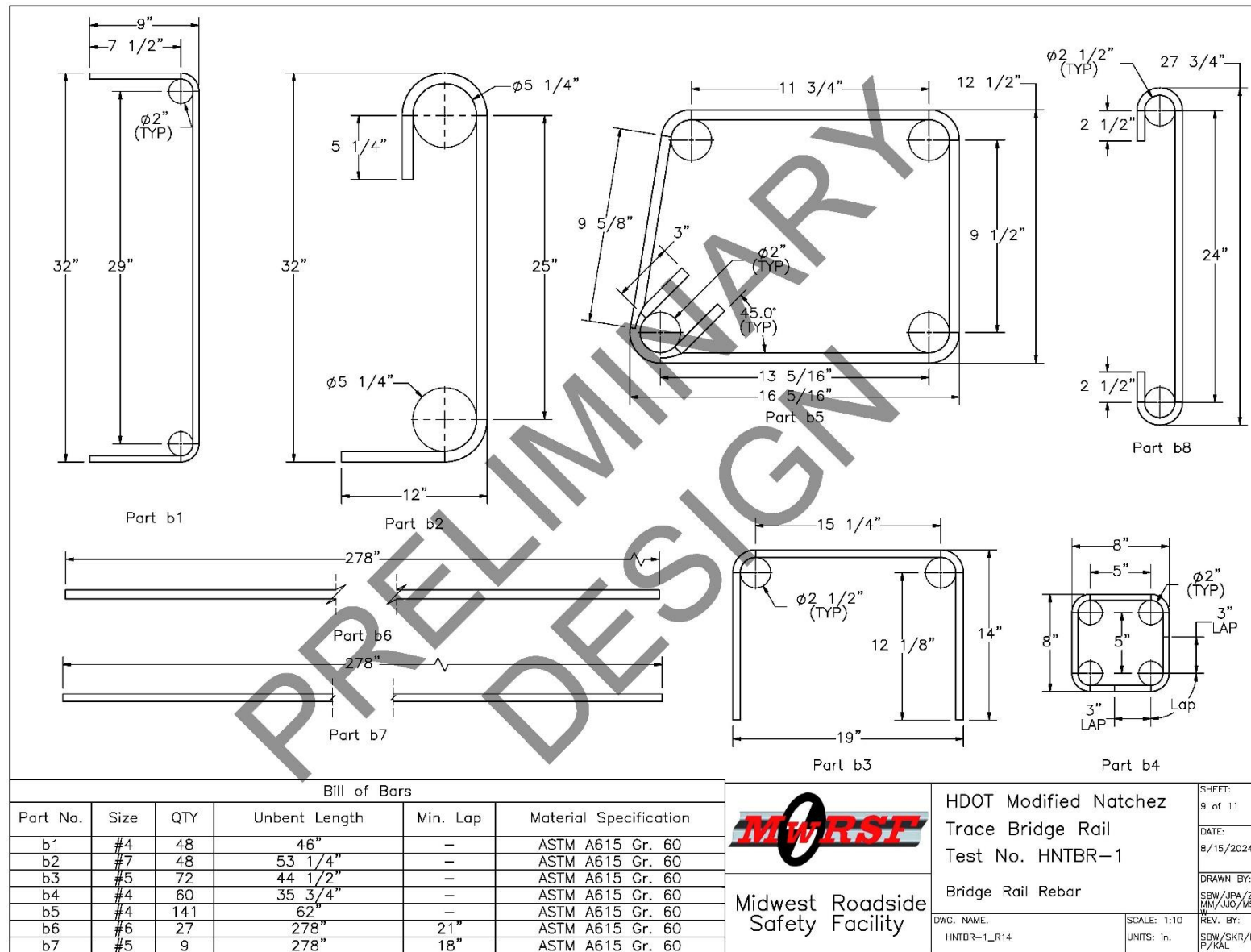


Figure 12. Rebar Details, Test No. HNTBR-1

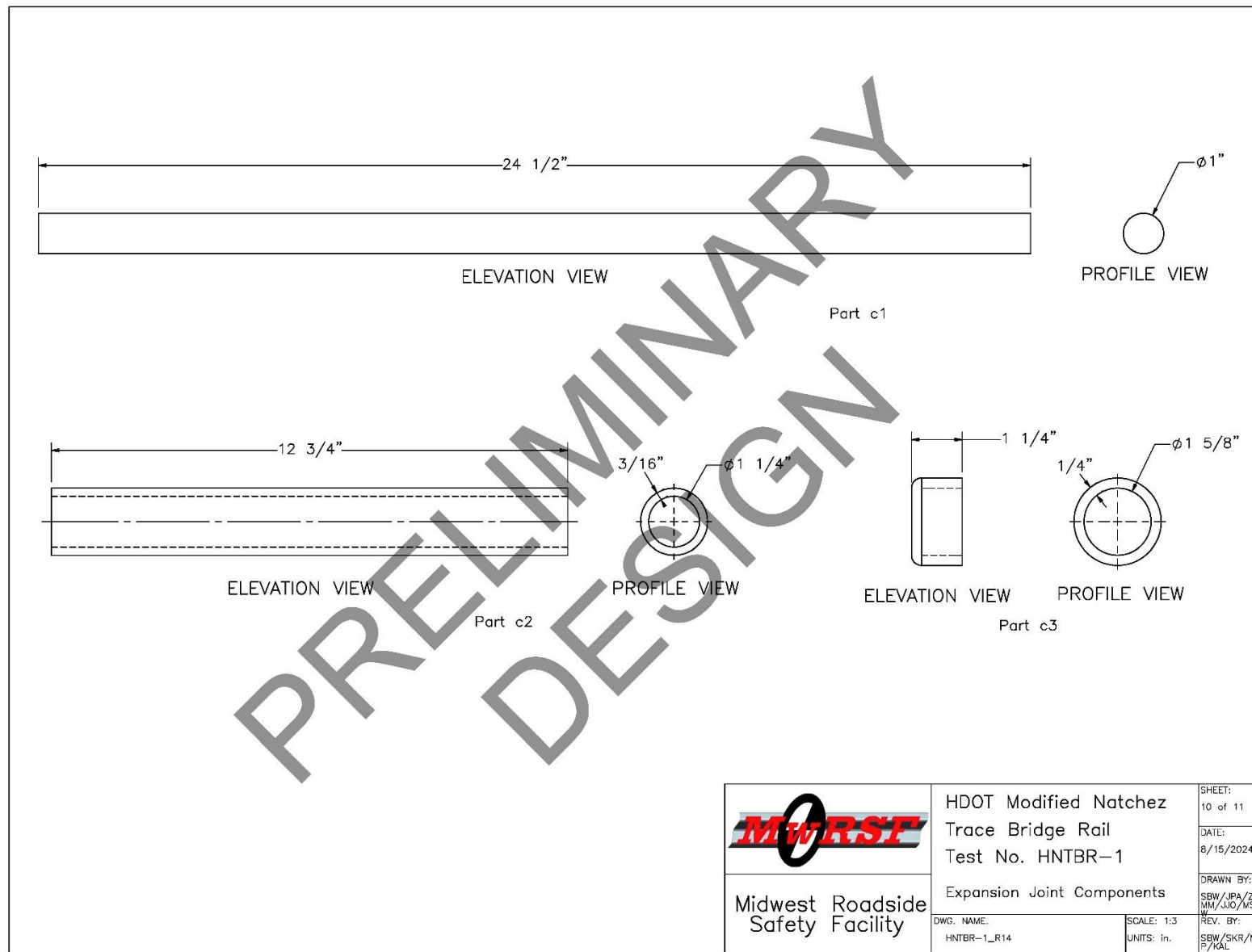



Figure 13. Pipe Details, Test No. HNTBR-1

| Item No. | QTY. | Description | Material Specification | Treatment Specification | Hardware Guide |
|----------|------|---------------------------------------|--|------------------------------------|----------------|
| a1 | 3 | Concrete* | Min. f'c = 4,000 psi | — | — |
| b1 | 48 | #4 Rebar, 46" Total Unbent Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b2 | 48 | #7 Rebar, 53 1/4" Total Unbent Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b3 | 72 | #5 Rebar, 44 1/2" Total Unbent Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b4 | 60 | #4 Rebar, 35 3/4" Total Unbent Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b5 | 141 | #4 Rebar, 62" Total Unbent Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b6 | 30 | #6 Rebar, 278" Total Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b7 | 9 | #5 Rebar, 278" Total Length | ASTM A615 Gr. 60 | **Epoxy-Coated (ASTM A775 or A934) | — |
| b8 | 8 | #5 Rebar, 38 7/8" Total Unbent Length | ASTM A615 Gr. 60 | **Epoxy Coated (ASTM A775 or A934) | — |
| c1 | 6 | #8 Smooth Rebar, 24 1/2" Long | ASTM A615 Gr. 60 | **Epoxy Coated (ASTM A775 or A934) | — |
| c2 | 6 | 1 1/4" Dia. PVC Pipe | Schedule 80 PVC Gr. 12454 | — | — |
| c3 | 6 | 1 1/4" Dia. PVC End Cap | Schedule 80 PVC Gr. 12454 | — | — |
| d1 | 3 | HSS 3"x3"x1/4", 281 1/2" Long | ASTM A500 Gr. B | See Assembly | — |
| d2 | 15 | HSS 2 1/2"x2 1/2"x1/4", 13 3/4" Long | ASTM A500 Gr. B | See Assembly | — |
| d3 | 15 | 2 1/4"x2 1/4"x1/4" Steel Plate | ASTM A36 | See Assembly | — |
| d4 | 15 | 8"x5"x3/4" Steel Plate | ASTM A36 | See Assembly | — |
| d5 | 12 | 7"x1 1/2"x3/16" Shim | ASTM A36 | See Assembly | — |
| d6 | 3 | HSS 2"x2"x1/4", 7" Long | ASTM A500 Gr. B | See Assembly | — |
| e1 | 60 | 5/8"—11 UNC Heavy Hex Nut | ASTM A563—15 Grade DH | ASTM F2329 | FNX18b |
| e2 | 60 | 5/8" Dia. Hardened Washer | ASTM F436 | ASTM F2329 | FWC18b |
| e3 | 60 | 5/8"—11 UNC, 7 7/8" Long Threaded Rod | ASTM F1554—15 Gr. 105 | ASTM F2329 | — |
| e4 | — | Epoxy Adhesive | Hilti HIT RE—500 V3 | — | — |
| e5 | — | Joint Filler | AASHTO M33, M153, or M213 | — | — |
| e6 | — | Expansion Joint Sealant | AASHTO M173, M282, M301, ASTM D3581, or ASTM D5893 | — | — |

* NE Mix 47B15/1PF4000HW was used for testing purposes.
** Rebar does not need to be epoxy-coated for testing purposes.



HDOT Modified Natchez
Trace Bridge Rail
Test No. HNTBR-1

HNTBR BOM

Midwest Roadside
Safety Facility

DWG. NAME:
HNTBR-1_R14

SHEET:
11 of 11

DATE:
8/15/2024

DRAWN BY:
SBW/JPA/Z
MM/JJO/MS

REV. BY:
SBW/SKR/M
P/KAL

SCALE: 1:192
UNITS: In.

Figure 14. Bill of Materials, Test No. HNTBR-1



Figure 15. Test Installation Photographs, Test No. HNTBR-1



Figure 16. Test Installation Photographs, Handrail Assembly, Test No. HNTBR-1

3 TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 Test Requirements

Longitudinal barriers, such as bridge rails, must satisfy impact safety standards to be declared eligible for federal reimbursement by the Federal Highway Administration (FHWA) for use on the National Highway System. For new hardware, these safety standards consist of the guidelines and procedures published in the 2016 edition of MASH. Note that for longitudinal barriers there is no difference between 2009 edition of MASH [6] and the current 2016 edition except that additional occupant compartment deformation measurements, photographs, and documentation are required by the 2016 edition. According to TL-3 of MASH, longitudinal barriers must be subjected to two full-scale vehicle crash tests, as summarized in Table 1. MASH test designation no. 3-11 was conducted on the Hawaii Modified Natchez Trace Bridge Railing and was documented herein.

Table 1. MASH TL-3 Crash Test Conditions for Longitudinal Barriers

| Test Article | Test Designation No. | Test Vehicle | Vehicle Weight lb | Impact Conditions | | Evaluation Criteria ¹ |
|----------------------|----------------------|--------------|-------------------|-------------------|------------|----------------------------------|
| | | | | Speed mph | Angle deg. | |
| Longitudinal Barrier | 3-10 | 1100C | 2,420 | 62 | 25 | A,D,F,H,I |
| | 3-11 | 2270P | 5,000 | 62 | 25 | A,D,F,H,I |

¹ Evaluation criteria explained in Table 2.

Table 2. MASH Evaluation Criteria for Longitudinal Barrier

| | | | | |
|---------------------|----|---|-----------|-----------|
| Structural Adequacy | A. | Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable. | | |
| Occupant Risk | D. | Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH 2016. | | |
| | F. | The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees. | | |
| | H. | Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits: | | |
| | | Occupant Impact Velocity Limits | | |
| | | Component | Preferred | Maximum |
| | | Longitudinal and Lateral | 30 ft/s | 40 ft/s |
| | I. | The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits: | | |
| | | Occupant Ridedown Acceleration Limits | | |
| | | Component | Preferred | Maximum |
| | | Longitudinal and Lateral | 15.0 g's | 20.49 g's |

3.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three factors: (1) structural adequacy, (2) occupant risk, and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the bridge railing to contain and redirect impacting vehicles. In addition, controlled lateral deflection of the test article is acceptable. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are summarized in Table 2 and defined in greater detail in MASH 2016. The full-scale vehicle crash test was conducted and reported in accordance with the procedures provided in MASH.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported. Additional discussion on PHD, THIV and ASI is provided in MASH.

4 TEST CONDITIONS

4.1 Test Facility

The Outdoor Test Site is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles northwest of the University of Nebraska-Lincoln.

4.2 Vehicle Tow and Guidance System

A reverse-cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle was one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [7] was used to steer the test vehicle. A guide flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the barrier system. The $\frac{3}{8}$ -in. diameter guide cable was tensioned to approximately 3,500 lb and supported both laterally and vertically every 100 ft by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

4.3 Test Vehicle

In test no. HNTBR-1, a 2017 Dodge Ram 1500 crew cab pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 5,264 lb, 5,032 lb, and 5,192 lb, respectively. The test vehicle is shown in Figures 17 and 18, and vehicle dimensions are shown in Figure 19. Note, the impact side of the vehicle, or the passenger's side, is referred to as the vehicle's right side throughout this report. The non-impact side, or driver's side, is referred to as the vehicle's left side.

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The Suspension Method [8] was used to determine the vertical component of the c.g. for the 2270P vehicle. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The final c.g. location is shown in Figure 19. Ballast information and data used to calculate the location of the c.g. are shown in Appendix C.

Square, black-and-white checkered targets were placed on the vehicle for reference, shown in Figure 20, to serve as a reference in the high-speed digital video and aid in the video analysis. Round, checkered targets were placed at the c.g. on the left-side door, the right-side door, and the roof of the vehicle.

The front wheels of the test vehicle were aligned to vehicle standards except the toe-in value was adjusted to zero such that the vehicle would track properly along the guide cable. A 5B flash bulb was mounted under the vehicle's right-side windshield wiper and was fired by a pressure

tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial impact with the test article to create a visual indicator of the precise time of impact on the high-speed digital videos. A radio-controlled brake system was installed in the test vehicle so the vehicle could be brought safely to a stop after the test.



Figure 17. Test Vehicle, Test No. HNTBR-1

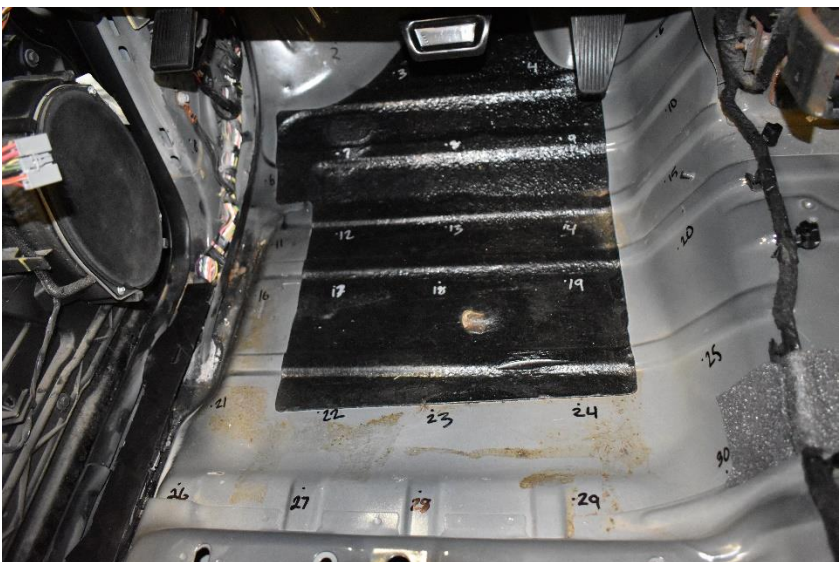


Figure 18. Vehicle's Interior Floorboards and Undercarriage, Test No. HNTBR-1

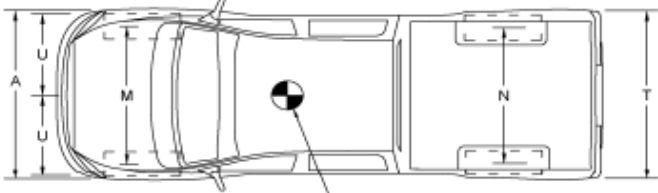
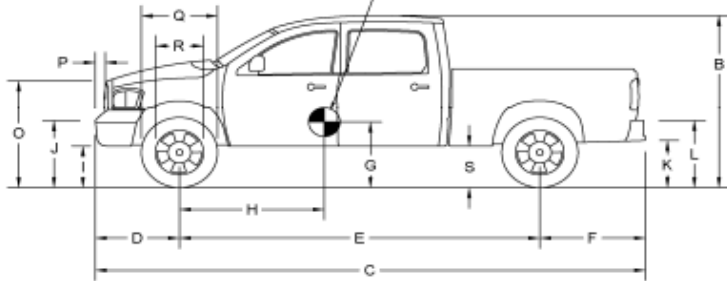
| | | | |
|---|--|--|--|
| Test Name: <u>HNTBR-1</u> | | VIN No: <u>1C6RR6LTXHS514323</u> | |
| Model Year: <u>2017</u> | | Make: <u>Dodge</u> | |
| Tire Size: <u>275/60R20</u> | | Tire Inflation Pressure: <u>39 psi</u> | |
| | | Odometer: <u>148148</u> | |
| Vehicle Geometry - in. (mm) Target Ranges listed below | | | |
|  | | A: 78 1981 1/5 78±2 (1950±50) | |
|  | | B: 75 1/2 1917 7/10 237±13 (6020±325) | |
| | | C: 229 5816 3/5 148±12 (3760±300) | |
| | | D: 39 1/2 1003 3/10 39±3 (1000±75) | |
| | | E: 140 3/4 3575 1/20 148±12 (3760±300) | |
| | | F: 48 3/4 1238 1/4 | |
| | | G: 28 15/16 735 1/80 min: 28 (710) | |
| | | H: 59 7/16 1509 57/80 63±4 (1575±100) | |
| | | I: 13 330 1/5 | |
| | | J: 26 660 2/5 | |
| | | K: 22 558 4/5 | |
| | | L: 30 3/4 781 1/20 | |
| | | M: 68 5/8 1743 3/40 67±1.5 (1700±38) | |
| | | N: 68 1/2 1739 9/10 67±1.5 (1700±38) | |
| | | O: 45 1/4 1149 7/20 43±4 (1100±75) | |
| | | P: 4 1/4 107 19/20 | |
| | | Q: 32 1/4 819 3/20 | |
| | | R: 21 3/8 542 37/40 | |
| | | S: 16 1/4 412 3/4 | |
| | | T: 77 1/4 1962 3/20 | |
| Mass Distribution - lb (kg) | | U (impact width): 37 5/8 955 27/40 | |
| Gross Static LF <u>1504 (682)</u> RF <u>1500 (680)</u> | | Wheel Center Height (Front): <u>15 1/4 387 7/20</u> | |
| LR <u>1073 (487)</u> RR <u>1115 (506)</u> | | Wheel Center Height (Rear): <u>15 1/2 393 7/10</u> | |
| Weights | | Wheel Well Clearance (Front): <u>35 3/4 908 1/20</u> | |
| lb (kg) | | Wheel Well Clearance (Rear): <u>39 990 3/5</u> | |
| Curb | | Bottom Frame Height (Front): <u>19 1/8 485 31/40</u> | |
| Test Inertial | | Bottom Frame Height (Rear): <u>26 5/8 676 11/40</u> | |
| Gross Static | | Engine Type: <u>Gasoline</u> | |
| W-front <u>3008 (1364)</u> <u>2906 (1318)</u> <u>3004 (1363)</u> | | Engine Size: <u>5.7L V8</u> | |
| W-rear <u>2256 (1023)</u> <u>2126 (964)</u> <u>2188 (992)</u> | | Transmission Type: <u>Automatic</u> | |
| W-total <u>5264 (2388)</u> <u>5032 (2282)</u> <u>5192 (2355)</u> | | Drive Type: <u>RWD</u> | |
| 5000±110 (2270±50) | | Cab Style: <u>Crew Cab</u> | |
| 5165±110 (2343±50) | | Bed Length: <u>67"</u> | |
| GVWR Ratings - lb | | Surrogate Occupant Data | |
| Front <u>3700</u> | | Type: <u>Hybrid II</u> | |
| Rear <u>3900</u> | | Mass: <u>160 lb</u> | |
| Total <u>6900</u> | | Seat Position: <u>Passenger</u> | |
| Note any damage prior to test: <u>Crack in windshield, Minor hail, Small dents in between driver side windows</u> | | | |

Figure 19. Vehicle Dimensions, Test No. HNTBR-1

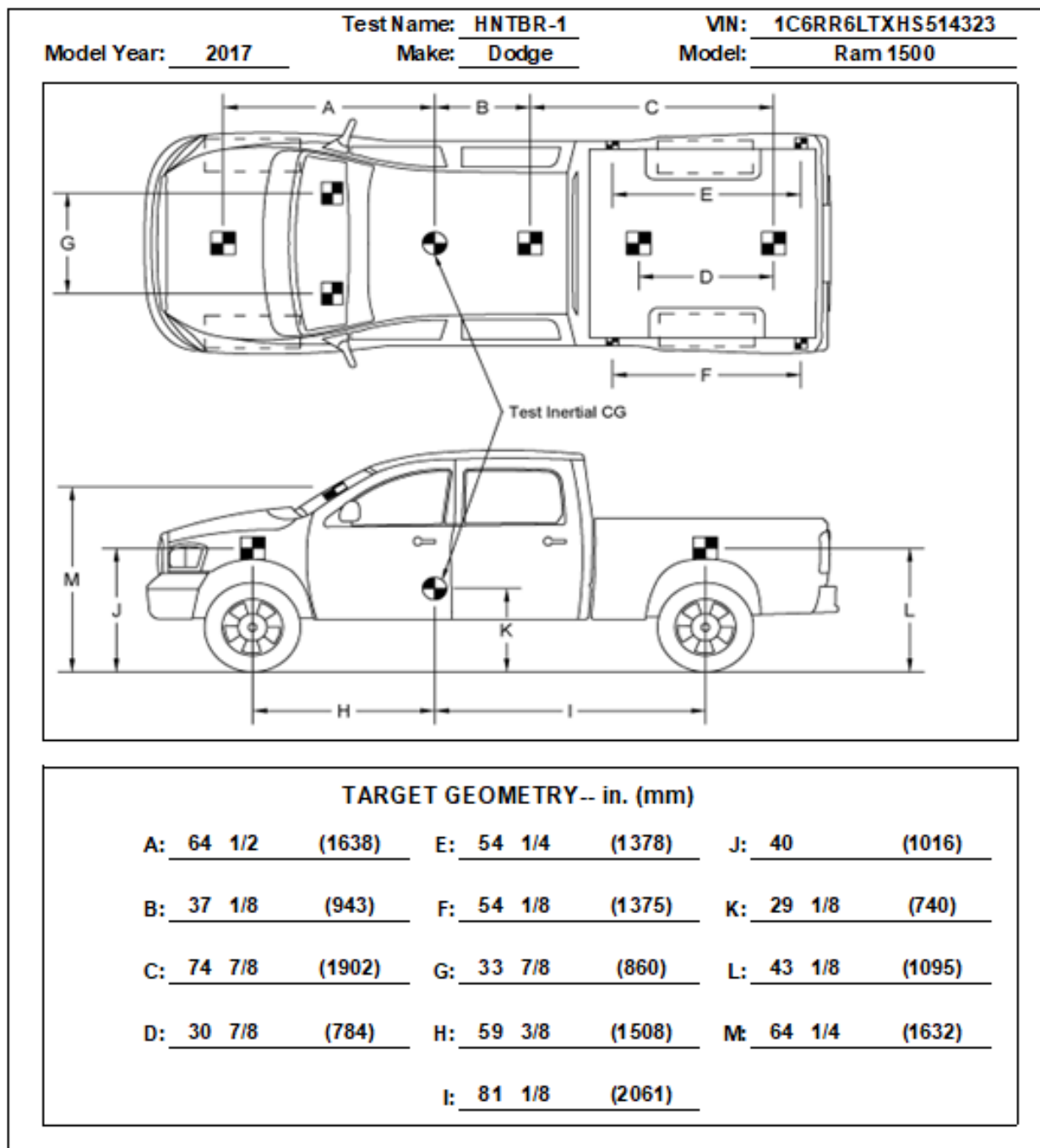


Figure 20. Target Geometry, Test No. HNTBR-1

4.4 Simulated Occupant

For test no. HNTBR-1, a Hybrid II 50th-Percentile Adult Male Dummy equipped with footwear was placed in the right-front seat of the test vehicle with the seat belt fastened. The simulated occupant had a final weight of 160 lb. As recommended by MASH, the simulated occupant weight was not included in calculating the c.g. location.

4.5 Data Acquisition Systems

4.5.1 Accelerometers and Rate Transducers

The accelerometer and rate transducer systems used in the full-scale crash testing were the SLICE-2 and TDAS units described below. Units were positioned near the c.g. of the test vehicle and the SLICE-2 unit was designated as primary. Data obtained in dynamic testing was filtered using the SAE Class 60 and the SAE Class 180 Butterworth filter conforming to the SAEJ211/1 specifications [9].

The SLICE-2 unit was a modular data acquisition system manufactured by Diversified Technical Systems, Inc. of Seal Beach, California. Triaxial acceleration and angular rate sensor modules were mounted inside the bodies of custom-built SLICE 6DX event data recorders equipped with 7GB of non-volatile flash memory and recorded data at 10,000 Hz to the onboard microprocessor. The accelerometers had a range of $\pm 500g$'s in each of three directions (longitudinal, lateral, and vertical) and a 1,650 Hz (CFC 1000) anti-aliasing filter. The SLICE MICRO Triax ARS had a range of 1,500 degrees/sec in each of three directions (roll, pitch, and yaw). The raw angular rate measurements were downloaded, converted to the proper Euler angles for analysis, and plotted. The "SLICEWare" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot both the accelerometer and angular rate sensor data.

The TDAS unit was a data acquisition system developed and manufactured by Diversified Technical Systems, Inc. of Seal Beach, California. Sensor data was collected using a DTS Sensor Input Module (SIM), Model TDAS3-SIM-16M mounted on the TDAS3-R4 module rack. The SIM was configured with 16 MB SRAM and eight sensor input channels with 250kB SRAM/channel. The module rack was configured with isolated power/event/communications, 10BaseT Ethernet and RS232 communication, and an internal backup battery. Both the SIM and module rack were crashworthy. The unit was configured to record one set of triaxial acceleration data and one set of triaxial angular rate data. The two-arm piezoresistive accelerometer module manufactured by Endevco of San Juan Capistrano, California measured longitudinal, lateral, and vertical accelerations independently at a sample rate of 10,000 Hz. The ARS-1500 angular rate sensors with a range of 1,500 degrees/sec measured the rates of rotation of the test vehicle in three directions (roll, pitch, and yaw) and recorded data at 10,000 Hz to the DTS SIM. The raw data measurements were downloaded, converted to the proper Euler angles for analysis, and plotted. The "DTS TDAS Control" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot both the accelerometer and angular rate sensor data.

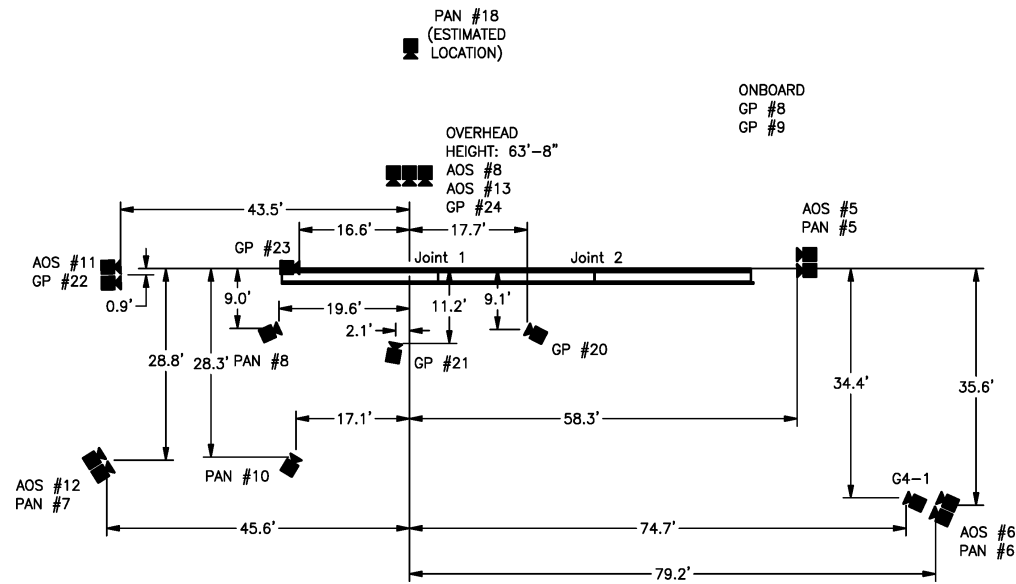
4.5.2 Retroreflective Optic Speed Trap

A retroreflective optic speed trap was used to determine the speed of the test vehicle before impact. Five retroreflective targets, spaced at approximately 18-in. intervals, were applied to the side of the vehicle. When the emitted beam of light was reflected by the targets and returned to the Emitter/Receiver, a signal was sent to the data acquisition computer, recording at 10,000 Hz, as well as the external LED box activating the LED flashes. The speed was then calculated using the spacing between the retroreflective targets and the time between the signals. LED lights and high-speed digital video analysis are used as a backup if vehicle speeds cannot be determined from electronic data.

4.5.3 Digital Photography

Six AOS high-speed digital video cameras, eight GoPro digital video cameras, five Panasonic digital video cameras, and one Ubiquiti G4 Plus camera were utilized to film test no. HNTBR-1. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 21.

The high-speed videos were analyzed using TEMA Motion and Redlake MotionScope software programs. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed videos. A digital still camera was also used to document pre- and post-test conditions for all tests.



| No. | Type | Operating Speed (frames/sec) | Lens | Lens Setting |
|--------|--------------------|---------------------------------|---------------------|--------------|
| AOS-5 | AOS X-PRI | 500 | 100 mm Fixed | - |
| AOS-6 | AOS X-PRI | 500 | KOWA 25 mm Fixed | - |
| AOS-8 | AOS S-VIT 1531 | 500 | KOWA 12 mm Fixed | - |
| AOS-11 | AOS J-PRI | 500 | Sigma 17-50 | 35 |
| AOS-12 | AOS J-PRI | 500 | 2Sigma 24-135 | 24 |
| AOS-13 | AOS J-PRI | 500 | Rokinon 12 mm Fixed | - |
| GP-8 | GoPro Hero 4 | 120 | | |
| GP-9 | GoPro Hero 4 | 120 | | |
| GP-18 | GoPro Hero 6 | 240 | | |
| GP-20 | GoPro Hero 6 | 240 | | |
| GP-21 | GoPro Hero 6 | 240 | | |
| GP-22 | GoPro Hero 7 | 120 | | |
| GP-23 | GoPro Hero 7 | 240 | | |
| GP-24 | GoPro Hero 7 | 240 | | |
| PAN-5 | Panasonic HC-VX981 | 120 | | |
| PAN-6 | Panasonic HC-VX981 | 120 | | |
| PAN-7 | Panasonic HC-VX981 | 120 | | |
| PAN-8 | Panasonic HC-VX981 | 120 | | |
| PAN-10 | Panasonic HC-VX981 | 120 | | |
| G4-1 | Ubiquiti G4 Plus | 20 | | |

Figure 21. Camera Locations, Speeds, and Lens Settings, Test No. HNTBR-1

5 FULL-SCALE CRASH TEST NO. HNTBR-1

5.1 Weather Conditions

Test no. HNTBR-1 was conducted on July 17, 2023, at approximately 1:30 p.m. The weather conditions as reported by the National Oceanic and Atmospheric Administration (station 14939/KLNK) are shown in Table 3.

Table 3. Weather Conditions, Test No. HNTBR-1

| | |
|------------------------------|---------------------|
| Temperature | 78°F |
| Humidity | 54% |
| Wind Speed | 10 mph |
| Wind Direction | 80° from True North |
| Sky Conditions | Partly Cloudy |
| Visibility | 10 |
| Pavement Surface | Dry |
| Previous 3-Day Precipitation | 0.79 in. |
| Previous 7-Day Precipitation | 1.07 in. |

5.2 Test Description

Initial vehicle impact was to occur 51½ in. upstream from the centerline of the expansion joint between post nos. 4 and 5, as shown in Figure 22, which was selected using MASH Table 2-7 to maximize loading to the railing joint. The 5,032-lb crew cab pickup truck impacted the concrete bridge rail at a speed of 62.3 mph and at an angle of 25.0 degrees. The actual point of impact was 56.5 in. upstream from the centerline of the expansion joint. The vehicle was contained and redirected and remained stable throughout the impact event. After exiting the bridge rail, the brakes were applied remotely and the vehicle came to rest 175.6 ft downstream from impact and 47.1 ft behind the system.

A detailed description of the sequential impact events is contained in Table 4. Sequential photographs are shown in Figures 23 and 24. Documentary photographs of the crash test are shown in Figure 25. The vehicle trajectory and final position are shown in Figure 26.

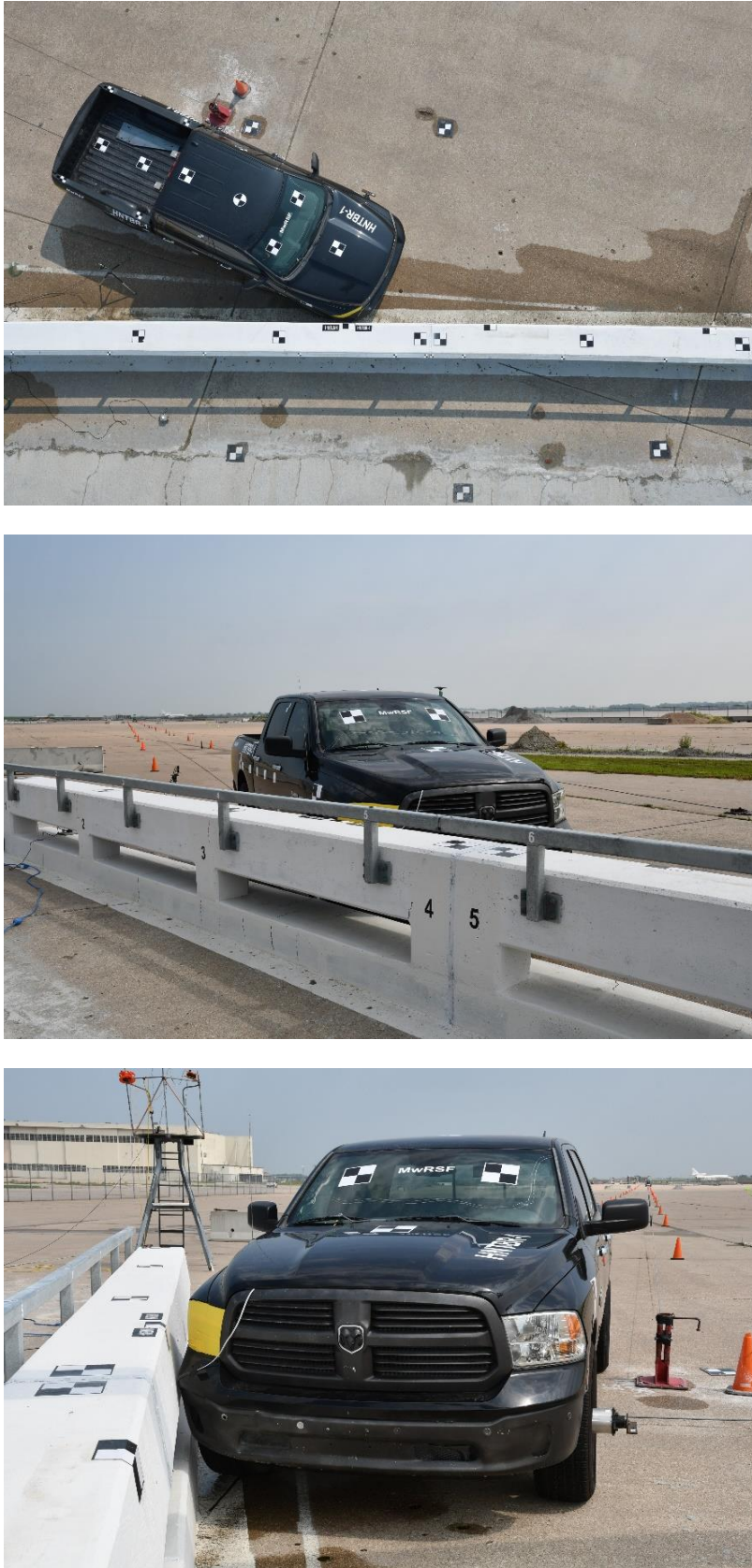


Figure 22. Target Impact Location, Test No. HNTBR-1

Table 4. Sequential Description of Impact Events, Test No. HNTBR-1

| Time (sec) | Event |
|---------------|--|
| 0.000 | Vehicle's front bumper and right-front tire contacted concrete bridge rail between post nos. 3 and 4. Concrete spalled. |
| 0.008 | Vehicle's right headlight crushed and disengaged, and fender deformed and dented. Vehicle's right-front tire deflated. |
| 0.020 | Vehicle's grille contacted railing and deformed. |
| 0.030 | Vehicle yawed away from and rolled toward system. Vehicle's right-front door contacted concrete bridge segment and deformed. |
| 0.044 | Vehicle's hood bent. |
| 0.060 | Vehicle's left headlight and right-front window glass disengaged. |
| 0.070 | Vehicle's grille disengaged. Vehicle's windshield cracked throughout. |
| 0.114 | Vehicle's left-front tire became airborne. |
| 0.140 | Vehicle's left-rear tire became airborne. |
| 0.196 | Vehicle's right-rear door contacted the railing. |
| 0.246 | Vehicle was parallel to system at a speed of 47.8 mph. |
| 0.268 | Vehicle's right quarter panel contacted railing and deformed. Vehicle pitched downward. |
| 0.282 | Vehicle's rear bumper contacted railing and deformed. |
| 0.476 | Vehicle rolled away from system. |
| 0.512 | Vehicle exited system at a speed of 44.0 mph and an angle of 10 degrees. Vehicle's front bumper contacted ground. |
| 0.618 | Vehicle's left-front tire contacted ground. |
| 0.662 | Vehicle's right-front tire detached. |
| 0.796 | Vehicle steered toward system. |
| 0.860 | Vehicle's left-rear tire contacted ground. |
| 4.750 | Vehicle came to rest. |



0.000 sec



0.200 sec



0.400 sec



0.600 sec



0.800 sec



1.000 sec



0.000 sec



0.200 sec



0.400 sec



0.600 sec



0.800 sec



1.000 sec

Figure 23. Sequential Photographs, Test No. HNTBR-1



0.000 sec



0.100 sec



0.200 sec



0.300 sec



0.400 sec



0.500 sec



0.000 sec



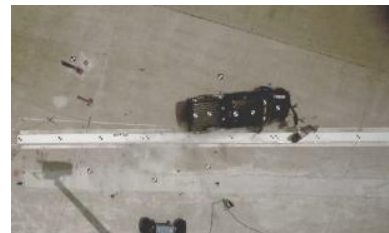
0.100 sec



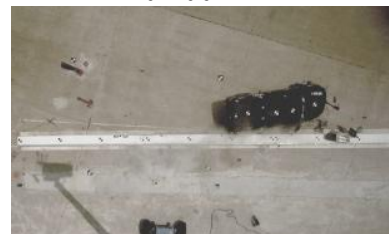
0.200 sec



0.300 sec



0.400 sec



0.500 sec

Figure 24. Sequential Photographs, Test No. HNTBR-1



Figure 25. Documentary Photographs, Test No. HNTBR-1

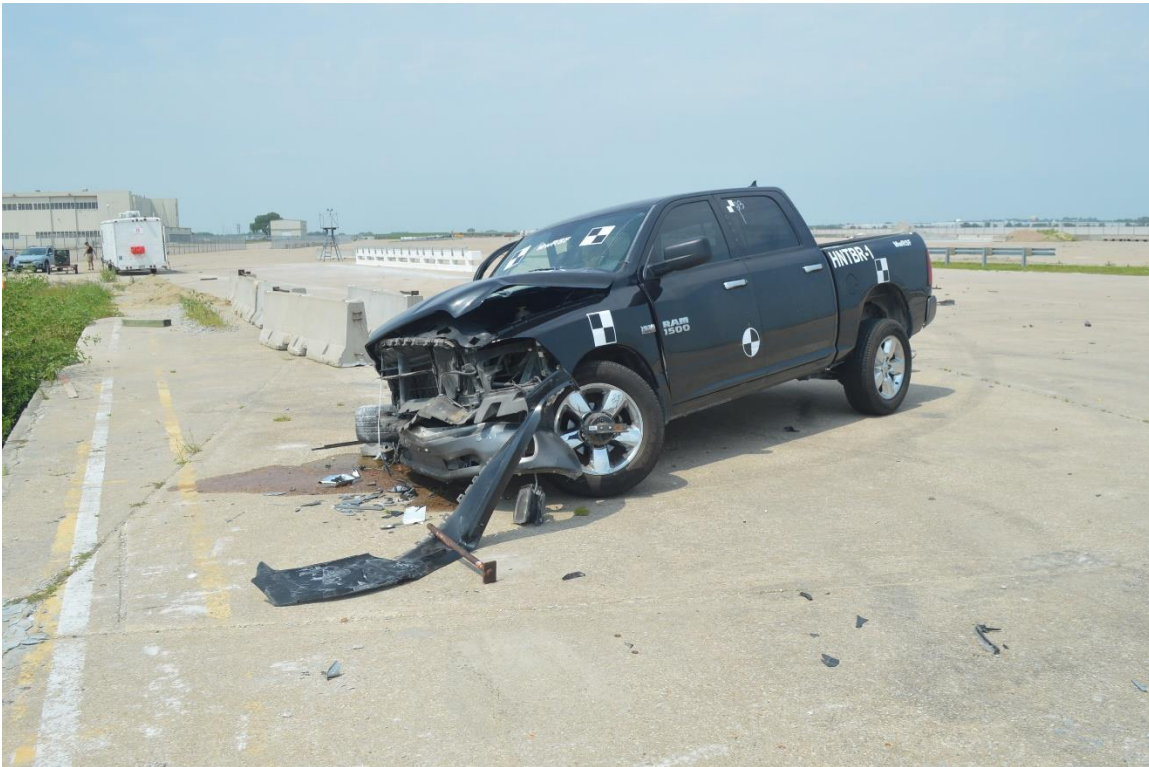


Figure 26. Vehicle Final Position and Trajectory Marks, Test No. HNTBR-1

5.3 Barrier Damage

Damage to the barrier was minimal, as shown in Figures 27 through 29. Barrier damage consisted of concrete spalling, contact marks on the front face of the concrete segments, and concrete cracking. The length of vehicle contact along the upper rail was 19 ft – 8 in., beginning approximately 11 in. upstream from the impact point and continuing downstream. The length of vehicle contact along the lower curb was 20 ft – 10 in., beginning 18 in. upstream from the impact point and continuing downstream.

Concrete spalling and cracking occurred during the impact event, including a 23-in. long by 8-in. wide spall located along the bottom edge of the upper concrete rail. Another significant spalled section was located on the top edge of the curb below the spalled section on the upper rail. Several other small gouges and cracks were observed on curb and upper railing around these spalled sections near initial impact. The curb was cracked on the top face adjacent to post no. 4, and a crack was found along the base of post no. 4.



Figure 27. System Damage, Test No. HNTBR-1



Figure 28. Curb and Concrete Rail Damage, Test No. HNTBR-1



Figure 29. Curb and Concrete Rail Damage, Test No. HNTBR-1

The maximum lateral dynamic barrier deflection was 1.0 in. at railing post no. 4, which was just upstream from the impacted expansion joint, as determined from high-speed digital video analysis. The maximum lateral permanent set of the barrier system was 0.7 in. measured at the handrail just downstream from the expansion joint, as measured in the field. The working width of the system was found to be 28.5 in., also determined from high-speed digital video analysis. A schematic of the permanent set deflection, dynamic deflection, and working width is shown in Figure 30.

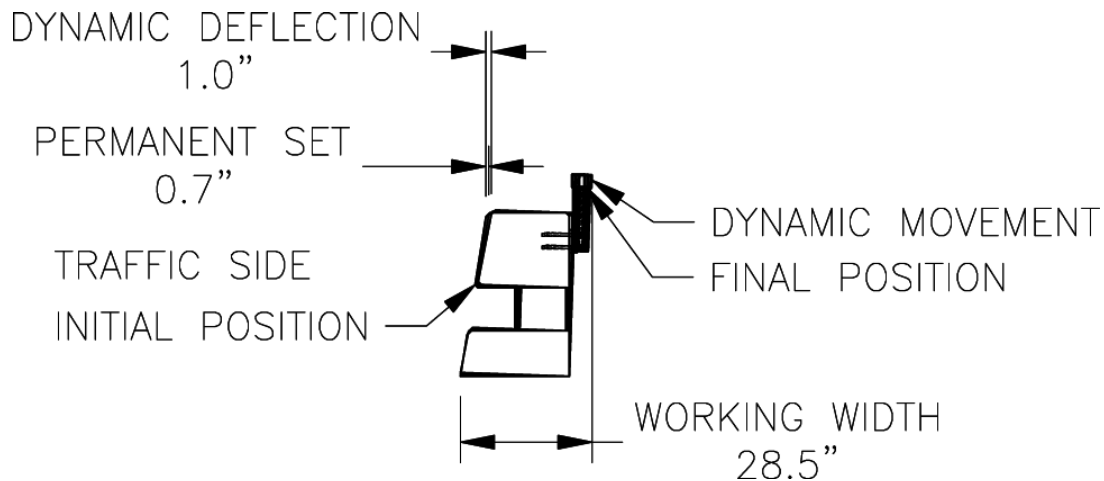


Figure 30. Permanent Set, Dynamic Deflection, and Working Width, Test No. HNTBR-1

5.4 Vehicle Damage

Damage to the vehicle was severe, as shown in Figures 31 through 34. The impact side of the vehicle, or the passenger's side, is referred to as the vehicle's right side. The non-impact side, or driver's side, is referred to as the vehicle's left side. Majority of the damage was concentrated on the right-front corner and right side of the vehicle where the impact occurred. The right side of the front bumper was dented and scraped, and the left side of the front bumper was bent. The headlights and grille were disengaged from the vehicle. The right side of the hood was dented and scraped. Scrapes and dents were observed throughout the right-side of the vehicle. The right fender and right-front door were crushed inward. The windshield was cracked, concentrated on the right side, and the right-front side window was shattered and disengaged.

The right-front suspension spring was disengaged, and the right-front shock was bent. The right-side end link was bent and detached, and the front and rear sway bar shifted. The right ball joint, right steering knuckle, and right lower control arm disengaged, and the right upper control arm was bent. The right outer tie rod disconnected from the control arm. The passenger side frame rail was bent and buckled. The right-front engine cross member was scraped and bent. The right side of the frame horn bent inward severely. The cab mounts were bent and shifted, and there were large deformations to the toe pan and floorboard on the right side of the vehicle.

The maximum occupant compartment intrusions are listed in Table 5, along with the intrusion limits established in MASH for various areas of the occupant compartment. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in

Appendix D. MASH defines intrusion or deformation as the occupant compartment being deformed and reduced in size with no observed penetration. The vehicle's toe pan was deformed 12.7 in., which exceeded the 9-in. MASH intrusion limit. Outward deformations, which are denoted as negative numbers in Appendix D, are not considered crush toward the occupant, and are not evaluated by MASH criteria.



Figure 31. Vehicle Damage, Test No. HNTBR-1

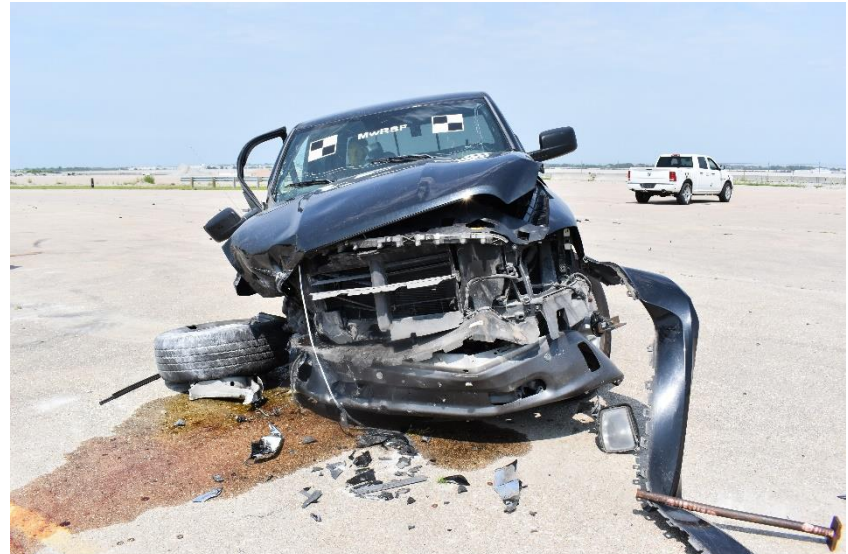


Figure 32. Vehicle Damage, Test No. HNTBR-1

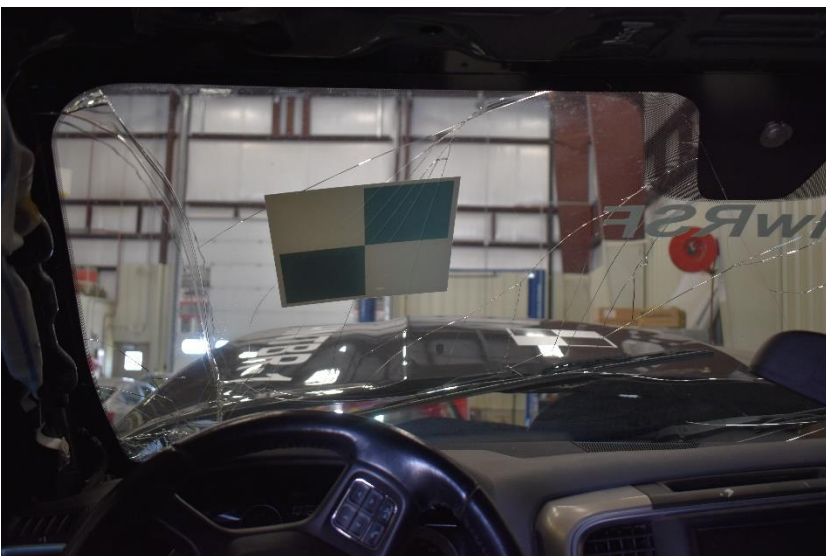


Figure 33. Vehicle's Interior Compartment Damage, Test No. HNTBR-1

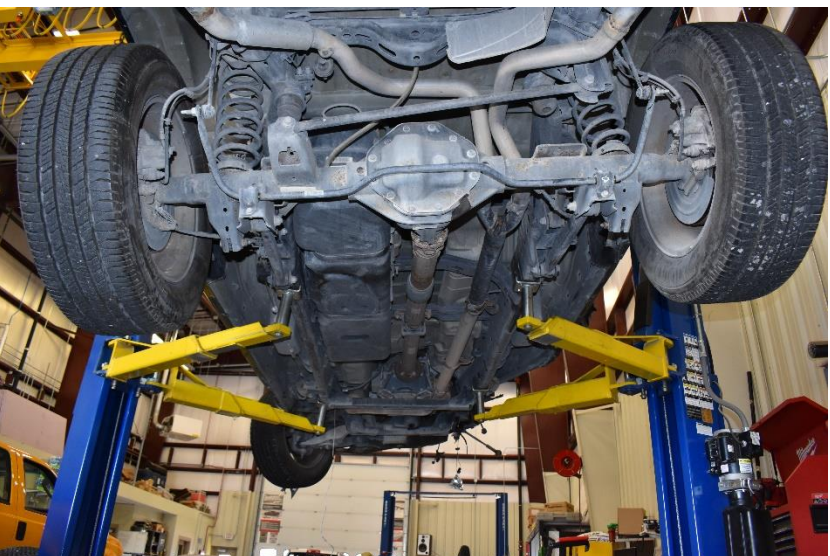


Figure 34. Vehicle's Undercarriage Damage, Test No. HNTBR-1

Table 5. Maximum Occupant Compartment Intrusion by Location, Test No. HNTBR-1

| Location | Maximum Intrusion in. | MASH 2016 Allowable Intrusion in. |
|---|--|---|
| Wheel Well & Toe Pan | 12.7 | ≤ 9 |
| Floor Pan & Transmission Tunnel | 5.4 | ≤ 12 |
| A-Pillar | 2.0 | ≤ 5 |
| A-Pillar (Lateral) | 0.0* | ≤ 3 |
| B-Pillar | 0.5 | ≤ 5 |
| B-Pillar (Lateral) | 0.0* | ≤ 3 |
| Side Front Panel (in Front of A-Pillar) | 11.9 | ≤ 12 |
| Side Door (Above Seat) | 0.0* | ≤ 9 |
| Side Door (Below Seat) | 0.0* | ≤ 12 |
| Roof | 0.0* | ≤ 4 |
| Windshield | 0.0 | ≤ 3 |
| Side Window | Shattered/disengaged due to contact with simulated occupant's head | No shattering resulting from contact with structural member of test article |
| Dash | 5.2 | N/A |

N/A – No MASH 2016 criteria exist for this location.

*Negative value reported as 0.0. See Appendix D for further information.

5.5 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec average occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions, as determined from the accelerometer data, are shown in Table 6. Note that the OIVs and ORAs were within suggested limits, as provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 6. The recorded data from the accelerometers and the rate transducers is shown graphically in Appendix E.

Table 6. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. HNTBR-1

| Evaluation Criteria | | Transducer | | MASH 2016 Limits |
|--|--------------|------------|----------------------|------------------------|
| | | TDAS | SLICE-2 (primary) | |
| OIV ft/s | Longitudinal | -24.4 | -24.5 | ±40 |
| | Lateral | -22.1 | -23.1 | ±40 |
| ORA g's | Longitudinal | -4.6 | -5.6 | ±20.49 |
| | Lateral | -8.9 | -7.6 | ±20.49 |
| Maximum Angular Displacement deg. | Roll | 20.62 | 18.85 | ±75 |
| | Pitch | -7.86 | -7.23 | ±75 |
| | Yaw | -38.95 | -39.34 | not required |
| THIV – ft/s | | 31.90 | 32.35 | not required |
| PHD – g's | | 9.29 | 10.41 | not required |
| ASI | | 1.27 | 1.35 | not required |

5.6 Discussion

The analysis of the test results for test no. HNTBR-1 showed that the system contained and redirected the 2270P vehicle with minimal lateral displacements of the barrier. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix E, were deemed acceptable because they did not adversely influence occupant risk nor cause rollover. After impact, the vehicle exited the barrier at an angle of 10.0 degrees, and its trajectory did not violate the bounds of the exit box. However, deformations of, or intrusions into, the occupant compartment could have caused serious injury. The floor pan deformation of 12.7 in. exceeded the MASH limit of 9 in. Therefore, test no. HNTBR-1 was determined to be unsatisfactory according to the safety performance criteria for MASH test designation no. 3-11. A summary of the test results and sequential photographs are shown in Figure 35.

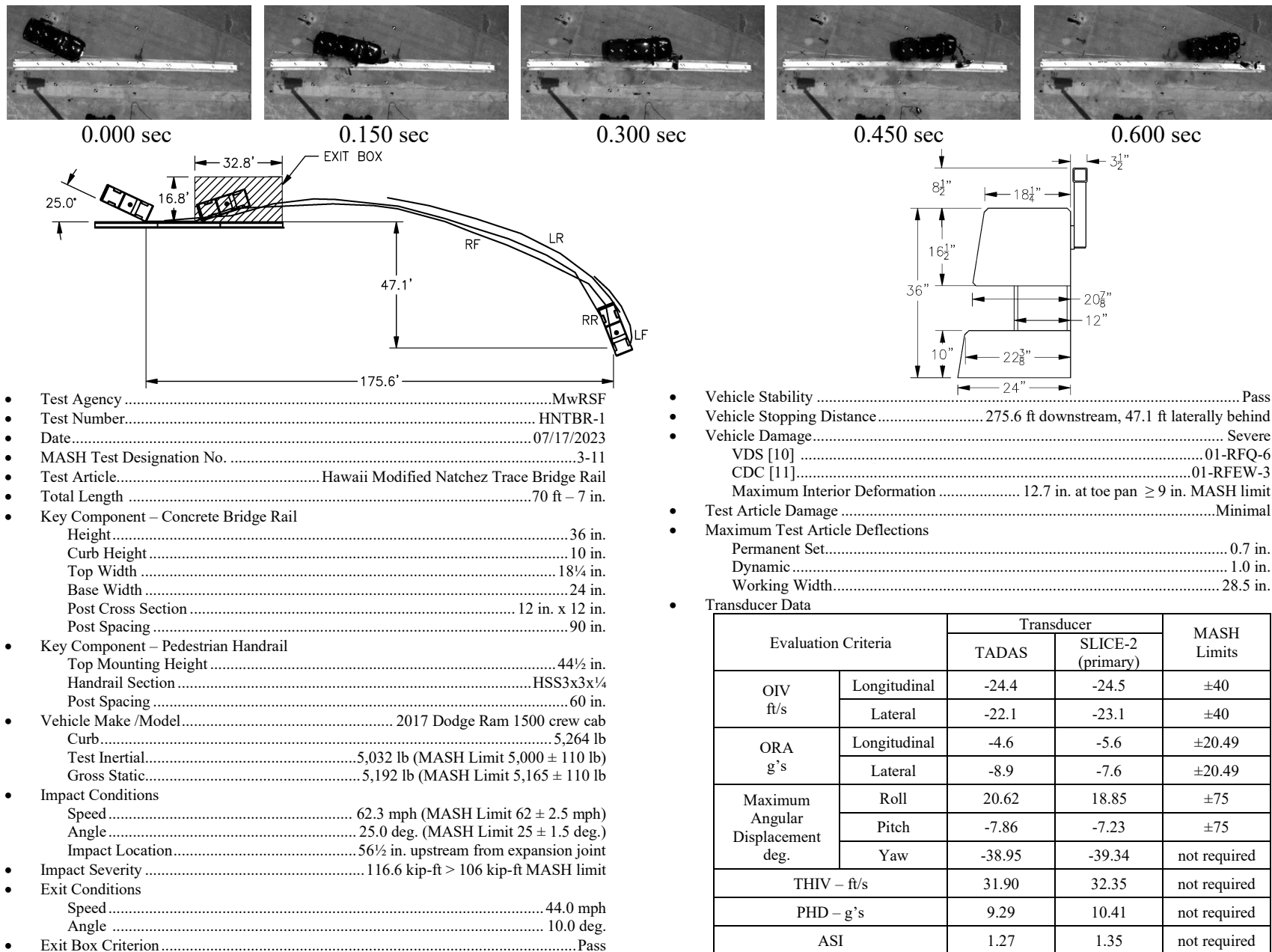


Figure 35. Summary of Test Results and Sequential Photographs, Test No. HNTBR-1

6 SUMMARY AND CONCLUSIONS

The Hawaii Modified Natchez Trace Bridge Rail evaluated herein consisted of a curb-mounted open concrete bridge rail and a pedestrian handrail. The concrete railing had a height of 36 in. and varied in width from 18¼ in. at the top to 24 in. at the bottom. The front of the concrete railing had a consistent single-slope face between the upper rail and the lower curb. The bridge rail design utilized 12-in. x 12-in. posts spaced 90 in. apart to support the upper rail. An HSS 3x3x¼ steel tube pedestrian handrail was mounted to the backside of the concrete railing with a top mounting height of 44½ in. The test installation had an overall length of 70 ft – 7 in. and incorporated three equal-length railing segments with ½-in. expansion joints placed between each segment.

The Hawaii Modified Natchez Trace Bridge Rail was subjected to one full-scale crash test in accordance with MASH test designation no. 3-11. The test evaluation is summarized in Table 7. In test no. HNTBR-1, a 5,032-lb crew cab pickup truck impacted the Hawaii Modified Natchez Trace Bridge Rail at a speed of 62.3 mph and an angle of 25.0 degrees. The impact occurred 56½ in. upstream from the expansion joint between post nos. 4 and 5 with an impact severity of 116.6 kip-ft. The vehicle was contained and redirected and exited the system at a speed of 44.0 mph and an angle of 10 degrees. Damage to the barrier was minimal, while damage to the vehicle was extensive. Intrusion to the occupant compartment at the toe pan was 12.7 in., which exceeded the MASH limit of 9 in. Therefore, test no. HNTBR-1 was unsatisfactory according to the safety performance criteria of MASH test designation no. 3-11.

Table 7. Summary of Safety Performance Evaluation

| Evaluation Factors | Evaluation Criteria | Test No. HNTBR-1 | | |
|---------------------------------|---|------------------|-----------|-----------|
| Structural Adequacy | A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underide, or override the installation although controlled lateral deflection of the test article is acceptable. | S | | |
| Occupant Risk | D. 1. Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. 2. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH 2016. | S U | | |
| | F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees. | S | | |
| | H. Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits: | S | | |
| | Occupant Impact Velocity Limits | | | |
| | Component | | Preferred | Maximum |
| | Longitudinal and Lateral | | 30 ft/s | 40 ft/s |
| | I. The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits: | S | | |
| | Occupant Ridedown Acceleration Limits | | | |
| | Component | | Preferred | Maximum |
| | Longitudinal and Lateral | | 15.0 g’s | 20.49 g’s |
| MASH 2016 Test Designation No. | | 3-11 | | |
| Final Evaluation (Pass or Fail) | | Fail | | |

S – Satisfactory

U – Unsatisfactory

N/A – Not Applicable

7 REFERENCES

1. *Manual for Assessing Safety Hardware* (MASH), Second Edition, American Association of State Highway and Transportation Officials (AASHTO), Washington, D.C., 2016.
2. Faller, R.K., Holloway, J.C., Pfeifer, B.G., and Luedke, J. K., *AASHTO PL-1 Performance Crash Tests on the Natchez Trace Parkway Bridge Rail*, Report No. TRP-03-34-92, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, October 1992.
3. *Guide Specifications for Bridge Railings*, American Association of State Highway and Transportation Officials, Washington, DC, 1989.
4. Bullard, D.L., Menges, W.L., Eugene C.B., and Haug, R.R., *Guardrail Testing Program IV Volume I: Technical Report*, Report No. FHWA-HRT-04-086, Texas Transportation Institute, TX, October 2003.
5. Ross, H. E. Sicking, D. L., Zimmer, R. A. and Michie, J. D., *Recommended Procedures for the Safety Performance Evaluation of Highway Features*, National Cooperative Highway Research Program Report 350, Transportation Research Board, National Research Council, Washington, D.C., 1993.
6. *Manual for Assessing Safety Hardware* (MASH), American Association of State Highway and Transportation Officials (AASHTO), Washington, D.C., 2009.
7. Hinch, J., Yang, T.L., and Owings, R., *Guidance Systems for Vehicle Testing*, ENSCO, Inc., Springfield, Virginia, 1986.
8. Center of Gravity Test Code - SAE J874 March 1981, SAE Handbook Vol. 4, Society of Automotive Engineers, Inc., Warrendale, Pennsylvania, 1986.
9. Society of Automotive Engineers (SAE), *Instrumentation for Impact Test – Part 1 – Electronic Instrumentation*, SAE J211/1 MAR95, New York City, New York, July 2007.
10. *Vehicle Damage Scale for Traffic Investigators*, Second Edition, Technical Bulletin No. 1, Traffic Accident Data (TAD) Project, National Safety Council, Chicago, Illinois, 1971.
11. *Collision Deformation Classification*, SAE International Surface Vehicle Recommended Practice, SAE Standard J224_201702, Society of Automotive Engineers, Warrendale, PA, February 2017.

8 APPENDICES

Appendix A. A2LA Accreditation Documents



Figure A-1. Midwest Roadside Safety Facility A2LA Accreditation Certificate No. 2937.01



SCOPE OF ACCREDITATION TO ISO/IEC 17025:2017

MIDWEST ROADSIDE SAFETY FACILITY (MwRSF)¹
University of Nebraska-Lincoln
4630 NW 36th Street
Lincoln, NE 68524
Ms. Karla Lechtenberg Phone: 402 472 9070

MECHANICAL

Valid To: November 30, 2025

Certificate Number: 2937.01

In recognition of the successful completion of the A2LA evaluation process, accreditation is granted to this laboratory to perform the following tests:

| <u>Tests</u> | <u>Test Methods</u> |
|---|---|
| Full-Scale Vehicle Crash Tests of Highway Safety Features | NCHRP Report 350; MASH; EN 1317 |
| Full-Scale Vehicle Crash Tests of Perimeter Protection Systems and Access Control Devices | ASTM F2656; SD-STD-02.01 Revision A |
| Bogie Dynamic Tests of Highway Safety Features | Non-Standard Test Method: Dynamic Testing of Steel Post and Rigid Foundation; Non-Standard Test Method: Dynamic Testing of Post in Soil; Non-Standard Test Method: Dynamic Testing of Spacer Blocks |
| Crushable Nose Bogie Testing for Breakaway Supports | Non-Standard Test Method: Dynamic Testing of Breakaway Supports; AASHTO Breakaway Poles and Supports; NCHRP Report 350 |

On the following types of products, materials, and/or structures:

Metal, Wood, Concrete and Plastic Structures, Components of Structures, Fasteners, and Roadway Pavements.

¹ Administrative office located at: 2200 Vine Street, 130 Whittier Building, Lincoln, NE 68583-0853.

(A2LA Cert. No. 2937.01) 06/27/2024

 Page 1 of 1

5202 Presidents Court, Suite 220 | Frederick, MD 21703-8515 | Phone: 301 644 3248 | Fax: 240 454 9449 | www.A2LA.org

Figure A-2. Midwest Roadside Safety Facility Scope of Accreditation to ISO/IEC 17025

Appendix B. Material Specifications, Test No. HNTBR-1

Table B-1. Bill of Materials, Test No. HNTBR-1

| Item No. | Description | Material Specification | Reference |
|----------|------------------------------------|--|-------------------|
| a1 | Concrete | Min. $f_c = 4,000$ psi | Sample 06052023.2 |
| b1 | #4 Rebar, 46" Total Unbent Length | ASTM A615 Gr. 60 | H#44000302131 |
| b2 | #7 Rebar, 53¼" Total Unbent Length | ASTM A615 Gr. 60 | H#7021691 |
| b3 | #5 Rebar, 44½" Total Unbent Length | ASTM A615 Gr. 60 | H#9700018828 |
| b4 | #4 Rebar, 35¾" Total Unbent Length | ASTM A615 Gr. 60 | H#44000302131 |
| b5 | #4 Rebar, 62" Total Unbent Length | ASTM A615 Gr. 60 | H#44000302131 |
| b6 | #6 Rebar, 278" Total Length | ASTM A615 Gr. 60 | H#9700017142 |
| b7 | #5 Rebar, 278" Total Length | ASTM A615 Gr. 60 | H#9700018828 |
| b8 | #5 Rebar, 38⅞" Total Unbent Length | ASTM A615 Gr. 60 | H#9700018828 |
| c1 | #8 Smooth Rebar, 24½" Long | ASTM A615 Gr. 60 | H#88924 |
| c2 | 1¼" Dia. PVC Pipe | Schedule 80 PVC Gr. 12454 | C.o.C. 5/5/2021 |
| c3 | 1¼" Dia. PVC End Cap | Schedule 80 PVC Gr. 12454 | C.o.C. 5/5/2021 |
| d1 | HSS 3" x 3" x ¼", 281½" Long | ASTM A500 Gr. B | H#NM5532 |
| d2 | HSS 2½" x 2½" x ¼", 13¾" Long | ASTM A500 Gr. B | H#05606D |
| d3 | 2¼" x 2¼" x ¼" Steel Plate | ASTM A36 | H#B2209440 |
| d4 | 8" x 5" x ¾" Steel Plate | ASTM A36 | H#A2K317 |
| d5 | 7" x 1½" x ⅜" Shim | ASTM A36 | H#22112982 |
| d6 | HSS 2" x 2" x ¼", 7" Long | ASTM A500 Gr. B | H#2125151 |
| e1 | ⅝"-11 UNC Heavy Hex Nut | ASTM A563-15 Grade DH | H#1000113771 |
| e2 | ⅝" Dia. Hardened Washer | ASTM F436 | H#22203720 |
| e3 | ⅝"-11 UNC, 7⅞" Long Threaded Rod | ASTM F1554-15 Gr. 105 | H#100209239 |
| e4 | Epoxy Adhesive | Hilti HIT RE-500 V3 | COC |
| e5 | Joint Filler | AASHTO M33, M153, or M213 | Data Tech Sheet |
| e6 | Expansion Joint Sealant | AASHTO M173, M282, M301, ASTM D3581, or ASTM D5893 | Data Tech Sheet |



Concrete Sample Test Report Cylinder Compressive Strength

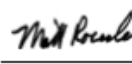






| | |
|-----------------|--|
| Project Name: | Midwest Roadside Safety - Misc Testing |
| Project Number: | 00110546.00 |
| Client: | Midwest Roadside Safety Facility |
| Location: | Midwest Roadside Safety |
| Sample: | 06052023.2 |
| Description: | HNTBR-1-2 , H3 Rail 3 |

Field Data (ASTM C172, C143, C173/C231, C138, C1064)

| | | | |
|----------------------|------------|-----------------------|-------------|
| Supplier: | | Property | Test Result |
| Mix Name: | | Slump (in): | |
| Ticket Number: | | Air Content (%): | |
| Truck Number: | | Unit Weight (lb/ft³): | |
| Load Volume (yd³): | | Air Temp (°F): | |
| Mold Date: | 06/05/2023 | Mix Temp (°F): | |
| Molded By: | | Min Temp (°F): | |
| Initial Cure Method: | | Max Temp (°F): | |

Laboratory Test Data (ASTM C39)

| | | | | | | |
|-----------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| Sample Number: | 06052023.2 | | | | | |
| Set Number: | 1 | | | | | |
| Specimen Number: | 1 | | | | | |
| Age: | 36 | | | | | |
| Length (in): | 12 | | | | | |
| Diameter (in): | 6 | | | | | |
| Area (in²): | 28.27 | | | | | |
| Density (lb/ft³): | 135 | | | | | |
| Test Date: | 07/11/2023 | | | | | |
| Break Type: | 5 | | | | | |
| Max Load (lbf): | 114,832 | | | | | |
| Strength (psi): | 4,060 | | | | | |
| Spec Strength (psi): | | | | | | |
| Excl in Avg Strength: | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |

| | |
|--|--|
| Remarks: | Sample Receive Date: 07/11/2023 |
| Set 1, Specimen 1, 36-day Compressive Strength (psi): 4,060 | Approved by: |
| |  |
| | Matt Roessler Manager |
|  Type 1 | Date: 07/11/2023 |
|  Type 2 | |
|  Type 3 | |
|  Type 4 | |
|  Type 5 | |
|  Type 6 | |

This report shall not be reproduced, except in full, without prior approval of Benesch. Results relate only to items tested.

825 M Street Suite 100
Lincoln, NE 68508

Benesch

Figure B-1. Concrete, Test No. HNTBR-1 (Item No. a1)

4400020131 06-28-22



Mill Certification
06/28/2022

MTR#: 1068214-3
Lot #: 440002013120
912 Cheney Avenue
Marion, OH 43302 US
800 333-4011
Fax: 740 383-6429

Sold To: SIMCOTE INC
250 N GREENWOOD ST
MARION, OH 43302 US

Ship To: SIMCOTE INC - MARION
250 N GREENWOOD ST
MARION, OH 43302 US

| | | | |
|---------------------------|--|----------------------|----------------|
| Customer PO | OH-2222 | Sales Order # | 44010643 - 1.1 |
| Product Group | Rebar | Product # | 1059653 |
| Grade | A615 Gr 60/M31 C | Lot # | 440002013120 |
| Size | #4 | Heat # | 4400020131 |
| BOL # | BOL-1167949 | Load # | 1068214 |
| Description | Rebar #4/13mm A615 Gr 60/M31 C 40' 0" [480"] Epoxy 4001-8000 lbs | Customer Part # | |
| Production Date | 06/21/2022 | Qty Shipped LBS | 25650 |
| Product Country Of Origin | United States | Qty Shipped EA | 960 |
| Original Item Description | | Original Item Number | |

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 06/20/2022

| C (%) | Mn (%) | P (%) | S (%) | Si (%) | Ni (%) | Cr (%) | Mo (%) | Cu (%) | V (%) | Sn (%) |
|-------|--------|-------|-------|--------|--------|--------|--------|--------|-------|--------|
| 0.20 | 0.63 | 0.013 | 0.026 | 0.184 | 0.16 | 0.18 | 0.05 | 0.27 | 0.004 | 0.017 |

Tensile testing

| | Yield (PSI) | Tensile (PSI) | Elongation in 8" (%) |
|-----|-------------|---------------|----------------------|
| (1) | 79100 | 96400 | 10.9 |

Mechanical

| | Average Deformation Height (IN) | Bend Test |
|-----|---------------------------------|-----------|
| (1) | 0.037 | Pass |

Other Test Results

Tensile / Yield Ratio : 1.22 Weight Percent Variance (%) : -4.19

Comments:

All manufacturing processes of the steel materials in this product, including melting, have occurred within the United States. All products produced are weld free. Mercury, in any form, has not been used in the production or testing of this material.

4400020131 06-28-22

Figure B-2. #4 Rebar, Test No. HNTBR-1 (Item Nos. b1, b4, and b5)



Mill Certification
09/24/2022

MTR#:1144239-4
Lot #:970001882820
500 REBAR RD
SEDALIA, MO 65301 US
660 951-1679
Fax: 660 951-1698

Sold To: SIMCOTE INC
1645 RED ROCK RD
ST PAUL, MN 55119 US

Ship To: SIMCOTE INC
1645 RED ROCK RD
ST PAUL, MN 55119 US

| | | | |
|---------------------------|---|----------------------|----------------|
| Customer PO | MN-3825 | Sales Order # | 97007522 - 7.1 |
| Product Group | Rebar | Product # | 2110230 |
| Grade | A615 Gr 60/AASHTO M31 | Lot # | 970001882820 |
| Size | #5 | Heat # | 9700018828 |
| BOL # | BOL-1242869 | Load # | 1144239 |
| Description | Rebar #5/16mm A615 Gr 60/AASHTO M31 40' 0" [480"] 4001-8000 lbs | Customer Part # | |
| Production Date | 09/20/2022 | Qty Shipped LBS | 71343 |
| Product Country Of Origin | United States | Qty Shipped EA | 1710 |
| Original Item Description | | Original Item Number | |

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 09/20/2022

| C (%) | Mn (%) | P (%) | S (%) | Si (%) | Ni (%) | Cr (%) | Mo (%) | V (%) | Nb (%) |
|-------|--------|-------|-------|--------|--------|--------|--------|-------|--------|
| 0.24 | 0.77 | 0.007 | 0.027 | 0.234 | 0.12 | 0.11 | 0.03 | 0.004 | 0.001 |

Tensile testing

| | Yield (PSI) | Tensile (PSI) | Elongation in 8" (%) |
|-----|-------------|---------------|----------------------|
| (1) | 77100 | 91000 | 13.7 |

Mechanical

| | Average Deformation Height (IN) | Bend Test |
|-----|---------------------------------|-----------|
| (1) | 0.039 | Pass |

Comments:

1. All manufacturing processes of the steel materials in this product, including melting, casting and rolling were performed in the USA.
2. Mercury, Radium, Hexavalent Chrome or Alpha source materials in any form have not been used in the production and testing of this material.
3. Weld repair was not performed on this material.

Figure B-4. #5 Rebar, Test No. HNTBR-1 (Item No. b3, b7, and b8)



Mill Certification
07/19/2022

MTR#:1087642-4
Lot #:970001714220
500 REBAR RD
SEDALIA, MO 65301 US
660 951-1679
Fax: 660 951-1698

Sold To: SIMCOTE INC
1645 RED ROCK RD
ST PAUL, MN 55119 US

Ship To: SIMCOTE DNS 232752 000
NEWPORT MN N11
NEWPORT, MN 55055 US

| | | | |
|---------------------------|--|----------------------|----------------|
| Customer PO | MN-3814 | Sales Order # | 97006876 - 3.1 |
| Product Group | Rebar | Product # | 2110264 |
| Grade | A615 Gr 60/AASHTO M31 | Lot # | 970001714220 |
| Size | #6 | Heat # | 9700017142 |
| BOL # | BOL-1185401 | Load # | 1087642 |
| Description | Rebar #6/19mm A615 Gr 60/AASHTO M31 40' 0" [480"] 6001-10000 lbs | Customer Part # | |
| Production Date | 07/10/2022 | Qty Shipped LBS | 54670 |
| Product Country Of Origin | United States | Qty Shipped EA | 910 |
| Original Item Description | | Original Item Number | |

I hereby certify that the material described herein has been manufactured in accordance with the specifications and standards listed above and that it satisfies those requirements.

Melt Country of Origin : United States

Melting Date: 07/10/2022

| C (%) | Mn (%) | P (%) | S (%) | Si (%) | Ni (%) | Cr (%) | Mo (%) | V (%) | Nb (%) |
|-------|--------|-------|-------|--------|--------|--------|--------|-------|--------|
| 0.29 | 0.98 | 0.009 | 0.020 | 0.177 | 0.14 | 0.16 | 0.04 | 0.005 | 0.002 |

Tensile testing

| | Yield (PSI) | Tensile (PSI) | Elongation in 8" (%) |
|-----|-------------|---------------|----------------------|
| (1) | 76300 | 95000 | 13.3 |

Mechanical

| | Average Deformation Height (IN) | Bend Test |
|-----|---------------------------------|-----------|
| (1) | 0.045 | Pass |

Comments:

1. All manufacturing processes of the steel materials in this product, including melting, casting and rolling were performed in the USA.
2. Mercury, Radium, Hexavalent Chrome or Alpha source materials in any form have not been used in the production and testing of this material.
3. Weld repair was not performed on this material.

Figure B-5. #6 Rebar, Test No. HNTBR-1 (Item No. b6)



CERTIFIED MILL TEST REPORT

Alton Steel Test Lab
#5 Cut Street
Alton, IL. 62002-9011
(618) 463-4490 EXT 2486
(618) 463-4491 (Fax)

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|------------------|--|---|-------|------|------|-------|---------------------|-------|-------|-------|----------|-------|------------|--------|--------|--------|----------|---------------------|--|--|--|--|--|--|--|---------------------|--|--|--|----------|--|------------|--|--------|--|----------|--|-------------|----|----|----|----|----|----|----|----|---|---|---|---|---|---|---|----|----|-----|-------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-----|-------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-----|-------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-----|-------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-----|-------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-----|
| BILL TO | | SHIP TO | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| WADY Industries, Inc 510 East Grove Street Maquoketa, IA 52060 | | WADY Industries, Inc 510 East Grove Street Maquoketa, IA 52060 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 11/12/2018 | Customer PO | 11352 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ASI Ord No. | 96071 | Customer PT. | 1.000-GRADE80-362 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ASI Ord Line Item | 1 | Specifications AASHTO M227 GR 80, ASTM A615-16 GR40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Item Description Steel Bar, Hot Rolled, 1.0000, 30' 2" | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Strand Cast, RR =62.39:1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Heat Number | Yield PSI | Tensile PSI | % Elongation % ROA Bend Test | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 188397 | 65100 | 97100 | 15 in 8" 32 Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 188829 | 74400 | 99700 | 15 in 8" 37 Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 188830 | 60200 | 90400 | 20 in 8" 36 Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 188924 | 66400 | 98900 | 19 in 8" 37 Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 188925 | 63500 | 94800 | 17 in 8" 36 Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CHEMICAL ANALYSIS TEST METHODS ASTM E-415 & E-1019 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Heat # | C | Mn | P | S | Si | Cu | Ni | Cr | Mo | Sn | Al | Nb/Cb | V | B | Ti | N | Pb | Ca | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88397 | 0.38 | 0.82 | 0.011 | 0.021 | 0.20 | 0.24 | 0.101 | 0.170 | 0.029 | 0.011 | 0.025 | 0.002 | 0.005 | 0.0002 | 0.0018 | 0.0107 | 0.0044 | 0.0024 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88829 | 0.34 | 0.75 | 0.010 | 0.023 | 0.23 | 0.27 | 0.079 | 0.139 | 0.024 | 0.010 | 0.001 | 0.001 | 0.046 | 0.0004 | 0.0007 | 0.0095 | 0.0023 | 0.0017 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88830 | 0.31 | 0.79 | 0.013 | 0.026 | 0.26 | 0.26 | 0.104 | 0.194 | 0.034 | 0.010 | 0.002 | 0.001 | 0.006 | 0.0003 | 0.0008 | 0.0104 | 0.0027 | 0.0023 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88924 | 0.32 | 0.78 | 0.012 | 0.023 | 0.25 | 0.28 | 0.110 | 0.207 | 0.033 | 0.011 | 0.002 | 0.002 | 0.006 | 0.0003 | 0.0006 | 0.0115 | 0.0034 | 0.0019 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88925 | 0.32 | 0.83 | 0.017 | 0.022 | 0.25 | 0.29 | 0.093 | 0.202 | 0.028 | 0.011 | 0.002 | 0.002 | 0.006 | 0.0004 | 0.0007 | 0.0115 | 0.0039 | 0.0015 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| JOMINY HARDENABILITY USING ASTM A-255 CALCULATED FROM CHEMICAL DI | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Heat Number | GS | DI | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88397 | 8 | 1.50 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88829 | 8 | 1.27 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88830 | | 1.28 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88924 | | 1.35 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88925 | | 1.40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SPECIAL TEST RESULTS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td colspan="8">ASTM E-45 Method A:</td> <td colspan="4">ASTM E-45 Method C:</td> <td colspan="2">SAE J422</td> <td colspan="2">ASTM E-381</td> <td colspan="2">Charpy</td> <td colspan="2">Hardness</td> </tr> <tr> <td>Heat Number</td> <td>TA</td> <td>TB</td> <td>TC</td> <td>TD</td> <td>HA</td> <td>HB</td> <td>HC</td> <td>HD</td> <td>S</td> <td>O</td> <td>S</td> <td>O</td> <td>S</td> <td>R</td> <td>C</td> <td>RC</td> <td>RB</td> <td>RHN</td> </tr> <tr> <td>88397</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>172</td> </tr> <tr> <td>88829</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>195</td> </tr> <tr> <td>88830</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>176</td> </tr> <tr> <td>88924</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>172</td> </tr> <tr> <td>88925</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>185</td> </tr> </table> | | | | | | | | | | | | | | | | | | | ASTM E-45 Method A: | | | | | | | | ASTM E-45 Method C: | | | | SAE J422 | | ASTM E-381 | | Charpy | | Hardness | | Heat Number | TA | TB | TC | TD | HA | HB | HC | HD | S | O | S | O | S | R | C | RC | RB | RHN | 88397 | | | | | | | | | | | | | | | | | | 172 | 88829 | | | | | | | | | | | | | | | | | | 195 | 88830 | | | | | | | | | | | | | | | | | | 176 | 88924 | | | | | | | | | | | | | | | | | | 172 | 88925 | | | | | | | | | | | | | | | | | | 185 |
| ASTM E-45 Method A: | | | | | | | | ASTM E-45 Method C: | | | | SAE J422 | | ASTM E-381 | | Charpy | | Hardness | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Heat Number | TA | TB | TC | TD | HA | HB | HC | HD | S | O | S | O | S | R | C | RC | RB | RHN | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88397 | | | | | | | | | | | | | | | | | | 172 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88829 | | | | | | | | | | | | | | | | | | 195 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88830 | | | | | | | | | | | | | | | | | | 176 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88924 | | | | | | | | | | | | | | | | | | 172 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 88925 | | | | | | | | | | | | | | | | | | 185 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ADDITIONAL COMMENTS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Figure B-6. #8 Smooth Rebar, Test No. HNTBR-1 (Item No. c1)



Certificate of Compliance

| | | |
|------------------------------|------------------------|------------|
| Sold To: | Purchase Order: | E000848414 |
| UNL / UNMC E-SHOP / PUNCHOUT | Job: | Shaun |
| | Invoice Date: | 05/5/2021 |

THIS IS TO CERTIFY THAT WE HAVE SUPPLIED YOU WITH THE FOLLOWING PARTS.
THESE PARTS WERE PURCHASED TO THE FOLLOWING SPECIFICATIONS.

12 PCS 1-1/4" Slip 300 lb PVC Flat Pipe Cap SUPPLIED UNDER OUR TRACE NUMBER l1ne49403 AND UNDER PART NUMBER 0470592

2 PCS 1-1/4" x 10 ft Gray Schedule 80 PVC Plain End Pipe SUPPLIED UNDER OUR TRACE NUMBER a042821 AND UNDER PART NUMBER 0472040

This is to certify that the above document is true
and accurate to the best of my knowledge.

Please check current revision to avoid using obsolete copies.


Fastenal Account Representative Signature

This document was printed on 05/05/2021 and was current at that
time.

Ross Schall
Printed Name

Fastenal Store Location/Address

3201 N. 23rd Street STE 1
LINCOLN, NE 68521
Phone #: (402)476-7900
Fax #: 402/476-7958

5/5/2021
Date

Figure B-7. PVC Tube Specifications, Test No. HNTBR-1 (Item Nos. c2 and c3)



6226 W. 74TH STREET
CHICAGO, IL 60638
Tel: 708-496-0380
Fax: 708-563-1950

<https://www.nucortubular.com>
<https://www.ntpportal.com>
Certificate Number: BHM 872827

Sold By:
NUCOR TUBULAR PRODUCTS INC.
BIRMINGHAM DIVISION
3525 RICHARD ARRINGTON JR. BLVD N
BIRMINGHAM, AL 35201
Tel: 205 251-1884
Fax: 205 251-1553

Purchase Order No: 4500539383
Sales Order No: BHM 593391 - 2
Bill of Lading No: BHM 51194 - 4
Invoice No:

Shipped: 10/28/2022
Invoiced:

Sold To:
5018 - STEEL & PIPE SUPPLY
4750 W. MARSHALL AVENUE
LONGVIEW, TX 75604

Ship To:
1 - STEEL & PIPE SUPPLY
4750 W. MARSHALL AVENUE
LONGVIEW, TX 75604

CERTIFICATE of ANALYSIS and TESTS

Certificate No: BHM 872827

Customer Part No:

Test Date: 10/26/2022

TUBING A500 GRADE B(C)
3" SQ X 1/4" X 24'

Total Pieces 100
Total Weight Lbs 21,145

| Bundle Tag | Mill | Heat | Specs | Y/T Ratio | Pieces | Weight Lbs |
|------------|------|--------|------------------------------|-----------|--------|------------|
| 197201 | 40N | SM5708 | YLD=65000/TEN=73500/ELG=25.5 | 0.8844 | 20 | 4,229 |
| 197206 | 40N | NM5532 | YLD=61800/TEN=74300/ELG=26 | 0.8318 | 20 | 4,229 |
| 197207 | 40N | NM5532 | YLD=61800/TEN=74300/ELG=26 | 0.8318 | 20 | 4,229 |
| 197210 | 40N | NM5148 | YLD=63500/TEN=72900/ELG=23 | 0.8711 | 20 | 4,229 |
| 197211 | 40N | NM5148 | YLD=63500/TEN=72900/ELG=23 | 0.8711 | 20 | 4,229 |

Mill #: 40N **Heat #:** NM5148 **Carbon Eq:** 0.2841 **Heat Src Origin:** MELTED AND MANUFACTURED IN THE USA

| C | Mn | P | S | Si | Al | Cu | Cr | Mo | V | Ni | Nb | Sn |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.2000 | 0.3900 | 0.0040 | 0.0020 | 0.0270 | 0.0340 | 0.1000 | 0.0400 | 0.0100 | 0.0020 | 0.0300 | 0.0060 | 0.0020 |
| N | B | Ti | Ca | | | | | | | | | |
| 0.0050 | 0.0001 | 0.0020 | 0.0020 | | | | | | | | | |

Mill #: 40N **Heat #:** NM5532 **Carbon Eq:** 0.2894 **Heat Src Origin:** MELTED AND MANUFACTURED IN THE USA

| | | | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| C | Mn | P | S | Si | Al | Cu | Cr | Mo | V | Ni | Nb | Sn |
| 0.2000 | 0.4100 | 0.0070 | 0.0010 | 0.0200 | 0.0290 | 0.1200 | 0.0400 | 0.0100 | 0.0020 | 0.0400 | 0.0060 | 0.0030 |
| N | B | Ti | Ca | | | | | | | | | |
| 0.0060 | 0.0002 | 0.0010 | 0.0011 | | | | | | | | | |

Mill #: 40N **Heat #:** SM5708 **Carbon Eq:** 0.2667 **Heat Src Origin:** MELTED AND MANUFACTURED IN THE USA

| C | Mn | P | S | Si | Al | Cu | Cr | Mo | V | Ni | Nb | Sn |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0.1900 | 0.3500 | 0.0050 | 0.0040 | 0.0230 | 0.0380 | 0.1200 | 0.0300 | 0.0100 | 0.0020 | 0.0300 | 0.0070 | 0.0020 |
| N | B | Ti | Ca | | | | | | | | | |
| 0.0053 | 0.0004 | 0.0010 | 0.0017 | | | | | | | | | |

Figure B-8. 3 x 3 x 1/4-in., 281 1/2-in. Long HSS, Test No. HNTBR-1 (Item No. d1)



1000 BURLINGTON STREET, NORTH KANSAS CITY, MO 64116 1-816-474-5210 TOLL FREE 1-800-892-TUBE

STEEL VENTURES, LLC dba EXLTUBE

Certified Test Report

| | | | |
|--|---------------------|---|-------------------|
| Customer: SPS - Tulsa 1020 Fort Gibson Road Catoosa OK 74015-3033 | Size: 02.50X02.50 | Customer Order No: | Customer Part No: |
| | Gauge: 1/4 | 4500524183 | 6521625040 |
| | Date: 02/09/2022 | Delivery No: 85142099 Load No: 7138474 | Length: 40 FT |
| Specification: ASTM A500-21 Gr.B/C | | | |

| | | | |
|---------|--------------|----------------|------------------------|
| Heat No | Yield KSI | Tensile KSI | Elongation % 2 inch |
| 05606D | 61.7 | 70.4 | 30.00 |

| | | | | | | | | | | |
|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Heat No | C | MN | P | S | SI | CU | NI | CR | MO | V |
| 05606D | 0.1600 | 0.7900 | 0.0120 | 0.0070 | 0.0110 | 0.0400 | 0.0200 | 0.0600 | 0.0000 | 0.0000 |

This material was melted & manufactured in the U.S.A. This material meets the Buy America requirement of 23 CFR 635.410.
Coil Producing Mill: UNITED STATES STEEL, Granite City, IL

We hereby certify that all test results shown in this report are correct as contained in the records of our company. All testing and manufacturing is in accordance to A.S.T.M. parameters encompassed within the scope of the specifications denoted in the specification and grade tiles above. This product was manufactured in accordance with your purchase order requirements.

This material has not come into direct contact with mercury, any of its compounds, or any mercury bearing devices during our manufacturing process, testing, or inspections.

This material is in compliance with EN 10204 Section 4.1 Inspection Certificate Type 3.1

Tensile test completed using test specimen with 3/4" reduced area.

STEEL VENTURES, LLC dba EXLTUBE

A handwritten signature in black ink, appearing to read "Jonathan Wolfe".

Jonathan Wolfe
Quality Assurance Manager

Figure B-9. 2½ x 2½ x ¼-in., 13¾-in. Long HSS, Test No. HNTBR-1 (Item No. d2)



SPS Coil Processing Tulsa
5275 Bird Creek Ave.
Port of Catoosa, OK 74015

METALLURGICAL TEST REPORT

PAGE 1 of 1
DATE 01/26/2023
TIME 07:05:13

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13716
Kansas City Warehouse
401 New Century Parkway
New Century KS 66031-1127

| Order | Material No. | Description | Quantity | Weight | Customer Part | Customer PO | Ship Date |
|---------------|--------------|------------------------------|----------|-----------|---------------|-------------|------------|
| 40397361-0020 | 70872120 | 1/4 72 X 120 A36 STP MIL PLT | 16 | 9,801.600 | | | 01/25/2023 |

Chemical Analysis

| | | | | | | | | | | | | | | | |
|-------------------|-----------|--------------------------------------|---------|----------|--------|------------------------------------|------------|--|--------|----------|----------|----------|-----------|----------|--------|
| Heat No. B2209440 | | Vendor STEEL DYNAMICS SOUTHWEST, LLC | | DOMESTIC | | Mill STEEL DYNAMICS SOUTHWEST, LLC | | Melted and Manufactured in the USA Produced from Coil | | | | | | | |
| Carbon | Manganese | Phosphorus | Sulphur | Silicon | Nickel | Chromium | Molybdenum | Boron | Copper | Aluminum | Titanium | Vanadium | Columbium | Nitrogen | Tin |
| 0.0500 | 0.8600 | 0.0060 | 0.0040 | 0.0200 | 0.0400 | 0.0400 | 0.0100 | 0.0000 | 0.1000 | 0.0290 | 0.0000 | 0.0040 | 0.0020 | 0.0080 | 0.0050 |

Mechanical / Physical Properties

Mill Coil No. 22B114642

| Tensile (PSI) | Yield (PSI) | % Elong (2 in) | Rckwl | Grain | Charpy | Charpy Dr | Charpy Sz | Temperature | Olsen |
|---------------|-------------|----------------|-------|-------|--------|-----------|-----------|-------------|-------|
| 64000.000 | 50700.000 | 36.50 | | | 0 | NA | | | |
| 62600.000 | 47600.000 | 36.50 | | | 0 | NA | | | |
| 64200.000 | 46300.000 | 37.50 | | | 0 | NA | | | |
| 63200.000 | 45800.000 | 36.00 | | | 0 | NA | | | |

Batch 1001159632 16 EA 9,801.600 LB

Figure B-10. 2¼ x 2¼ x ¼-in. Steel Plate, Test No. HNTBR-1 (Item No. d3)



Test Certificate

1770 Bill Sharp Boulevard, Muscatine, IA 52761-9412, US

WARNING: This product can expose you to chemicals including nickel and nickel compounds, which are known to the State of California to cause cancer. For more information go to www.P65Warnings.ca.gov.

Form TC1: Revision 5: Date 22 Aug 2022

| | | | | | | | | | | | | | | | | |
|--|-----------------|--|----------------|--|------------------|--|------------------------|--|-----------------|---------------------------------------|--------------------------|----------------|----------------|---------------------|-----------------------|-------------|
| Customer: STEEL & PIPE SUPPLY P.O. BOX 1688 MANHATTAN KS 66502 | | Customer P.O.No.: 4500540178 | | Mill Order No. 41-692042-02 | | Shipping Manifest: MT476914 | | | | | | | | | | |
| | | Product Description: ASTM A36(19)/A709(21)36/ASME SA36(21) AASHTO M270(20)36 | | | | Ship Date: 02 Dec 22 Cert Date: 02 Dec 22 | | Cert No: 061199049 (Page 1 of 1) | | | | | | | | |
| | | Size: 0.750 X 96.00 X 120.0 (IN) | | | | | | | | | | | | | | |
| Tested Pieces: | | | | Tensiles: | | | | Charpy Impact Tests | | | | | | | | |
| Heat Id | Piece Id | Tested Thickness | Tst Loc | YS (KSI) | UTS (KSI) | %RA | Elong % 2in 8in | Tst Dir | Hardness | Abs. Energy(FTLB) 1 2 3 Avg | % Shear 1 2 3 Avg | Tst Tmp | Tst Dir | Tst Siz (mm) | BDWTT Tmp %Shr | |
| A2J254 | B33 | 0.747 (DISCRT) | L 42 | 65 | | | 38 | T | | | | | | | | |
| A2K317 | B13 | 0.745 (DISCRT) | L 43 | 67 | | | 39 | T | | | | | | | | |
| A2K317 | B14 | 0.746 (DISCRT) | L 43 | 67 | | | 37 | T | | | | | | | | |
| Chemical Analysis | | | | | | | | | | | | | | | | |
| Heat Id | C | Mn | P | S | Si | Tot Al | Cu | Ni | Cr | Mo | Co | V | Ti | B | N | ORGN |
| A2J254 | .20 | .53 | .009 | .001 | .06 | .032 | .34 | .11 | .11 | .03 | .000 | .003 | .008 | .0000 | .0068 | USA |
| A2K317 | .19 | .53 | .015 | .001 | .06 | .031 | .36 | .10 | .16 | .03 | .001 | .003 | .007 | .0000 | .0080 | USA |
| <p>KILLED STEEL MERCURY IS NOT A METALLURGICAL COMPONENT OF THE STEEL AND NO MERCURY WAS INTENTIONALLY ADDED DURING THE MANUFACTURE OF THIS PRODUCT. MTR EN 10204:2004 INSPECTION CERTIFICATE 3.1 COMPLIANT 100% MELTED, POURED, AND ROLLED IN THE USA PRODUCTS SHIPPED: A2K317 B12 PCES: 8, LBS: 19600 A2J254 B33 PCES: 2, LBS: 4900</p> | | | | | | | | | | | | | | | | |
| (P) Cust Part #:722496120 | | | | WE HEREBY CERTIFY THAT THIS MATERIAL WAS TESTED IN ACCORDANCE WITH, AND MEETS THE REQUIREMENTS OF, THE APPROPRIATE SPECIFICATION | | | | | | Brian Wales PRINCIPAL METALLURGIST | | | | | | |

Figure B-11. 8 x 5 x 3/4-in. Steel Plate, Test No. HNTBR-1 (Item No. d4)



SPS Coil Processing Tulsa
5275 Bird Creek Ave.
Port of Catoosa, OK 74015

METALLURGICAL TEST REPORT

PAGE 1 of 1
DATE 12/13/2022
TIME 07:22:11

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13716
Kansas City Warehouse
401 New Century Parkway
New Century KS 66031-1127

| Order | Material No. | Description | Quantity | Weight | Customer Part | Customer PO | Ship Date |
|---------------|--------------|-------------------------------|----------|-----------|---------------|-------------|------------|
| 40395681-0020 | 70672120 | 3/16 72 X 120 A36 STP MIL PLT | 6 | 2,757.600 | | | 12/12/2022 |

Chemical Analysis

| | | | | | | | | | | | | | | | |
|--------------------|-----------|------------|----------------------------|---------|--------|----------|------------|--------|--------------------------|----------|----------|------------------------------------|-----------|----------|--------|
| Heat No. 22112982 | | | Vendor BIG RIVER STEEL LLC | | | DOMESTIC | | | Mill BIG RIVER STEEL LLC | | | Melted and Manufactured in the USA | | | |
| Produced from Coil | | | | | | | | | | | | | | | |
| Carbon | Manganese | Phosphorus | Sulphur | Silicon | Nickel | Chromium | Molybdenum | Boron | Copper | Aluminum | Titanium | Vanadium | Columbium | Nitrogen | Tin |
| 0.0600 | 0.8100 | 0.0060 | 0.0030 | 0.0200 | 0.0300 | 0.0300 | 0.0100 | 0.0001 | 0.0600 | 0.0250 | 0.0000 | 0.0020 | 0.0010 | 0.0095 | 0.0028 |

Mechanical / Physical Properties

| Mill Coil No. 22112982-03 | | | | | | | | | | | | | | | |
|---------------------------|-------------|----------------|-------|-------|--------|-----------|-----------|-------------|-------|--|--|--|--|--|--|
| Tensile (PSI) | Yield (PSI) | % Elong (2 in) | Rckwl | Grain | Charpy | Charpy Dr | Charpy Sz | Temperature | Olsen | | | | | | |
| 64100.000 | 46800.000 | 31.00 | | | 0 | NA | | | | | | | | | |
| 64100.000 | 47200.000 | 30.00 | | | 0 | NA | | | | | | | | | |
| 66700.000 | 48000.000 | 27.50 | | | 0 | NA | | | | | | | | | |
| 66200.000 | 48300.000 | 31.00 | | | 0 | NA | | | | | | | | | |

Batch 1001086664 6 EA 2,757.600 LB

Batch 1001086661 21 EA 9,651.600 LB

Figure B-12. 7 x 1½ x 3/16-in. Shim, Test No. HNTBR-1 (Item No. d5)

Atlas Tube Arkansas
6651 E Hwy 137
Blytheville Arkansas USA
72315
Tel:
Fax:



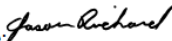
REF.B/L: 81115225
Date: 10/13/2022
Customer: 179

MATERIAL TEST REPORT

Sold To
Steel & Pipe Supply Company
PO Box 1688
MANHATTAN KS 66505
USA

Shipped To
Steel & Pipe c/o Longview Whse
4750 West Marshall Avenue
LONGVIEW TX 75604
USA

| | | | | | | | | | | | | | | | | | |
|-----------------------------------|-------|---------------|------------|------------|--------|----------------------------|---------------|--------------------------------|-------|-------|-------|----------------------------|--------------------------|--------|--------|--------|--|
| Material: 2.0x2.0x250x40"0(10x3). | | | | | | Material No: 200202504000 | | | | | | Made in: USA | | | | | |
| Sales Order: 1832937 | | | | | | Purchase Order: 4500537759 | | | | | | Melted and Poured in: USA | | | | | |
| | | | | | | | | | | | | Cust Material#: 6520025040 | | | | | |
| Heat No | C | Mn | P | S | Si | Al | Cu | Cb | Mo | Ni | Cr | V | Ti | B | N | Ca | |
| 2125151 | 0.200 | 0.780 | 0.011 | 0.002 | 0.030 | 0.020 | 0.080 | 0.002 | 0.010 | 0.040 | 0.040 | 0.003 | 0.002 | 0.0000 | 0.0060 | 0.0020 | |
| Bundle No | | PCs | Yield | Tensile | | Elon.2in | | Certification | | | | | CE: 0.35 | | | | |
| M400217625 | | 30 | 066583 Psi | 081008 Psi | | 29 % | | ASTM A500-21 GRADE B&C | | | | | | | | | |
| Heat | MILL | Mill Location | | | Method | Recycled_Content | Post_Consumer | Pre-Consumer (Post Industrial) | | | | % Harvested | Within Miles of Location | | | | |
| 2125151 | NUCOR | HICKMAN,AR | | | EAF | 52.50% | 31.80% | 20.70% | | | | 74% | 500 | | | | |
| Material Note: | | | | | | | | | | | | | | | | | |
| Sales Or. Note: | | | | | | | | | | | | | | | | | |

Authorized by Quality Assurance: 
Jason Richard

The results reported on this report represent the actual attributes of the material furnished and indicate full compliance with all applicable specification and contract requirements. CE calculated using the AWS D1.1 method. This document is in compliance with the requirements of EN 10204 type 3.1



Figure B-13. 2 x 2 x 1/4-in., 7-in. Long HSS, Test No. HNTBR-1 (Item No. d6)

NUCOR
FASTENER DIVISION

CUSTOMER NO/NAME
9311 STELFAST INC.

TEST REPORT SERIAL# FB707265
TEST REPORT ISSUE DATE 6/03/22
DATE SHIPPED 6/13/22

NUCOR ORDER # 335684
CUST PART # ADHHGBW0625CSKD

CUSTOMER P.O. # A-32815

NAME OF LAB SAMPLER: AMY HULLINGER, LAB TECHNICIAN

*****CERTIFIED MATERIAL TEST REPORT*****

NUCOR PART NO QUANTITY LOT NO. DESCRIPTION
175747C 6800 469660C 5/8-11 GR DH HV H.D.G.
MANUFACTURE DATE 3/16/22 HEX NUT HOT DIP GAL.

Post Office Box 6100
Saint Joe, Indiana 46785
Telephone 260/337-1800



--CHEMISTRY MATERIAL GRADE -1026L

| MATERIAL | HEAT | **CHEMISTRY COMPOSITION (WT% HEAT ANALYSIS) BY MATERIAL SUPPLIER | | | | |
|----------|------------|--|-----|------|------|-----|
| NUMBER | NUMBER | C | MN | P | S | SI |
| RM035653 | 1000113771 | .25 | .70 | .015 | .011 | .25 |

NUCOR STEEL - NEBRASKA
2911 EAST NUCOR RD
NORFOLK, NE 68701

--MECHANICAL PROPERTIES IN ACCORDANCE WITH ASTM A563/A563M-21ae1

| SURFACE | CORE | PROOF LOAD | TENSILE STRENGTH |
|----------|----------|------------|------------------|
| HARDNESS | HARDNESS | 33900 LBS | DEG-WEDGE |
| (R30N) | (RC) | | (LBS) |
| N/A | 30.7 | PASS | N/A |
| N/A | 29.4 | PASS | N/A |
| N/A | 30.9 | PASS | N/A |
| N/A | 30.6 | PASS | N/A |
| N/A | 28.8 | PASS | N/A |

STRESS (PSI)

AVERAGE VALUES FROM TESTS
30.1

PRODUCTION LOT SIZE 188000 PCS

--VISUAL INSPECTION IN ACCORDANCE WITH ASTM A563/A563M-21ae1 160 PCS. SAMPLED LOT PASSED

--COATING - HOT DIP GALVANIZED TO ASTM F2329-15 - GALVANIZING PERFORMED IN THE U.S.A.

| | | | | | | |
|-------------|------------|-------------|-------------|-------------|-------------|-------------|
| 1. 0.00331 | 2. 0.00517 | 3. 0.00220 | 4. 0.00328 | 5. 0.00412 | 6. 0.00407 | 7. 0.00285 |
| 8. 0.00282 | 9. 0.00316 | 10. 0.00225 | 11. 0.00429 | 12. 0.00270 | 13. 0.00264 | 14. 0.00335 |
| 15. 0.00265 | | | | | | |

AVERAGE THICKNESS FROM 15 TESTS .00326 (INCHES) THICKNESS METHODS PER ASTM E375, B487, AND B499 UNLESS CUSTOMER SPECIFIES

--HEAT TREATMENT - AUSTENITIZED, OIL QUENCHED & TEMPERED (MIN 800 DEG F)

--DIMENSIONS PER ASME B18.2.6-2010

| CHARACTERISTIC | #SAMPLES TESTED | MINIMUM | MAXIMUM (in IN/MM) |
|----------------------|-----------------|---------|--------------------|
| Width Across Corners | 8 | 1.187 | 1.193 |
| Thickness | 32 | 0.596 | 0.612 |

--SAMPLING PLAN PER ASTM F1470-19 UNLESS SPECIFIED BY CUSTOMER

ALL TESTS ARE IN ACCORDANCE WITH THE LATEST REVISIONS OF THE METHODS PRESCRIBED IN THE APPLICABLE SAE AND ASTM SPECIFICATIONS. THE SAMPLES TESTED CONFORM TO THE SPECIFICATIONS AS DESCRIBED/LISTED ABOVE AND WERE MANUFACTURED FREE OF MERCURY CONTAMINATION. NO INTENTIONAL ADDITIONS OF BISMUTH, SELENIUM, TELLURIUM, OR LEAD WERE USED IN THE STEEL USED TO PRODUCE THIS PRODUCT.

THE STEEL WAS MELTED AND MANUFACTURED IN THE U.S.A. AND THE PRODUCT WAS MANUFACTURED AND TESTED IN THE U.S.A. PRODUCT COMPLIES WITH DFARS 252.225-7014. WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY. THIS CERTIFIED MATERIAL TEST REPORT RELATES ONLY TO THE ITEMS LISTED ON THIS DOCUMENT AND MAY NOT BE REPRODUCED EXCEPT IN FULL. CERTIFICATION FORMAT MEETS EN10204 3.1




MECHANICAL FASTENER
CERTIFICATE NO. A2LA 0139.01
EXPIRATION DATE 12/31/23

NUCOR FASTENER
A DIVISION OF NUCOR CORPORATION



SAHIL PRABHUDESAI
QUALITY ASSURANCE SUPERVISOR

Figure B-14. 5/8-in.-11 UNC Heavy Hex Nut, Test No. HNTBR-1 (Item No. e1)

| CUSTOMER NAME | | CUSTOMER ORDER NUMBER | | DATE | | | | |
|---|----------|---|-----|--------------------|------|----------|------|----------|
| Portland Bolt & Mfg Co | | 54763 | | 6/2/2022 | | | | |
| PART NUMBER | | CUSTOMER LOT NO. | | LOT NUMBER | | QUANTITY | | |
| 5/8" F436 Hdg | | | | 0322-248 | | 10,000 | | |
| STEEL GRADE | HEAT | C | MN | P | S | SI | AL | REVISION |
| | 22203720 | .53 | .73 | .008 | .002 | .23 | .020 | F436-19 |
| SPECIFICATION | | ACTUAL | | GAUGE | | | | |
| O.D - 1.281 - 1.345 | | 1.286 - 1.289 | | CALIPER | | | | |
| I.D - .688 - .720 | | .715 - .718 | | CALIPER, PIN GAUGE | | | | |
| THICKNESS- .122 - .177 | | .134 - .137 | | MICROMETER | | | | |
| FLAT- Max .010 | | .009 | | CALIPER | | | | |
| HEAT TREAT - 38 - 45HRC | | 41 - 44 | | | | | | |
| PLATING- | | See Attached Cert | | | | | | |
| OTHER | | N/A | | | | | | |
| <p>WE HEREBY CERTIFY THIS PRODUCT WAS PRODUCED UNDER A ISO 9001:2015 QUALITY ASSURANCE SYSTEM. ISO 9001:2015 ALL MATERIALS ARE MADE AND MILED IN THE U.S.A. THIS PRODUCT WAS MANUFACTURED IN CHESTERFIELD, MICHIGAN, U.S.A. THIS PRODUCT CONFORMS TO ALL REQUIREMENTS FOR WASHERS AS PRODUCED ACCORDING TO A S.T.M. F-436-19. THE ABOVE TEST RESULTS APPLY ONLY TO THE ITEMS TESTED. THIS TEST REPORT MUST NOT BE REPRODUCED EXCEPT IN FULL WITHOUT PRIOR WRITTEN APPROVAL.</p> | | | | | | | | |
| CERTIFIED ISO 9001: | |  AUTHORIZED SIGNATURE | | | | | | |
| "MADE AND MANUFACTURED IN THE USA" | | | | | | | | |

54763-2

Figure B-15. 5/8-in. Dia. Hardened Washer, Test No. HNTBR-1 (Item No. e2)

| | | | | | | | | | | | |
|---|---|--|--------|--------|------|----------|------|---------|---------|---------|-------|
|  <p>Vulcan THREADED PRODUCTS, INC.</p> | <p>Vulcan Threaded Products 10 Cross Creek Trail Pelham, AL 35124 Tel (205) 620-5100 Fax (205) 620-5150</p> | <h2 style="margin: 0;">JOB MATERIAL CERTIFICATION</h2> | | | | | | | | | |
| <p>Job No: 721458 Job Information Certified Date: 7/7/21</p> | | | | | | | | | | | |
| <p>Containers: S18661829 S18663941</p> | | | | | | | | | | | |
| <p>Customer: Conklin and Conklin</p> | | <p>Ship To: 34201 Seventh Street Union City, CA 94587</p> | | | | | | | | | |
| <p>Vulcan Part No: BAR B7 .5626x144 SC</p> | | | | | | | | | | | |
| <p>Customer Part No: BAR B7 .562x144</p> | | | | | | | | | | | |
| <p>Customer PO No: 20594</p> | | <p>Shipped Qty: 6018 lbs</p> | | | | | | | | | |
| <p>Order No: 432165</p> | | <p>Line No: 2</p> | | | | | | | | | |
| <p>Note:</p> | | | | | | | | | | | |
| <p>Applicable Specifications</p> | | | | | | | | | | | |
| Type | Specification | Rev | Amend | Option | | | | | | | |
| Heat Treat | ASTM F1554 Gd 105 S4 | 2020 | | | | | | | | | |
| | ASME SA-193/SA-193M B7 | 2019 | | | | | | | | | |
| | ASTM A193 B7 | 2020 | | | | | | | | | |
| <p>Test Results</p> | | | | | | | | | | | |
| <p>See following pages for tests</p> | | | | | | | | | | | |
| <p>Certified Chemical Analysis</p> | | | | | | | | | | | |
| <p>Heat No: 100209239 Lot 5/8 Origin: USA</p> | | | | | | | | | | | |
| C | Mn | P | S | Si | Cr | Mo | Ni | V | Cu | Al | Cb |
| 0.41 | 0.93 | 0.008 | 0.025 | 0.28 | 0.98 | 0.18 | 0.07 | 0.004 | 0.18 | 0.026 | 0.004 |
| Sn | Ti | B | Ca | As | DI | RR | G.S. | Macro S | Macro R | Macro C | J1 |
| 0.008 | 0.001 | 0.0004 | 0.0021 | 0.005 | 5.65 | 143.06:1 | 8 | 1 | 1 | 2 | 57 |
| J2 | J3 | J4 | J5 | J6 | J7 | J8 | J9 | J10 | J11 | J12 | J13 |
| 57 | 57 | 57 | 57 | 57 | 57 | 57 | 56 | 54 | 53 | 51 | 51 |
| J14 | J15 | J16 | J18 | J20 | J22 | J24 | J26 | J28 | J30 | J32 | |
| 50 | 49 | 48 | 48 | 47 | 46 | 45 | 44 | 43 | 41 | 40 | |
| <p>Notes</p> | | | | | | | | | | | |
| <p>Processed material is Tempered - Stress Relieved. No weld repair performed on the material. No Mercury used in the production of this material. Melted and Manufactured in the USA. Grade - 4140/42 EAF Melted</p> | | | | | | | | | | | |

Plex 7/7/21 3:46 PM vulc.sano Page 1 of 2

PORTLAND BOLT
PO 53756
INV 084399
100 5/8" x 144" B7 ATR HDG 10F2
JAN 24, 2022

Figure B-16. 5/8-in. 11 UNC, 7 7/8-in. Long Threaded Rod, Test No. HNTBR-1 (Item No. e3)



Date: 12/13/2016

Subject: Certificate of Conformance

Product: HIT RE-500 V3 Adhesive

To Whom it May Concern:

This is to certify that the HIT-RE 500 V3 is a high-strength, slow cure two-part epoxy adhesive contained in two cartridges separating the resin from the hardener.

Additionally, this certifies that the product has been seismically and cracked concrete qualified as represented in ICC-ES report ESR- 3814.

Sincerely,

Hilti, Inc.

5400 South 122 East Avenue


Tulsa, Oklahoma 74146

800-879-8000

800-879-7000 fax


US-Sales@hilti.com

Figure B-17. Epoxy Adhesive, Test No. HNTBR-1 (Item No. e4)



NO. 320-F

MasterFormat: 03 15 00



APRIL 2018
(Supersedes March 2016)

FIBRE EXPANSION JOINT

Multi-Purpose, Expansion-Contraction Joint Filler

DESCRIPTION

FIBRE EXPANSION JOINT is composed of cellular fibers securely bonded together and uniformly saturated with asphalt to assure longevity. Wherever a cost-effective joint filler is required, FIBRE EXPANSION JOINT meets the need. Manufactured and marketed by W. R. MEADOWS since the early 1930s, FIBRE EXPANSION JOINT is backed by over 80 years of proven application experience. FIBRE EXPANSION JOINT is versatile, resilient, flexible, and non-extruding. When compressed to half of its original thickness, it will recover to a minimum of 70% of its original thickness. FIBRE EXPANSION JOINT will not deform, twist, or break with normal on-the-job handling. Breakage, waste and functional failure resulting from the use of inferior, foreign fiber materials can cost you time and dollars and can result in a substandard finished job, generating costly callbacks and rework expenses. However, the purchase and installation of FIBRE EXPANSION JOINT (a small segment of the total project's cost) contributes to both the final cost efficiency and functional success, far greater in proportion than its original cost.

Representative United States patents: USPNs 7,815,722; 8,057,638; 8,038,845; and D558,305. (See also www.wrmeadows.com/patents for further patent/intellectual property information.)

USES

FIBRE EXPANSION JOINT is ideal for use on highways, streets, airport runways, sidewalks, driveways, flatwork, and scores of commercial and industrial applications subject to pedestrian and vehicular traffic.

FEATURES/BENEFITS

- Provides the ideal product for the majority of all expansion/contraction joint requirements.
- Non-extruding ... versatile ... offers a minimum 70% recovery after compression.
- This tough, lightweight, easy-to-use, semi-rigid joint filler is available in strips and shapes fabricated to your requirements.
- Easy to cut ... dimensionally stable ... not sticky in summer or brittle in winter.
- Provides neat, finished joints requiring no trimming.
- Often copied ... but never equaled.
- Remains the standard of the industry today ... with over 80 years of proven and satisfactory performance.
- Can be punched for dowel bars and laminated to thicknesses greater than 1" (25.4 mm).



| Conforms to or meets: | Thickness | Slab Widths | Standard Lengths | Weight per ft. ³ |
|--|--|-------------------------|--|-----------------------------|
| <ul style="list-style-type: none"> • AASHTO M 213 • ASTM D1751 • Corps of Engineers CRD-C 508 • FAA Specification Item P-610-2.7 • HH-F-341 F, Type 1 | 3/8", 1/2" 3/4", 1" (9.5, 12.7, 19.1, 25.4 mm) | 36", 48" (91, 122 m) | 10' (3.05 m) Also available: 5', 6', 12' (1.5, 1.83, 3.66 m) | >19 lb. |

CONTINUED ON REVERSE SIDE...

W. R. MEADOWS, INC.
P.O. Box 338 • HAMPSHIRE, IL 60140-0338
Phone: 847/214-2100 • Fax: 847/683-4544
1-800-342-6976
www.wrmeadows.com

HAMPSHIRE, IL / CARTERSVILLE, GA / YORK, PA
FORT WORTH, TX / BENICIA, CA / POMONA, CA
GOODYEAR, AZ / MILTON, ON / ST. ALBERT, AB

Figure B-18. Joint Filler, Test No. HNTBR-1 (Item No. e5)

Pecora 301 NS

Non-Sag Silicone Highway & Pavement Joint Sealant

Specification Data Sheet

PECORA CORPORATION
Architectural/Weatherproofing Products
USA - since 1982

1. BASIC USES

Sealing of transverse contraction and expansion joints, longitudinal, centerline and shoulder joints in Portland cement concrete (PCC) and asphalt.

2. MANUFACTURER

Pecora Corporation
165 Wambold Road
Harleysville, PA 19438
Phone: 215-723-6051
800-523-6688
Fax: 215-721-0286
Website: www.pecora.com

3. PRODUCT DESCRIPTION

Pecora 301 NS Silicone Pavement Sealant is a one part, ultra low modulus product designed for sealing joints in concrete or asphalt pavement. It has excellent unprimed adhesion to concrete, metal and asphalt substrates, superior weather resistance and remains flexible at extremely low temperatures.

Pecora 301 NS Silicone Pavement Sealant is a non-sag product designed for applications on flat and sloped surfaces.

Advantages:

- Reduces pavement deterioration by restricting surface water penetration into underlying base and sub base layers.
- Convenient one component, neutral moisture curing system.
- Ultra low modulus resulting in high movement capability.
- Ease of application with standard automated bulk dispensing equipment such as Graco or Pyles.
- VOC compliant.
- Primerless adhesion to concrete and asphalt.
- Aids in elimination of non-compressibles entering expansion joints.

Limitations:
Pecora 301 NS Silicone Pavement Sealant should not be used:

- for continuous water immersion conditions.
- when ambient temperatures is below 40°F (4°C) or above 120°F (49°C).
- flush with traffic surface. (**Sealant must be recessed below surface.**)
- for applications requiring support of hydrostatic pressures.
- with solvents for dilution purposes.
- with concrete that is cured less than 7 days.

- with newly applied asphalt until cooled to ambient temperature (usually 24-48 hours).
- as a structural component or in longitudinal joints greater than 3/4" in width that are intended to be used as a constant travelling surface.

PACKAGING

- 30 fl. oz. (887ml) cartridges
- 20 fl. oz. (592ml) sausages
- 4.5 gallon pails (17.0L)
- 50 gallon drum (188.9L)

Color: pavement gray

| SEALANT COVERAGE CHART RECESS GUIDELINES | | | | | |
|---|---------------------------|--------------------|-----------------------------|-----------------------------|-------------------|
| Joint Width (Inches) | Sealant Depth (Inches) | Recess (Inches) | Backer Rod Diameter (in) | Minimum Joint Depth (in) | Linear ft./gal |
| 1/4 | 1/4 | 1/8 | 3/8 | 3/4 | 308 |
| 3/8 | 1/4 | 1/8 | 1/2 | 7/8 | 205 |
| 1/2 | 1/4 | 1/8 | 5/8 | 1-1/4 | 154 |
| 3/4 | 3/8 | 1/4 | 7/8 | 1-1/4 | 68 |
| 1.0 | 1/2 | 1/4 | 1-1/4 | 2 | 38 |

| TABLE 1: TYPICAL UNCURED PROPERTIES | | |
|-------------------------------------|---------|--------------------|
| Test Property | Value | Test Procedure |
| Cure Through (days) | 7 | 0.5" cross section |
| Extrusion Rate (grams/min) | 90-250 | MIL-S-8802 |
| Rheological Properties | non-sag | |
| Tack Free Time (mins) | 60 | ASTM C679 |
| VOC Content (g/L) | 50 | ASTM D3960 |

| TABLE 2: TYPICAL CURED PROPERTIES (After 7 days cure at 77°F (25°C), 50% RH) | | |
|---|-------|----------------|
| Test Property | Value | Test Procedure |
| Adhesion, minimum elongation | | ASTM D5329* |
| Asphalt | 500 | |
| Concrete | 500 | |
| Metal | 500 | |
| Elongation (%) | >1400 | ASTMD412 |
| Resilience (%) | >95 | ASTM D5329 |
| Stress @ 150% Elongation (psi) | 22 | ASTMD412 |
| Hardness, maximum | | |
| 21 day cure (Shore 00) Joint | 60 | ASTM C661 |
| Movement Capability | | |
| +100/-50%; 10 cycles | Pass | ASTM C719 |

*modified section 14

Figure B-19. Expansion Joint Sealant, Test No. HNTBR-1 (Item No. e6)

Appendix C. Vehicle Center of Gravity Determination

| | | |
|--------------------------------|----------------------------------|--------------------------------------|
| Model Year: <u>2017</u> | Test Name: <u>HNTBR-1</u> | VIN: <u>1C6RR6LTXHS514323</u> |
| Make: <u>Dodge</u> | Model: <u>Ram 1500</u> | |

Vehicle CG Determination

| Vehicle Equipment | Weight (lb) | Vertical CG (in.) | Vertical M (lb-in.) |
|-----------------------------------|-------------|-------------------|---------------------|
| Unballasted Truck (Curb) | 5264 | 28.901833 | 152139.25 |
| Hub | 19 | 15.25 | 289.75 |
| Brake activation cylinder & frame | 7 | 28 1/4 | 197.75 |
| Pneumatic tank (Nitrogen) | 23 | 27 1/2 | 632.5 |
| Strobe/Brake Battery | 5 | 26 | 130 |
| Brake Receiver/Wires | 5 | 54 | 270 |
| CG Plate including DAQ | 46 | 30 5/8 | 1408.75 |
| Battery | -39 | 42 | -1638 |
| Oil | -11 | 16 1/2 | -181.5 |
| Interior | -98 | 39 | -3822 |
| Fuel | -191 | 19 | -3629 |
| Coolant | -10 | 33 | -330 |
| Washer fluid | -3 | 37 | -111 |
| Water Ballast (In Fuel Tank) | | | 0 |
| Air bag Battery | 5 | 26 | 130 |
| Tdas | 17 | 26 | 442 |
| | | | 0 |
| | | | 145928.5 |

Note: (+) is added equipment to vehicle, (-) is removed equipment from vehicle

| | |
|-----------------------------|-----------------|
| Estimated Total Weight (lb) | <u>5039</u> |
| Vertical CG Location (in.) | <u>28.95981</u> |

Vehicle Dimensions for C.G. Calculations

| | |
|-------------------------------|--------------------------------------|
| Wheel Base: <u>140.75</u> in. | Front Track Width: <u>68.625</u> in. |
| | Rear Track Width: <u>68.5</u> in. |

| Center of Gravity | 2270P MASH Targets | Test Inertial | Difference |
|---------------------------|--------------------|---------------|------------|
| Test Inertial Weight (lb) | 5000 ± 110 | 5032 | 32.0 |
| Longitudinal CG (in.) | 63 ± 4 | 59.466316 | -3.53368 |
| Lateral CG (in.) | NA | -0.313382 | NA |
| Vertical CG (in.) | 28 or greater | 28.96 | 0.95981 |

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

| | Left | Right |
|-------|------|-------|
| Front | 1555 | 1453 |
| Rear | 1125 | 1131 |
| | | |
| FRONT | 3008 | lb |
| REAR | 2256 | lb |
| TOTAL | 5264 | lb |

| | Left | Right |
|-------|------|-------|
| Front | 1488 | 1418 |
| Rear | 1051 | 1075 |
| | | |
| FRONT | 2906 | lb |
| REAR | 2126 | lb |
| TOTAL | 5032 | lb |

Figure C-1. Vehicle Mass Distribution, Test No. HNTBR-1

Appendix D. Vehicle Deformation Records

The following figures and tables describe all occupant compartment measurements taken on the test vehicle used in full-scale crash testing herein. MASH defines intrusion as the occupant compartment being deformed and reduced in size with no penetration. Outward deformations, which are denoted as negative numbers within this appendix, are not considered as crush toward the occupant, and are not subject to evaluation by MASH criteria.

| | | | | | |
|------------------|--|--------------------|--|------------------------|--|
| Model Year: 2017 | | Test Name: HNTBR-1 | | VIN: 1C6RR6LTXHS514323 | |
| | | Make: Dodge | | Model: Ram 1500 | |

| VEHICLE DEFORMATION | | | | | | | | | | | | | |
|----------------------------------|-------|-----------------|-----------------|-----------------|------------------|------------------|------------------|-----------------------|-----------------------|-----------------------|---------------|--------------------------|-----------------------------------|
| PASSENGER SIDE FLOOR PAN - SET 1 | | | | | | | | | | | | | |
| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX ^A (in.) | ΔY ^A (in.) | ΔZ ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
| TOE PAN - WHEEL WELL (X, Z) | 1 | 34.6283 | -6.8382 | 0.0000 | 34.2294 | -7.1555 | | 0.3989 | -0.3173 | | NA | NA | X, Z |
| | 2 | 37.1975 | -3.7676 | 0.0000 | 28.6616 | -44.4173 | | 8.5359 | -40.6497 | | NA | No Data | X, Z |
| | 3 | 40.9450 | -2.9387 | 0.0000 | 26.6542 | -45.0397 | | 14.2908 | -42.1010 | | NA | No Data | X, Z |
| | 4 | 44.9446 | -3.0245 | 0.0000 | 36.0955 | -8.7948 | | 8.8491 | -5.7703 | | NA | NA | X, Z |
| | 5 | 49.1562 | -4.7291 | 0.0000 | 38.8020 | -11.0080 | | 10.3542 | -6.2789 | | NA | NA | X, Z |
| | 6 | 30.9834 | -5.6677 | 0.0000 | 30.0330 | -7.2325 | | 0.9504 | -1.5648 | | NA | NA | X, Z |
| | 7 | 34.7572 | -3.3744 | 0.0000 | 33.5831 | -4.4074 | | 1.1741 | -1.0330 | | NA | NA | X, Z |
| | 8 | 39.6091 | -0.2123 | 0.0000 | 21.7519 | -46.9958 | | 17.8572 | -46.7835 | | NA | No Data | X, Z |
| | 9 | 44.3116 | -0.1149 | 0.0000 | 24.8171 | -43.4117 | | 19.4945 | -43.2968 | | NA | No Data | X, Z |
| | 10 | 49.6969 | -0.0911 | 0.0000 | 37.7111 | -7.4751 | | 11.9858 | -7.3840 | | NA | NA | X, Z |
| FLOOR PAN (Z) | 11 | 30.5309 | -3.3790 | 0.0000 | 28.0977 | -4.4101 | | 2.4332 | -1.0311 | | NA | | Z |
| | 12 | 34.5631 | -0.1294 | 0.0000 | 25.8412 | -34.0492 | | 8.7219 | -33.9198 | | NA | No Data | Z |
| | 13 | 38.8103 | 1.0368 | 0.0000 | 27.3256 | -32.6122 | | 11.4847 | 33.6490 | | NA | No Data | Z |
| | 14 | 44.5867 | 1.0597 | 0.0000 | 27.6542 | -32.2440 | | 16.9325 | 33.3037 | | NA | No Data | Z |
| | 15 | 48.6031 | 1.1536 | 0.0000 | 39.0098 | -4.2249 | | 9.5933 | 5.3785 | | NA | | Z |
| | 16 | 29.8357 | -1.5679 | 0.0000 | 28.4890 | -2.6868 | | 1.3467 | -1.1189 | | NA | | Z |
| | 17 | 33.1920 | 1.0320 | 0.0000 | 34.7974 | -27.9448 | | -1.6054 | 28.9768 | | NA | No Data | Z |
| | 18 | 39.3200 | 1.0571 | 0.0000 | 33.1866 | -27.0560 | | 6.1334 | 28.1131 | | NA | No Data | Z |
| | 19 | 44.4828 | 1.0609 | 0.0000 | 35.8601 | -22.8640 | | 8.6227 | 23.9249 | | NA | No Data | Z |
| | 20 | 48.4132 | 1.1684 | 0.0000 | 40.9658 | -1.4744 | | 7.4474 | 2.6428 | | NA | | Z |
| | 21 | 29.4942 | -1.5141 | 0.0000 | 29.5199 | -2.5416 | | -0.0257 | -1.0275 | | NA | | Z |
| | 22 | 32.8898 | 1.1364 | 0.0000 | 33.0205 | -0.2432 | | -0.1307 | 1.3796 | | NA | | Z |
| | 23 | 38.6943 | 1.1066 | 0.0000 | 38.3670 | -1.7528 | | 0.3273 | 2.8594 | | NA | | Z |
| | 24 | 43.8995 | 1.1275 | 0.0000 | 42.5119 | -0.8357 | | 1.3876 | 1.9632 | | NA | | Z |
| | 25 | 48.8743 | 1.1419 | 0.0000 | 28.2488 | -38.6772 | | 20.6255 | 39.8191 | | NA | No Data | Z |
| | 26 | 29.5614 | -1.5277 | 0.0000 | 30.1884 | -2.3887 | | -0.6270 | -0.8610 | | NA | | Z |
| | 27 | 34.2050 | 0.3231 | 0.0000 | 34.3558 | -0.3168 | | -0.1508 | 0.6399 | | NA | | Z |
| | 28 | 39.3983 | 0.1061 | 0.0000 | 39.5161 | -0.8096 | | -0.1178 | 0.9157 | | NA | | Z |
| | 29 | 43.9499 | 0.1186 | 0.0000 | 44.0087 | -1.1572 | | -0.0588 | 1.2758 | | NA | | Z |
| | 30 | 49.0133 | 0.1000 | 0.0000 | -3.8951 | -25.4815 | | 52.9084 | 25.5815 | | NA | No Data | Z |

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



| | |
|---|--|
| Due to damage points 2-3, 8-9, 12-14, 17-19, 25, & 30 are unusable | |
| Pretest Floor Pan | Posttest Floor Pan |
|  |  |

Figure D-1. Passenger Side Floor Pan Deformation Data – Set 1, Test No. HNTBR-1

Model Year:2017

Test Name:HNTBR-1

VIN:1C6RR6LTXHS514323

Make:Dodge

Model:Ram 1500

VEHICLE DEFORMATION

PASSENGER SIDE FLOOR PAN - SET 2

| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX ^A (in.) | ΔY ^A (in.) | ΔZ ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
|-----------------------------------|-------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|--------------------------|--------------------------|--------------------------|------------------|-----------------------------|---|
| TOE PAN - WHEEL WELL (X, Z) | 1 | 59.6794 | 18.5962 | -2.3991 | 56.7822 | 18.3406 | -3.1998 | 2.8972 | 0.2556 | 0.8007 | 3.0167 | 3.0058 | X, Z |
| | 2 | 60.6310 | 21.1691 | 0.6725 | 18.8485 | 13.1526 | -40.0792 | 41.7825 | 8.0165 | 40.7517 | 58.9130 | No Data | X, Z |
| | 3 | 60.8902 | 24.9177 | 1.5010 | 18.3797 | 11.1526 | -40.7267 | 42.5105 | 13.7651 | 42.2277 | 61.4801 | No Data | X, Z |
| | 4 | 61.3180 | 28.9187 | 1.4150 | 53.3418 | 20.2142 | -4.7681 | 7.9762 | 8.7045 | 6.1831 | 13.3274 | 10.0921 | X, Z |
| | 5 | 60.8978 | 33.1285 | -0.2913 | 50.7575 | 22.9412 | -6.9080 | 10.1403 | 10.1873 | 6.6167 | 15.8236 | 12.1081 | X, Z |
| | 6 | 53.9494 | 14.9333 | -1.2378 | 52.2159 | 14.1225 | -3.2850 | 1.7335 | 0.8108 | 2.0472 | 2.8024 | 2.6825 | X, Z |
| | 7 | 54.8453 | 18.7105 | 1.0563 | 52.1908 | 17.6287 | -0.4053 | 2.6545 | 1.0818 | 1.4616 | 3.2176 | 3.0303 | X, Z |
| | 8 | 55.9262 | 23.5666 | 4.2191 | 1.0008 | 6.1921 | -42.5443 | 54.9254 | 17.3745 | 46.7634 | 74.1990 | No Data | X, Z |
| | 9 | 55.8339 | 28.2689 | 4.3153 | -2.8982 | 9.1818 | -38.8655 | 58.7321 | 19.0871 | 43.1808 | 75.3549 | No Data | X, Z |
| | 10 | 56.1048 | 33.6551 | 4.3383 | 45.8647 | 21.7711 | -3.3319 | 10.2401 | 11.8840 | 7.6702 | 17.4620 | 12.7942 | X, Z |
| FLOOR PAN (Z) | 11 | 50.4739 | 14.4703 | 1.0450 | 50.3328 | 12.1343 | -0.4692 | 0.1411 | 2.3360 | 1.5142 | 2.7874 | 1.5142 | Z |
| | 12 | 51.8288 | 18.5076 | 4.2961 | 3.1268 | 10.0927 | -29.5616 | 48.7020 | 8.4149 | 33.8577 | 59.9086 | No Data | Z |
| | 13 | 52.3774 | 22.7569 | 5.4623 | 2.7968 | 11.5531 | -28.0979 | 49.5806 | 11.2038 | 33.5602 | 60.9102 | No Data | Z |
| | 14 | 52.4827 | 28.5336 | 5.4840 | 2.7171 | 11.8756 | -27.7237 | 49.7656 | 16.6580 | 33.2077 | 62.1036 | No Data | Z |
| | 15 | 52.5537 | 32.5503 | 5.5772 | 44.6641 | 23.0135 | -0.0472 | 7.8896 | 9.5368 | 5.6244 | 13.5952 | 5.6244 | Z |
| | 16 | 47.1865 | 13.7651 | 2.8507 | 46.9306 | 12.4818 | 1.3018 | 0.2559 | 1.2833 | 1.5489 | 2.0277 | 1.5489 | Z |
| | 17 | 48.1872 | 17.1252 | 5.4515 | 3.3075 | 18.9549 | -23.3225 | 44.8797 | -1.8297 | 28.7740 | 53.3430 | No Data | Z |
| | 18 | 48.3195 | 23.2537 | 5.4754 | 3.9624 | 17.3340 | -22.4666 | 44.3571 | 5.9197 | 27.9420 | 52.7575 | No Data | Z |
| | 19 | 48.7508 | 28.4178 | 5.4788 | 3.3147 | 19.9394 | -18.2258 | 45.4361 | 8.4784 | 23.7046 | 51.9445 | No Data | Z |
| | 20 | 48.5491 | 32.3477 | 5.5850 | 43.1594 | 24.9193 | 2.7516 | 5.3897 | 7.4284 | 2.8334 | 9.6051 | 2.8334 | Z |
| | 21 | 41.8000 | 13.4065 | 2.8952 | 41.6159 | 13.4831 | 1.5281 | 0.1841 | -0.0766 | 1.3671 | 1.3816 | 1.3671 | Z |
| | 22 | 41.5769 | 16.8020 | 5.5445 | 41.6653 | 16.9482 | 3.8794 | -0.0884 | -0.1462 | 1.6651 | 1.6738 | 1.6651 | Z |
| | 23 | 41.4390 | 22.6062 | 5.5132 | 40.9763 | 22.3138 | 2.4602 | 0.4627 | 0.2924 | 3.0530 | 3.1017 | 3.0530 | Z |
| | 24 | 41.5300 | 27.8116 | 5.5330 | 40.2220 | 26.4404 | 3.4500 | 1.3080 | 1.3712 | 2.0830 | 2.8160 | 2.0830 | Z |
| | 25 | 42.9424 | 32.7909 | 5.5488 | 0.0403 | 12.5554 | -34.1147 | 42.9021 | 20.2355 | 39.6635 | 61.8325 | No Data | Z |
| | 26 | 37.4289 | 13.4598 | 2.8740 | 37.3249 | 14.1273 | 1.7440 | 0.1040 | -0.6675 | 1.1300 | 1.3165 | 1.1300 | Z |
| | 27 | 37.2201 | 18.1032 | 4.7234 | 37.1990 | 18.2617 | 3.8812 | 0.0211 | -0.1585 | 0.8422 | 0.8572 | 0.8422 | Z |
| | 28 | 37.5232 | 23.2974 | 4.5057 | 37.5629 | 23.4309 | 3.4629 | -0.0397 | -0.1335 | 1.0428 | 1.0521 | 1.0428 | Z |
| | 29 | 37.6273 | 27.8494 | 4.5173 | 37.5431 | 27.9282 | 3.1844 | 0.0842 | -0.0788 | 1.3329 | 1.3379 | 1.3329 | Z |
| | 30 | 37.4951 | 32.9125 | 4.4974 | 1.9788 | -19.7782 | -21.4357 | 35.5163 | 52.6907 | 25.9331 | 68.6312 | No Data | Z |

Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Due to damage points 2-3, 8-9, 12-14, 17-19, 25, & 30 are unusable

Pretest Floor Pan

Posttest Floor Pan

Figure D-2. Passenger Side Floor Pan Deformation Data – Set 2, Test No. HNTBR-1

| | | | | | | | | | | | | | |
|---------------------------------------|-------|--------------------|--------------------|------------------------|---------------------|---------------------|---------------------|-----------------------|-----------------------|-----------------------|-------------------------|-----------------------------|---|
| Model Year: 2017 | | Test Name: HNTBR-1 | | VIN: 1C6RR6LTXHS514323 | | | | | | | | | |
| | | Make: Dodge | | Model: Ram 1500 | | | | | | | | | |
| VEHICLE DEFORMATION | | | | | | | | | | | | | |
| PASSENGER SIDE INTERIOR CRUSH - SET 1 | | | | | | | | | | | | | |
| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX^A (in.) | ΔY^A (in.) | ΔZ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
| DASH (X, Y, Z) | 1 | 46.1303 | 20.9117 | -30.8991 | 44.9173 | 20.1409 | -31.9748 | 1.2130 | 0.7708 | -1.0757 | 1.7952 | 1.7952 | X, Y, Z |
| | 2 | 49.2774 | 36.0297 | -30.1571 | 47.3351 | 35.4721 | -31.6238 | 1.9423 | 0.5576 | -1.4667 | 2.4969 | 2.4969 | X, Y, Z |
| | 3 | 49.5438 | 49.4135 | -29.6590 | 46.7254 | 48.8669 | -31.5042 | 2.8184 | 0.5466 | -1.8452 | 3.4128 | 3.4128 | X, Y, Z |
| | 4 | 43.3421 | 21.6144 | -20.2152 | 40.6863 | 21.1551 | -21.7037 | 2.6558 | 0.4593 | -1.4885 | 3.0789 | 3.0789 | X, Y, Z |
| | 5 | 45.6565 | 38.2316 | -20.4787 | 42.6534 | 37.0375 | -22.4899 | 3.0031 | 1.1941 | -2.0112 | 3.8065 | 3.8065 | X, Y, Z |
| | 6 | 46.7121 | 50.2547 | -20.1757 | 42.3116 | 49.2129 | -22.6437 | 4.4005 | 1.0418 | -2.4680 | 5.1518 | 5.1518 | X, Y, Z |
| SIDE PANEL (Y) | 7 | 55.7826 | 51.9105 | -10.5619 | 48.3338 | 43.8914 | -13.2715 | 7.4488 | 8.0191 | -2.7096 | 11.2753 | 8.0191 | Y |
| | 8 | 55.5094 | 51.9094 | -3.4563 | 47.0756 | 40.0055 | -7.2327 | 8.4338 | 11.9039 | -3.7764 | 15.0696 | 11.9039 | Y |
| | 9 | 60.0648 | 51.7271 | -7.1702 | 51.5480 | 41.4193 | -10.3244 | 8.5168 | 10.3078 | -3.1542 | 13.7381 | 10.3078 | Y |
| IMPACT SIDE DOOR (Y) | 10 | 45.9721 | 53.3625 | -26.6047 | 42.7463 | 59.1036 | -26.6437 | 3.2258 | -5.7411 | -0.0390 | 6.5854 | -5.7411 | Y |
| | 11 | 34.6387 | 53.6728 | -26.8670 | 31.6462 | 58.2875 | -27.7972 | 2.9925 | -4.6147 | -0.9302 | 5.5782 | -4.6147 | Y |
| | 12 | 21.6159 | 54.0449 | -27.0125 | 19.1348 | 56.5343 | -27.9481 | 2.4811 | -2.4894 | -0.9356 | 3.6371 | -2.4894 | Y |
| | 13 | 42.0019 | 55.1108 | -5.1116 | 35.6022 | 55.2495 | -6.1210 | 6.3997 | -0.1387 | -1.0094 | 6.4803 | -0.1387 | Y |
| | 14 | 34.5653 | 54.9492 | -3.2989 | 28.2402 | 57.1190 | -4.9128 | 6.3251 | -2.1698 | -1.6139 | 6.8789 | -2.1698 | Y |
| | 15 | 21.6514 | 54.5671 | -7.7269 | 18.9227 | 58.3607 | -9.4285 | 2.7287 | -3.7936 | -1.7016 | 4.9732 | -3.7936 | Y |
| ROOF - (Z) | 16 | 42.0888 | 21.1023 | -46.9817 | 41.7629 | 21.3703 | -47.4826 | 0.3259 | -0.2680 | -0.5009 | 0.6549 | -0.5009 | Z |
| | 17 | 40.6675 | 34.3895 | -46.7899 | 40.2029 | 34.6522 | -47.6441 | 0.4646 | -0.2627 | -0.8542 | 1.0072 | -0.8542 | Z |
| | 18 | 38.1686 | 44.3840 | -46.1709 | 37.6549 | 44.6488 | -47.3222 | 0.5137 | -0.2648 | -1.1513 | 1.2882 | -1.1513 | Z |
| | 19 | 32.1853 | 22.4173 | -50.3309 | 31.8784 | 22.5189 | -50.9674 | 0.3069 | -0.1016 | -0.6365 | 0.7139 | -0.6365 | Z |
| | 20 | 31.6426 | 30.4965 | -50.2043 | 31.2649 | 30.6284 | -51.0020 | 0.3777 | -0.1319 | -0.7977 | 0.8924 | -0.7977 | Z |
| | 21 | 30.1140 | 41.0119 | -49.7121 | 29.6035 | 41.1950 | -50.7759 | 0.5105 | -0.1831 | -1.0638 | 1.1941 | -1.0638 | Z |
| | 22 | 15.8247 | 23.5973 | -51.4759 | 15.5146 | 23.5362 | -52.0805 | 0.3101 | 0.0611 | -0.6046 | 0.6822 | -0.6046 | Z |
| | 23 | 15.7334 | 32.6578 | -51.2227 | 15.2857 | 32.6064 | -52.0842 | 0.4477 | 0.0514 | -0.8615 | 0.9722 | -0.8615 | Z |
| | 24 | 15.8742 | 41.3566 | -50.6662 | 15.3457 | 41.2833 | -51.4617 | 0.5285 | 0.0733 | -0.7955 | 0.9579 | -0.7955 | Z |
| | 25 | -4.9722 | 22.5199 | -51.6843 | -5.4013 | 22.2275 | -52.1641 | 0.4291 | 0.2924 | -0.4798 | 0.7070 | -0.4798 | Z |
| | 26 | -5.0146 | 31.8246 | -51.5320 | -5.4752 | 31.5497 | -52.1272 | 0.4606 | 0.2749 | -0.5952 | 0.8012 | -0.5952 | Z |
| | 27 | -4.8418 | 41.7295 | -51.0400 | -5.4343 | 41.4412 | -51.7441 | 0.5925 | 0.2883 | -0.7041 | 0.9643 | -0.7041 | Z |
| | 28 | -21.8418 | 23.1315 | -51.1232 | -22.3068 | 22.7379 | -51.4773 | 0.4650 | 0.3936 | -0.3541 | 0.7047 | -0.3541 | Z |
| | 29 | -21.5876 | 32.3738 | -51.0002 | -22.1483 | 31.9756 | -51.4740 | 0.5607 | 0.3982 | -0.4738 | 0.8351 | -0.4738 | Z |
| | 30 | -21.0668 | 42.4851 | -50.6133 | -21.6971 | 42.0790 | -51.1897 | 0.6303 | 0.4061 | -0.5764 | 0.9457 | -0.5764 | Z |
| A-PILLAR Maximum (X, Y, Z) | 31 | 52.9063 | 50.3056 | -33.3799 | 50.9249 | 50.7606 | -33.2933 | 1.9814 | -0.4550 | 0.0866 | 2.0348 | 1.9833 | X, Z |
| | 32 | 50.0415 | 49.0085 | -35.5712 | 48.4866 | 49.2874 | -35.8000 | 1.5549 | -0.2789 | -0.2288 | 1.5962 | 1.5549 | X |
| | 33 | 47.7846 | 48.1451 | -36.6944 | 46.3250 | 48.4611 | -37.1255 | 1.4596 | -0.3160 | -0.4311 | 1.5544 | 1.4596 | X |
| | 34 | 44.3807 | 47.7281 | -39.5964 | 43.2182 | 48.0719 | -40.3294 | 1.1625 | -0.3438 | -0.7330 | 1.4166 | 1.1625 | X |
| | 35 | 41.1245 | 46.6748 | -41.1903 | 40.1195 | 47.0245 | -42.2224 | 1.0050 | -0.3497 | -1.0321 | 1.4824 | 1.0050 | X |
| | 36 | 38.6190 | 46.8857 | -44.2027 | 37.9881 | 47.1889 | -45.3609 | 0.6309 | -0.3032 | -1.1582 | 1.3533 | 0.6309 | X |
| A-PILLAR Lateral (Y) | 31 | 52.9063 | 50.3056 | -33.3799 | 50.9249 | 50.7606 | -33.2933 | 1.9814 | -0.4550 | 0.0866 | 2.0348 | -0.4550 | Y |
| | 32 | 50.0415 | 49.0085 | -35.5712 | 48.4866 | 49.2874 | -35.8000 | 1.5549 | -0.2789 | -0.2288 | 1.5962 | -0.2789 | Y |
| | 33 | 47.7846 | 48.1451 | -36.6944 | 46.3250 | 48.4611 | -37.1255 | 1.4596 | -0.3160 | -0.4311 | 1.5544 | -0.3160 | Y |
| | 34 | 44.3807 | 47.7281 | -39.5964 | 43.2182 | 48.0719 | -40.3294 | 1.1625 | -0.3438 | -0.7330 | 1.4166 | -0.3438 | Y |
| | 35 | 41.1245 | 46.6748 | -41.1903 | 40.1195 | 47.0245 | -42.2224 | 1.0050 | -0.3497 | -1.0321 | 1.4824 | -0.3497 | Y |
| | 36 | 38.6190 | 46.8857 | -44.2027 | 37.9881 | 47.1889 | -45.3609 | 0.6309 | -0.3032 | -1.1582 | 1.3533 | -0.3032 | Y |
| B-PILLAR Maximum (X, Y, Z) | 37 | 14.4012 | 47.1759 | -45.7805 | 13.8813 | 47.2248 | -46.6408 | 0.5199 | -0.0489 | -0.8603 | 1.0064 | 0.5199 | X |
| | 38 | 11.4054 | 48.8463 | -41.3177 | 10.9493 | 48.8553 | -42.1572 | 0.4561 | -0.0090 | -0.8395 | 0.9554 | 0.4561 | X |
| | 39 | 14.8776 | 50.6679 | -36.1135 | 14.4241 | 50.8012 | -37.0100 | 0.4535 | -0.1333 | -0.8965 | 1.0135 | 0.4535 | X |
| | 40 | 11.9306 | 51.9339 | -29.7208 | 11.4852 | 52.0392 | -30.6014 | 0.4454 | -0.1053 | -0.8806 | 0.9924 | 0.4454 | X |
| B-PILLAR Lateral (Y) | 37 | 14.4012 | 47.1759 | -45.7805 | 13.8813 | 47.2248 | -46.6408 | 0.5199 | -0.0489 | -0.8603 | 1.0064 | -0.0489 | Y |
| | 38 | 11.4054 | 48.8463 | -41.3177 | 10.9493 | 48.8553 | -42.1572 | 0.4561 | -0.0090 | -0.8395 | 0.9554 | -0.0090 | Y |
| | 39 | 14.8776 | 50.6679 | -36.1135 | 14.4241 | 50.8012 | -37.0100 | 0.4535 | -0.1333 | -0.8965 | 1.0135 | -0.1333 | Y |
| | 40 | 11.9306 | 51.9339 | -29.7208 | 11.4852 | 52.0392 | -30.6014 | 0.4454 | -0.1053 | -0.8806 | 0.9924 | -0.1053 | Y |

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure D-3. Occupant Compartment Deformation Data - Passenger Side – Set 1, Test No. HNTBR-1

| Model Year: 2017 | | Test Name: HNTBR-1 | | VIN: 1C6RR6LTXHS514323 | | | | | | | | | |
|---------------------------------------|-------|--------------------|--------------------|------------------------|---------------------|---------------------|---------------------|--------------------------|--------------------------|--------------------------|------------------|-----------------------------|---|
| | | Make: Dodge | | Model: Ram 1500 | | | | | | | | | |
| VEHICLE DEFORMATION | | | | | | | | | | | | | |
| PASSENGER SIDE INTERIOR CRUSH - SET 2 | | | | | | | | | | | | | |
| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX ^A (in.) | ΔY ^A (in.) | ΔZ ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
| DASH (X, Y, Z) | 1 | 45.0548 | 4.8990 | -26.4950 | 43.4868 | 4.5872 | -28.0633 | 1.5680 | 0.3118 | -1.5683 | 2.2395 | 2.2395 | X, Y, Z |
| | 2 | 48.1159 | 20.0348 | -25.7557 | 45.8205 | 19.9255 | -27.5099 | 2.2954 | 0.1093 | -1.7542 | 2.8910 | 2.8910 | X, Y, Z |
| | 3 | 48.3064 | 33.4201 | -25.2636 | 45.1352 | 33.3131 | -27.1802 | 3.1712 | 0.1070 | -1.9166 | 3.7069 | 3.7069 | X, Y, Z |
| | 4 | 42.2480 | 5.5910 | -15.8153 | 39.3768 | 5.4215 | -17.7270 | 2.8712 | 0.1695 | -1.9117 | 3.4536 | 3.4536 | X, Y, Z |
| | 5 | 44.4693 | 22.2209 | -16.0834 | 41.2427 | 21.3253 | -18.2968 | 3.2266 | 0.8956 | -2.2134 | 4.0140 | 4.0140 | X, Y, Z |
| | 6 | 45.4569 | 34.2498 | -15.7847 | 40.8290 | 33.4993 | -18.2621 | 4.6279 | 0.7505 | -2.4774 | 5.3027 | 5.3027 | X, Y, Z |
| SIDE PANEL (Y) | 7 | 54.5047 | 35.9611 | -6.1592 | 46.9967 | 28.0732 | -9.0458 | 7.5080 | 7.8879 | -2.8866 | 11.2659 | 7.8879 | Y |
| | 8 | 54.2216 | 35.9617 | 0.9461 | 45.8354 | 24.0894 | -3.0516 | 8.3862 | 11.8723 | -3.9977 | 15.0752 | 11.8723 | Y |
| | 9 | 58.7832 | 35.8034 | -2.7615 | 50.2611 | 25.5761 | -6.1761 | 8.5221 | 10.2273 | -3.4146 | 13.7435 | 10.2273 | Y |
| IMPACT SIDE DOOR (Y) | 10 | 44.7083 | 37.3504 | -22.2162 | 41.1574 | 43.4516 | -22.1170 | 3.5509 | -6.1012 | 0.0992 | 7.0600 | -6.1012 | Y |
| | 11 | 33.3738 | 37.5969 | -22.4943 | 30.0488 | 42.5871 | -23.1468 | 3.3250 | -4.9902 | -0.6525 | 6.0319 | -4.9902 | Y |
| | 12 | 20.3493 | 37.8957 | -22.6578 | 17.5468 | 40.7621 | -23.1712 | 2.8025 | -2.8664 | -0.5134 | 4.0415 | -2.8664 | Y |
| | 13 | 40.6987 | 39.0864 | -0.7294 | 34.2889 | 39.2465 | -1.5691 | 6.4098 | -0.1601 | -0.8397 | 6.4665 | -0.1601 | Y |
| | 14 | 33.2607 | 38.8839 | 1.0732 | 26.9317 | 41.0537 | -0.2428 | 6.3290 | -2.1698 | -1.3160 | 6.8188 | -2.1698 | Y |
| | 15 | 20.3552 | 38.4271 | -3.3725 | 17.5523 | 42.3080 | -4.6250 | 2.8029 | -3.8809 | -1.2525 | 4.9484 | -3.8809 | Y |
| ROOF - (Z) | 16 | 41.0345 | 5.0594 | -42.5832 | 40.1346 | 6.0313 | -43.5110 | 0.8999 | -0.9719 | -0.9278 | 1.6172 | -0.9278 | Z |
| | 17 | 39.5384 | 18.3385 | -42.3996 | 38.4963 | 19.3047 | -43.4524 | 1.0421 | -0.9662 | -1.0528 | 1.7686 | -1.0528 | Z |
| | 18 | 36.9824 | 28.3190 | -41.7889 | 35.8950 | 29.2800 | -42.9481 | 1.0874 | -0.9610 | -1.1592 | 1.8573 | -1.1592 | Z |
| | 19 | 31.1284 | 6.3171 | -45.9467 | 30.2015 | 7.1736 | -46.8569 | 0.9269 | -0.8565 | -0.9102 | 1.5560 | -0.9102 | Z |
| | 20 | 30.5401 | 14.3932 | -45.8246 | 29.5410 | 15.2789 | -46.7613 | 0.9991 | -0.8857 | -0.9367 | 1.6310 | -0.9367 | Z |
| | 21 | 28.9518 | 24.9001 | -45.3396 | 27.8217 | 25.8308 | -46.3550 | 1.1301 | -0.9307 | -1.0154 | 1.7817 | -1.0154 | Z |
| | 22 | 14.7631 | 7.4047 | -47.1148 | 13.8196 | 8.1103 | -47.7543 | 0.9435 | -0.7056 | -0.6395 | 1.3405 | -0.6395 | Z |
| | 23 | 14.6205 | 16.4647 | -46.8660 | 13.5385 | 17.1780 | -47.6179 | 1.0820 | -0.7133 | -0.7519 | 1.4983 | -0.7519 | Z |
| | 24 | 14.7117 | 25.1643 | -46.3135 | 13.5563 | 25.8447 | -46.8649 | 1.1554 | -0.6804 | -0.5514 | 1.4498 | -0.5514 | Z |
| | 25 | -6.0272 | 6.2104 | -47.3513 | -7.0879 | 6.6788 | -47.6019 | 1.0607 | -0.4684 | -0.2506 | 1.1863 | -0.2506 | Z |
| | 26 | -6.1220 | 15.5147 | -47.2035 | -7.2149 | 15.9988 | -47.4230 | 1.0929 | -0.4841 | -0.2195 | 1.2153 | -0.2195 | Z |
| | 27 | -6.0056 | 25.4207 | -46.7160 | -7.2263 | 25.8834 | -46.8908 | 1.2207 | -0.4627 | -0.1748 | 1.3171 | -0.1748 | Z |
| | 28 | -22.9007 | 6.7274 | -46.8138 | -23.9862 | 7.0784 | -46.7007 | 1.0855 | -0.3510 | 0.1131 | 1.1464 | 0.1131 | Z |
| | 29 | -22.6986 | 15.9710 | -46.6948 | -23.8809 | 16.3157 | -46.5596 | 1.1823 | -0.3447 | 0.1352 | 1.2389 | 0.1352 | Z |
| | 30 | -22.2351 | 26.0852 | -46.3119 | -23.4844 | 26.4162 | -46.1279 | 1.2493 | -0.3310 | 0.1840 | 1.3054 | 0.1840 | Z |
| A-PILLAR Maximum (X, Y, Z) | 31 | 51.6689 | 34.3294 | -28.9804 | 49.3014 | 35.2585 | -28.9916 | 2.3675 | -0.9291 | -0.0112 | 2.5433 | 2.3675 | X |
| | 32 | 48.8145 | 33.0152 | -31.1750 | 46.8409 | 33.8088 | -31.4903 | 1.9736 | -0.7936 | -0.3153 | 2.1504 | 1.9736 | X |
| | 33 | 46.5641 | 32.1385 | -32.3009 | 44.6680 | 32.9897 | -32.8016 | 1.8961 | -0.8512 | -0.5007 | 2.1379 | 1.8961 | X |
| | 34 | 43.1666 | 31.7011 | -35.2074 | 41.5242 | 32.6303 | -35.9729 | 1.6424 | -0.9292 | -0.7655 | 2.0364 | 1.6424 | X |
| | 35 | 39.9186 | 30.6288 | -36.8053 | 38.4086 | 31.5932 | -37.8434 | 1.5100 | -0.9644 | -1.0381 | 2.0707 | 1.5100 | X |
| | 36 | 37.4161 | 30.8242 | -39.8212 | 36.2377 | 31.7922 | -40.9528 | 1.1784 | -0.9680 | -1.1316 | 1.8990 | 1.1784 | X |
| A-PILLAR Lateral (Y) | 31 | 51.6689 | 34.3294 | -28.9804 | 49.3014 | 35.2585 | -28.9916 | 2.3675 | -0.9291 | -0.0112 | 2.5433 | -0.9291 | Y |
| | 32 | 48.8145 | 33.0152 | -31.1750 | 46.8409 | 33.8088 | -31.4903 | 1.9736 | -0.7936 | -0.3153 | 2.1504 | -0.7936 | Y |
| | 33 | 46.5641 | 32.1385 | -32.3009 | 44.6680 | 32.9897 | -32.8016 | 1.8961 | -0.8512 | -0.5007 | 2.1379 | -0.8512 | Y |
| | 34 | 43.1666 | 31.7011 | -35.2074 | 41.5242 | 32.6303 | -35.9729 | 1.6424 | -0.9292 | -0.7655 | 2.0364 | -0.9292 | Y |
| | 35 | 39.9186 | 30.6288 | -36.8053 | 38.4086 | 31.5932 | -37.8434 | 1.5100 | -0.9644 | -1.0381 | 2.0707 | -0.9644 | Y |
| | 36 | 37.4161 | 30.8242 | -39.8212 | 36.2377 | 31.7922 | -40.9528 | 1.1784 | -0.9680 | -1.1316 | 1.8990 | -0.9680 | Y |
| B-PILLAR Maximum (X, Y, Z) | 37 | 13.1993 | 30.9776 | -41.4325 | 12.1171 | 31.7041 | -41.9371 | 1.0822 | -0.7265 | -0.5046 | 1.3977 | 1.0822 | X |
| | 38 | 10.1879 | 32.6332 | -36.9746 | 9.2313 | 33.2495 | -37.3939 | 0.9566 | -0.6163 | -0.4193 | 1.2127 | 0.9566 | X |
| | 39 | 13.6427 | 34.4767 | -31.7666 | 12.7579 | 35.1383 | -32.2606 | 0.8848 | -0.6616 | -0.4940 | 1.2102 | 0.8848 | X |
| | 40 | 10.6798 | 35.7291 | -25.3785 | 9.8912 | 36.2621 | -25.7986 | 0.7886 | -0.5330 | -0.4201 | 1.0404 | 0.7886 | X |
| B-PILLAR Lateral (Y) | 37 | 13.1993 | 30.9776 | -41.4325 | 12.1171 | 31.7041 | -41.9371 | 1.0822 | -0.7265 | -0.5046 | 1.3977 | -0.7265 | Y |
| | 38 | 10.1879 | 32.6332 | -36.9746 | 9.2313 | 33.2495 | -37.3939 | 0.9566 | -0.6163 | -0.4193 | 1.2127 | -0.6163 | Y |
| | 39 | 13.6427 | 34.4767 | -31.7666 | 12.7579 | 35.1383 | -32.2606 | 0.8848 | -0.6616 | -0.4940 | 1.2102 | -0.6616 | Y |
| | 40 | 10.6798 | 35.7291 | -25.3785 | 9.8912 | 36.2621 | -25.7986 | 0.7886 | -0.5330 | -0.4201 | 1.0404 | -0.5330 | Y |

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure D-4. Occupant Compartment Deformation Data - Passenger Side – Set 2, Test No. HNTBR-1

| | | | | | |
|------------------|--|--------------------|--|------------------------|--|
| Model Year: 2017 | | Test Name: HNTBR-1 | | VIN: 1C6RR6LTXHS514323 | |
| | | Make: Dodge | | Model: Ram 1500 | |

| VEHICLE DEFORMATION | | | | | | | | | | | | | |
|-----------------------------------|-------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|-----------------------|-----------------------|-----------------------|-------------------------|-----------------------------|---|
| DRIVER SIDE FLOOR PAN - SET 1 | | | | | | | | | | | | | |
| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX^A (in.) | ΔY^A (in.) | ΔZ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
| TOE PAN - WHEEL WELL (X, Z) | 1 | 61.8218 | -10.1403 | -5.7352 | 61.8020 | -10.0477 | -5.8829 | 0.0198 | 0.0926 | 0.1477 | 0.1754 | 0.1490 | X, Z |
| | 2 | 62.9436 | -6.2632 | -4.4636 | 62.8957 | -6.1265 | -4.5981 | 0.0479 | 0.1367 | 0.1345 | 0.1977 | 0.1428 | X, Z |
| | 3 | 62.1074 | -3.0644 | -2.8220 | 62.0435 | -2.9357 | -2.8736 | 0.0639 | 0.1287 | 0.0516 | 0.1527 | 0.0821 | X, Z |
| | 4 | 62.1883 | 4.3594 | -2.8601 | 62.1564 | 4.4780 | -2.6870 | 0.0319 | -0.1186 | -0.1731 | 0.2122 | 0.0319 | X |
| | 5 | 59.7479 | 10.8749 | -5.1837 | 59.6608 | 11.0073 | -4.9285 | 0.0871 | -0.1324 | -0.2552 | 0.3004 | 0.0871 | X |
| | 6 | 56.4943 | -10.3309 | 0.1859 | 56.5150 | -10.2766 | 0.0125 | -0.0207 | 0.0543 | 0.1734 | 0.1829 | 0.1734 | Z |
| | 7 | 57.4428 | -6.0594 | -0.6638 | 57.4474 | -5.9985 | -0.7066 | -0.0046 | 0.0609 | 0.0428 | 0.0746 | 0.0428 | Z |
| | 8 | 57.6269 | 0.0378 | -0.7389 | 57.5933 | 0.1048 | -0.6896 | 0.0336 | -0.0670 | -0.0493 | 0.0897 | 0.0336 | X |
| | 9 | 57.6771 | 6.1765 | -0.7232 | 57.6163 | 6.2441 | -0.5608 | 0.0608 | -0.0676 | -0.1624 | 0.1861 | 0.0608 | X |
| | 10 | 55.8076 | 10.8596 | -3.4249 | 55.7179 | 11.0412 | -3.0929 | 0.0897 | -0.1816 | -0.3320 | 0.3889 | 0.0897 | X |
| FLOOR PAN (Z) | 11 | 52.4785 | -9.2792 | 1.3475 | 52.4854 | -9.2746 | 1.1722 | -0.0069 | 0.0046 | 0.1753 | 0.1755 | 0.1753 | Z |
| | 12 | 53.0201 | -5.7353 | 1.2434 | 53.0146 | -5.6866 | 1.1791 | 0.0055 | 0.0487 | 0.0643 | 0.0808 | 0.0643 | Z |
| | 13 | 53.2398 | 0.0949 | 1.2409 | 53.2464 | 0.1426 | 1.3329 | -0.0066 | -0.0477 | -0.0920 | 0.1038 | -0.0920 | Z |
| | 14 | 53.3234 | 6.2793 | 1.2335 | 53.3254 | 6.2927 | 1.4611 | -0.0020 | -0.0134 | -0.2276 | 0.2280 | -0.2276 | Z |
| | 15 | 52.1966 | 10.3874 | -2.0114 | 52.1303 | 10.5260 | -1.6888 | 0.0663 | -0.1386 | -0.3226 | 0.3573 | -0.3226 | Z |
| | 16 | 48.8300 | -9.2114 | 1.3410 | 48.8462 | -9.1674 | 1.1835 | -0.0162 | 0.0440 | 0.1575 | 0.1643 | 0.1575 | Z |
| | 17 | 49.2268 | -5.1543 | 1.2433 | 49.2168 | -5.1094 | 1.1935 | 0.0100 | 0.0449 | 0.0498 | 0.0678 | 0.0498 | Z |
| | 18 | 49.3319 | 0.0736 | 1.2319 | 49.3332 | 0.0903 | 1.3298 | -0.0013 | -0.0167 | -0.0979 | 0.0993 | -0.0979 | Z |
| | 19 | 49.2329 | 5.9593 | 1.2283 | 49.2036 | 5.9853 | 1.4489 | 0.0293 | -0.0260 | -0.2206 | 0.2241 | -0.2206 | Z |
| | 20 | 48.2041 | 10.3174 | -1.6643 | 48.1690 | 10.2861 | -1.3994 | 0.0351 | 0.0313 | -0.2649 | 0.2690 | -0.2649 | Z |
| | 21 | 42.3068 | -9.4769 | 1.2748 | 42.3239 | -9.4699 | 1.1591 | -0.0171 | 0.0070 | 0.1157 | 0.1172 | 0.1157 | Z |
| | 22 | 42.0653 | -4.5232 | 1.2361 | 42.0584 | -4.5361 | 1.2026 | 0.0069 | -0.0129 | 0.0335 | 0.0366 | 0.0335 | Z |
| | 23 | 42.2120 | 0.2688 | 1.2305 | 42.1771 | 0.3087 | 1.3068 | 0.0349 | -0.0399 | -0.0763 | 0.0929 | -0.0763 | Z |
| | 24 | 42.5420 | 6.1409 | 1.2438 | 42.5245 | 6.1396 | 1.4312 | 0.0175 | 0.0013 | -0.1874 | 0.1882 | -0.1874 | Z |
| | 25 | 42.6756 | 10.3031 | -1.4116 | 42.6425 | 10.3875 | -1.1280 | 0.0331 | -0.0844 | -0.2836 | 0.2977 | -0.2836 | Z |
| | 26 | 38.1637 | -9.0982 | 0.2554 | 38.2149 | -9.0607 | 0.1654 | -0.0512 | 0.0375 | 0.0900 | 0.1101 | 0.0900 | Z |
| | 27 | 38.2515 | -4.1161 | 0.2566 | 38.2231 | -4.0226 | 0.2386 | 0.0284 | 0.0935 | 0.0180 | 0.0994 | 0.0180 | Z |
| | 28 | 38.2873 | 0.2430 | 0.2438 | 38.2670 | 0.3187 | 0.2994 | 0.0203 | -0.0757 | -0.0556 | 0.0961 | -0.0556 | Z |
| | 29 | 38.1739 | 5.6702 | 0.4394 | 38.1468 | 5.6609 | 0.5826 | 0.0271 | 0.0093 | -0.1432 | 0.1460 | -0.1432 | Z |
| | 30 | 38.2900 | 10.3054 | -1.3699 | 38.2689 | 10.3863 | -1.1354 | 0.0211 | -0.0809 | -0.2345 | 0.2490 | -0.2345 | Z |

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



| Pretest Floor Pan | Posttest Floor Pan |
|---|--|
|  |  |

Figure D-5. Driver Side Floor Pan Deformation Data – Set 1, Test No. HNTBR-1

| | | | | | |
|------------------|--|--------------------|--|------------------------|--|
| Model Year: 2017 | | Test Name: HNTBR-1 | | VIN: 1C6RR6LTXHS514323 | |
| | | Make: Dodge | | Model: Ram 1500 | |

| VEHICLE DEFORMATION | | | | | | | | | | | | | |
|-------------------------------|-------|-----------------|-----------------|-----------------|------------------|------------------|------------------|-----------------------|-----------------------|-----------------------|---------------|--------------------------|-----------------------------------|
| DRIVER SIDE FLOOR PAN - SET 2 | | | | | | | | | | | | | |
| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX ^A (in.) | ΔY ^A (in.) | ΔZ ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
| TOE PAN - WHEEL WELL (X, Z) | 1 | 60.8848 | -26.0569 | -1.2869 | 60.8737 | -25.8540 | -2.6295 | 0.0111 | 0.2029 | 1.3426 | 1.3579 | 1.3426 | X, Z |
| | 2 | 61.9828 | -22.1723 | -0.0176 | 61.9585 | -21.9435 | -1.3051 | 0.0243 | 0.2288 | 1.2875 | 1.3079 | 1.2877 | X, Z |
| | 3 | 61.1263 | -18.9766 | 1.6195 | 61.1077 | -18.7819 | 0.4733 | 0.0186 | 0.1947 | 1.1462 | 1.1628 | 1.1464 | X, Z |
| | 4 | 61.1658 | -11.5525 | 1.5740 | 61.1756 | -11.3709 | 0.7595 | -0.0098 | 0.1816 | 0.8145 | 0.8346 | 0.8145 | Z |
| | 5 | 58.6928 | -5.0530 | -0.7601 | 58.6101 | -4.8283 | -1.3613 | 0.0827 | 0.2247 | 0.6012 | 0.6471 | 0.6069 | X, Z |
| | 6 | 55.5490 | -26.2712 | 4.6259 | 55.6631 | -26.1974 | 3.3280 | -0.1141 | 0.0738 | 1.2979 | 1.3050 | 1.2979 | Z |
| | 7 | 56.4751 | -21.9954 | 3.7734 | 56.5589 | -21.9040 | 2.6557 | -0.0838 | 0.0914 | 1.1177 | 1.1246 | 1.1177 | Z |
| | 8 | 56.6253 | -15.8973 | 3.6924 | 56.6660 | -15.8006 | 2.7541 | -0.0407 | 0.0967 | 0.9383 | 0.9441 | 0.9383 | Z |
| | 9 | 56.6412 | -9.7584 | 3.7020 | 56.6514 | -9.6636 | 2.9663 | -0.0102 | 0.0948 | 0.7357 | 0.7419 | 0.7357 | Z |
| | 10 | 54.7499 | -5.0885 | 0.9926 | 54.6906 | -4.8453 | 0.5238 | 0.0593 | 0.2432 | 0.4688 | 0.5314 | 0.4725 | X, Z |
| FLOOR PAN (Z) | 11 | 51.5256 | -25.2408 | 5.7802 | 51.6421 | -25.2377 | 4.5517 | -0.1165 | 0.0031 | 1.2285 | 1.2340 | 1.2285 | Z |
| | 12 | 52.0476 | -21.6940 | 5.6733 | 52.1484 | -21.6468 | 4.6008 | -0.1008 | 0.0472 | 1.0725 | 1.0783 | 1.0725 | Z |
| | 13 | 52.2348 | -15.8627 | 5.6652 | 52.3448 | -15.8188 | 4.8312 | -0.1100 | 0.0439 | 0.8340 | 0.8424 | 0.8340 | Z |
| | 14 | 52.2839 | -9.6779 | 5.6517 | 52.3861 | -9.6706 | 5.0423 | -0.1022 | 0.0073 | 0.6094 | 0.6180 | 0.6094 | Z |
| | 15 | 51.1393 | -5.5794 | 2.4009 | 51.1244 | -5.4029 | 1.9655 | 0.0149 | 0.1765 | 0.4354 | 0.4701 | 0.4354 | Z |
| | 16 | 47.8768 | -25.1933 | 5.7679 | 48.0027 | -25.1546 | 4.6100 | -0.1259 | 0.0387 | 1.1579 | 1.1654 | 1.1579 | Z |
| | 17 | 48.2511 | -21.1341 | 5.6666 | 48.3475 | -21.0948 | 4.6707 | -0.0964 | 0.0393 | 0.9959 | 1.0013 | 0.9959 | Z |
| | 18 | 48.3271 | -15.9058 | 5.6501 | 48.4323 | -15.8967 | 4.8764 | -0.1052 | 0.0091 | 0.7737 | 0.7809 | 0.7737 | Z |
| | 19 | 48.1953 | -10.0208 | 5.6404 | 48.2665 | -10.0049 | 5.0774 | -0.0712 | 0.0159 | 0.5630 | 0.5677 | 0.5630 | Z |
| | 20 | 47.1467 | -5.6713 | 2.7417 | 47.1686 | -5.6727 | 2.3013 | -0.0219 | -0.0014 | 0.4404 | 0.4409 | 0.4404 | Z |
| | 21 | 41.3553 | -25.4953 | 5.6917 | 41.4827 | -25.4995 | 4.6631 | -0.1274 | -0.0042 | 1.0286 | 1.0365 | 1.0286 | Z |
| | 22 | 41.0862 | -20.5431 | 5.6476 | 41.1862 | -20.5687 | 4.7772 | -0.1000 | -0.0256 | 0.8704 | 0.8765 | 0.8704 | Z |
| | 23 | 41.2063 | -15.7503 | 5.6373 | 41.2752 | -15.7250 | 4.9460 | -0.0689 | 0.0253 | 0.6913 | 0.6952 | 0.6913 | Z |
| | 24 | 41.5034 | -9.8765 | 5.6452 | 41.5869 | -9.8942 | 5.1455 | -0.0835 | -0.0177 | 0.4997 | 0.5069 | 0.4997 | Z |
| | 25 | 41.6181 | -5.7162 | 2.9858 | 41.6454 | -5.6114 | 2.6432 | -0.0273 | 0.1048 | 0.3426 | 0.3593 | 0.3426 | Z |
| | 26 | 37.2117 | -25.1407 | 4.6654 | 37.3590 | -25.1040 | 3.7266 | -0.1473 | 0.0367 | 0.9388 | 0.9510 | 0.9388 | Z |
| | 27 | 37.2717 | -20.1582 | 4.6617 | 37.3358 | -20.0673 | 3.8684 | -0.0641 | 0.0909 | 0.7933 | 0.8011 | 0.7933 | Z |
| | 28 | 37.2833 | -15.7990 | 4.6445 | 37.3527 | -15.7271 | 3.9878 | -0.0694 | 0.0719 | 0.6567 | 0.6643 | 0.6567 | Z |
| | 29 | 37.1393 | -10.3723 | 4.8344 | 37.2020 | -10.3901 | 4.3453 | -0.0627 | -0.0178 | 0.4891 | 0.4934 | 0.4891 | Z |
| | 30 | 37.2324 | -5.7383 | 3.0206 | 37.2722 | -5.6411 | 2.6906 | -0.0398 | 0.0972 | 0.3300 | 0.3463 | 0.3300 | Z |

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



| Pretest Floor Pan | Posttest Floor Pan |
|---|--|
|  |  |

Figure D-6. Driver Side Floor Pan Deformation Data – Set 2, Test No. HNTBR-1

| Model Year: 2017 | | Test Name: HNTBR-1 Make: Dodge | | VIN: 1C6RR6LTXHS514323 Model: Ram 1500 | | | | | | | | | |
|---|-------|-----------------------------------|--------------------|---|---------------------|---------------------|---------------------|--------------------------|--------------------------|--------------------------|------------------|-----------------------------|---|
| VEHICLE DEFORMATION DRIVER SIDE INTERIOR CRUSH - SET 1 | | | | | | | | | | | | | |
| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX ^A (in.) | ΔY ^A (in.) | ΔZ ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
| DASH (X, Y, Z) | 1 | 48.8207 | -10.4865 | -29.5464 | 48.9153 | -10.6130 | -29.7431 | -0.0946 | -0.1265 | -0.1967 | 0.2523 | 0.2523 | X, Y, Z |
| | 2 | 47.2740 | 0.4057 | -33.6677 | 47.2346 | -0.0318 | -34.1372 | 0.0394 | 0.4375 | -0.4695 | 0.6430 | 0.6430 | X, Y, Z |
| | 3 | 46.0525 | 17.6892 | -30.8582 | 45.0758 | 16.9744 | -31.7083 | 0.9767 | 0.7148 | -0.8501 | 1.4790 | 1.4790 | X, Y, Z |
| | 4 | 45.9447 | -10.8609 | -20.0142 | 45.9352 | -11.1234 | -20.2643 | 0.0095 | -0.2625 | -0.2501 | 0.3627 | 0.3627 | X, Y, Z |
| | 5 | 44.1232 | 0.4326 | -19.5130 | 43.7001 | 0.0150 | -19.8075 | 0.4231 | 0.4176 | -0.2945 | 0.6634 | 0.6634 | X, Y, Z |
| | 6 | 43.2753 | 16.7647 | -20.1723 | 41.2413 | 16.3601 | -21.3556 | 2.0340 | 0.4046 | -1.1833 | 2.3877 | 2.3877 | X, Y, Z |
| SIDE PANEL (Y) | 7 | 54.6711 | -12.4111 | -8.1718 | 54.6914 | -12.3120 | -8.3338 | -0.0203 | 0.0991 | -0.1620 | 0.1910 | 0.0991 | Y |
| | 8 | 54.5026 | -12.5339 | -3.4009 | 54.5310 | -12.4770 | -3.5456 | -0.0284 | 0.0569 | -0.1447 | 0.1581 | 0.0569 | Y |
| | 9 | 58.9020 | -12.4929 | -6.5330 | 58.9552 | -12.3611 | -6.6954 | -0.0532 | 0.1318 | -0.1624 | 0.2158 | 0.1318 | Y |
| IMPACT SIDE DOOR (Y) | 10 | 19.9049 | -13.8350 | -27.0064 | 19.9577 | -13.7455 | -27.1011 | -0.0528 | 0.0895 | -0.0947 | 0.1406 | 0.0895 | Y |
| | 11 | 30.8418 | -13.8456 | -26.7849 | 30.8954 | -13.7103 | -26.8970 | -0.0536 | 0.1353 | -0.1121 | 0.1837 | 0.1353 | Y |
| | 12 | 42.0128 | -13.8010 | -26.6440 | 42.0705 | -13.6155 | -26.7549 | -0.0577 | 0.1855 | -0.1109 | 0.2237 | 0.1855 | Y |
| | 13 | 20.5645 | -14.3385 | -7.5840 | 20.6121 | -14.3599 | -7.6992 | -0.0476 | -0.0214 | -0.1152 | 0.1265 | -0.0214 | Y |
| | 14 | 32.6503 | -15.0346 | -4.0395 | 32.7164 | -15.0118 | -4.1359 | -0.0661 | 0.0228 | -0.0964 | 0.1191 | 0.0228 | Y |
| | 15 | 40.2197 | -15.4441 | -5.2580 | 40.2583 | -15.3970 | -5.3955 | -0.0386 | 0.0471 | -0.1375 | 0.1504 | 0.0471 | Y |
| ROOF - (Z) | 16 | 37.4691 | -5.2250 | -46.0621 | 37.4004 | -4.9943 | -46.1369 | 0.0687 | 0.2307 | -0.0748 | 0.2521 | -0.0748 | Z |
| | 17 | 40.3262 | 4.8520 | -46.7031 | 40.1335 | 5.1463 | -46.9180 | 0.1927 | -0.2943 | -0.2149 | 0.4122 | -0.2149 | Z |
| | 18 | 42.0956 | 16.8720 | -46.9067 | 41.6832 | 17.1689 | -47.3846 | 0.4124 | -0.2969 | -0.4779 | 0.6976 | -0.4779 | Z |
| | 19 | 29.7180 | -3.2758 | -49.3864 | 29.6063 | -3.1667 | -49.5402 | 0.1117 | 0.1091 | -0.1538 | 0.2192 | -0.1538 | Z |
| | 20 | 30.3039 | 5.1243 | -50.0854 | 30.1284 | 5.2653 | -50.3889 | 0.1755 | -0.1410 | -0.3035 | 0.3779 | -0.3035 | Z |
| | 21 | 31.3583 | 15.4064 | -50.3779 | 31.0994 | 15.5529 | -50.8797 | 0.2589 | -0.1465 | -0.5018 | 0.5833 | -0.5018 | Z |
| | 22 | 15.3053 | -1.9748 | -50.5510 | 15.1878 | -1.9640 | -50.7163 | 0.1175 | 0.0108 | -0.1653 | 0.2031 | -0.1653 | Z |
| | 23 | 15.6364 | 8.8477 | -51.2526 | 15.4434 | 8.7725 | -51.6113 | 0.1930 | 0.0752 | -0.3587 | 0.4142 | -0.3587 | Z |
| | 24 | 15.6018 | 17.5369 | -51.4680 | 15.3067 | 17.4722 | -51.9736 | 0.2951 | 0.0647 | -0.5056 | 0.5890 | -0.5056 | Z |
| | 25 | -5.2872 | -1.7258 | -50.8835 | -5.5025 | -1.9689 | -51.0176 | 0.2153 | -0.2431 | -0.1341 | 0.3513 | -0.1341 | Z |
| | 26 | -5.2825 | 7.5941 | -51.4279 | -5.5165 | 7.3296 | -51.6796 | 0.2340 | 0.2645 | -0.2517 | 0.4337 | -0.2517 | Z |
| | 27 | -5.2816 | 17.0853 | -51.6460 | -5.6120 | 16.7913 | -52.0367 | 0.3304 | 0.2940 | -0.3907 | 0.5901 | -0.3907 | Z |
| | 28 | -21.8582 | -1.9946 | -50.4425 | -22.0262 | -2.3941 | -50.5487 | 0.1680 | -0.3995 | -0.1062 | 0.4462 | -0.1062 | Z |
| | 29 | -21.7321 | 7.9861 | -50.9269 | -21.9319 | 7.5407 | -51.1492 | 0.1998 | 0.4454 | -0.2223 | 0.5364 | -0.2223 | Z |
| | 30 | -21.9191 | 16.9386 | -51.0773 | -22.1889 | 16.5480 | -51.3944 | 0.2698 | 0.3906 | -0.3171 | 0.5709 | -0.3171 | Z |
| A-PILLAR Maximum (X, Y, Z) | 31 | 52.0910 | -10.8523 | -33.5286 | 52.0894 | -10.5820 | -33.5931 | 0.0016 | 0.2703 | -0.0645 | 0.2779 | 0.2703 | X, Y |
| | 32 | 49.2691 | -9.7432 | -35.2558 | 49.2213 | -9.4651 | -35.3338 | 0.0478 | 0.2781 | -0.0780 | 0.2928 | 0.2822 | X, Y |
| | 33 | 46.9836 | -8.7275 | -36.5946 | 46.9427 | -8.4417 | -36.6795 | 0.0409 | 0.2858 | -0.0849 | 0.3009 | 0.2887 | X, Y |
| | 34 | 43.4636 | -8.2209 | -39.5772 | 43.4180 | -7.9667 | -39.6370 | 0.0456 | 0.2542 | -0.0598 | 0.2651 | 0.2583 | X, Y |
| | 35 | 40.7081 | -7.2639 | -40.8078 | 40.6381 | -7.0354 | -40.8598 | 0.0700 | 0.2285 | -0.0520 | 0.2446 | 0.2390 | X, Y |
| | 36 | 37.8752 | -7.3637 | -43.9462 | 37.7728 | -7.1184 | -44.0333 | 0.1024 | 0.2453 | -0.0871 | 0.2797 | 0.2658 | X, Y |
| A-PILLAR Lateral (Y) | 31 | 52.0910 | -10.8523 | -33.5286 | 52.0894 | -10.5820 | -33.5931 | 0.0016 | 0.2703 | -0.0645 | 0.2779 | 0.2703 | Y |
| | 32 | 49.2691 | -9.7432 | -35.2558 | 49.2213 | -9.4651 | -35.3338 | 0.0478 | 0.2781 | -0.0780 | 0.2928 | 0.2781 | Y |
| | 33 | 46.9836 | -8.7275 | -36.5946 | 46.9427 | -8.4417 | -36.6795 | 0.0409 | 0.2858 | -0.0849 | 0.3009 | 0.2858 | Y |
| | 34 | 43.4636 | -8.2209 | -39.5772 | 43.4180 | -7.9667 | -39.6370 | 0.0456 | 0.2542 | -0.0598 | 0.2651 | 0.2542 | Y |
| | 35 | 40.7081 | -7.2639 | -40.8078 | 40.6381 | -7.0354 | -40.8598 | 0.0700 | 0.2285 | -0.0520 | 0.2446 | 0.2285 | Y |
| | 36 | 37.8752 | -7.3637 | -43.9462 | 37.7728 | -7.1184 | -44.0333 | 0.1024 | 0.2453 | -0.0871 | 0.2797 | 0.2453 | Y |
| B-PILLAR Maximum (X, Y, Z) | 37 | 13.2797 | -6.8285 | -45.9986 | 13.2091 | -6.9034 | -46.0018 | 0.0706 | -0.0749 | -0.0032 | 0.1030 | 0.0706 | X |
| | 38 | 10.6732 | -8.5499 | -41.0407 | 10.6233 | -8.6069 | -41.1181 | 0.0499 | -0.0570 | -0.0774 | 0.1083 | 0.0499 | X |
| | 39 | 14.3893 | -10.9436 | -33.7418 | 14.3679 | -10.9868 | -33.8060 | 0.0214 | -0.0432 | -0.0642 | 0.0803 | 0.0214 | X |
| | 40 | 11.0715 | -11.5300 | -29.3358 | 11.0188 | -11.5914 | -29.3783 | 0.0527 | -0.0614 | -0.0425 | 0.0914 | 0.0527 | X |
| B-PILLAR Lateral (Y) | 37 | 13.2797 | -6.8285 | -45.9986 | 13.2091 | -6.9034 | -46.0018 | 0.0706 | -0.0749 | -0.0032 | 0.1030 | -0.0749 | Y |
| | 38 | 10.6732 | -8.5499 | -41.0407 | 10.6233 | -8.6069 | -41.1181 | 0.0499 | -0.0570 | -0.0774 | 0.1083 | -0.0570 | Y |
| | 39 | 14.3893 | -10.9436 | -33.7418 | 14.3679 | -10.9868 | -33.8060 | 0.0214 | -0.0432 | -0.0642 | 0.0803 | -0.0432 | Y |
| | 40 | 11.0715 | -11.5300 | -29.3358 | 11.0188 | -11.5914 | -29.3783 | 0.0527 | -0.0614 | -0.0425 | 0.0914 | -0.0614 | Y |

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure D-7. Occupant Compartment Deformation Data - Driver Side – Set 1, Test No. HNTBR-1

Model Year: 2017

Test Name: HNTBR-1

VIN: 1C6RR6LTXHS514323

Make: Dodge

Model: Ram 1500

VEHICLE DEFORMATION

DRIVER SIDE INTERIOR CRUSH - SET 2

| | POINT | Pretest X (in.) | Pretest Y (in.) | Pretest Z (in.) | Posttest X (in.) | Posttest Y (in.) | Posttest Z (in.) | ΔX^A (in.) | ΔY^A (in.) | ΔZ^A (in.) | Total Δ (in.) | Crush ^B (in.) | Directions for Crush ^C |
|----------------------------------|-------|--------------------|--------------------|--------------------|---------------------|---------------------|---------------------|-----------------------|-----------------------|-----------------------|-------------------------|-----------------------------|---|
| DASH (X, Y, Z) | 1 | 47.9180 | -26.4960 | -25.1321 | 47.6693 | -26.2058 | -26.3493 | 0.2487 | 0.2902 | -1.2172 | 1.2758 | 1.2758 | X, Y, Z |
| | 2 | 46.3172 | -15.6157 | -29.2641 | 45.8746 | -15.5731 | -30.5705 | 0.4426 | 0.0426 | -1.3064 | 1.3800 | 1.3800 | X, Y, Z |
| | 3 | 44.9962 | 1.6629 | -26.4697 | 43.6520 | 1.3842 | -27.8722 | 1.3442 | 0.2787 | -1.4025 | 1.9625 | 1.9625 | X, Y, Z |
| | 4 | 45.0300 | -26.8791 | -15.6039 | 44.8114 | -26.8680 | -16.8421 | 0.2186 | 0.0111 | -1.2382 | 1.2574 | 1.2574 | X, Y, Z |
| | 5 | 43.1454 | -15.5954 | -15.1140 | 42.5203 | -15.7501 | -16.1986 | 0.6251 | -0.1547 | -1.0846 | 1.2614 | 1.2614 | X, Y, Z |
| | 6 | 42.2084 | 0.7313 | -15.7872 | 39.9513 | 0.6009 | -17.4823 | 2.2571 | 0.1304 | -1.6951 | 2.8258 | 2.8258 | X, Y, Z |
| SIDE PANEL (Y) | 7 | 53.7473 | -28.3720 | -3.7474 | 53.7234 | -28.1756 | -5.0401 | 0.0239 | 0.1964 | -1.2927 | 1.3078 | 0.1964 | Y |
| | 8 | 53.5724 | -28.4921 | 1.0233 | 53.6241 | -28.4095 | -0.2532 | -0.0517 | 0.0826 | -1.2765 | 1.2802 | 0.0826 | Y |
| | 9 | 57.9762 | -28.4292 | -2.1023 | 58.0076 | -28.2235 | -3.4560 | -0.0314 | 0.2057 | -1.3537 | 1.3696 | 0.2057 | Y |
| IMPACT SIDE DOOR (Y) | 10 | 19.0173 | -30.0022 | -22.6322 | 18.7650 | -29.5417 | -23.3909 | 0.2523 | 0.4605 | -0.7587 | 0.9227 | 0.4605 | Y |
| | 11 | 29.9539 | -29.9522 | -22.3945 | 29.7041 | -29.4467 | -23.3228 | 0.2498 | 0.5055 | -0.9283 | 1.0861 | 0.5055 | Y |
| | 12 | 41.1241 | -29.8459 | -22.2372 | 40.8794 | -29.2897 | -23.3189 | 0.2447 | 0.5562 | -1.0817 | 1.2407 | 0.5562 | Y |
| | 13 | 19.6510 | -30.4872 | -3.2085 | 19.6666 | -30.4279 | -4.0094 | -0.0156 | 0.0593 | -0.8009 | 0.8032 | 0.0593 | Y |
| | 14 | 31.7352 | -31.1139 | 0.3544 | 31.8182 | -31.0609 | -0.6071 | -0.0830 | 0.0530 | -0.9615 | 0.9665 | 0.0530 | Y |
| | 15 | 39.3085 | -31.4826 | -0.8526 | 39.3457 | -31.3848 | -1.9662 | -0.0372 | 0.0978 | -1.1136 | 1.1185 | 0.0978 | Y |
| ROOF - (Z) | 16 | 36.5619 | -21.3099 | -41.6686 | 35.9182 | -20.4210 | -42.5161 | 0.6437 | 0.8889 | -0.8475 | 1.3866 | -0.8475 | Z |
| | 17 | 39.3643 | -11.2177 | -42.3131 | 38.5847 | -10.2548 | -43.1864 | 0.7796 | 0.9629 | -0.8733 | 1.5158 | -0.8733 | Z |
| | 18 | 41.0676 | 0.8116 | -42.5234 | 40.0615 | 1.7819 | -43.5006 | 1.0061 | -0.9703 | -0.9772 | 1.7055 | -0.9772 | Z |
| | 19 | 28.8051 | -19.4061 | -45.0058 | 28.0719 | -18.5900 | -45.7953 | 0.7332 | 0.8161 | -0.7895 | 1.3516 | -0.7895 | Z |
| | 20 | 29.3457 | -11.0034 | -45.7104 | 28.5363 | -10.1440 | -46.5300 | 0.8094 | 0.8594 | -0.8196 | 1.4372 | -0.8196 | Z |
| | 21 | 30.3438 | -0.7158 | -46.0093 | 29.4438 | 0.1549 | -46.8860 | 0.9000 | 0.8707 | -0.8767 | 1.5286 | -0.8767 | Z |
| | 22 | 14.3872 | -18.1855 | -46.1927 | 13.6333 | -17.4536 | -46.7740 | 0.7539 | 0.7319 | -0.5813 | 1.2008 | -0.5813 | Z |
| | 23 | 14.6596 | -7.3619 | -46.9022 | 13.8178 | -6.7042 | -47.5187 | 0.8418 | 0.6577 | -0.6165 | 1.2334 | -0.6165 | Z |
| | 24 | 14.5774 | 1.3268 | -47.1243 | 13.6282 | 1.9989 | -47.7551 | 0.9492 | -0.6721 | -0.6308 | 1.3231 | -0.6308 | Z |
| | 25 | -6.2059 | -18.0505 | -46.5557 | -7.0589 | -17.5730 | -46.8169 | 0.8530 | 0.4775 | -0.2612 | 1.0119 | -0.2612 | Z |
| | 26 | -6.2518 | -8.7311 | -47.1073 | -7.1329 | -8.2663 | -47.3459 | 0.8811 | 0.4648 | -0.2386 | 1.0244 | -0.2386 | Z |
| | 27 | -6.3029 | 0.7597 | -47.3328 | -7.2855 | 1.1988 | -47.5667 | 0.9826 | -0.4391 | -0.2339 | 1.1014 | -0.2339 | Z |
| | 28 | -22.7758 | -18.4104 | -46.1390 | -23.5728 | -18.0997 | -46.1479 | 0.7970 | 0.3107 | -0.0089 | 0.8555 | -0.0089 | Z |
| | 29 | -22.7040 | -8.4296 | -46.6309 | -23.5413 | -8.1570 | -46.6076 | 0.8373 | 0.2726 | 0.0233 | 0.8809 | 0.0233 | Z |
| | 30 | -22.9403 | 0.5216 | -46.7885 | -23.8514 | 0.8512 | -46.7210 | 0.9111 | -0.3296 | 0.0675 | 0.9712 | 0.0675 | Z |
| A-PILLAR Maximum (X, Y, Z) | 31 | 51.1961 | -26.8468 | -29.1092 | 50.7945 | -26.1019 | -30.2377 | 0.4016 | 0.7449 | -1.1285 | 1.4106 | 0.8463 | X, Y |
| | 32 | 48.3707 | -25.7547 | -30.8414 | 47.8986 | -24.9769 | -31.9263 | 0.4721 | 0.7778 | -1.0849 | 1.4159 | 0.9099 | X, Y |
| | 33 | 46.0816 | -24.7526 | -32.1844 | 45.5976 | -23.9475 | -33.2287 | 0.4840 | 0.8051 | -1.0443 | 1.4046 | 0.9394 | X, Y |
| | 34 | 42.5632 | -24.2677 | -35.1725 | 42.0335 | -23.4508 | -36.1349 | 0.5297 | 0.8169 | -0.9624 | 1.3690 | 0.9736 | X, Y |
| | 35 | 39.8043 | -23.3269 | -36.4079 | 39.2332 | -22.5183 | -37.3095 | 0.5711 | 0.8086 | -0.9016 | 1.3390 | 0.9899 | X, Y |
| | 36 | 36.9767 | -23.4447 | -39.5504 | 36.3288 | -22.5726 | -40.4478 | 0.6479 | 0.8721 | -0.8974 | 1.4091 | 1.0864 | X, Y |
| A-PILLAR Lateral (Y) | 31 | 51.1961 | -26.8468 | -29.1092 | 50.7945 | -26.1019 | -30.2377 | 0.4016 | 0.7449 | -1.1285 | 1.4106 | 0.7449 | Y |
| | 32 | 48.3707 | -25.7547 | -30.8414 | 47.8986 | -24.9769 | -31.9263 | 0.4721 | 0.7778 | -1.0849 | 1.4159 | 0.7778 | Y |
| | 33 | 46.0816 | -24.7526 | -32.1844 | 45.5976 | -23.9475 | -33.2287 | 0.4840 | 0.8051 | -1.0443 | 1.4046 | 0.8051 | Y |
| | 34 | 42.5632 | -24.2677 | -35.1725 | 42.0335 | -23.4508 | -36.1349 | 0.5297 | 0.8169 | -0.9624 | 1.3690 | 0.8169 | Y |
| | 35 | 39.8043 | -23.3269 | -36.4079 | 39.2332 | -22.5183 | -37.3095 | 0.5711 | 0.8086 | -0.9016 | 1.3390 | 0.8086 | Y |
| | 36 | 36.9767 | -23.4447 | -39.5504 | 36.3288 | -22.5726 | -40.4478 | 0.6479 | 0.8721 | -0.8974 | 1.4091 | 0.8721 | Y |
| B-PILLAR Maximum (X, Y, Z) | 37 | 12.3816 | -23.0469 | -41.6395 | 11.7415 | -22.4708 | -42.1062 | 0.6401 | 0.5761 | -0.4667 | 0.9795 | 0.8612 | X, Y |
| | 38 | 9.7774 | -24.7789 | -36.6842 | 9.2268 | -24.2583 | -37.2154 | 0.5506 | 0.5206 | -0.5312 | 0.9254 | 0.7577 | X, Y |
| | 39 | 13.4958 | -27.1465 | -29.3779 | 13.0761 | -26.7202 | -29.9854 | 0.4197 | 0.4263 | -0.6075 | 0.8526 | 0.5982 | X, Y |
| | 40 | 10.1748 | -27.7477 | -24.9764 | 9.7863 | -27.4069 | -25.5253 | 0.3885 | 0.3408 | -0.5489 | 0.7539 | 0.5168 | X, Y |
| B-PILLAR Lateral (Y) | 37 | 12.3816 | -23.0469 | -41.6395 | 11.7415 | -22.4708 | -42.1062 | 0.6401 | 0.5761 | -0.4667 | 0.9795 | 0.5761 | Y |
| | 38 | 9.7774 | -24.7789 | -36.6842 | 9.2268 | -24.2583 | -37.2154 | 0.5506 | 0.5206 | -0.5312 | 0.9254 | 0.5206 | Y |
| | 39 | 13.4958 | -27.1465 | -29.3779 | 13.0761 | -26.7202 | -29.9854 | 0.4197 | 0.4263 | -0.6075 | 0.8526 | 0.4263 | Y |
| | 40 | 10.1748 | -27.7477 | -24.9764 | 9.7863 | -27.4069 | -25.5253 | 0.3885 | 0.3408 | -0.5489 | 0.7539 | 0.3408 | Y |

A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

^A Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure D-8. Occupant Compartment Deformation Data - Driver Side – Set 2, Test No. HNTBR-1

Model Year: 2017

Test Name: HNTBR-1

VIN: 1C6RR6LTXHS514323

Make: Dodge

Model: Ram 1500

Passenger Side Maximum Deformation

| Reference Set 1 | | | | Reference Set 2 | | | |
|----------------------------|---|----------------------------------|--|----------------------------|---|----------------------------------|--|
| Location | Maximum Deformation ^{A,B} (in.) | MASH Allowable Deformation (in.) | Directions of Deformation ^C | Location | Maximum Deformation ^{A,B} (in.) | MASH Allowable Deformation (in.) | Directions of Deformation ^C |
| Roof | -1.2 | ≤ 4 | Z | Roof | 0.2 | ≤ 4 | Z |
| Windshield ^D | 0.0 | ≤ 3 | X, Z | Windshield ^D | NA | ≤ 3 | X, Z |
| A-Pillar Maximum | 2.0 | ≤ 5 | X, Z | A-Pillar Maximum | 2.4 | ≤ 5 | X |
| A-Pillar Lateral | -0.5 | ≤ 3 | Y | A-Pillar Lateral | -1.0 | ≤ 3 | Y |
| B-Pillar Maximum | 0.5 | ≤ 5 | X | B-Pillar Maximum | 1.1 | ≤ 5 | X |
| B-Pillar Lateral | -0.1 | ≤ 3 | Y | B-Pillar Lateral | -0.7 | ≤ 3 | Y |
| Toe Pan - Wheel Well | 12.7 | ≤ 9 | X, Z | Toe Pan - Wheel Well | 12.8 | ≤ 9 | X, Z |
| Side Front Panel | 11.9 | ≤ 12 | Y | Side Front Panel | 11.9 | ≤ 12 | Y |
| Side Door (above seat) | -5.7 | ≤ 9 | Y | Side Door (above seat) | -6.1 | ≤ 9 | Y |
| Side Door (below seat) | -3.8 | ≤ 12 | Y | Side Door (below seat) | -3.9 | ≤ 12 | Y |
| Floor Pan | 5.4 | ≤ 12 | Z | Floor Pan | 5.6 | ≤ 12 | Z |
| Dash - no MASH requirement | 5.2 | NA | X, Y, Z | Dash - no MASH requirement | 5.3 | NA | X, Y, Z |

^A Items highlighted in red do not meet MASH allowable deformations.

^B Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^C For Toe Pan - Wheel Well the direction of deformation may include X and Z direction. For A-Pillar Maximum and B-Pillar Maximum the direction of deformation may include X, Y, and Z directions. The direction of deformation for Toe Pan -Wheel Well, A-Pillar Maximum, and B-Pillar Maximum only include components where the deformation is positive and intruding into the occupant compartment. If direction of deformation is "NA" then no intrusion is recorded and deformation will be 0.

^D If deformation is observed for the windshield then the windshield deformation is measured posttest with an exemplar vehicle, therefore only one set of reference is measured and recorded.

Notes on vehicle interior crush:

Figure D-9. Maximum Occupant Compartment Deformation by Location – Passenger Side, Test No. HNTBR-1

| | | |
|-------------------------|---|---|
| Model Year: <u>2017</u> | Test Name: <u>HNTBR-1</u> Make: <u>Dodge</u> | VIN: <u>1C6RR6LTXHS514323</u> Model: <u>Ram 1500</u> |
|-------------------------|---|---|

| Driver Side Maximum Deformation | | | | | | | |
|---------------------------------|---|----------------------------------|--|----------------------------|---|----------------------------------|--|
| Reference Set 1 | | | | Reference Set 2 | | | |
| Location | Maximum Deformation ^{A,B} (in.) | MASH Allowable Deformation (in.) | Directions of Deformation ^C | Location | Maximum Deformation ^{A,B} (in.) | MASH Allowable Deformation (in.) | Directions of Deformation ^C |
| Roof | -0.5 | ≤ 4 | Z | Roof | 0.1 | ≤ 4 | Z |
| Windshield ^D | 0.0 | ≤ 3 | X, Z | Windshield ^D | NA | ≤ 3 | X, Z |
| A-Pillar Maximum | 0.3 | ≤ 5 | X, Y | A-Pillar Maximum | 1.1 | ≤ 5 | X, Y |
| A-Pillar Lateral | 0.3 | ≤ 3 | Y | A-Pillar Lateral | 0.9 | ≤ 3 | Y |
| B-Pillar Maximum | 0.1 | ≤ 5 | X | B-Pillar Maximum | 0.9 | ≤ 5 | X, Y |
| B-Pillar Lateral | 0.3 | ≤ 3 | Y | B-Pillar Lateral | 0.6 | ≤ 3 | Y |
| Toe Pan - Wheel Well | 0.2 | ≤ 9 | Z | Toe Pan - Wheel Well | 1.3 | ≤ 9 | X, Z |
| Side Front Panel | 0.1 | ≤ 12 | Y | Side Front Panel | 0.2 | ≤ 12 | Y |
| Side Door (above seat) | 0.2 | ≤ 9 | Y | Side Door (above seat) | 0.6 | ≤ 9 | Y |
| Side Door (below seat) | 0.0 | ≤ 12 | Y | Side Door (below seat) | 0.1 | ≤ 12 | Y |
| Floor Pan | 0.2 | ≤ 12 | Z | Floor Pan | 1.2 | ≤ 12 | Z |
| Dash - no MASH requirement | 2.4 | NA | X, Y, Z | Dash - no MASH requirement | 2.4 | NA | X, Y, Z |

^A Items highlighted in red do not meet MASH allowable deformations.

^B Positive values denote deformation as inward toward the occupant compartment, negative values denote deformations outward away from the occupant compartment.

^C For Toe Pan - Wheel Well the direction of deformation may include X and Z direction. For A-Pillar Maximum and B-Pillar Maximum the direction of deformation may include X, Y, and Z directions. The direction of deformation for Toe Pan -Wheel Well, A-Pillar Maximum, and B-Pillar Maximum only include components where the deformation is positive and intruding into the occupant compartment. If direction of deformation is "NA" then no intrusion is recorded and deformation will be 0.

^D If deformation is observed for the windshield then the windshield deformation is measured posttest with an exemplar vehicle, therefore only one set of reference is measured and recorded.

Notes on vehicle interior crush:

Figure D-10. Maximum Occupant Compartment Deformation by Location – Driver Side, Test No. HNTBR-1

Test Name: HNTBR-1

VIN: 1C6RR6LTXHS514323

Model Year: 2017

Make: Dodge

Model: Ram 1500

| | in. | (mm) |
|--|---------|--------|
| Distance from C.G. to reference line - L _{REF} : | 107 1/2 | (2731) |
| Total Vehicle Width: | 78 | (1981) |
| Width of contact and induced crush - Field L: | 78 | (1981) |
| Crush measurement spacing interval (L/5) - I: | 15 5/8 | (397) |
| Distance from center of vehicle to center of Field L - D _{FL} : | 0 | () |
| Width of Contact Damage: | 78 | (1981) |
| Distance from center of vehicle to center of contact damage - D _C : | 0 | () |

NOTE: Enter "NA" for crush measurement if distance can not be measured (i.e., side of vehicle has been pushed inward)

NOTE: All values must be filled out above before crush measurements are filled out.

| Crush Measurement | in. | (mm) |
|-------------------|--------|-------|
| C ₁ | N/a | N/A |
| C ₂ | 11 | (279) |
| C ₃ | 10 1/8 | (257) |
| C ₄ | 16 1/8 | (410) |
| C ₅ | 28 | (711) |
| C ₆ | N/a | N/A |
| C _{MAX} | 33 1/4 | (845) |

| Lateral Location | in. | (mm) |
|------------------|---------|--------|
| | -39 | -(991) |
| | -23 3/8 | -(594) |
| | -7 3/4 | -(197) |
| | 7 7/8 | (200) |
| | 23 1/2 | (597) |
| | 39 1/8 | (994) |
| | 28 | (711) |

| Original Profile Measurement | in. | (mm) |
|------------------------------|--------|-------|
| | 22 1/2 | (572) |
| | 6 5/8 | (168) |
| | 4 1/4 | (108) |
| | 4 1/4 | (108) |
| | 6 1/4 | (159) |
| | 20 1/2 | (521) |
| | 8 | (203) |

| Dist. Between Ref. Lines | in. | (mm) |
|--------------------------|-------|-------|
| | 4 1/3 | (110) |

| Actual Crush | in. | (mm) |
|--------------|--------|-------|
| | N/A | N/A |
| | 0 | (2) |
| | 1 4/7 | (40) |
| | 7 4/7 | (192) |
| | 17 4/9 | (443) |
| | N/A | N/A |
| | 21 | (532) |

Figure D-11. Exterior Vehicle Crush (NASS) – Front, Test No. HNTBR-1

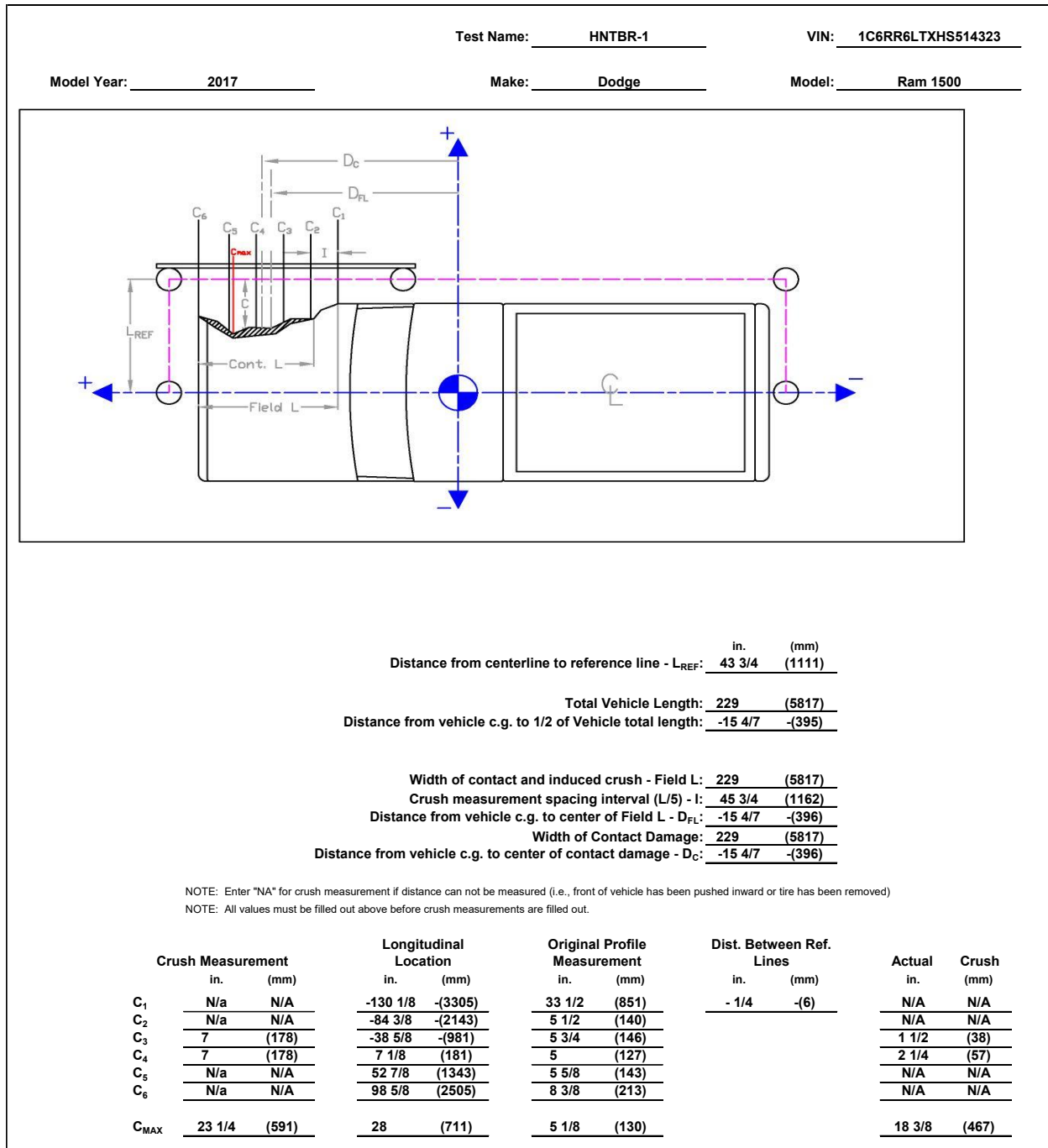


Figure D-12. Exterior Vehicle Crush (NASS) – Side, Test No. HNTBR-1

Appendix E. Accelerometer and Rate Transducer Data Plots, Test No. HNTBR-1

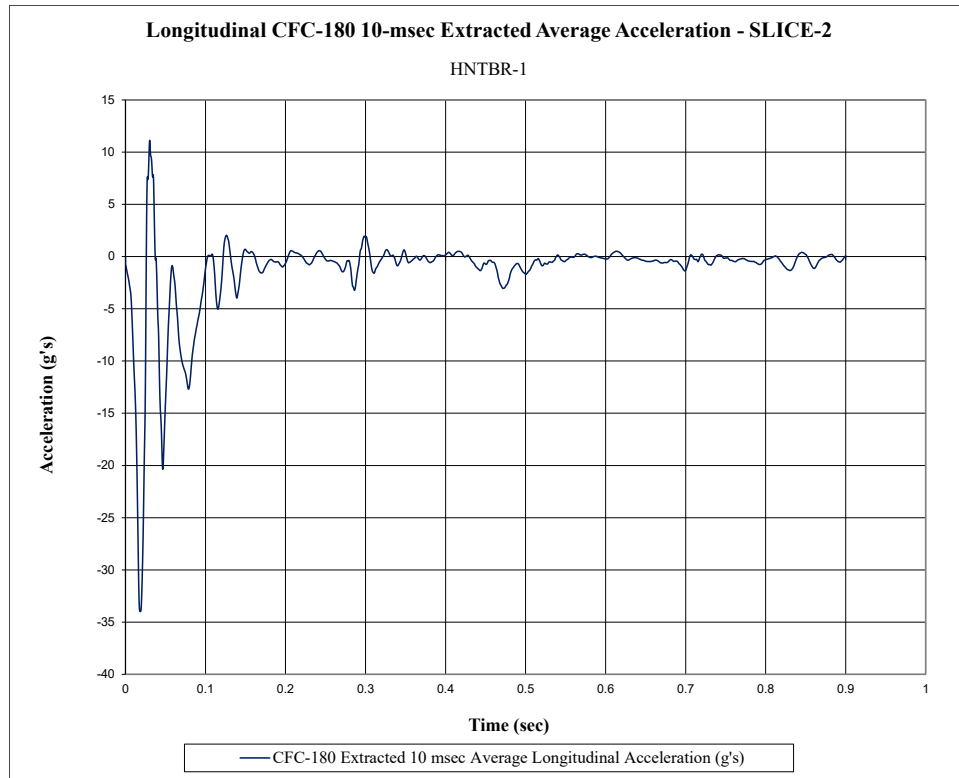


Figure E-1. 10-ms Average Longitudinal Deceleration (SLICE-2), Test No. HNTBR-1

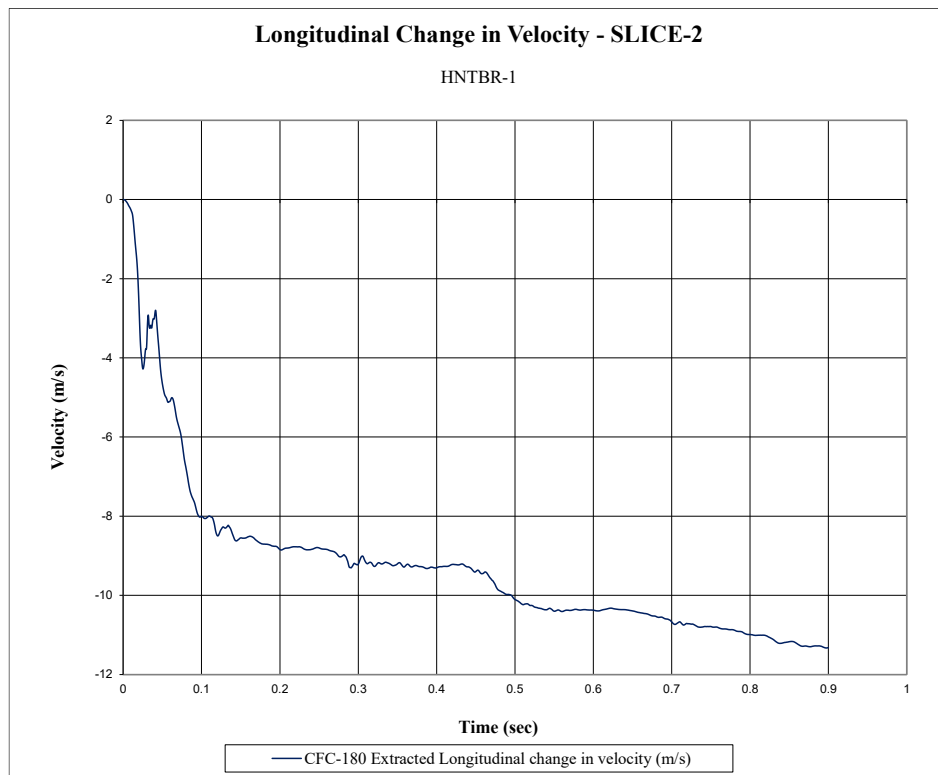


Figure E-2. Longitudinal Occupant Impact Velocity (SLICE-2), Test No. HNTBR-1

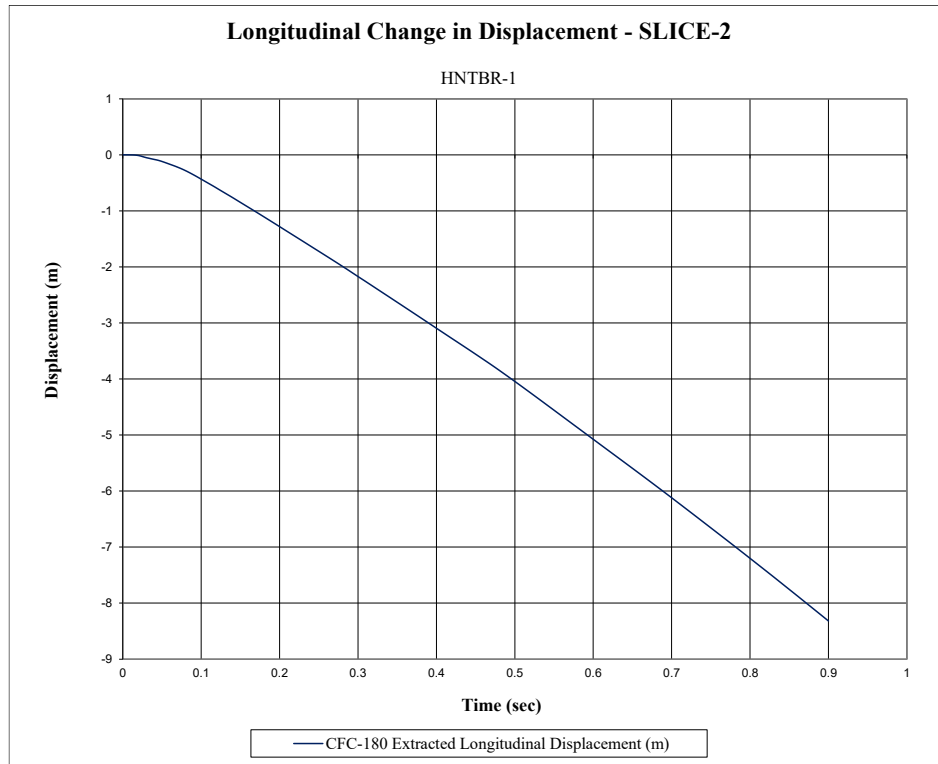


Figure E-3. Longitudinal Occupant Displacement (SLICE-2), Test No. HNTBR-1

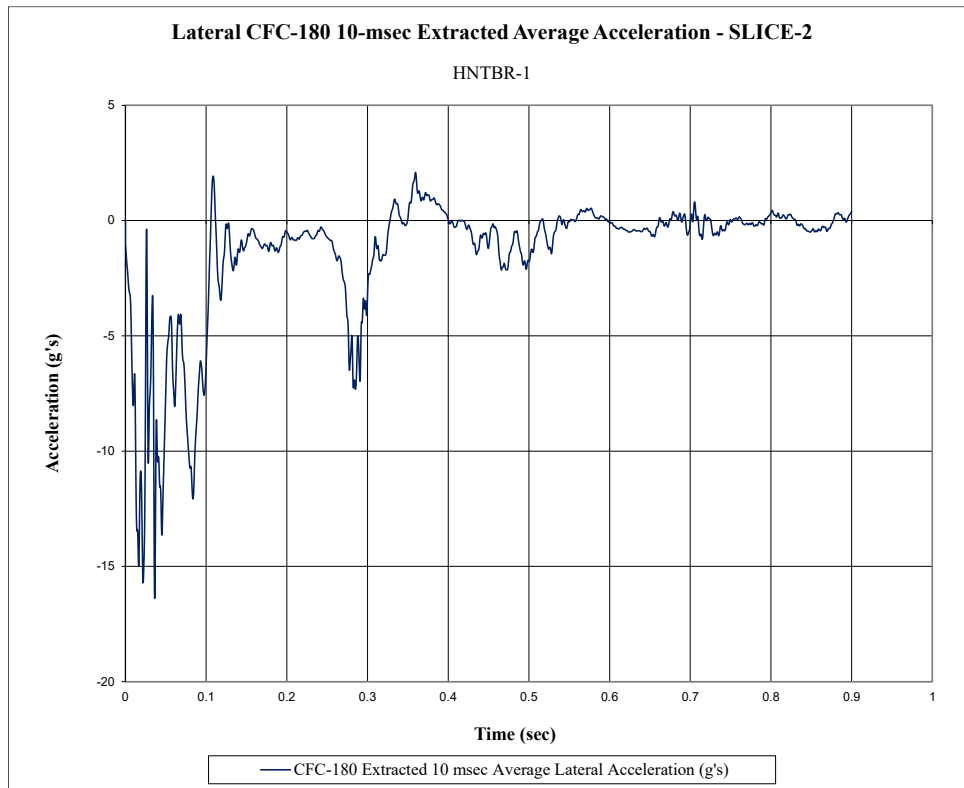


Figure E-4. 10-ms Average Lateral Deceleration (SLICE-2), Test No. HNTBR-1

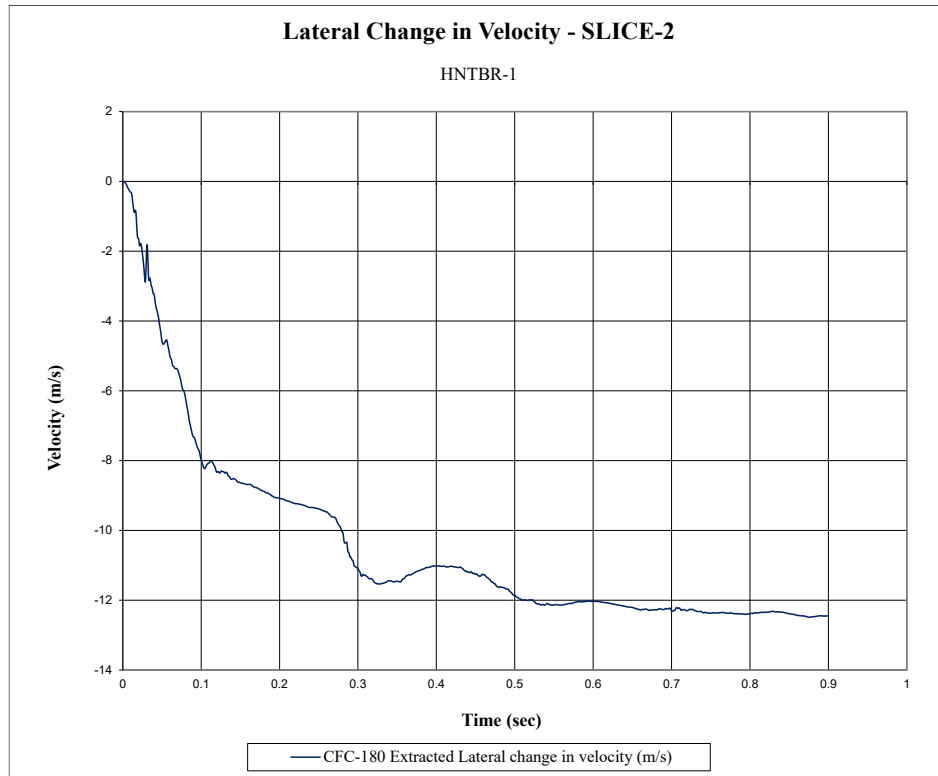


Figure E-5. Lateral Occupant Impact Velocity (SLICE-2), Test No. HNTBR-1

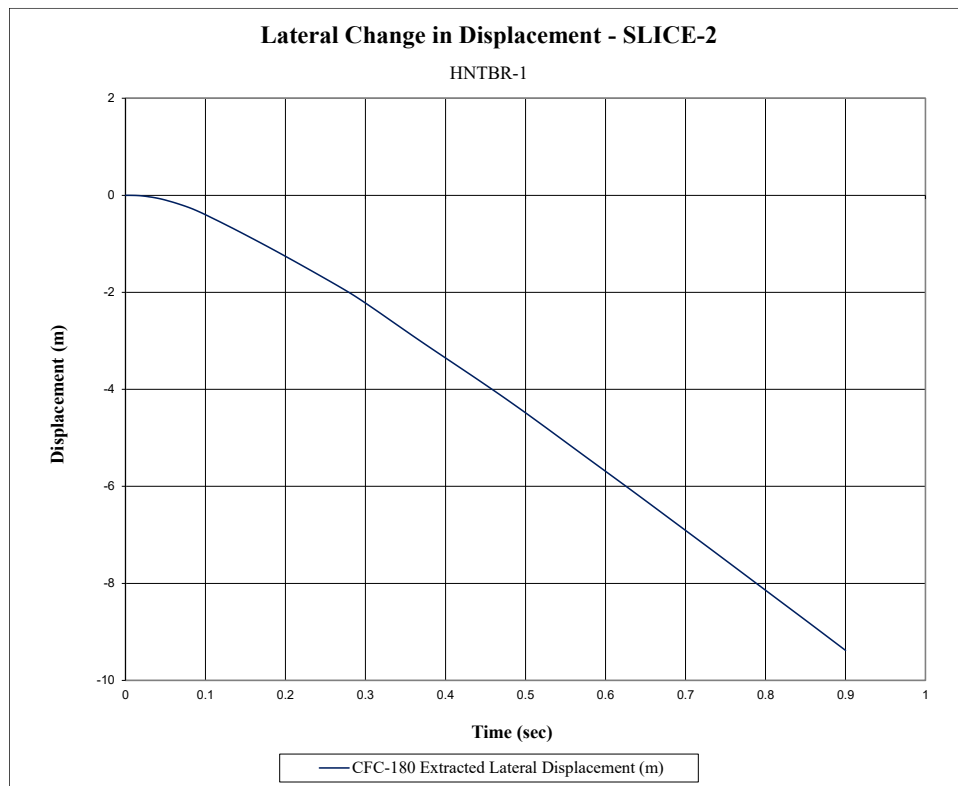


Figure E-6. Lateral Occupant Displacement (SLICE-2), Test No. HNTBR-1

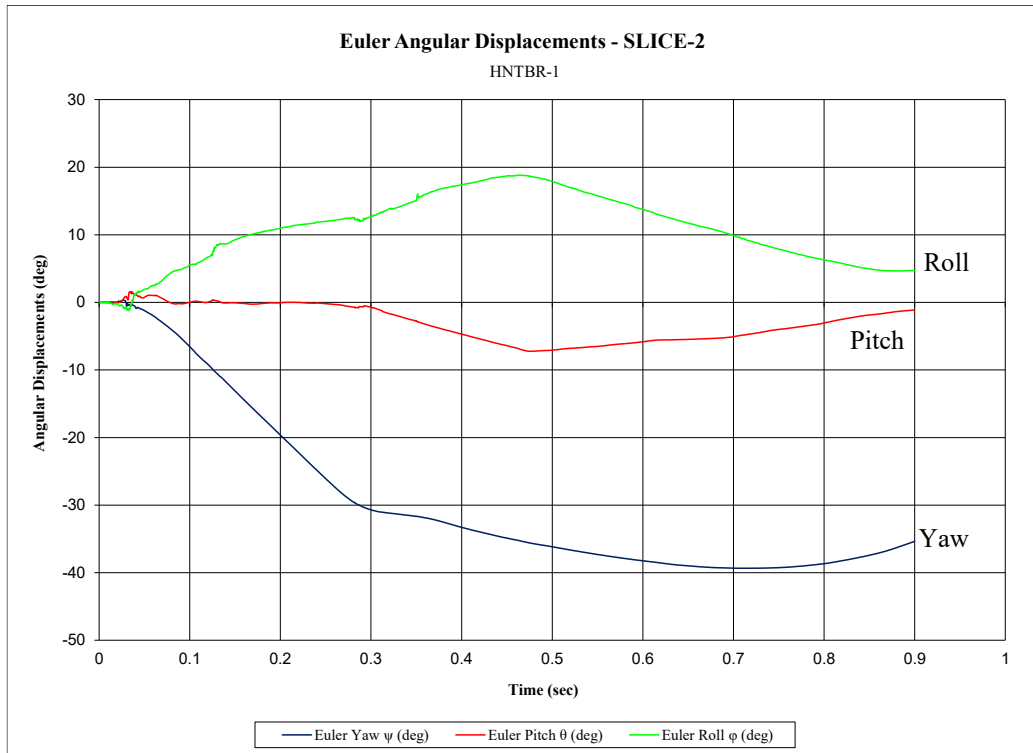


Figure E-7. Vehicle Angular Displacements (SLICE-2), Test No. HNTBR-1

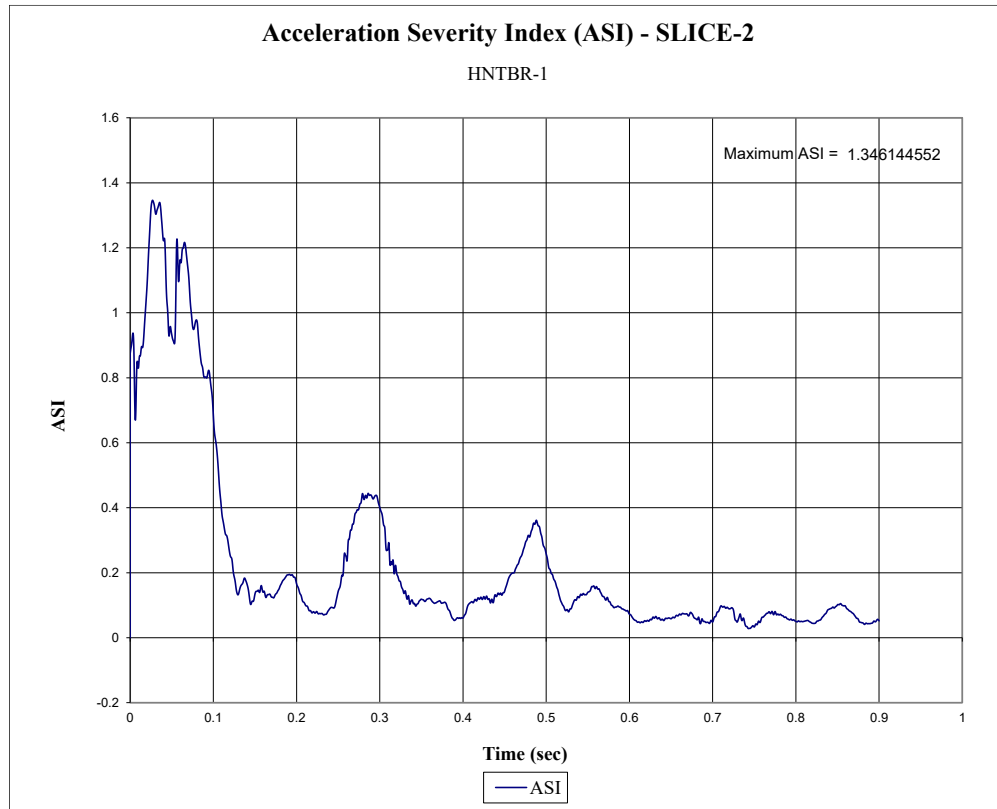


Figure E-8. Acceleration Severity Index (SLICE-2), Test No. HNTBR-1

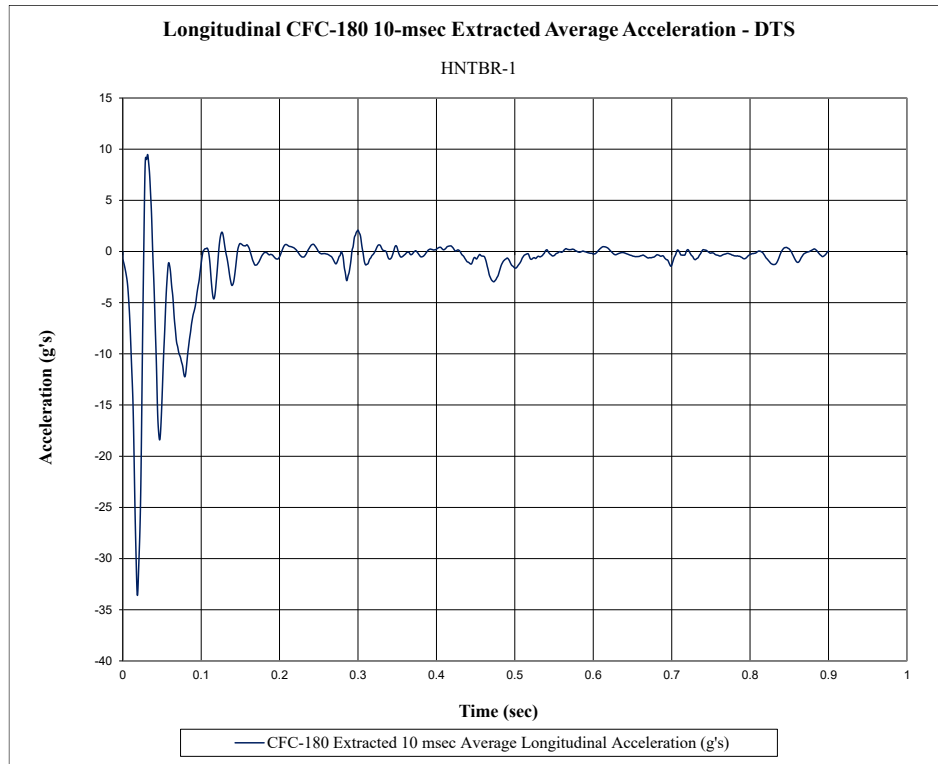


Figure E-9. 10-ms Average Longitudinal Deceleration (DTS), Test No. HNTBR-1

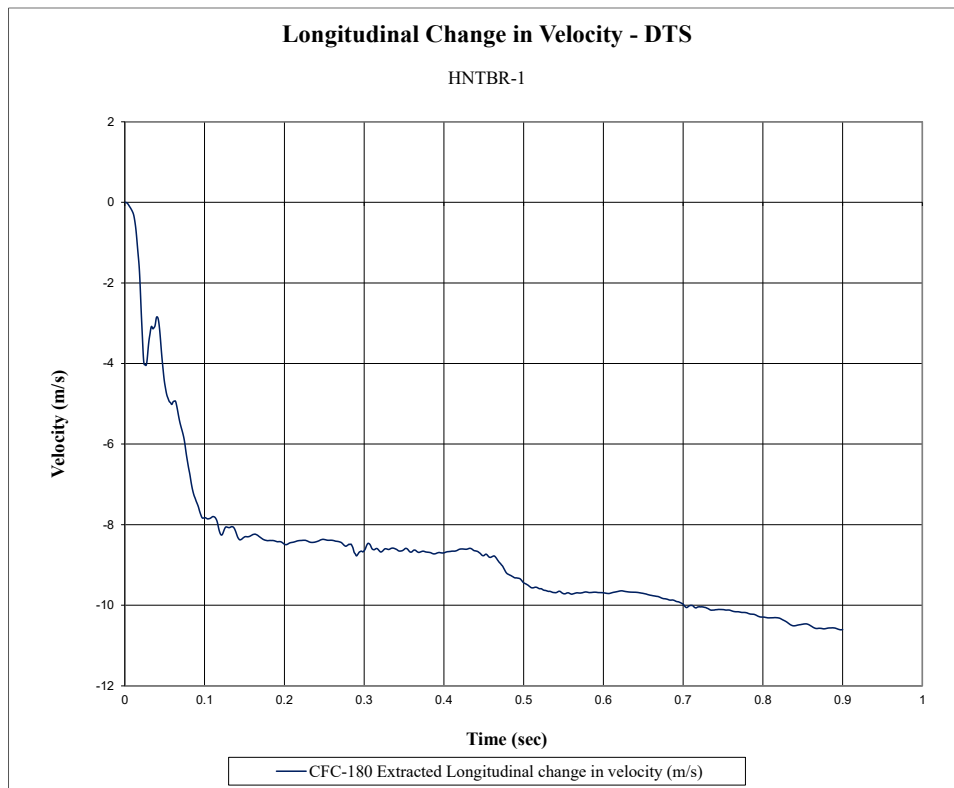


Figure E-10. Longitudinal Occupant Impact Velocity (DTS), Test No. HNTBR-1

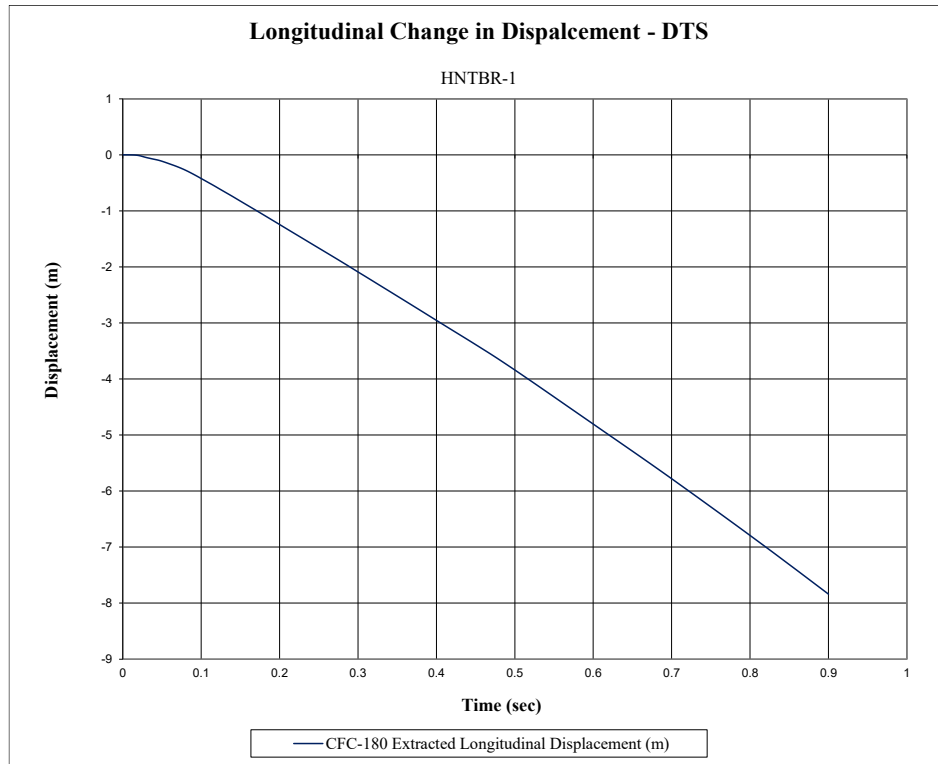


Figure E-11. Longitudinal Occupant Displacement (DTS), Test No. HNTBR-1

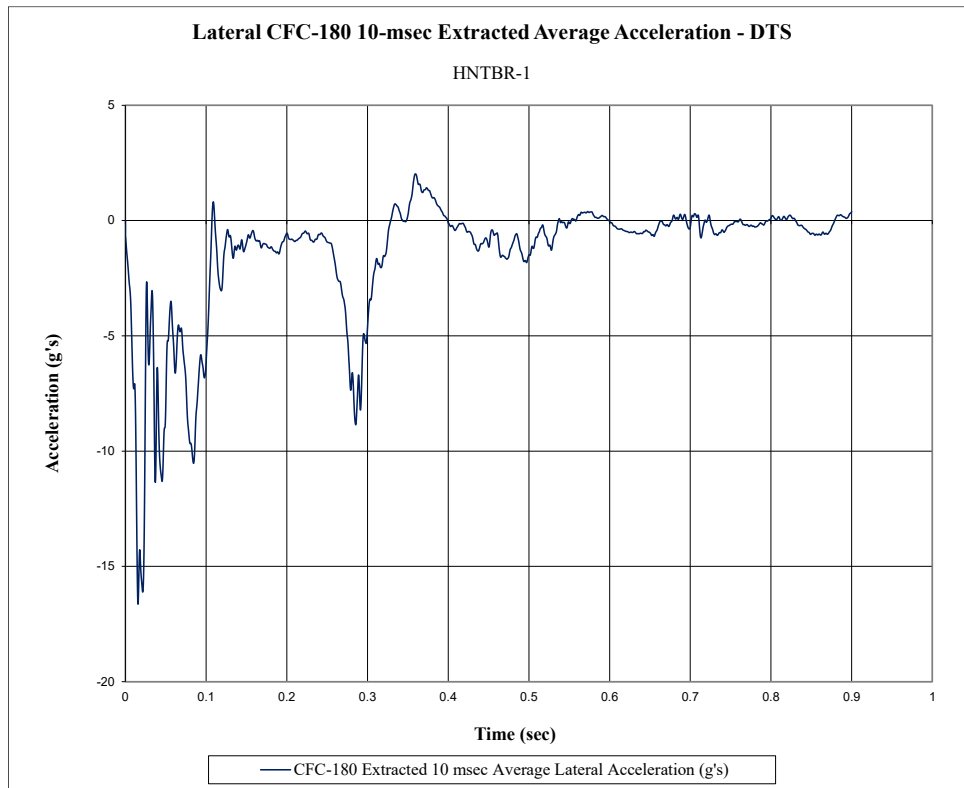


Figure E-12. 10-ms Average Lateral Deceleration (DTS), Test No. HNTBR-1

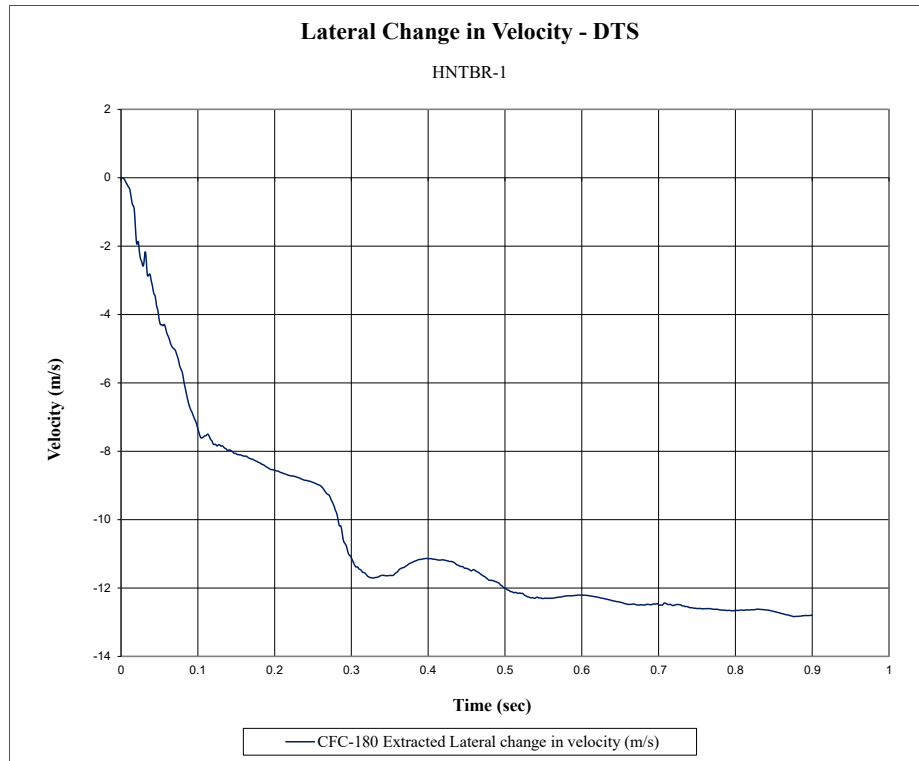


Figure E-13. Lateral Occupant Impact Velocity (DTS), Test No. HNTBR-1

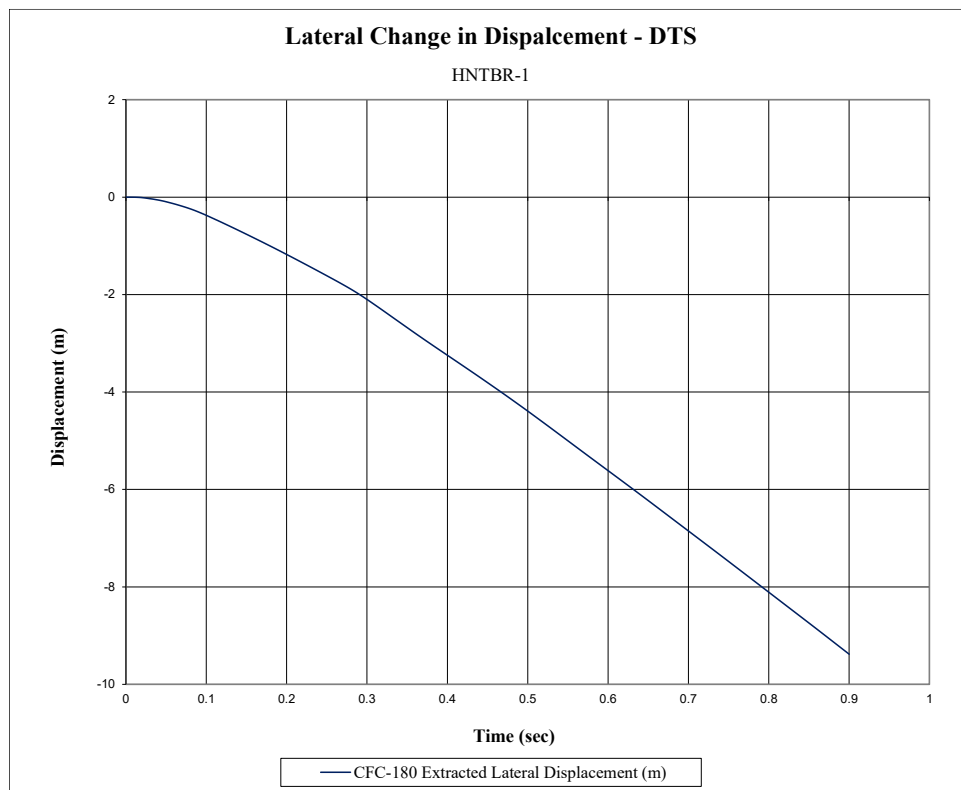


Figure E-14. Lateral Occupant Displacement (DTS), Test No. HNTBR-1

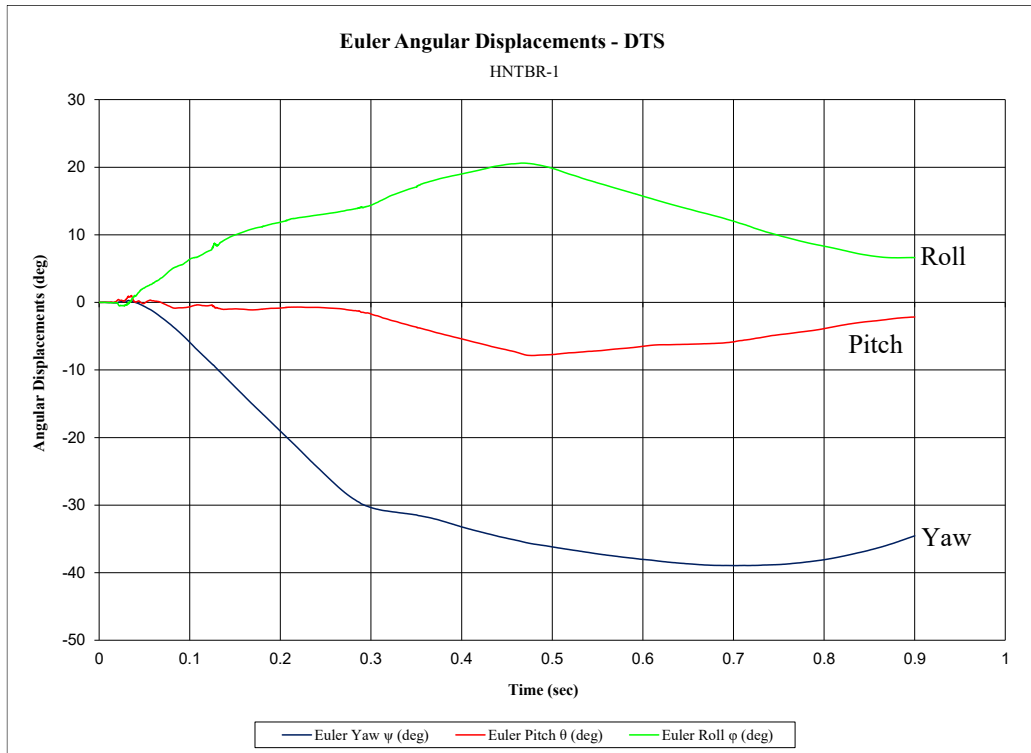


Figure E-15. Vehicle Angular Displacements (DTS), Test No. HNTBR-1

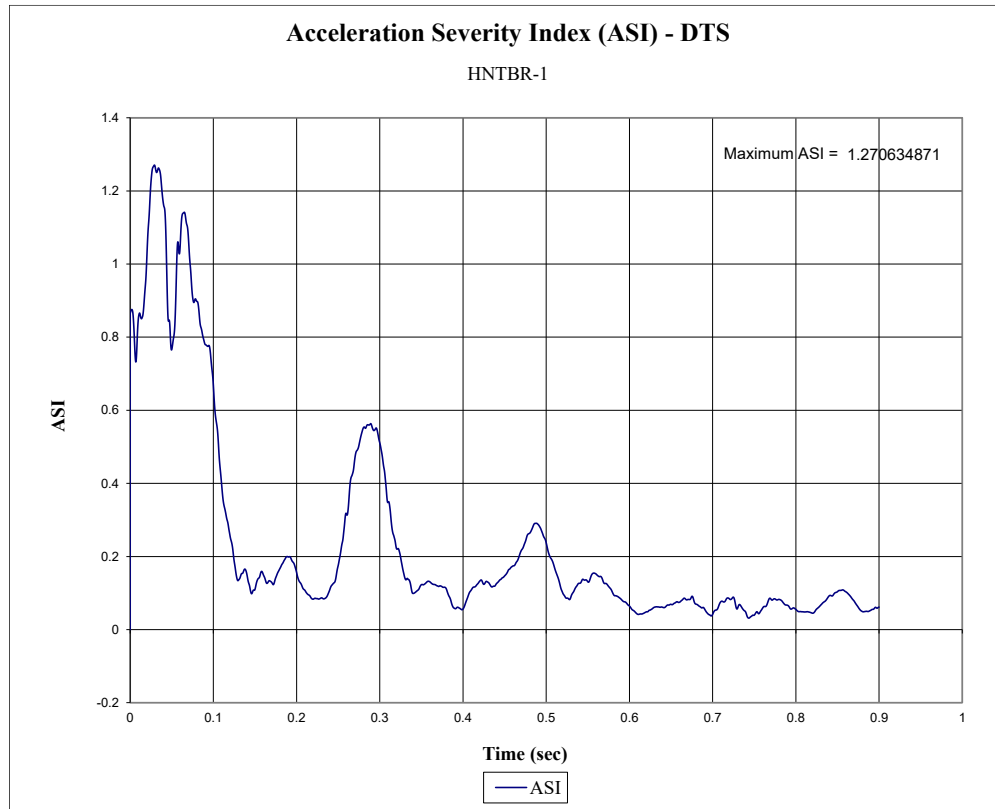


Figure E-16. Acceleration Severity Index (DTS), Test No. HNTBR-1

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