





MASH 2016 EVALUATION OF A NON-PROPRIETARY TYPE III BARRICADE:

MASH TEST DESIGNATION NO. 3-72

Submitted by

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16. Abstract Several work-zone traffic control devices have not yet been evaluated to the American Association of State Highway and Transportation Officials' (AASHTO's) <i>Manual for Assessing Safety Hardware, Second Edition</i> (MASH 2016) safety performance criteria. In this study, two identical Type III barricades were evaluated in the same crash test, according to MASH 2016, test designation no. 3-72. In test no. WZNP-2, a 5,001-lb (2,268-kg) pickup truck impacted System A, oriented at 90 degrees or perpendicular to the vehicle, at a speed of 64.7 mph (104.2 km/h) and System B, oriented at 0 degrees or head on to the vehicle, at a speed of 62.6 mph (100.8 km/h), respectively. The devices were spaced 60 ft (18.3 m) apart and each device impacted at the quarter-points on the front bumper. Each Type III barricade consisted of three horizontal High Density Polyethylene (HDPE) panels, measuring 96 in. (2,428 mm) in length, with a 48-in. x 30-in. x 0.08-in. (1,219-mm x 762-mm x 2-mm) aluminum sign attached to the top two barricade panels. The barricade panel was targeted to have a cross-sectional dimension of 8 in. (203 mm) x 1 in. (25 mm). During test no. WZNP-2, the 2270P pickup truck readily disengaged both				

barricades from their support. Both tests successfully met all evaluation criteria in MASH 2016 for test designation no. 3-72. 17. Key Words **18. Distribution Statement** Highway Safety, Crash Test, Roadside Appurtenances, No restrictions. Document available from: National Compliance Test, MASH 2016, Test Level 3, Work-Zone Technical Information Services, Springfield, Virginia Traffic Control Device, Non-Proprietary, Road Closed 22161 Barricade, Roadside Appurtenances, and Type III Barricade 22 D. 21 No .e n

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This is an uncorrected draft as submitted by the research agency. The opinions and conclusions expressed or implied in the report are those of the research agency. They are not necessarily those of the Transportation Research Board, the National Research Council, the Federal Highway Administration, the American Association of State Highway and Transportation Officials, or the individual states participating in the National Cooperative Highway Research Program.

UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority (IAA) for the data contained herein was Mr. Scott Rosenbaugh, Research Engineer.

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1 INTRODUCTION

1.1 Background

Through a project funded jointly by Dicke Safety Products, the Mid-America Transportation Center, and the Smart Work Zone Deployment Initiative (SWZDI) from 2008 to 2010, several work-zone sign stands were evaluated [1-2]. These sign stands were crashworthy according to the crash testing and safety performance criteria in National Cooperative Highway Research Program (NCHRP) Report No. 350 [3]. In 2009,

the American Association of State Highway and Transportation Officials (AASHTO) implemented an updated standard for the evaluation of roadside hardware [4]. The new standard, entitled the *Manual for Assessing Safety Hardware* (MASH 2009), improved the criteria for evaluating roadside hardware beyond the previous NCHRP Report No. 350 standard through updates to test vehicles, test matrices, and impact conditions. However, when NCHRP Report No. 350 work-zone devices were subjected to the new MASH 2009 crash testing and safety performance criteria, several of the work-zone sign stands produced undesirable results, including windshield and floorboard penetration and excessive windshield and roof deformation [1-2]. This testing indicated that devices tested under previous NCHRP Report No. 350 safety performance standards. Subsequently, an updated version of MASH, MASH 2016, was published, which contained no changes to the impact conditions or evaluation criteria for work-zone devices [5].

In an effort to encourage state departments of transportation (DOTs) and hardware developers to advance hardware designs, the Federal Highway Administration (FHWA) and AASHTO collaborated to develop a MASH implementation policy that included sunset dates for various roadside hardware categories. The new policy by the FHWA and AASHTO required that temporary work-zone devices manufactured after December 31, 2019 be evaluated to MASH 2016.

SWZDI and the Midwest Roadside Safety Facility (MwRSF) collaborated to conduct testing on a Type III barricade in accordance with MASH 2016 [6]. Three full-scale crash tests are required to evaluate a Type III barricade to MASH 2016 Test Level 3 (TL-3) criteria. According to MASH Section 2.2.4.2, test designations nos. 3-70, 3-71, and 3-72 are required, although test designation no. 3-70 is optional since the Type III barricade weighs less than 220 lb (100 kg) [5]. Test designation no. 3-71 (test no. WZNP-1) was conducted, which involved a 2,420-lb (1,100-kg) car (designated 1100C) impacting the barricade at 62 mph (100 km/h) at both 0 and 90 degrees [6]. Test designation no. 3-72, which involves a 5,000-lb (2,270-kg) pickup truck (designated 2270P) impacting the barricade at 62 mph (100 km/h) at both 0 and 90 degrees, was not conducted as part of the previous research effort with SWZDI.

The Type III barricade consisted of three reflective panels connected to two steel upright legs, which was held to the ground by sandbags placed on the legs. The panels supported a "Road Closed" aluminum sign and two lights, which were not connected to the legs. In test no. WZNP-1, two Type III barricades were placed 60 ft (18.3 m) apart on level terrain with one sandbag on the end of each leg. During the test, the 1100C small car impacted and disengaged both barricades from their supports. The systems readily activated in a predicable manner and allowed the 1100C vehicle to continue traveling without any major obstruction of the windshield. There were no

detached elements or fragments which showed potential for penetrating the occupant compartment or presented undue hazard to other traffic. No penetration or deformation of the occupant compartment that could have caused serious injury occurred. Therefore, test no. WZNP-1 was determined to be acceptable according to the MASH 2016 safety performance criteria for test designation no. 3-71. Test designation no. 3-72 was still required to complete the evaluation of the system to MASH TL-3 criteria.

1.2 Objective

The objective of this research effort was to evaluate the Type III barricade to MASH 2016 TL-3 safety criteria through two full-scale crash tests at 0-degree and 90-degree impact angles. For test designation no. 3-72, the Type III barricade was impacted by a 2270P pickup truck at an impact speed of 62 mph (100 km/h), as required by MASH 2016.

1.3 Scope

The research objective was achieved through the completion of several tasks. Two fullscale crash tests were conducted on a Type III barricade according to MASH 2016 test designation no. 3-72. Next, vehicle crash test results were analyzed, evaluated, and documented. Conclusions and recommendations were then made pertaining to the safety performance of the Type III barricade.

2 TEST REQUIREMENTS AND EVALUATION CRITERIA

2.1 Test Requirements

Category 2 work-zone traffic control devices, such as Type III barricades, must satisfy impact safety standards in order to be declared eligible for federal reimbursement by the Federal Highway Administration (FHWA) for use on the National Highway System (NHS). For new hardware, these safety standards consist of the guidelines and procedures published in MASH 2016 [5]. Note that there is no difference between MASH 2009 [4] and MASH 2016 for work-zone traffic control devices, such as Type III barricades tested in this project. According to TL-3 of MASH 2016, work-zone traffic control devices must be subjected to three full-scale vehicle crash tests, as summarized in Table 1. Note, only one of the prescribed full-scale crash tests, test designation no. 3-72, was conducted with two critical impact angles and reported herein.

	Test		Vehicle	Impact C	onditions	
Test	Designation	Test	Weight,	Speed,	Angle	Evaluation
Article	No.	Vehicle	lb	mph	(degrees)	Criteria ¹
			(Kg)	(km/h)	× 0 /	
	3 70	1100C	2,425	19	CIA	PDEEUIN
Work-Zone	3-70	11000	(1,100)	(30)	CIA	D,D,E,F,I1,I,I
Traffic	2 71	1100C	2,425	62	CIA	PDEEUIN
Control	5-71	11000	(1,100)	(100)	CIA	D, D, L, L', L', L', L', L', L', L', L', L',
Devices	2 72	22700	5,000	62	CIA	DDEEIIIN
	5-72	2270P	(2,270)	(100)	CIA	D,D,E,F,H,I,N

Table 1. MASH 2016 TL-3 Crash Test Conditions for Work-Zone Traffic Control Devices

¹ Evaluation criteria explained in Table 2.

CIA= Critical Impact Angle

The low-speed test, test designation no. 3-70, was not required, since the Type III barricade weighed less than 220 lb (100 kg) [5]. Test designation no. 3-71 was previously successfully conducted on the barricade [6]. MASH 2016 recommends test designation no. 3-72 be conducted both perpendicular to the device (0 degrees) and parallel to the device (90 degrees), as both orientations may occur along roadsides. MwRSF has developed a procedure for testing multiple work-zone traffic control devices in one test run. The barricade was evaluated at two impact angles, 90 degrees (System A) and 0 degrees (System B), in one full-scale crash test. The devices were spaced 60 ft (18.3 m) apart and each device impacted at the quarter points on the front bumper. Thus, two MASH 2016 test designation no. 3-72 crash tests were conducted at two critical impact angles (CIAs) and are reported herein.

2.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the work-zone traffic control device to break away, fracture, or yield in a predictable manner. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential

of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are summarized in Table 2 and defined in greater detail in MASH 2016. The full-scale vehicle crash test documented herein was conducted and reported in accordance with the procedures provided in MASH 2016.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported. Additional discussion on PHD, THIV and ASI is provided in MASH 2016.

Appraisal area	Evaluation criteria				
Structural Adequacy	В.	The test article should readily activate in a predictable manner by breaking away, fracturing, or yielding.			
	D.	Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.2.2 and Appendix E of MASH 2016.			
	E.	Detached elements, fragments, or other debris from the test article, or vehicular damage should not block the driver's vision or otherwis cause the driver to lose control of the vehicle. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.			
	F.				
Occupant Risk	Occupant Risk H. Occupant Impact Velocity (OIV) (see Appendix A, Section MASH 2016 for calculation procedure) should satisfy the limits:			, Section A5.2.2 of tisfy the following	
		Occupant Impact Velocity Limits			
		Component	Preferred	Maximum	
		Longitudinal	10 ft/s (3.0 m/s)	16 ft/s (4.9 m/s)	
	I. The Occupant Ridedown Acceleration (ORA) (see Appen Section A5.2.2 of MASH 2016 for calculation procedure) satisfy the following limits:			(see Appendix A, procedure) should	
		Occupant Ridedown Acceleration Limits			
		Component	Preferred	Maximum	
		Longitudinal and Lateral	15.0 g's	20.49 g's	
Post-Impact Vehicular Response	N.	Vehicle trajectory behind the test article is acceptable.			

Table 2. MASH 2016 Evaluation Criteria for Work-Zone Traffic Control Devices

3 DESIGN DETAILS

The test installation consisted of two Type III barricades, as shown in Figures 1 through 8. Photographs of the test installation are shown in Figures 9 and 10. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix A.

Each Type III barricade consisted of three horizontal High Density Polyethylene (HDPE) panels, measuring 96 in. (2,428 mm) in length, with a 48-in. x 30-in. x 0.08-in. (1,219-mm x 762-mm x 2-mm) aluminum sign attached to the top two barricade panels. The barricade panel was targeted to have nominal cross-sectional dimensions of 8 in. (203 mm) tall x 1 in. (25 mm) thick. However, the dimensions vary between manufacturers, and the supplied barricade panel was 8¹/₄ in. (210 mm) x ³/₄ in. (19 mm). The barricade panels were attached to two 1³/₄-in. (44-mm) x 14-ga (1.9-mm) thick Perforated Square Steel Tubing (PSST) uprights, which were inserted into two 2-in. (51-mm) x 14-ga (1.9-mm) thick x 6-in. (152-mm) long PSST vertical stubs that were each welded to one of the two legs. The legs were 2-in. (51-mm) x 14-ga (1.9-mm) thick x 60-in. (1,524-mm) long PSST. All PSST used was galvanized ASTM 1011 Grade 55 steel with a minimum yield strength of 60 ksi (414 MPa). A 50-lb (23-kg) sandbag was placed on top of both ends of each leg. A Type A/C warning light was attached to the front of the top barricade panel and to the upright at both upright locations.

Two identical Type III barricades were evaluated. System A was oriented at 90 degrees, end-on to the vehicle. System B was oriented at 0 degrees, or head-on to the vehicle. Initial vehicle impact with System A was to occur with a right quarter-point offset from the centerline of the vehicle and initial vehicle impact with System B was to occur with a left quarter-point offset from the centerline of the vehicle, as shown in Figure 11.



Figure 1. Test Installation Layout, Test No. WZNP-2



Figure 2. Barricade Overview, Test No. WZNP-2



UNITS: in.[mm] MAP

Figure 3. Barricade Details, Test No. WZNP-2



Figure 4. Plastic Beam Details, Test No. WZNP-2



Figure 5. Perforated Steel Tube Details, Test No. WZNP-2



Figure 6. Sign and Warning Light Details, Test No. WZNP-2



Item No.	QTY.	Description	Material Specification	Treatment Specification
a1	2	Plastic Panel, 96" [2,438] Long	High Density Polyethylene	_
۵2	4	Plastic Panel, 96" [2,438] Long	High Density Polyethylene	-
b1	4	1 3/4"x1 3/4"x14-gauge [44x44x1.9], 58" [1,473] Long Perforated Square Tubing	ASTM 1011 Gr. 55 Min. yield 60 ksi [414 MPa]	ASTM A653-G90 or AASHTO M-120
b2	4	2"x2"x14—gauge [51x51x1.9], 60" [1,524] Long Perforated Square Tubing	ASTM 1011 Gr. 55 Min. yield 60 ksi [414 MPa]	ASTM A653-G90 or AASHTO M-120
b3	4	2"x2"x14—gauge [51x51x1.9], 6" [152] Long Perforated Square Tubing	ASTM 1011 Gr. 55 Min. yield 60 ksi [414 MPa]	ASTM A653-G90 or AASHTO M-120
c1	2	48"x30"x0.08" [1,219x762x2] Sign with Reflective Sheeting	Aluminum Alloy 5052 or similar	-
c2	4	Warning Light (Type A or C)	As Supplied	-
d1	20	3/8"—16 UNC [M10x1.5], 3 1/2" [89] Long Hex Head Bolt	ASTM A307 Gr. A or equivalent	Fe/Zn 3AN per ASTM F1941
d2	4	1/2"—13 UNC [M14x2], 6" [152] Long Hex Head Bolt	ASTM A307 Gr. A or equivalent	Fe/Zn 3AN per ASTM F1941
d3	8	1/4"—20 UNC [M6x1], 1 3/4" [44] Long Hex Head Bolt	ASTM A307 Gr. A or equivalent	Fe/Zn 3AN per ASTM F1941
d4	40	3/8" [10] Dia. Plain USS Washer	Low Carbon Steel	Fe/Zn 3AN per ASTM F1941
d5	4	1/2" [13] Dia. Plain USS Washer	Low Carbon Steel	Fe/Zn 3AN per ASTM F1941
d6	16	1/4" [6] Dia. Plain USS Washer	Low Carbon Steel	Fe/Zn 3AN per ASTM F1941
d7	20	3/8"-16 UNC [M10x1.5] Lock Nut	SAE J995 Gr. 2 or equivalent	Fe/Zn 3AN per ASTM F1941
d8	8	1/4"-20 UNC [M6x1] Lock Nut	SAE J995 Gr. 2 or equivalent	Fe/Zn 3AN per ASTM F1941
	•	·		

	MURSE	Type III Barricade Test No. WZNP—2		SHEET: 8 of 8 DATE: 7/22/2020	-
Note: (1) Part c1 shall have a reflective sheeting.	 Midwest Roadside	Bill of Materials		DRAWN BY: DJW/SBW	
(2) Parts a1 & a2 will have orange and white striped reflective sheeting on at least one side (sign panel side).	Safety Facility	DWG. NAME. S WZNP-2_R1 U	SCALE: None UNITS: in.[mm]	REV. BY: MAP	

Figure 8. Bill of Materials, Test No. WZNP-2



Figure 9. Test Installation, Test No. WZNP-2



Figure 10. Test Installation, Test No. WZNP-2



Figure 11. Test Impact Point, Test No. WZNP-2

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4 TEST CONDITIONS

4.1 Test Facility

The Outdoor Test Site is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles (8.0 km) northwest of the University of Nebraska-Lincoln.

4.2 Vehicle Tow and Guidance System

A reverse-cable, tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the first barricade. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [7] was used to steer the test vehicle. A guide flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the second system. The $\frac{3}{8}$ -in. (9.5-mm) diameter guide cable was tensioned to approximately 3,500 lb (15.6 kN) and supported both laterally and vertically every 100 ft (30.5 m) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

4.3 Test Vehicle

For test no. WZNP-2 a 2011 Dodge Ram 1500 quad cab pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 5,105 lb (2,316 kg), 5,001 lb (2,268 kg), and 5,165 lb (2,343 kg), respectively. MASH recommends using test vehicles within 6 model years on the day the test is conducted. Additionally, vehicles within 6 model years of the award date of the research project, which was in 2015, were allowed at the time. Thus, a test vehicle older than 6 years from the test date was utilized, and all dimensions and properties of the test vehicle met the requirements in MASH. The test vehicle is shown in Figures 12 and 13, and vehicle dimensions are shown in Figure 14.

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The Suspension Method [7] was used to determine the vertical component of the c.g. for the pickup truck. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The location of the final c.g. is shown in Figures 14 and 15. Data used to calculate the location of the c.g. and ballast information are shown in Appendix B.

Square, black- and white-checkered targets were placed on the vehicle for reference to be viewed from the high-speed digital video cameras and aid in the video analysis, as shown in Figure 15. Round, checkered targets were placed at the c.g. on the left-side door, the right-side door, and the roof of the vehicle.







Figure 12. Test Vehicle, Test No. WZNP-2



Figure 13. Test Vehicle's Interior Floorboards and Undercarriage





Date:	3/21/2019	9	Test Name	WZNP-2	VIN No: _	1D7RB10	GP6BS634520
Year:	2011		Make	Dodge	Model:	Model: Ram 1500	
Tire Size:	P265/70R	<u>17 Ti</u>	re Inflation Pressure	40 psi	Odometer:	2	62517
					Vehicle Ge Target Ranges	eometry - in. (r s listed below	nm)
			Test Inertial CG		A: 77 1/8 78±2 (19 C: 229 1/2 237±13 (6) E: 140 3/4 148±12 (3) G: 28 5/16 min: 28	(1959) B: (50±50) D: (5829) D: (32535) F: (3575) F: (719) H:	74 1/4 (1886) 38 3/8 (975) 39±3 (1000±75) (1226) 48 1/4 (1226) 61 9/16 (1564) 63±4 (1575±100) (1575±100)
			s contractions		I: <u>10 1/2</u> 3 K: <u>20 3/8</u> M: <u>67 7/8</u> 67±1.5 (1 O: <u>43 7/8</u> 43±4 (11		27 (686) 29 7/8 (759) 67 3/8 (1711) 67±1.5 (1700±38) (114)
-		HE 	+ +	— F — •	Q: <u>31 1/4</u> S: 13 7/8	(794) R:	<u>18 1/2 (470)</u> 77 1/4 (1962)
					U (ir	npact width):	38 4/7 (979)
Gross Static	LF <u>1422</u> LR <u>1131</u>	(645) RF (513) RR	1485 (674) 1127 (511)		Cle	Wheel Center Height (Front): _ Wheel Center Height (Rear): _ Wheel Well arance (Front):	<u>15 1/4 (387)</u> <u>15 1/4 (387)</u> 35 1/4 (895)
Weights Ib (kg)	Curk	b	Test Inertial	Gross Static	Cle	Wheel Well earance (Rear):	37 7/8 (962)
W-front	2875	(1304)	2814 (1276)	2907 (1319)	Bottom Frame Height (Front): _	9 1/2 (241)
W-rear	2230	(1012)	2187 (992)	2258 (1024)	Bottom Frame Height (Rear):	10 3/8 (264)
W-total	5105	(2316)	5001 (2268) 5000±110 (2270±50)	5165 (2343 5165±110 (2343±50)))	Engine Type: _	Gasoline
GVWR Ratin	as - Ib	Su	urrogate Occupant D	ata	Transn	nission Type	Automatic
Front	3700		Type:	Hybrid II	Tunan	Drive Type:	RWD
Rear	3900		Mass:	164 lb		Cab Style:	Quad Cab
Total	6700		Seat Position:	Right/Passenger	_	Bed Length:	76"
Note any damage prior to test: Right front bumper cover is deformed slightly.							

Figure 14. Vehicle Dimensions, Test No. WZNP-2



Figure 15. Target Geometry, Test No. WZNP-2

The front wheels of the test vehicle were aligned to vehicle standards except the toe-in value was adjusted to zero such that the vehicles would track properly along the guide cable. 5B flash bulbs were mounted under the vehicle's left and right-side windshield wipers and were fired by pressure tape switches mounted on both quarter points of the bumper. The flash bulbs fired upon initial impact with the test article to create a visual indicator of the precise time of impact on the high-speed digital videos. A remote-controlled brake system was installed in the test vehicle so the vehicle could be brought safely to a stop after the test.

4.4 Simulated Occupant

For test no. WZNP-2, a Hybrid II 50th-Percentile, Adult Male Dummy, equipped with clothing and footwear, was placed in the right-front seat of the test vehicle with the seat belt fastened. The dummy had a final weight of 164 lb (74 kg). As recommended by MASH 2016, the dummy was not included in calculating the c.g. location.

4.5 Data Acquisition Systems

4.5.1 Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. Both accelerometer systems were mounted near the c.g. of the test vehicle. The electronic accelerometer data obtained in dynamic testing was filtered using SAE Class 60 and SAE Class 180 Butterworth filters conforming to the SAE J211/1 specifications [8].

The two systems, the SLICE-1 and SLICE-2 units, were modular data acquisition systems manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. The SLICE-2 unit was designated as the primary system. The acceleration sensors were mounted inside the bodies of custom-built, SLICE 6DX event data recorders and recorded data at 10,000 Hz to the onboard microprocessor. The SLICE 6DX was configured with 7 GB of non-volatile flash memory, a range of ± 500 g's, a sample rate of 10,000 Hz, and a 1,650 Hz (CFC 1000) anti-aliasing filter. The "SLICEWare" computer software programs and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

4.5.2 Rate Transducers

Two identical angular rate sensor systems mounted inside the bodies of the SLICE-1 and SLICE-2 event data recorders were used to measure the rates of rotation of the test vehicle. Each SLICE MICRO Triax ARS had a range of 1,500 degrees/sec in each of the three directions (roll, pitch, and yaw) and recorded data at 10,000 Hz to the onboard microprocessors. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The "SLICEWare" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

4.5.3 Retroreflective Optic Speed Trap

The retroreflective optic speed trap was used to determine the speed of the test vehicle before impact. Four retroreflective targets, spaced at approximately 18-in. (457-mm) intervals,

were applied to the side of the vehicle. When the emitted beam of light was reflected by the targets and returned to the Emitter/Receiver, a signal was sent to the data acquisition computer, recording at 10,000 Hz, as well as the external LED box activating the LED flashes. The speed was then calculated using the spacing between the retroreflective targets and the time between the signals. LED lights and high-speed digital video analysis are only used as a backup in the event that vehicle speeds cannot be determined from the electronic data.

4.5.4 Digital Photography

Five AOS high-speed digital video cameras, six GoPro digital video cameras, four Panasonic digital video cameras, and one SoloShot digital video camera were utilized to film test no. WZNP-2. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 16.

The high-speed videos were analyzed using the Redlake MotionScope software program. Actual camera speed and camera divergence factors were considered in the analysis of the highspeed videos. A digital still camera was also used to document pre- and post-test conditions for the test.



No.	Туре	Operating Speed (frames/sec)	Lens	Lens Setting
AOS-1	AOS Vitcam CTM	500	KOWA 25 mm	-
AOS-5	AOS X-PRI Gigabit	500	100 mm	-
AOS-7	AOS X-PRI Gigabit	500	Fujinon 50 mm	-
AOS-9	AOS TRI-VIT	500	KOWA 12 mm	-
AOS MINI	AOS Smize	500	Fujinon 35mm	-
GP-7	GoPro Hero 4	120		
GP-8	GoPro Hero 4	120		
GP-18	GoPro Hero 6	240		
GP-19	GoPro Hero 6	240		
GP-20	GoPro Hero 6	240		
GP-21	GoPro Hero 6	240		
PAN-1	Panasonic HC-V770	60		
PAN-2	Panasonic HC-V770	60		
PAN-3	Panasonic HC-V770	60		
PAN-4	Panasonic HC-V770	60		
SoloShot	SoloShot	120		

Figure 16. Camera Locations, Speeds, and Lens Settings, Test No. WZNP-2

5 FULL-SCALE CRASH TEST NO. WZNP-2

5.1 Weather Conditions

Test no. WZNP-2 was conducted on March 21, 2019 at approximately 3:00 p.m. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported and are shown in Table 3.

Table 3. Weather Conditions, Test No. WZNP-2

Temperature	59° F
Humidity	38 %
Wind Speed	7 mph
Wind Direction	Variable
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0.34 in.
Previous 7-Day Precipitation	0.40 in.

5.2 Test Description

MwRSF has developed a procedure for testing multiple work-zone traffic control devices in one test run. However, in order to have two devices impacted in one test run using the previously established method, it was necessary to align the systems with the quarter points of the vehicle to distinguish damage between the two systems. Additionally, MASH 2016 does not provide specific guidance on how to align the test vehicle and test article. Therefore, impacting the centerline of each barricade with a quarter point of the test vehicle seemed adequate.

During test no. WZNP-2, initial vehicle impact with System A was to occur with a right quarter-point offset from the centerline of the vehicle, and initial vehicle impact with System B was to occur with a left quarter-point offset from the centerline of the vehicle, as shown in Figure 17. The centerlines of both Systems A and B impacted the vehicle at the right and left quarter-point offsets from the centerline of the vehicle, respectively. The 5,001-lb (2,268-kg) 2011 Dodge Ram 1500 quad cab pickup truck impacted System A at a speed of 64.7 mph (104.2 km/h). The pickup truck impacted System B 0.694 seconds after the initial impact with System A at a speed of 62.6 mph (100.8 km/h). Note, the HDPE panel from System A impacted the outer edge of the middle panel on System B 0.002 seconds before the vehicle impacted System B as System A was sliding off to the right side of the pickup truck. The contact lasted approximately 0.004 seconds. However, this contact occurred outside of the vehicle contact area on System A did not affect the evaluation of System B. The vehicle came to rest 277 ft – 6 in. (84.6 m) downstream after brakes were applied.

A detailed description of the sequential impact events is contained in Tables 4 and 5. Sequential photographs are shown in Figure 18. Documentary photographs of the crash test are shown in Figures 20 through 22. The vehicle trajectory and final position are shown in Figure 23.






Figure 17. Impact Location, Test No. WZNP-2

TIME (sec)	EVENT
0.000	Vehicle's front bumper contacted System A's bottom panel.
0.002	Vehicle's grille contacted System A's middle panel.
0.010	Vehicle's front bumper contacted System A's upstream support, and System A deflected downstream.
0.012	Vehicle's hood contacted System A's upstream support, and System A's upstream support bent upstream.
0.014	System A's middle panel deformed.
0.016	Vehicle's front bumper deformed.
0.018	System A's top panel contacted vehicle's hood, and bottom panel of System A deformed.
0.020	System A's top panel deformed.
0.022	System A's upstream leg detached, and downstream support rotated downstream.
0.028	System A's sign deformed from contact with vehicle's grille.
0.032	Vehicle's hood contacted System A's sign.
0.054	System A's middle panel detached from upstream support.
0.080	System A's downstream leg detached, and System A became airborne.
0.164	Bottom panel of System A contacted ground.

Table 4. Sequential Description of Impact Events, Test No. WZNP-2, System A

TIME	EVENT
(sec)	
-0.002	System A's middle panel contacted System B's middle panel, and System B's middle panel slightly deformed.
0.000	Vehicle's front bumper contacted System B's bottom panel; vehicle's front bumper contacted System B's right support.
0.002	Vehicle's hood contacted System B's sign.
0.004	Vehicle's grille contacted System B's middle panel, System B's right support bent upstream, and System B's bottom panel deformed.
0.006	Vehicle's hood deformed, and System B's top panel and sign deformed.
0.012	Vehicle's left headlight contacted System B's sign.
0.014	System B's right support deflected left.
0.016	System B's left leg deflected downstream.
0.022	System A lost contact with vehicle and became airborne.
0.030	System B's right leg detached.
0.056	System B's left support contacted vehicle's left fender.
0.058	Vehicle's left fender deformed.
0.072	System B's left support snagged on left-front fender deformations.
0.106	System B's left leg detached, and System B became airborne.
0.114	System B's left support contacted vehicle's left-side mirror.
0.228	System A contacted ground target.
0.358	Vehicle's right headlight became disengaged.
0.412	System B contacted ground.
0.440	System B's left light detached.
0.448	System B's middle panel detached from left support.
1.210	Vehicle yawed clockwise.

Table 5. Sequential Description of Impact Events, Test No. WZNP-2, System B



0.000 sec



0.250 sec



0.450 sec



0.700 sec







1.100 sec



0.000 sec



0.050 sec



0.100 sec



0.150 sec



0.200 sec



0.250 sec

Figure 18. Sequential Photographs, Test No. WZNP-2



Figure 19. Documentary Photographs, Test No. WZNP-2



Figure 20. Additional Documentary Photographs, Test No. WZNP-2











Figure 21. Additional Documentary Photographs, Test No. WZNP-2















Figure 22. Additional Documentary Photographs, Test No. WZNP-2





Figure 23. Vehicle Trajectory and Final Position, Test No. WZNP-2

5.3 System Damage

Damage to the barricades was extensive, as shown in Figures 24 through 28. Barricade damage consisted of punctured sandbags, bent uprights and legs, bent and torn barricade panels, and bolts pulled through the barricade panels. The vehicle readily disengaged both barricades from their bases.

System A was facing perpendicular to the direction of travel. The centerline of the system was aligned to the right quarter-point and offset from the centerline of the vehicle. The two uprights disengaged from each leg upon impact. The upstream left and downstream left sandbags were torn open. The upstream end of the middle barricade panel tore. The upstream upright was bent inward toward the center of the sign. The bottom barricade panel was deformed. Three bolts were partially pulled out of the bottom barricade panel. Two bolts were pulled out of the middle barricade panel, and one was partially pulled out. Three bolts were pulled out of the aluminum sign.

System B was oriented to face the direction of travel. The centerline of the system was aligned to the left quarter-point and offset from the centerline of the vehicle. The downstream right and the downstream left sandbags were torn open. The upstream leg was deformed. The right upright was bent 17 in. (432 mm) from the bottom. The aluminum sign was bent. Both warning lights were rotated, and the left light lens disengaged from the warning light system. One bolt was pulled out of the bottom barricade panel, and three bolts were partially pulled out. The two left side bolts on the middle barricade panel were pulled out. The aluminum sign bolts were partially pulled out of the middle barricade panel and thoroughly pulled out of the top barricade panel.



Figure 24. Overall System A and System B Damage, Test No. WZNP-2



Figure 25. System A Damage, Test No. WZNP-2



Figure 26. Additional System A Damage, Test No. WZNP-2





Figure 27. System B Damage, Test No. WZNP-2



Figure 28. Additional System B Damage, Test No. WZNP-2



5.4 Vehicle Damage

The damage to the vehicle was minimal, as shown in Figures 29 through 31. The maximum occupant compartment intrusions are listed in Table 6 along with the intrusion limits established in MASH 2016 for various areas of the occupant compartment. MASH 2016 defines intrusion or deformation as the occupant compartment being deformed and reduced in size with no observed penetration. Note that none of the established MASH 2016 deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix C.

The majority of the damage was concentrated on the right-front corner where the vehicle impacted System A. The torn piece of the middle panel from System A was stuck inside the right side of the grille. A small dent was found on the left side of the front bumper. A vertical crush line extending from the bottom of the bumper to the top of the hood was found on the vehicle. The right headlight was disengaged from the vehicle. A dent was found on the left-front fender. The left mirror was partially disengaged from the vehicle. The roof, remaining window glass, and undercarriage remained undamaged.







Figure 29. Vehicle Damage, Test No. WZNP-2





Figure 30. Vehicle Damage Details, Test No. WZNP-2



Figure 31. Occupant Compartment and Undercarriage Damage, Test No. WZNP-2

LOCATION	MAXIMUM INTRUSION in. (mm)	MASH 2016 ALLOWABLE INTRUSION in. (mm)
Wheel Well & Toe Pan	0.2 (5.1)	≤ 9 (229)
Floor Pan & Transmission Tunnel	0.1 (2.5)	≤ 12 (305)
A-Pillar	0.6 (15.2)	≤ 5 (127)
B-Pillar	0.6 (15.2)	≤ 5 (127)
A-Pillar (Lateral)	0.3 (7.6)	≤ 3 (76)
B-Pillars (Lateral)	0.3 (7.6)	≤3 (76)
Side Front Panel (in Front of A-Pillar)	1.2 (30.5)	≤ 12 (305)
Side Door (Above Seat)	0.2 (5.1)	≤ 9 (229)
Side Door (Below Seat)	0.1 (2.5)	≤ 12 (305)
Roof	0.3 (7.6)	≤4 (102)
Windshield	0.0 (0)	≤3 (76)
Side Window	Intact	No shattering resulting from contact with structural member of test article
Dash	1.5 (38.1)	N/A

Table 6. Maximum Occupant Compartment Intrusion by Location, Test No. WZNP-2

Note: Negative values denote outward deformation N/A . Not appliable

N/A - Not applicable

5.5 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec average occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions, as determined from the accelerometer data, for System A and System B are shown in Table 7. Note that lateral and longitudinal occupant displacements do not meet the required distances specified in MASH. Therefore, the ORA values are not applicable, and the OIV numbers are determined from the change in velocity at the time where the vehicle clears the footing according to MASH 2016. The calculated THIV, PHD, and ASI values for each system are also shown in Table 7. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix D.

			Transducer										
Evaluatio	on Criteria	SYST	TEM A	SYST	MASH 2016								
		SLICE-1	SLICE-2 (primary)	SLICE-1	SLICE-2 (primary)								
ΟΙV	Longitudinal	-1.44 (-0.44)	-1.34 (-0.41)	-1.28 (-0.39)	-1.13 (-0.34)	±16 (4.9)							
ft/s (m/s)	Lateral	0.91 (0.28)	0.72 (0.22)	-0.39 (-0.12)	-0.23 (-0.07)	±16 (4.9)							
ORA	Longitudinal	N/A	N/A	N/A	N/A	±20.49							
g's	Lateral	N/A	N/A	N/A	N/A	±20.49							
MAX.	Roll	-0.78	1.16	-0.78	1.16	±75							
ANGULAR DISPL.	Pitch	5.93	2.87	5.93	2.87	±75							
deg.	Yaw	1.22	-2.45	1.22	-2.45	not required							
THIV ft/s (m/s) PHD g's		N/A	N/A	N/A	N/A	not required							
		N/A	N/A	N/A	N/A	not required							
A	SI	0.054	0.055	0.087	0.065	not required							

Table 7. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. WZNP-2

N/A - Not applicable (due to reasons explained in section 5.5)

5.6 Discussion

A summary of the test results and sequential photographs for System A and System B are shown in Figures 32 and 33, respectively. The analysis of the test results for test no. WZNP-2 showed that both systems readily activated in a predicable manner and allowed the 2270P vehicle to continue traveling without any major obstruction of the windshield. Detached elements, fragments, or other debris from the test article did not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or work-zone personnel. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix D, were deemed acceptable because they did not adversely influence occupant risk nor cause rollover. After impact, the vehicle's trajectory did not violate the bounds of the exit box. Therefore, test no. WZNP-2 was determined to be acceptable according to the MASH 2016 safety performance criteria for test designation no. 3-72.



Figure 32. Summary of Test Results and Sequential Photographs for System A, Test No. WZNP-2

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0.100 sec

0.000 sec





0.150 sec

0.200 sec

Transducer Data

		Trans	MASH 2016	
Evaluatio	on Criteria	SLICE-1	SLICE-2 (primary)	Limit
OIV ft/a	Longitudinal	-1.28 (-0.39)	-1.13 (-0.34)	±16 (4.9)
(m/s)	Lateral	-0.39 (-0.12)	-0.23 (-0.07)	±16 (4.9)
ORA	Longitudinal	N/A	N/A	±20.49
g's	Lateral	N/A	N/A	±20.49
MAX	Roll	-0.78	1.16	±75
ANGULAR DISP.	Pitch	5.93	2.87	±75
deg.	Yaw	1.22	-2.45	Not required
THIV –	ft/s (m/s)	N/A	N/A	Not required
PHD) – g's	N/A	N/A	Not required
A	SI	0.087	0.065	Not required

N/A - Not applicable (due to reasons explained in section 5.5)

Figure 33. Summary of Test Results and Sequential Photographs for System B, Test No. WZNP-2

6 SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

Test no. WZNP-2 was conducted on a non-proprietary Type III barricade according to MASH 2016 test designation no. 3-72. Two barricades were impacted sequentially by the same test vehicle. In test no. WZNP-2, the 5,001-lb (2,268-kg) 2011 Dodge Ram 1500 quad cab pickup truck impacted System A, oriented at 90 degrees or perpendicular to the vehicle, at a speed of 64.7 mph (104.2 km/h) and System B, oriented at 0 degrees or head-on to the vehicle, at a speed of 62.6 mph (100.8 km/h), respectively. During test no. WZNP-2, the 2270P pickup truck impacted and disengaged both barricades from their bases. The systems readily activated and allowed the 2270P vehicle to continue travelling without any major obstruction of the windshield. There were no detached elements or fragments that showed potential for penetrating the occupant compartment nor present undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle remained upright during and after the collisions. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix D, were deemed acceptable, because they did not adversely influence occupant risk nor cause rollover. After impact, the vehicle's trajectory did not violate the bounds of the exit box. Therefore, test no. WZNP-2 was determined to be acceptable according to the MASH 2016 safety performance criteria for test designation no. 3-72. A summary of the test evaluation and sequential photos are shown in Table 8.

When assembling this Type III barricade, hardware parts and materials that are similar to those used in the as-tested system should be utilized. Sandbags, weighing approximately 50 lb, should be placed on the ends of each leg. One Type A/C warning light was attached to the top and front-side of the HDPE panels at each PSST upright on each barricade to evaluate a worst-case configuration with attachments. Thus, two warning lights were attached to each barricade. Utilizing one or no warning lights would also be acceptable. The warning lights were attached to the top barricade panel but could also be attached to the backside of the top barricade panel, as that would be a less critical configuration.

An aluminum sign panel can be attached to the Type III, with a maximum sign size and location similar to the as-tested installation. Smaller aluminum sign panels attached with a top height that is even with the top barricade panel or lower, or omitting the aluminum sign panel would also be acceptable configurations.

The Type III barricade panels consisted of three horizontal High Density Polyethylene (HDPE) panels, measuring 96 in. (2,428 mm) in length. The barricade panel was targeted to have nominal cross-sectional dimensions of 8 in. (203 mm) tall x 1 in. (25 mm) thick. However, the dimensions vary between manufacturers, and the supplied barricade panel was 8¼ in. (210 mm) x $^{3}4$ in. (19 mm). HDPE panels that are similar to those in the as-tested installation or with the nominal dimensions could also be used for this Type III barricade.

Evaluation Factors		Evaluation Criteria									
Structural Adequacy	В	The test article should readily breaking away, fracturing, or yie	activate in a predic lding.	table manner by	S						
	D.	1. Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.									
		2. Deformations of, or intrusions not exceed limits set forth in Se 2016.	into, the occupant contection 5.2.2 and Appen	npartment should ndix E of MASH	S						
	E. Detached elements, fragments, or other debris from the test article, or vehicular damage should not block the driver's vision or otherwise cause the driver to lose control of the vehicle										
	F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.									
Occupant Risk	H. Occupant Impact Velocity (OIV) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits:										
		Occupant Impact Velocity Limits									
		Component	Preferred	Maximum							
		Longitudinal and Lateral	30 ft/s (9.1 m/s)	16 ft/s (4.9 m/s)							
	I.	The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.2.2 of MASH 2016 for calculation procedure) should satisfy the following limits:									
		Occupant Rided	own Acceleration Lim	its	S						
		Component	Maximum								
		Longitudinal and Lateral	15.0 g's	20.49 g's							
		MASH 2016 Test Desig	gnation No.		3-72						
		Final Evaluation (Pas	s or Fail)		Pass						
S - Satisfactory $U - Unsatisfactory$ $N/A - Not Applicable$											

Table 8. Summary of Safety Performance Evaluation

7 MASH EVALUATION

This Type III barricade had three horizontal High Density Polyethylene (HDPE) panels, measuring 96 in. (2,428 mm) in length, with a 48-in. x 30-in. x 0.08-in. (1,219-mm x 762-mm x 2-mm) aluminum sign attached to the top two barricade panels. The barricade panel was targeted to have nominal cross-sectional dimensions of 8 in. (203 mm) x 1 in. (25 mm). However, the dimensions vary between manufacturers, and the supplied barricade panel was 8¹/₄ in. (210 mm) x $^{3}/_{4}$ in. (19 mm). The barricade panels were attached to two 1³/₄-in. (44-mm) x 14-ga (1.9-mm) thick Perforated Square Steel Tubing (PSST) uprights, which were inserted into two 2-in. (51-mm) x 14-ga (1.9-mm) thick x 6-in. (152-mm) long PSST vertical stubs that were welded to two legs. The legs were 2-in. (51-mm) x 14-ga (1.9-mm) thick x 60-in. (1,524-mm) long PSST. All PSST used was galvanized ASTM 1011 Grade 55 steel with a minimum yield strength of 60 ksi (414 MPa). A 50-lb (23-kg) sandbag was placed on top of the end of each leg. A Type A/C warning light was attached to the front of the top barricade panel and upright at both upright locations.

According to TL-3 of MASH 2016, work-zone traffic control devices, such as a Type III barricade, must be subjected to three full-scale vehicle crash tests, as summarized in Table 9. The low-speed test, test designation no. 3-70, was optional according to MASH Section 2.2.4.2 and was not conducted, since the Type III barricade weighed less than 220 lb (100 kg) [5]. MASH 2016 recommends these tests be conducted both perpendicular to the device (0 degrees) and parallel to the device (90 degrees), as both orientations may occur along roadsides. Test designation no. 3-71 was previously successfully conducted on the barricade at two critical impact angles, both perpendicular to the device (0 degrees) and parallel to the device (90 degrees) [6]. Test designation no. 3-72 was successfully conducted on the barricade at two critical impact angles, both perpendicular to the device (0 degrees) and parallel to the device (90 degrees), as reported herein.

Test	Test		Vehicle	Impact Conditions				
	Designation	Test	Weight,	Speed,	Angle			
Article	No	Vehicle	lb	mph	(degrees)			
	110.		(kg)	(km/h)	(degrees)			
Work-Zone Traffic Control Devices	3 70*	1100C	2,425	19	CIA			
	5-70*	11000	(1,100)	(30)	CIA			
	2 71	11000	2,425	62	CIA			
	3-71	11000	(1,100)	(100)	CIA			
	2 72	22700	5,000					
	5-72	2270P	(2,270)	(100)	CIA			

Table 9. MASH 2016 TL-3 Crash Test Conditions for Work-Zone Traffic Control Devices

* Optional for devices weighing less than 220 lb (100 kg)

CIA= Critical Impact Angle

In test no. WZNP-1, two identical Type III barricades were impacted by an 1100C small car in accordance with MASH 2016 test designation no. 3-71 [6]. The two Type III barricades were placed 60 ft (18.3 m) apart on level terrain with one sandbag on the end of each leg. Initial vehicle impact with System A, oriented at 90 degrees or perpendicular to the vehicle, was to occur with a right quarter-point and offset from the centerline of the car and initial vehicle impact with

System B, oriented at 0 degrees or head on to the vehicle, was to occur with a left quarter-point and offset from the centerline of the car. The 2,426-lb (1,100-kg) small car impacted System A at a speed of 64.7 mph (104.2 km/h) and System B at a speed of 61.2 mph (98.6 km/h). During the test, the 1100C small car impacted and disengaged both barricades from their bases. The systems readily activated in a predictable manner and allowed the 1100C vehicle to continue traveling without any major obstruction of the windshield. There were no detached elements or fragments which showed potential for penetrating the occupant compartment or presented undue hazard to other traffic

In test no. WZNP-2, two identical Type III barricades were impacted by a 2270P pickup truck in accordance with MASH 2016 test designation no. 3-72. The two Type III barricades were placed 60 ft (18.3 m) apart on level terrain with one sandbag on the end of each leg. Initial vehicle impact with System A, oriented at 90 degrees or perpendicular to the vehicle, was to occur with a right quarter-point and offset from the centerline of the car and initial vehicle impact with System B, oriented at 0 degrees or head on to the vehicle, was to occur with a left quarter-point and offset from the centerline of the car and initial vehicle impact with System B, oriented at 0 degrees or head on to the vehicle, was to occur with a left quarter-point and offset from the centerline of the car. The 5,001-lb (2,268-kg) 2011 Dodge Ram 1500 quad cab pickup truck impacted System A at a speed of 64.7 mph (104.2 km/h) and System B at a speed of 62.6 mph (100.8 km/h). During the test, the 2270P pickup truck impacted and disengaged both barricades from their bases. The systems readily activated and allowed the 2270P vehicle to continue travelling without any major obstruction of the windshield. Thus, this Type III barricade satisfied all of the requirements for the crash tests in the TL-3 test matrix and, therefore, is a MASH TL-3 crashworthy device.

8 REFERENCES

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- Ross, H.E., Sicking, D.L., Zimmer, R.A., and Michie, J.D., *Recommended Procedures for* the Safety Performance Evaluation of Highway Features, National Cooperative Highway Research Program (NCHRP) Report 350, Transportation Research Board, Washington, D.C., 1993. <u>http://onlinepubs.trb.org/onlinepubs/nchrp/nchrp_rpt_350-a.pdf</u>.
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9 APPENDICES

Appendix A. Material Specifications

Table A-1. Bill of Materials, Test No. WZNP-2

Item No.	Description	Material Specification	Reference
a1	Plastic Panel, 96" [2,438] Long	Petrothene LR734001	Technical Data Sheet
a2	Plastic Panel, 96" [2,438] Long	Petrothene LR734001	Technical Data Sheet
b1	1 3/4"x1 3/4"x14-gauge [44x44x1.9], 58" [1,473] Long Perforated Square Tubing	ASTM 1011 Gr. 55	H#A90050 (Coil#168755)
b2	2"x2"x14-gauge [51x51x1.9], 60" [1,524] Long Perforated Square Tubing	ASTM 1011 Gr. 55	H#C87907 (Coil#4169112)
b3	2"x2"x14-gauge [51x51x1.9], 6" [152] Long Perforated Square Tubing	ASTM 1011 Gr. 55	H#C87907 (Coil#4169112)
c 1	48" x 30" x 0.08" [1,219 x 762 x 2] Sign with Reflective Sheeting	Aluminum Alloy 5052	RTS-154299 COC
c2	Warning Light (Type A or C)	As Supplied	Fastenal COC
d1	3/8"-16 UNC [M10x1.5], 3 1/2" [89] Long Hex Head Bolt	ASTM A307 Gr. A or equivalent	H#18205931-3 (Coil#130075362)
d2	1/2"-13 UNC [M14x2], 6" [152] Long Hex Head Bolt	ASTM A307 Gr. A or equivalent	H#G1808306001 (Coil#210170612)
d3	1/4"-20 UNC [M6x1], 1 3/4" [44] Long Hex Head Bolt	ASTM A307 Gr. A or equivalent	H#18300616-3 (Coil#180154274)
d4	3/8" [10] Dia. Plain Round Washer	Low Carbon Steel	L#1831501 (C#210163871) (P#133008)
d5	1/2" [13] Dia. Plain Round Washer	Low Carbon Steel	C#480006818 (P#1133012)
d6	1/4" [6] Dia. Plain Round Washer	Low Carbon Steel	L#M-SWE0412056-1 (C#110243322) (P#1133004)
d7	3/8"-16 UNC [M10x1.5] Lock Nut	SAE J995 Gr. 2 or equivalent	H#321605150 (Coil#210115915)
d8	1/4"-20 UNC [M6x1] Lock Nut	SAE J995 Gr. 2 or equivalent	H#G1711322002 (Coil#210151171)

Product Comparison

PROSPECTOR®

ne LR734001 is a high density polyeth ack resistance. Typical applications inc care products. Process Hexene Copolymer Petrothene® LR734001 - LyondellBasell Industries - HDPE - Commercial: Active - Processing - Mold Shrink (English) - Processing - Polyolefin Injection Mol (English) - Technical Datasheet (English) - E62552-100622145 - LyondellBasell Industries - Petrothene® - North America - Good ESCR (Stress Crack Resist.) - Good Stiffness - Bottles - Packaging - Rigid Packaging - Extrusion Blow Molding - Petrothene®	Vene resin that exhibits g aude bottles for househol HDPE 0039 - Arnoo Pol - HDPE - Commerc ding Guide - Technical - Arnco Pol - North Arn - Copolyme - Food Con - High ESC - High Stiffr - Blow Mole - Sheet - FDA 21 C - Blow Mole - Sheet Ext - Thermofo	ood stiffness an d chemicals, foo 555P ymers ial: Active Datasheet Datasheet erica tact Acceptable omonomer R (Stress Crack ness ding Applications FR 177.1520 ding rming	d environmental d products, and Resist.)				
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Petrothene® LR734001	PRIMATOP®	1011110	- Blow Molaing - Sheet Extrusion - Thermoforming				
	HDPE 003955P	Unit	Test Method				
		ter ter	ASTM D1505				
0.953	-	g/cm*					
52	0.955	g/cm*					
(g) 0.38	0.35	g/10 min	ASTM D1238				
3							
	25.0	he	ACTM D1802D				
	45.0	br	ASTM D1803A				
25.0	40.0	br	ASTM D1693B				
Petrothene® LR734001	PRIMATOP® HDPE 003955P	Unit	Test Method				
1994 - 1990 - 2000			ASTM D638				
	4000	psi					
4000	15 4 15 4 G V V	psi					
			ASTM D638				
> 500	6.74	%					
1000 Jack 100	> 600	%					
		1	ASTM D790				
-	200000	psi	2000 A 12 19 19 19 19 19				
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Figure A-1. Plastic Panel Material Certificate, Test No. WZNP-2



ALLIED TUBE & CONDUIT PRODUCT CERTIFICATION

A PART OF A atkore

A01				A02 TYP	E OF DOCU	JMENT			A03 D	OC NO.							A06 CI	USTOMER	
ALLIED TUBE & CONDUIT PRODUCT TEST REPORT AS F 16100 S. LATHROP AVE A500; TEST METHOD AS PER HARVEY, IL 60426					ort as pe) as per	R ASTH ASTM A370		ALLIED MTR NO. 0041950								M61014 ATC/TELES	SPAR		
A07 CUST	OMER ORDER	ER PRODUCT DATE PART NO.						DIAM	ETER			GAGE		THICKNE	SS	B06 MARI	INGS		
		10/ 10/ 10/ 10/	19/18 19/18 19/18 19/18 19/18	695983 TEL-SQ PGAL/H 1.750 14 289.750 730052 TEL-SQ PGAL/H 1.750 14 216.750 914656 TELSQ PG/H 1.750 14 241.7550H0 914657 TELSQ PG/H 1.750 14 289.7550H0					750 1.750 750 1.750 ОНО 1.750 ОНО 1.750				14 .083 14 .083 14 .083 14 .083 14 .083			COATING WT908			
B01 PRODUCT: STEEL TUBING B02 SPECIFICATION: 60 MD				60 MIN	/IELD							803 Made and Manufactured in the USA			TUBE MECHANICAL TEST				
B07	B16	STEEL G	ADE:	A1011GR55				CHEMI	CAL COMP	OSITION :	z		1				C11	C12	C13
		C71	C73	C74	C75	C72	C76	C82	C80	C81	C79	C78	C77	C83		CEV	YIELD STR	TENSILE STR	El in 2"
COIL NO.	HEAT NO.	с	Mn	р	s	Si	Al	Cu	Ni	Cr	Mo	v	СЬ	Ti	N	z	KSI	KSI	z
168755 A90050 .22		.85	.011	.003	.030	.031	.120	.040	.060	.020	.001	.001	.001	.008	. 387	64.7	76.5	16.6	
ZO1 TEF	RMS AND CONDI	TIONS OF	THE SALE				Z05 C	ERTIFIC	ATIONS			Z04				202/203	Giulio Sca	rtozzi	
WE HEREBY CERTIFY THAT THE ABOVE MENTIONED MATERIAL HAS BEEN DELIVERED IN ACCORDANCE WITH THE TERMS OF THE ORDER				QS-SYST	QS-SYSTEM:ISD 9001:2008 ALLIED T 16100 S. HARVEY,					LLIED TUBE & CONDUIT MET 6100 S. LATHROP AVE ARVEY, IL 60426 USA Sign			Signature	atio Scartozzi ture: Giulio Goartozzi ALLIEDMTR-REV 00					

Figure A-2. Square Tubing Material Certificate, Test No. WZNP-2



ALLIED TUBE & CONDUIT PRODUCT CERTIFICATION

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A01	A02 TYPE OF DOCUMENT							A03 D	DC NO.				_			A06 CI	JSTOMER		
ALLIED TUBE & CONDUIT PRODUCT TEST REPORT AS P 16100 S. LATHROP AVE A500; TEST METHOD AS PER HARVEY, IL 60426					DRT AS PE D AS PER	ER ASTM ASTM A370 ALLIED MTR				ED MTR NO. 0041951				M61014 ATC/TELESPAR					
A07 CUSTOMER ORDER PRODUCT DATE PART NO.							DIAM	IETER			GAGE		THICKNE	SS	BOG MAR	INGS			
		10/ 10/	24/18 24/18	695799 914661	TEL-SQ TELSQ	PGAL/H 2 PG/H 2.00	.000 14 2 0 14 289.	289.750 75SOHO	2.00	0			14 14		.083 .083		COATING N	VT:.920	
B01 PRODU	JCT: STEEL TU	BING		B02 SPE	CIFICATIO	N: MIN 60	YIELD						B03 Made and	l Manufac ⁺	tured in t	the USA			
807	816	STEEL C	DADE	A1011CRE5			1	CHEMT			,		1				TUBE MECHAN	C12	C13
507	510	671	C73	C74	C75	672	676	CR2	CRA COMP	CRI		679	677	C 97	1	CEV	VIELD CTD	TENETIE CTD	E1 in 21
COTL NO	HEAT NO		6/3	C/4	C	C/2	41	Cu	<u> </u>	Col	679	<u> </u>	Ch				VET	TENSILE STR	EI 10 2
169112	C87907	.21	.84	.013	. 003	.040	.031	.120	.040	.080	.020	.001	.001	.001	.006	. 380	69.9	87.9	23.2
														-					
ZO1 TEF	RMS AND CONDI	TIONS OF	THE SALE				Z05 C	ERTIFICA	TIONS			Z04	TUBE & COL			Z02/Z03	Giulio Sca	rtozzi	
WE HEREBY DELIVEREI	Y CERTIFY THA D IN ACCORDAN	T THE ABOV CE WITH TH	E MENTION	NED MATERI OF THE ORD	AL HAS BE ER	EN	QS-SYST	EM:ISO 9	001:2008			16100 S	IL 60426	AVE USA		Signature	Giulio Soa	ntozzi DMTR-REV 00	

Figure A-3. Square Tubing Material Certificate, Test No. WZNP-2

60



300 Cadman Plaza West, ste 1303 Brooklyn NY 11201 Phone: 1-800-952-1457

2/13/19

CERTIFICATE OF COMPLIANCE

Smartsign hereby certifies that all materials supplied against purchase order PO: WZNP-2 / RTS-154299 shipped on 2/7/19 conforms to the material and/ or manufacturing specifications as called on this said purchase order without expectations.

Item # x-R11-2

Description: Road Closed Engineer Grade Reflective Aluminum Sign, 80 mil]

Sincerely,

Tahyna Colon Call Center Manager <u>tahyna@smartsign.com</u> 800-952-1457 x 7140

Figure A-4. Sign Certificate of Conformance, Test No. WZNP-2



Certificate of Compliance

			-	
Sold To:	Purchase Order:	WZNP-2		
UNL TRANSPORTATION/Midwest Roadside Safe	Job:	Item#c2, d1, d2, d3, d4		
	Invoice Date:	02/8/2019		
	Invoice Date:	02/8/2019		

THIS IS TO CERTIFY THAT WE HAVE SUPPLIED YOU WITH THE FOLLOWING PARTS. THESE PARTS WERE PURCHASED TO THE FOLLOWING SPECIFICATIONS.

4 PCS 7" 3V D-Cell Polycarbonate Flashing or Steady Barricade Light SUPPLIED UNDER OUR TRACE NUMBER IIne38754 AND UNDER PART NUMBER 1076058

24 PCS 3/8"-16 x 3-1/2" ASTM A307 Grade A Zinc Finish Hex Bolt SUPPLIED UNDER OUR TRACE NUMBER 130075362 AND UNDER PART NUMBER 11117

This is to certify that the above document is true and accurate to the best of my knowledge.

Fastenal Account Representative Signature

Printed Name

Date

Please check current revision to avoid using obsolete copies.

This document was printed on 02/11/2019 and was current at that time.

Fastenal Store Location/Address

3201 N. 23rd Street STE 1 LINCOLN, NE 68521 Phone #: (402)476-7900 Fax #: 402/476-7958

Page 1 of 1

Figure A-5. Warning Light Certificate of Compliance, Test No. WZNP-2


MANUFACTURER : GEM-YEAR INDUSTRIAL CO., LTD. ADDRESS : NO.8 GEM-YEAR ROAD, E.D.Z., JIASHAN, ZHEJIANG, P.R.CHINA

PURCHASER : FASTENAL COMPANY PURCHASING PO. NUMBER : 130075362 COMMODITY : HEX MACHINE BOLT GR-A SIZE : 3/8-16X3-1/2 NC LOT NO : 1B1862839 SHIP QUANTITY: 24, 400 PCS LOT QUANTITY 65, 045 PCS HEADMARKS: CYI & 307A MANUFACTURE DATE : 2018/08/14

COUNTRY OF ORIGIN : CHINA Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567 DATE : 2019/02/13 PACKING NO: GEM181024041 INVOICE NO: GEM/FNL-181112SL PART NO: 11117 SAMPLING PLAN : ASME B18. 18-2011 (Category. 2) / ASTM F1470-2012 HEAT NO : 18205931-3 MATERIAL : X1008A FINISH : Fe/Zn 3AN ASTM F1941/F1941M-2016

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO ASTM A307-2014

Chemistry	AL%	C%	MN%	P%	S%	SI%
Spec. : MIN.		1992 De 1918 991 438 19				
MAX.		0.3300	1.2500	0.0410		
Test Value	0.0300	0.0600	0. 2900	0.0090	0.0100	0. 0200

DIMENSIONAL INSPECTIONS : ACCORDING TO ASME B18. 2. 1-2012

		SAMPLEL	JET: HQIN		
INSPECTIONS ITEM	SAMPLE	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
THREAD LENGTH	15 PCS	1.0000 inch	1.1200-1.1250 inch	15	0
MAJOR DIAMETER	15 PCS	0.3640-0.3740 inch	0.3650-0.3720 inch	15	0
BODY DIAMETER	5 PCS	0.3600-0.3880 inch	0.3690-0.3730 inch	5	0
WIDTH ACROSS CORNERS	5 PCS	0.6200-0.6500 inch	0.6240-0.6490 inch	5	0
HEIGHT	5 PCS	0.2260-0.2680 inch	0.2380-0.2430 inch	5	0
NOMINAL LENGTH	15 PCS	3.4400-3.5400 inch	3.4630-3.4750 inch	15	0
WIDTH ACROSS FLATS	5 PCS	0.5440-0.5620 inch	0.5460-0.5550 inch	5	0
SURFACE DISCONTINUITIES	29 PCS	ASTM F788-2013	PASSED	29	0
THREAD	15 PCS	ASME B1. 1-2003 3A GO 2A NOGO	PASSED	15	0

MECHANICAL PROPERTIES : ACCORDING TO ASTM A 307-2014

				SAMPLE	DBY: GDAN LIAN		
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
CORE HARDNESS	15 PCS	ASTM F606-2016		Max. 100 HRB	82-84 HRB	15	0
TENSILE STRENGTH	4 PCS	ASTM F606-2016		Min. 60 KSI	77-78 KSI	4	0
PLATING THICKNESS (µ m)	29 PCS	ASTM B568-1998		>=3	3. 63–3. 89	29	0
SALT SPRAY TEST	15 PCS	ASTM B117-16		6 HOURS NO WHITE RUST, 12 HOURS NO RED RUST	ОК	15	0

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER:3358.01) WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER. WE CERTIFY THAT ALL PRODUCTS WE SUPPLIED ARE IN COMPLIANCE WITH DIN EN 10204 3.1 CONTENT

Figure A-6. Hex Bolt Material Certificate, Test No. WZNP-2



MANUFACTURER :GEM-YEAR INDUSTRIAL CO., LTD. ADDRESS : NO.8 GEM-YEAR ROAD,E.D.Z.,JIASHAN,ZHEJIANG,P.R.CHINA

PURCHASER : FASTENAL COMPANY PURCHASING PO. NUMBER : 210170612 COMMODITY : HEX MACHINE BOLT GR-A SIZE : 1/2-13X6 NC LOT NO : 1B1891613 SHIP QUANTITY : 4, 320 PCS LOT QUANTITY : 17, 397 PCS HEADMARKS : CYI & 307A

MANUFACTURE DATE : 2018/11/07

COUNTRY OF ORIGIN : CHINA

Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567 DATE: 2019/01/31 PACKING NO: GEM181114014 INVOICE NO: GEM/FNL-181128ED PART NO: 11225 SAMPLING PLAN: ASME B18. 18-2011 (Category. 2) /ASTM F1470-2012 HEAT NO: G1808306001 MATERIAL: ML08 FINISH: Fe/Zn 3AN ASTM F1941/F1941M-2016

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO ASTM A307-2014

Chemistry	AL%	C%	MN%	P%	S%	SI%
Spec. : MIN.						
MAX.		0.3300	1.2500	0.0410		
Test Value	0.0330	0.0800	0.3900	0.0210	0.0040	0.0400

DIMENSIONAL INSPECTIONS : ACCORDING TO ASME B18. 2. 1-2012

		SAMPLED	BY: HQIN		
INSPECTIONS ITEM	SAMPLE	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
THREAD LENGTH	15 PCS	1.2500 inch	1.3570-1.3590 inch	15	0
MAJOR DIAMETER	15 PCS	0.4880-0.4980 inch	0.4910-0.4930 inch	15	0
BODY DIAMETER	4 PCS	0.4820-0.5150 inch	0.5040-0.5070 inch	4	0
WIDTH ACROSS CORNERS	4 PCS	0.8260-0.8660 inch	0.8350-0.8400 inch	4	0
HEIGHT	4 PCS	0.3020-0.3640 inch	0.3360-0.3390 inch	4	0
NOMINAL LENGTH	15 PCS	5.9000-6.0000 inch	5.9160-5.9630 inch	15	0
WIDTH ACROSS FLATS	4 PCS	0.7250-0.7500 inch	0.7390-0.7450 inch	4	0
SURFACE DISCONTINUITIES	29 PCS	ASTM F788-2013	PASSED	29	0
THREAD	15 PCS	ASME B1.1-2003 3A GO 2A NOGO	PASSED	15	0

MECHANICAL PROPERTIES : ACCORDING TO ASTM A 307-2014

				SAMPLE	DBY: ZLINGLING						
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ.				
CORE HARDNESS	15 PCS	ASTM F606-2016		Max. 100 HRB	82–86 HRB	15	0				
TENSILE STRENGTH	4 PCS	ASTM F606-2016		Min. 60 KSI	76-81 KSI	4	0				
PLATING THICKNESS(µm)	4 PCS	ASTM B568-1998		>=3	3. 22-3. 36	4	0				
SALT SPRAY TEST	15 PCS	ASTM B117-16		6 HOURS NO WHITE RUST, 12 HOURS NO RED RUST	ОК	15	0				

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER:3358.01) WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER WE CERTIFY THAT ALL PRODUCTS WE SUPPLIED ARE IN COMPLIANCE WITH DIN EN 10204 3.1 CONTENT

page 1 of 2

Figure A-7. Hex Bolt Material Certificate, Test No. WZNP-2



MANUFACTURER :GEM-YEAR INDUSTRIAL CO., LTD. ADDRESS : NO.8 GEM-YEAR ROAD,E.D.Z.,JIASHAN,ZHEJIANG,P.R.CHINA

PURCHASER : FASTENAL COMPANY PURCHASING PO. NUMBER : 180154274 COMMODITY : HEX MACHINE BOLT GR-A SIZE : 1/4-20X1-3/4 NC LOT NO : 1B1840908 SHIP QUANTITY : 115, 200 PCS LOT QUANTITY 173, 017 PCS HEADMARKS : CYI & 307A

MANUFACTURE DATE : 2018/07/03

COUNTRY OF ORIGIN : CHINA

Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567 DATE : 2019/01/31 PACKING NO : GEM180718006 INVOICE NO : GEM/FNL-180806DE PART NO : 11010 SAMPLING PLAN : ASWE B18. 18-2011 (Category. 2) /ASTM F1470-2012 HEAT NO : 18300616-3 MATERIAL : X1008A FINISH : Fe/Zn 3AN ASTM F1941/F1941M-2016

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO ASTM A307-2014

Chemistry	AL%	C%	MN%	P%	S%	SI%
Spec. : MIN.		1992 De 1918 991 438 19				
MAX.		0.3300	1.2500	0.0410		
Test Value	0.0500	0.0700	0. 2900	0.0140	0.0090	0. 0300

DIMENSIONAL INSPECTIONS : ACCORDING TO ASME B18. 2. 1-2012

		SAMPLED	BY: WDANDAN		
INSPECTIONS ITEM	SAMPLE	SPECIFIED	ACTUAL RESULT	ACC.	REJ
THREAD LENGTH	15 PCS	0.7500 inch	0.8260-0.8420 inch	15	0
MAJOR DIAMETER	15 PCS	0.2410-0.2490 inch	0.2460-0.2480 inch	15	0
BODY DIAMETER	6 PCS	0.2370-0.2600 inch	0.2450-0.2480 inch	6	0
WIDTH ACROSS CORNERS	6 PCS	0.4840-0.5050 inch	0.4910-0.4930 inch	6	0
HEIGHT	6 PCS	0.1500-0.1880 inch	0.1570-0.1600 inch	6	0
NOMINAL LENGTH	15 PCS	1.7100-1.7700 inch	1.7330-1.7400 inch	15	0
WIDTH ACROSS FLATS	6 PCS	0.4250-0.4380 inch	0.4320-0.4340 inch	6	0
SURFACE DISCONTINUITIES	29 PCS	ASTM F788-2013	PASSED	29	0
THREAD	15 PCS	ASME B1. 1-2003 3A GO 2A NOGO	PASSED	15	0

MECHANICAL PROPERTIES : ACCORDING TO ASTM A 307-2014

		,		SAMPLE	DBY: ZLINGLING					
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ.			
CORE HARDNESS	15 PCS	ASTM F606-2016		Max. 100 HRB	76–78 HRB	15	0			
TENSILE STRENGTH	5 PCS	ASTM F606-2016		Min. 60 KSI	67-70 KSI	5	0			
PLATING THICKNESS (µ m)	4 PCS	ASTM B568-1998		>=3	3. 21-3. 44	4	0			
SALT SPRAY TEST	15 PCS	ASTM B117-16	1	6 HOURS NO WHITE RUST, 12 HOURS NO RED RUST	ОК	15	0			

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER:3358.01) WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER WE CERTIFY THAT ALL PRODUCTS WE SUPPLIED ARE IN COMPLIANCE WITH DIN EN 10204 3.1 CONTENT

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Figure A-8. Hex Bolt Material Certificate, Test No. WZNP-2

CERTIFIED MATERIAL TEST REPORT FOR USS FLAT WASHERS ZP

FACTORY: IFI & Morg	an Ltd	II. '	REPORT DATE:	12/2/2019	
ADDRESS: Chang an N	iorth Road, wuyuan Town	, Haiyan,Znejiang	MFG LOT NUMBER:	1831501	
SAMPLING PLAN PER AS	SME B18.18-11	1 (10000.00	PO NUMBER:	210163871	
HEADMARKS: NO MARK	QNTY(Lot size):	144000PCS	PART NO:	133008	1
DIMENSIONAL INSPECTI	IONS	SPECIFICA	TION: ASTM B18.21.1-	2011	
CHARACTERISTICS	SPECIFIED ************	****	ACTUAL RESULT	ACC. *******	REJ. *******
APPEARANCE	ASTM F844		PASSED	100	0
OUTSIDE DIA	0.993-1.030		0.996-1.004	10	0
INSIDE DIA	0.433-0.453		0.443-0.450	10	0
THICKNESS	0.064-0.104		0.064-0.079	10	0
CHARACTERISTICS	TEST METHOD ************************************	SPECIFIED	ACTUAL RESULT	ACC. *******	REJ. *******
ZINC PLATED	ASTM F1941	Min 3 um	3-4um	8	0
ALL TESTS IN ACCO ASTM SPECIFICATION INFORMATION PROVI ISO 9001:2015 SGS Certi	RDANCE WITH THE M N. WE CERTIFY THA' DED BY THE MATERI/ ficate # HK04/0105	ethods prescr F THIS DAIA IS AL SUPPLIER 检验 QUANLI	ATRUE REPRES A TRUE REPRES ORGAN TESTING 专用章 TY CONTROL	ICABLE ENTATION LABORAT	N OF ORY.

Figure A-9. Flat Washer Material Certificate, Test No. WZNP-2

CERTIFIED MATERIAL TEST REPORT FOR USS FLAT WASHERS ZP

FACTORY: IFI & Mon	rgan Ltd North Road, Wuwung	Town Haiyan Zhaijar	REPORT DATE:	2018-05-09	
ADDRESS. Chang an	North Road, wuyuan	10wii, Maryan,Zhejiai	MANUFACTURE DAT	ГЕ:	
CUSTOMER:			MFG LOT NUMBER:		
SAMPLING PLAN PER A	SME B18.18-11	A (A 50 D 30	PO NUMBER:	480006818	
SIZE: USS 1/2 ZP HEADMARKS: NO MAR	QNTY(Lot s K	ize): 26250PCS	PART NO:	1133012	
DIMENSIONAL INSPEC	TIONS	SPECIFICA	TION: ASTM B18 21 1-	2011	
CHARACTERISTICS	SPECII ***********	TED ******	ACTUAL RESULT ****************	ACC.	REJ. ******
APPEARANCE	ASTM F8	344	PASSED	100	0
OUTSIDE DIA	1.368-1.405		1.370-1.378	10	0
INSIDE DIA	0.557-0.577		0.567-0.575	10	0
THICKNESS	0.086-0.132		0.086-0.102	10	0
CHARACTERISTICS ******	TEST METHOD ******	SPECIFIED ******	ACTUAL RESULT *********	ACC. ******	REJ. ******
ZINC PLATED	ASTM F1941	Min 3 um	3-4um	8	0
ALL TESTS IN ACCO ASTM SPECIFICATION INFORMATION PROVID MFG ISO9002 CERTIFIC.	DRDANCE WITH TH I. WE CERTIFY TH DED BY THE MATER ATE NO. HK04/0105	E METHODS PRESCH AT THIS DALA FOR IAL SUPPLIER AND (检验专 (SIGNATOLE OF Q.A (NAME OF MANU	RIBED IN THE APPL ROP REPRESENTAT DUR TESEING LABOR 用章 CONTROL . LAB (KIR.) FACTURER)	ICABLE ION OF ATORY.	

Figure A-10. Flat Washer Material Certificate, Test No. WZNP-2

TEST REPORT

USS FLAT WASHER, ZP

CUSTOMER:			DATE: 2018-11-12	1	
PO NUMBER: 110243322		MFG LOT	NUMBER: M-SWE041	2056-1	
SIZE: 1/4		F	PART NO: 1133004		
HEADMARKS:			QNTY:	540,000	PCS
DIMENSIONAL INSPECTION	S	SPECIFI	ICATION: ASME B18	.21.1(2009)
CHARACTERISTICS	SPE	CIFIED	ACTUAL RESULT	ACC.	REJ.
*****	********	*****	******	******	******
APPEARANCE	AS	TM F788-07	PASSED	100	0
OUTSIDE DIA	0.	727-0.749	0.730-0.732	8	0
INSIDE DIA	0.	307-0.327	0.321-0.323	8	0
THICKNESS	0.	.051-0.080	0.053-0.056	8	0
	ASTM 1941/F1941M	Min 2 um	36-41 um	8	•
ZINGTERTED	FE/ZN 3AN		5.5-4.1 µ III	Ŭ	U
Salt Spray test result	ASTM B117	Min 6 hrs No White Rust	Pass	8	0
ALL TESTS IN ACCORDANCE W WE CERTIFY THAT THIS DAIA I SUPPLIER AND OUR TESTING I MFG ISO 9001:2015 SGS Certific	/ITH THE METHO S A TRUE REPR _ABORATORY. ate # HK04/0105	DDS PRESCRIBED IN THE APPRESENTATION OF INFORMATIO	DICABLE ASTM SPECIF DN PROVIDED BY THE 他整专用章 QUALITY CONTROL JRE OF Q.A. LAB M OF MANUFACTURE	FICATION. MATERIAL GR.) :R)	-

IFI & MORGAN LTD.

ADDRESS: Chang'an North Road, Wuyuan Town, Haiyan, Zhejiang, China

Figure A-11. Flat Washer Test Report, Test No. WZNP-2



MANUFACTURER GEM-YEAR INDUSTRIAL CO., LTD. ADDRESS : NO.8 GEM-YEAR ROAD,E.D.Z., JIASHAN, ZHEJIANG, P.R. CHINA

PURCHASER : FASTENAL COMPANY PURCHASING PO. NUMBER : 210115915 COMMODITY : NYLON INSERT NUT GR-A SIZE : 3/8-16 NC LOT NO : IN1680060 SHIP QUANTITY : 150,000 PCS LOT QUANTITY : 150,000 PCS LOT QUANTITY : 378,534 PCS HEADMARKS : GENIUS SYMBOL MANUFACTURE DATE : 2016/09/06 COUNTRY OF ORIGIN : CHINA Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567 DATE: 2018/05/09 PACKING NO: GEM/61201020 INVOICE NO: GEM/FNL-161213ED PART NO: 1137024 SAMPLING PLAN: ASME B18.18-2011(Category.2)/ASTM F1470-2012 HEAT NO: 321605150 MATERIAL: ML08 FINISH: FeZn3AN ASTM F1941/F1941M-2016

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO IFI 100/107 GR-A

Chemistry	AL%	С%	MN%	P%	S%	SI%
Spec. : MIN.						
MAX.		0.5800		0.1300	0.2300	
Test Value	0.0380	0.0800	0.4300	0.0130	0.0040	0.0600

DIMENSIONAL INSPECTIONS ACCORDING TO ASIME B18.16.6-2014

		UCIMIT LEL	DI TYÓNG
INSPECTIONS ITEM	SAMPLE	SPECIFIED	ACTUAL RESULT ACC. REJ
WIDTH ACROSS CORNERS	6PCS	Min. 0.6220 inch	0.6250-0.6290 inch 6 0
THICKNESS	6 PCS	0.4380-0.4680 inch	0.4410-0.4640 inch 6 0
WIDTH ACROSS FLATS	6PCS	0.5510-0.5640 inch	0.5540-0.5610 inch 6 0
SURFACE DISCONTINUITE	S 29 PCS	ASTM F812-2012	PASSED 29 0
THREAD	15PCS	GAGING SYSTEM 21	PASSED 15 0

MECHANICAL PROPERTIES : ACCORDING TO IFI 100/107 GR-A

SAMPLED BY : GDAN LIAN

PAMPIED BY . I VOINTO

			ODIN' DUN	
INSPECTIONS ITEM	SAMPLE TEST METHOD	REF SPECIFIED	A CTUAL RESULT	ACC. REJ.
CORE HARDNESS	15PCS ASTMF606-2014	Max 104 HRB	86-87 HRB	15 (
PROOF LOAD	5PCS ASTMF606-2014	Min. 7,000 LBF	OK	5 0
PLATING THICKNESS(µm)	29 PCS ASTM B568-1998	>=3	3.21-5	29; 0
SALT SPRAY TEST	15 PCS ASTM B117-16	6 HOURS NO WHITE RUS 12 HOURS NO RED RUST	r, ok	15 0

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER: 3358.01) WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER

Quality Supervisor.

Grin

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Figure A-12. Material Certification 3/8-16 UNC Lock Nut, Test No. WZNP-2



MANUFACTURER :GEM-YEAR INDUSTRIAL CO., LTD. ADDRESS : NO.8 GEM-YEAR

ROAD, E. D. Z., JIASHAN, ZHEJIANG, P.R. CHINA PURCHASER : FASTENAL COMPANY PURCHASING PO. NUMBER : 210151171 COMMODITY : NYLON INSERT NUT GR-A SIZE : 1/4-20 NC LOT NO : 1N1820357 SHIP QUANTITY : 120, 000 PCS LOT QUANTITY 481, 402 PCS HEADMARKS : GENIUS SYMBOL MANUFACTURE DATE : 2018/05/10

COUNTRY OF ORIGIN : CHINA

Tel: (0573)84185001(48Lines) Fax: (0573)84184488 84184567 DATE: 2019/01/31 PACKING NO: GEM180628004 INVOICE NO: GEM/FNL-180713ED-1 PART NO: 1137018 SAMPLING PLAN: ASME B18. 18-2011 (Category. 2) /ASTM F1470-2012 HEAT NO: G1711322002 MATERIAL: ML08 FINISH: Fe/Zn 3AN ASTM F1941/F1941M-2016

PERCENTAGE COMPOSITION OF CHEMISTRY: ACCORDING TO ASTM A563-2015 Chemistry AL% C% MN% P% S% SI% Spec. : MIN. MAX. 0.5800 0.1300 0.2300 **Test Value** 0.0510 0.0700 0.3900 0.0110 0.0060 0.0200

DIMENSIONAL INSPECTIONS : ACCORDING TO ASME B18. 16. 6-2014

SAMPLED BY : WANGYAN ACTUAL RESULT INSPECTIONS ITEM SAMPLE SPECIFIED ACC. REJ. WIDTH ACROSS CORNERS 6 PCS Min. 0.4860 inch 0.4950-0.4960 inch 6 0 0.2980-0.3270 inch THICKNESS 6 PCS 0.3090-0.3110 inch 6 0 0.4300-0.4370 inch 0.4330-0.4350 inch WIDTH ACROSS FLATS 6 PCS 6 0 ASTM F812-2012 SURFACE DISCONTINUITIES **29 PCS** PASSED 29 0 THREAD 15 PCS GAGING SYSTEM 21 PASSED 15 0

MECHANICAL PROPERTIES : ACCORDING TO IFI 100/107 GR-A-2002

				SAMPLE	DBY: PAN LU		
INSPECTIONS ITEM	SAMPLE	TEST METHOD	REF	SPECIFIED	ACTUAL RESULT	ACC.	REJ.
PROOF LOAD	7 PCS	ASTM F606-2014		Min. 2,900 LBF	OK	7	0
FIRST INSTALL	7 PCS			Max. 40 LB.IN	12.3-13.9 LB.IN	7	0
FIRST REMOVAL	7 PCS			Min. 5 LB.IN	10.2-11.99 LB.IN	7	0
THIRD REMOVAL	7 PCS			Min. 1.5 LB.IN	6.3-7.8 LB.IN	7	0
CORE HARDNESS	15 PCS	ASTM F606-2014		Max. 104 HRB		15	0
PLATING THICKNESS(µm)	29 PCS	ASTM B568-1998		>=3	3. 06-3. 6	29	0
SALT SPRAY TEST	15 PCS	ASTM B117-16		6 HOURS NO WHITE RUST, 12 HOURS NO RED RUST	OK	15	0

WE CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED BY THE MATERIAL SUPPLIER AND OUR TESTING LABORATORY .WHICH ACCREDITED BY ISO/IEC17025(CERTIFICATE NUMBER:3358.01) WE CERTIFY THAT THE PRODUCTS SUPPLIED ARE IN COMPLIANCE WITH THE REQUIREMENTS OF THE ORDER WE CERTIFY THAT ALL PRODUCTS WE SUPPLIED ARE IN COMPLIANCE WITH DIN EN 10204 3.1 CONTENT

Quality Supervisor:

nn

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Figure A-13. Material Certification ¹/₄-20 UNC Lock Nut, Test No. WZNP-2

Appendix B. Vehicle Center of Gravity Determination

Year: Vehicle CG De Vehicle Equipme + U + H + Bit + Pit + Bit + C -	2011 etermination ent Juballasted Jub Brake activa Preumatic ta Brobe/Brake Brake Recei CG Plate inc Battery Dil Interior Gelate inc Battery Dil Coolant Vasher fluic Vasher fluic Vater Ballas Duboard Su	Make:	Dodge frame	Model: Weight (lb) 5105 19 8 31 5 6 42 -10 -104 -166 -11 -6 110 14	Vertical CG (in.) 28.378869 15.25 31 1/8 29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	Ram 1500 Vertical M (lb-in.) 144874.13 289.75 249 914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
Vehicle CG De Vehicle Equipme + U + H + Bi + Pi + Si + Si + Si - Si - O - In - Fi - C - W + W + O	eterminatio ent Inballasted Iub Brake activa Preumatic ta Probe/Brake Brake Recei CG Plate inc Battery Dil Interior Gelate inc Battery Dil Noter Fallas Daboard Su	Truck (Curb) tion cylinder & ank (Nitrogen) e Battery ver/Wires cluding DAQ	frame frame	Weight (lb) 5105 19 8 31 5 6 42 -42 -42 -10 -104 -166 -11 -6 110 14	Vertical CG (in.) 28.378869 15.25 31 1/8 29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	Vertical M (lb-in.) 144874.13 289.75 249 914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
Vehicle Equipme + U + H + B + P + Si + Bi + C - Bi - Bi - C - In - C - Note: + O	ent Inballasted Jub Brake activa Pneumatic ta Strobe/Brake Brake Recei CG Plate inc Battery Dil Interior Coolant Vasher fluic Vater Ballas Dnboard Su	Truck (Curb) tion cylinder & ank (Nitrogen) e Battery ver/Wires cluding DAQ	frame frame	Weight (lb) 5105 19 8 31 5 6 42 -42 -42 -10 -104 -166 -11 -6 110 14	Vertical CG (in.) 28.378869 15.25 31 1/8 29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	Vertical M (lb-in.) 144874.13 289.75 249 914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ U + H + B + P + Si + Si + Si + C - Bi - O - In - Fu - C - V + W + O	Jnballasted Jub Brake activa Preumatic ta Strobe/Brake Brake Recei CG Plate inc Battery Dil Interior Fuel Coolant Vasher fluic Vasher fluic Vater Ballas Dnboard Su	Truck (Curb) ition cylinder & ank (Nitrogen) e Battery iver/Wires cluding DAQ d st (In Fuel Tank pplemental Bat	frame () tery	5105 19 8 31 5 6 42 -42 -10 -104 -166 -11 -6 110 14	28.378869 15.25 31 1/8 29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	144874.13 289.75 249 914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ H + B + P + S + B + C - B - O - In - Fu - C - V + W + O	lub Brake activa Preumatic ta Strobe/Brake Brake Recei CG Plate inc Battery Dil Interior Guel Coolant Vasher fluic Vater Ballas Dnboard Su	tion cylinder & ank (Nitrogen) e Battery iver/Wires cluding DAQ d st (In Fuel Tank pplemental Bat	frame (x) tery	19 19 8 31 5 6 42 -42 -10 -104 -166 -11 -6 110 14	15.25 31 1/8 29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	289.75 249 914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ B + P + Si + B + C - Bi - O - In - Fi - C - W + W + O	Brake activa Preumatic ta Strobe/Brake Brake Recei CG Plate inc Battery Dil Interior Suel Coolant Vasher fluic Vater Ballas Dinboard Su	tion cylinder & ank (Nitrogen) e Battery ver/Wires cluding DAQ d st (In Fuel Tank pplemental Bat	frame () tery	8 31 5 6 42 -42 -10 -104 -104 -166 -11 -6 110 14	31 1/8 29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	249 914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ P + Si + B + C - Bi - O - In - Fi - C - V + W + O	Pneumatic ta Strobe/Brake Brake Recei CG Plate inc Battery Dil Interior Uel Coolant Vasher fluic Vater Ballas Onboard Su	ank (Nitrogen) e Battery ver/Wires cluding DAQ st (In Fuel Tank pplemental Bat	k) tery	31 5 6 42 -42 -10 -104 -104 -166 -11 -6 110 14	29 1/2 27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	914.5 136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ Si + B - Bi - O - In - In - Fr - C - W + W + O	Strobe/Brake Brake Recei CG Plate inc Battery Dil Interior Fuel Coolant Vasher fluic Vasher fluic Vater Ballas Dnboard Su	e Battery iver/Wires cluding DAQ st (In Fuel Tank pplemental Bat	k) tery	5 6 42 -42 -10 -104 -166 -11 -6 110 14	27 1/4 52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	136.25 313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ B + C - B; - O - In - Fr - C - V + W + O	Brake Recei CG Plate inc Battery Dil Interior Guel Coolant Vasher fluic Vater Ballas Dinboard Su	ver/Wires cluding DAQ d st (In Fuel Tank pplemental Bat	k) tery	6 42 -42 -10 -104 -166 -11 -6 110 14	52 1/4 30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	313.5 1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
+ C - Bi - O - In - Fr - C - W + W + O	CG Plate ind Battery Dil Interior Guel Coolant Vasher fluic Vater Ballas Onboard Su	cluding DAQ I st (In Fuel Tank pplemental Bat	k) tery	42 -42 -10 -104 -166 -11 -6 110 14	30 7/8 38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	1296.75 -1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
- B - O - In - Fu - C - W + W + O	Battery Dil Fuel Coolant Vasher fluic Vater Ballas Onboard Su	l st (In Fuel Tank pplemental Bat	k) tery	-42 -10 -104 -166 -11 -6 110 14	38 1/4 8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	-1606.5 -85 -3523 -3071 -401.5 -222.75 1966.25	
- O - In - Fr - C - W + W + O	Dil Interior Coolant Vasher fluic Vater Ballas Onboard Su	l st (In Fuel Tank pplemental Bat	k) tery	-10 -104 -166 -11 -6 110 14	8 1/2 33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	-85 -3523 -3071 -401.5 -222.75 1966 25	
- In - Fi - C - W + W + O	nterior Goolant Vasher fluic Vater Ballas Onboard Su	l st (In Fuel Tank pplemental Bat	() tery	-104 -166 -11 -6 110 14	33 7/8 18 1/2 36 1/2 37 1/8 17 7/8	-3523 -3071 -401.5 -222.75 1966 25	
- Fi - C - W + W + O	uel Coolant Vasher fluic Vater Ballas Onboard Su	t st (In Fuel Tank pplemental Bat	() tery	-166 -11 -6 110 14	18 1/2 36 1/2 37 1/8 17 7/8	-3071 -401.5 -222.75 1966 25	
- C - W + W + O	Coolant Vasher fluic Vater Ballas Onboard Su	l st (In Fuel Tank pplemental Bat	() tery	-11 -6 110 14	36 1/2 37 1/8 17 7/8	-401.5 -222.75 1966 25	
- W + N + O	Vasher fluic Vater Ballas Onboard Su equipment to v	l st (In Fuel Tank pplemental Bat	⁽⁾ tery	-6 110 14	37 1/8 17 7/8	-222.75 1966.25	
+ W + O	Vater Ballas Onboard Su equipment to v	st (In Fuel Tanl pplemental Bat	() tery	110 14	17 7/8	1966 25	
+ O	Onboard Su	pplemental Bat	tery	14		1000.20	
Note: (+) is added ea	equipment to v				24 1/2	343	1
Note: (+) is added ea	equipment to v					0	1
Note: (+) is added e	equipment to v					0	
Vehicle Dimens	sions for C	G Calculatio	ins				
Wheel Base:	140.75	in.	Front Tr Rear Tr	ack Width: ack Width:	67.875 67.375	in. in.	
Center of Gravi	ity	2270P MAS	H Targets	5	Test Inertial		Difference
Test Inertial Wei	eight (lb)	5000 :	± 110		5001		1.0
Longitudinal CG	6 (in.)	63 :	± 4		61.55174		-1.44820
Lateral CG (in.))	NA			-0.223118		NA
Vertical CG (in.)	.)	28 0	or greater		28.29		0.28902
Note: Long. CG is n	measured fror	n front axle of test	vehicle				
Note: Lateral CG m	neasured from	ı centerline - positi	ve to vehicle rig	ht (passenger) side		
					TEST INER	TIAL WEIGH	T (lb)
CURB WEIGHT	Г (Ib)					l off	Diaht
CURB WEIGHT	Г (Ib)	Diaht			Front		1206
CURB WEIGHT	Left	Right				1410	1090
CURB WEIGHT	Г (Ib) Left 1439	Right 1436			Poar		1000
CURB WEIGHT Front Rear	Г (Ib) Left 1439 1132	Right 1436 1098			Rear	1099	
CURB WEIGHT Front Rear	Left 1439 1132	Right 1436 1098			Rear	2814	lb
CURB WEIGHT Front Rear FRONT REAR	r (lb) Left 1439 1132 2875 2230	Right 1436 1098 Ib			Rear FRONT REAR	2814 2187	lb lb

Figure B-1. Vehicle Mass Distribution, Test No. WZNP-2

Appendix C. Vehicle Deformation Records

Date: Year:	3/14/ 20	2019 11			Test Name: Make:	WZ Do	NP-2 dge			VIN: Model:	1D7R	B1GP6BS6 Ram 1500	34520
					VE DRIVE	HICLE DE R SIDE FL	FORMATIO	ON - SET 1					
	POINT	Pretest X (in.)	Pretest Y (in.)	Pretest Z (in.)	Posttest X (in.)	Posttest Y (in.)	Posttest Z (in.)	∆X ^A (in.)	ΔΥ ^Α (in.)	∆Z ^A (in.)	Total ∆ (in.)	Crush ^B (in.)	Directions for Crush ^C
	1	51.8916	-6.6450	2.5037	51.9362	-6.5510	2.6133	-0.0446	0.0940	-0.1096	0.1511	0.0000	NA
	2	51.8723	-10.9186	2.5255	51.9275	-10.8757	2.6115	-0.0552	0.0429	-0.0860	0.1108	0.0000	NA
	3	52.0198	-14.9467	2.4394	52.0644	-14.7746	2.5336	-0.0446	0.1721	-0.0942	0.2012	0.0000	NA
ż	4	52.1428	-18.7576	2.3779	52.2189	-18.6352	2.4563	-0.0761	0.1224	-0.0784	0.1641	0.0000	NA
Z VAI	5	52.2128	-23.3626	2.3547	52.2589	-23.3181	2.4527	-0.0461	0.0445	-0.0980	0.1171	0.0000	NA
ШШ×	6	48.8720	-7.3045	4.1454	48.9605	-7.2282	4.2111	-0.0885	0.0763	-0.0657	0.1341	0.0000	NA
은 뿐 이	7	48.7919	-12.3588	4.1818	48.8456	-12.2710	4.2676	-0.0537	0.0878	-0.0858	0.1340	0.0000	NA
` >	8	48.6769	-15.8111	4.2517	48.7174	-15.7080	4.3454	-0.0405	0.1031	-0.0937	0.1451	0.0000	NA
	9	48.6398	-20,5447	4.2734	48,7246	-20.4539	4.3451	-0.0848	0.0908	-0.0717	0.1434	0.0000	NA
	10	48.6334	-23.2506	4.2853	48.6774	-23.2441	4.3807	-0.0440	0.0065	-0.0954	0.1053	0.0000	NA
	11	45.6275	-7.0316	4.9671	45.6655	-6.9442	5.0526	-0.0380	0.0874	-0.0855	0.1280	-0.0855	Z
	12	45.3625	-10.6772	4,9531	45,4544	-10.6120	5.0407	-0.0919	0.0652	-0.0876	0.1427	-0.0876	Z
	13	45,3505	-14.8207	4,9455	45,4544	-14,7488	5.0288	-0.1039	0.0719	-0.0833	0.1513	-0.0833	Z
	14	45.1717	-18.8420	4.9357	45.2436	-18,7276	5.0216	-0.0719	0.1144	-0.0859	0.1601	-0.0859	z
	15	44,9526	-23,1484	4,9350	45.0728	-23.0885	5.0214	-0.1202	0.0599	-0.0864	0.1597	-0.0864	Z
	16	40.0968	-7.0930	5.0053	40.1746	-6,9956	5.0845	-0.0778	0.0974	-0.0792	0.1477	-0.0792	z
	17	39 7516	-10.1620	5 0081	39 8443	-10.0536	5.0920	-0.0927	0 1084	-0.0839	0.1655	-0.0839	Z
-	18	39.6125	-14.8832	4,9861	39,7387	-14.8093	5.0701	-0.1262	0.0739	-0.0840	0.1687	-0.0840	Z
AN	19	39.3352	-18.6599	4.9736	39.4107	-18.5685	5.0588	-0.0755	0.0914	-0.0852	0.1460	-0.0852	z
d \sim	20	39 0867	-22 8627	4 9777	39 2563	-22 8507	5 0617	-0 1696	0.0120	-0.0840	0 1896	-0.0840	7
Ϋ́Ν	21	34.6751	-7.2307	5.0420	34,7866	-7.1182	5.1202	-0.1115	0.1125	-0.0782	0.1766	-0.0782	z
2	22	34,7240	-10,4481	5.0430	34.8201	-10.3638	5.1355	-0.0961	0.0843	-0.0925	0.1578	-0.0925	z
ш	23	34,7073	-13.6927	5.0213	34,8027	-13.6150	5.1115	-0.0954	0.0777	-0.0902	0.1526	-0.0902	Z
	24	34.6600	-17.8361	4,9983	34,7723	-17,7863	5.0860	-0.1123	0.0498	-0.0877	0.1509	-0.0877	z
	25	34,9396	-22,9962	5.0184	35.0635	-22.9491	5.1074	-0.1239	0.0471	-0.0890	0.1597	-0.0890	Z
	26	30,9602	-8,1917	4.3196	31.0421	-8.0920	4.3975	-0.0819	0.0997	-0.0779	0.1507	-0.0779	Z
	27	31.0995	-11.5599	4.3043	31,1627	-11.5403	4.3879	-0.0632	0.0196	-0.0836	0.1066	-0.0836	z
	28	31.2355	-14,9993	4.0673	31.3688	-14.9636	4.1619	-0.1333	0.0357	-0.0946	0.1673	-0.0946	Z
	29	31,2803	-18.6329	4.2668	31.3556	-18.5869	4.3467	-0.0753	0.0460	-0.0799	0.1190	-0.0799	z
	30	31.3844	-23.5078	4.2554	31.4496	-23.4208	4.3373	-0.0652	0.0870	-0.0819	0.1361	-0.0819	Z

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



Figure C-1. Left Floor Pan Deformation Data – Set 1, Test No. WZNP-2

Date:	3/14/	2019			Test Name:	wz	NP-2			VIN:	1D7R	B1GP6BS6	34520
Year:	20	111			Make:	Do	dge			Model:	-	Ram 1500	
					VE DRIVE	HICLE DE R SIDE FL	FORMATIO	ON - SET 2					
	POINT	Pretest X (in.)	Pretest Y (in)	Pretest Z	Posttest X (in.)	Posttest Y (in.)	Posttest Z (in.)	∆X ^A (in.)	ΔΥ ^Α (in.)	∆Z ^A (in.)	Total ∆ (in.)	Crush ^B (in.)	Directions for
	1	54 2701	25 1445	1 3346	54.0635	25 1045	1 1967	0.2156	0.0400	0 1470	0.2645	0.2156	v
	2	54 3452	-29.1445	-1.3340	54.0055	-29.1043	-1.7007	0.2198	0.0400	-0.1473	0.2045	0.2130	Ŷ
801	3	54 5516	-23.4525	-1 3945	54.3286	-33 3245	-1.2020	0.2230	0.1329	-0.1237	0.2323	0.2100	X
그 규	4	54 7471	-37 2543	-1 4512	54 5475	-37 1818	-1.3809	0.2200	0.0725	-0.0703	0.2237	0.1996	X
Z NA	5	54 8732	-41 9008	-1 4484	54 6651	-41 8634	-1.3994	0.2081	0.0374	-0.0490	0.2170	0.2081	X
ШЩ×	6	51 2412	-25 8844	0 2952	51 0862	-25 8362	0 3838	0 1550	0.0482	-0.0886	0 1849	0 1550	X
응필)	7	51 2340	-30 8952	0.3501	51 0544	-30 8804	0 4228	0 1796	0.0148	-0.0727	0 1943	0 1796	X
	8	51,1895	-34.3910	0.4205	50.9825	-34.3193	0.4884	0.2070	0.0717	-0.0679	0.2293	0.2070	X
	9	51,2450	-39.0883	0.4480	51.0682	-39.0644	0.4726	0.1768	0.0239	-0.0246	0.1801	0.1768	X
	10	51.2992	-41.8327	0.4597	51.0669	-41.8551	0.4987	0.2323	-0.0224	-0.0390	0.2366	0.2323	X
	11	47.9996	-25.6892	1.0933	47.7801	-25.6096	1.1985	0.2195	0.0796	-0.1052	0.2561	-0.1052	Z
	12	47.7716	-29.3258	1.0948	47.6298	-29.2803	1.1729	0.1418	0.0455	-0.0781	0.1682	-0.0781	Z
	13	47.8531	-33.4732	1.0886	47.6984	-33.4165	1.1475	0.1547	0.0567	-0.0589	0.1750	-0.0589	Z
	14	47.7344	-37.4559	1.0886	47.5536	-37.3981	1.1255	0.1808	0.0578	-0.0369	0.1934	-0.0369	Z
	15	47.6623	-41.8009	1.0949	47.4550	-41.7613	1.1096	0.2073	0.0396	-0.0147	0.2116	-0.0147	Z
	16	42.4830	-25.8186	1.1129	42.2907	-25.7518	1.1842	0.1923	0.0668	-0.0713	0.2157	-0.0713	Z
	17	42.1521	-28.9059	1.1195	42.0110	-28.8149	1.1790	0.1411	0.0910	-0.0595	0.1781	-0.0595	Z
7	18	42.1579	-33.6165	1.1081	41.9843	-33.5716	1.1407	0.1736	0.0449	-0.0326	0.1823	-0.0326	Z
A	19	41.8901	-37.3951	1.1028	41.7187	-37.3357	1.1143	0.1714	0.0594	-0.0115	0.1818	-0.0115	Z
4 61	20	41.7933	-41.6316	1.1170	41.6352	-41.6198	1.1019	0.1581	0.0118	0.0151	0.1593	0.0151	Z
NO N	21	37.0754	-26.0307	1.1270	36.9053	-25.9636	1.1743	0.1701	0.0671	-0.0473	0.1889	-0.0473	Z
L C	22	37.1407	-29.2867	1.1390	36.9925	-29.2083	1.1793	0.1482	0.0784	-0.0403	0.1724	-0.0403	Z
<u>ш</u>	23	37.2109	-32.5154	1.1222	37.0291	-32.4592	1.1446	0.1818	0.0562	-0.0224	0.1916	-0.0224	Z
	24	37.2474	-36.6499	1.1068	37.0680	-36.6303	1.1051	0.1794	0.0196	0.0017	0.1805	0.0017	Z
	25	37.6381	-41.8321	1.1419	37.4444	-41.7877	1.1121	0.1937	0.0444	0.0298	0.2009	0.0298	Z
	26	33.3372	-27.0516	0.3880	33.1836	-26.9967	0.4171	0.1536	0.0549	-0.0291	0.1657	-0.0291	Z
	27	33.5837	-30.4838	0.3852	33.3614	-30.4425	0.3972	0.2223	0.0413	-0.0120	0.2264	-0.0120	Z
	28	33.7798	-33.8859	0.1593	33.6261	-33.8611	0.1618	0.1537	0.0248	-0.0025	0.1557	-0.0025	Z
	29	33.8447	-37.5328	0.3623	33.6713	-37.4848	0.3346	0.1734	0.0480	0.0277	0.1820	0.0277	Z
	30	34.0531	-42.3419	0.3665	33.8453	-42.3164	0.3102	0.2078	0.0255	0.0563	0.2168	0.0563	Z

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



Figure C-2. Left Floor Pan Deformation Data – Set 2, Test No. WZNP-2

Prove Provided Provid	Year:	20	11			Make:	Do	dge			Model:	10713	Ram 1500	04020
VENICLE DE-DYNMAILON DRIVER DISCIPCION DRIVER DISCIPCION TOTAL DISCIPCION Colspan="2">Colspan="2" <colspan="2">Colspan="2"Colspan="2"<colspan="2"<colspan="2"<colspan="2"<colspan="2"<colspa< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>~~~</th><th></th><th></th><th>8</th><th></th><th></th></colspan="2"<colspan="2"<colspan="2"<colspan="2"<colspa<></colspan="2">									~~~			8		
UNIVER SIDE INTERNOR CRUSH - Set 1 POINT Pretest Pretest Postest X Postest Z N/L N/L N/L Dire 1 42.5702 47.324 24.16471 -7.237 24.8667 41.3715 -5.8213 28.766 0.0365 1.3059 0.0683 1.3892 1.3891 1.3891 1.28						VE	HICLE DE	FORMATIO						
Protest POINT Protest (n) Protest POINT Protest (n) Postest X (n) Postest X (n) Postest X (n) Ax^A (n) Ax^A (n) Ax^A (n) Ax^A (n) Ax^A (n) Disc (n) Pointest Z (n) Pointest Z (n)						DRIVER S	IDE INTER	RIOR CRUS	5H - SET 1					
POINT Ym Ym Ym Ym Postest Y Postes Y	Г		Pretest	Pretest	Pretest			100 - 100 - 1000				675276 1 N 1 N		Direction
POINT (in) (in) </td <td></td> <td></td> <td>X</td> <td>Y</td> <td>Z</td> <td>Posttest X</td> <td>Posttest Y</td> <td>Posttest Z</td> <td>ΔX^A</td> <td>ΔY^A</td> <td>ΔZ^A</td> <td>Total ∆</td> <td>Crush^B</td> <td>for</td>			X	Y	Z	Posttest X	Posttest Y	Posttest Z	ΔX ^A	ΔY ^A	ΔZ ^A	Total ∆	Crush ^B	for
1 42.5702 4.52702 4.52702 4.52702 4.52702 4.52702 4.52702 1.5079 X. 3 4.15465 1-9.1544 29.3166 1.7373 -59.266 1.3763 0.0995 1.3982 X. 3.3982 X. 5 37.6341 7.2376 2.8261 7.7333 -29.2481 0.1802 1.3763 0.0966 1.4441 X. 6 381.395 -26.2796 1.6221 35.6657 2.42395 1.62239 0.4272 1.3401 0.0564 1.3383 1.3383 X. 9 50.5436 -27.75146 1.6335 42.2352 -22.2303 -0.0214 0.1264 0.1294 0.0245 0.1711 0.2485 0.1524 0.1741 0.2485 0.1524 0.1711 0.2485 0.1524 0.0266 0.1284 0.0267 0.1411 0.2485 0.1524 0.0267 0.1414 0.0487 0.4245 0.0267 0.1414 0.1426 0.22750 0.1110 0.2425 0.2750		POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(In.)	(in.)	(in.)	(in.)	(in.)	(in.)	Crush
Product 2 41.5871 -7.2876 -28.6667 -1.3715 -5.9213 -28.7664 0.2256 1.3705 0.0863 1.3982 1.3982 X. 4 35.6617 4.6981 -17.5158 38.4472 5.9183 -17.4292 0.8065 1.2851 X. 6 33.1395 -26.2766 -16.3221 0.3331 1.2946 0.0664 1.3851 X. 6 33.1395 -26.2766 -16.3221 0.23315 -16.2237 0.3331 1.2946 1.2841 1.2841 X. 7 47.5542 -27.5193 -52.855 47.8794 -26.2793 -0.03168 1.2444 0.0651 1.2891 1.2441 9 50.5436 -27.4897 3.7301 -20.2064 0.1524 0.1734 0.2254 0.0596 10 37.4867 -29.5391 9.9758 15.803 -29.2478 -0.0587 0.1000 0.1224 0.1734 0.2256 0.0596 112 127.739 -28.5685		1	42.5702	4.5249	-28.2140	41.9196	5.8818	-28.1181	0.6506	-1.3569	0.0959	1.5079	1.5079	X, Y, Z
3 41.5465 -19.1544 -29.3166 41.7347 -17.7339 -29.2481 -0.1882 1.7370 -0.0885 1.3851 1.3851 1.3851 1.3851 X. 5 37.6341 -7.2334 -16.2971 5.9183 -7.2324 -0.0222 1.2401 0.0686 1.4441 X. 6 38.1395 -28.2786 -16.2327 0.4227 1.3401 1.4100 X. 9 50.5436 -27.5447 -3.2585 74.835 -22.2393 -0.2221 1.4441 0.1264 1.2481 0.0284 0.1524 0.1791 0.2485 0.1524 0.1791 0.2485 0.1524 0.1791 0.2485 0.1524 0.0896 0.0896 0.0896 0.0896 0.0171 0.2485 0.2750 0.1110 0.2425 0.2750 0.1110 0.2425 0.2750 0.1110 1.2245 0.2750 0.1100 0.0425 0.2750 0.1110 1.2245 0.2750 0.1100 0.0426 0.2455 0.2750 0.1110	- 🗊	2	41.5971	-7.2976	-28.8657	41.3715	-5.9213	-28.7664	0.2256	1.3763	0.0993	1.3982	1.3982	X, Y, Z
A 35.8617 4.6981 -17.5158 34.4472 5.9183 -17.4292 0.0066 1.4041 1.4641 1.4411 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611 1.4611	5×	3	41.5465	-19.1544	-29.3166	41.7347	-17.7839	-29.2481	-0.1882	1.3705	0.0685	1.3851	1.3851	X, Y, Z
5 37 6341 -7.2341 -16.2371 0.3331 1.2446 0.0682 1.4100 1.3383 1.2414 0.16981 1.2414 0.16981 1.2414	0×	4	35.6517	4.6981	-17.5158	34.8472	5.9183	-17.4292	0.8045	-1.2202	0.0866	1.4641	1.4641	X, Y, Z
b 39.395 -26.296 -16.229 -16.229 -0.42/2 1.340 0.0962 1.4100 1.41100 1.41100 1.41100 1.41100 1.41100 1.41100 1.41100 1.41100 1.41100 1.41100 1.41100 </td <td>Ŭ</td> <td>5</td> <td>37.6341</td> <td>-7.2334</td> <td>-16.2971</td> <td>37.3010</td> <td>-5.9388</td> <td>-16.2327</td> <td>0.3331</td> <td>1.2946</td> <td>0.0644</td> <td>1.3383</td> <td>1.3383</td> <td>X, Y, Z</td>	Ŭ	5	37.6341	-7.2334	-16.2971	37.3010	-5.9388	-16.2327	0.3331	1.2946	0.0644	1.3383	1.3383	X, Y, Z
y jj </td <td></td> <td>6</td> <td>39.1395</td> <td>-26.2796</td> <td>-16.3221</td> <td>39.5667</td> <td>-24.9395</td> <td>-16.2239</td> <td>-0.4272</td> <td>1.3401</td> <td>0.0982</td> <td>1.4100</td> <td>1.4100</td> <td>X, Y, Z</td>		6	39.1395	-26.2796	-16.3221	39.5667	-24.9395	-16.2239	-0.4272	1.3401	0.0982	1.4100	1.4100	X, Y, Z
No. 8 40.9165 -27.4827 -32242 50.6240 -27.3827 -20.8168 -1.2461 0.01615 1.2481 0.01615 1.2481 0.02455 0.1524 00 37.4657 -29.5302 -20.4868 37.5466 -29.4106 -20.3134 -0.0630 0.0796 0.0796 0.2465 0.1524 00 00 11 27.0071 -29.530 -10.9796 16.8035 -29.6267 -11.6613 -0.0465 0.0687 0.1000 0.1224 0.0687 14 30.1439 -30.9640 -4.4488 30.2273 -30.8305 -4.3370 -0.0631 0.1335 0.1096 0.1224 0.0687 16 34.0372 6.018 -29.9277 -30.8461 -2.4982 0.0398 0.0438 0.1036 0.1135 0.1096 0.1241 0.1506 0.1241 0.1506 0.1335 0.1096 0.1411 0.1536 0.1265 0.1262 0.1431 0.1045 0.1636 0.1135 0.1086 0.1187 0.1356	빌린		47.5542	-27.5193	-5.2855	47.8794	-26.2779	-5.1591	-0.3252	1.2414	0.1264	1.2895	1.2414	Y
L 9 003436 7-28,502 20,2486 72,300 20,3013 -0,0638 0,1824 0.0264 0.0425 0.0135 0.0466 0.1135 0.0135 0.0135 0.0135 0.0135 0.0135 0.0135 0.0135 0.0135 0.0136 0.1193 0.1036 0.1193 0.1036 0.1193 0.1036 0.1193 0.1036 0.1193 0.1036 0.1193 0.1036 0.1193 0.1133 0.1103 0.1103 0.1103	SAS	8	47.9185	-27.5146	-1.6335	48.2353	-26.2665	-1.5/20	-0.3168	1.2481	0.0615	1.2891	1.2481	Y
10 37.4657 -29.3002 -20.304 -20.3134 -20.311678 -20.3136	ш	9	30.3430	-27.4027	-3.2342	30.6240	-27.3303	-3.0751	-0.0604	0.1524	0.1791	0.2465	0.1524	T
No. 11 21/201 29/203 11/201 29/203 11/201 29/203 11/201 20/203 11/201	8	10	37.4037	-29.5002	-20.4000	27 27/1	-29.4100	10 7373	-0.0639	0.0096	0.1734	0.2054	0.0096	Y V
VAC 12 13 37.6686 -28.055 6.6801 37.685 -28.4356 -18.007 -0.0165 0.0697 0.1000 0.1224 0.0567 14 30.1439 -30.9640 -4.448 30.2273 -30.8306 -4.3370 -0.0831 0.1200 0.0721 0.1536 0.1204 0.0567 .01606 0.0687 0.1008 0.1193 0.1204 0.0120 0.0721 0.1536 0.1204 0.01204 0.0069 0.1441 0.1036 0.1193 0.1206 0.1204 0.0040 0.1441 0.1036 0.1193 0.1206 0.1204 0.1181 0.1206 0.1204 0.1264 0.1762 0.1181 0.1036 0.1191 0.1264 0.1762 0.1411 1.1553 0.1224 0.0040 0.1441 0.1667 0.1461 0.1667 0.1461 0.1562 0.1316 0.0042 0.1807 0.1848 0.1672 0.1843 0.1976 0.1417 0.1627 0.1627 0.1627 0.1562 0.1316 0.1776 0.1569	Ω M	12	16 7630	-29.5339	-19.9790	16 8035	-29.4229	-19.7373	-0.0670	0.0789	0.2423	0.2750	0.0789	Y
V C 13 37.333 30.3660 4.4468 30.2273 30.830 4.3370 -0.0834 0.1336 0.1098 0.1191 0.1335 15 19.1626 -30.1845 -2.9504 19.2273 -30.806 -2.8783 -0.0634 0.1336 0.1098 0.1193 0.1136 0.11200 17 34.1631 0.2256 +42.9564 43.9573 42.9560 +42.942 0.0399 0.0438 0.1036 0.1193 0.1136 0.1100 19 32.4850 -12.4984 +42.7376 32.5197 -12.5469 +42.5614 -0.0367 -0.0485 0.1762 0.1864 0.1762 20 31.1678 -17.3893 +42.3427 31.2054 +17.3895 +42.3665 -0.0376 -0.0092 0.1807 0.1846 0.1762 0.1867 0.1867 0.1265 0.1627 0.1848 0.1627 0.1868 0.1627 0.1867 0.0254 0.1035 0.1627 0.1636 0.1874 0.1647 0.1926 0.1867 0.1844 </td <td>588F</td> <td>12</td> <td>37 6688</td> <td>-28.5055</td> <td>-6.6801</td> <td>37 6853</td> <td>-29.0207</td> <td>-6.5801</td> <td>-0.0403</td> <td>0.0703</td> <td>0.2402</td> <td>0.1224</td> <td>0.0703</td> <td>V</td>	588F	12	37 6688	-28.5055	-6.6801	37 6853	-29.0207	-6.5801	-0.0403	0.0703	0.2402	0.1224	0.0703	V
▲ 15 19.1626 -30.1845 -2.9504 19.2257 -30.0645 -2.8783 -0.0831 0.1200 0.0721 0.1536 0.11200 16 34.0372 5.0018 -43.0528 33.9973 4.9580 -42.9492 0.0839 0.0438 0.1036 0.1193 0.1036 0.1193 0.1036 0.1191 0.2165 0.1411 0.1550 0.1411 0.1550 0.1411 0.1550 0.14141 0.1550 0.14141 0.1550 0.14141 0.1550 0.14141 0.1550 0.1467 0.1426 0.1177 0.1184 0.11807 0.1280 0.1467 0.1467 0.1265 0.1467 0.01457 0.1167 0.1867 0.		14	30 1439	-30,9640	-4 4468	30 2273	-30,8305	-4.3370	-0.0834	0.1335	0.1000	0.1224	0.1335	Y
16 34.0372 5.0018 +43.0528 33.9973 4.9580 +42.9492 0.0399 0.0438 0.1036 0.1193 0.1036 17 34.1631 0.2956 42.9584 34.1774 0.2247 +42.8143 0.0143 0.0499 0.1441 0.1505 0.1441 19 32.2886 -62.2844 42.8176 0.2597 +0.28464 -0.0367 -0.0485 0.1762 0.1848 0.1840 0.1848 0.1807 20 31.1678 17.393 42.3665 -0.0325 0.1205 0.1847 0.1848 0.1807 21 23.9012 6.1360 +46.3854 23.9337 6.0155 +46.2387 -0.0325 0.1467 0.1847 0.1847 0.1667 22 24.4740 -5.4586 -46.355 45.17 -45.9968 0.0234 0.0169 0.1667 0.1627 0.2289 0.1762 0.2289 0.1766 0.2298 0.1766 0.2298 0.1766 0.2298 0.17766 0.1291 0.2298 <t< td=""><td>≥ </td><td>15</td><td>19 1626</td><td>-30 1845</td><td>-2 9504</td><td>19 2257</td><td>-30.0645</td><td>-2 8783</td><td>-0.0631</td><td>0.1200</td><td>0.0721</td><td>0.1536</td><td>0.1200</td><td>Y</td></t<>	≥	15	19 1626	-30 1845	-2 9504	19 2257	-30.0645	-2 8783	-0.0631	0.1200	0.0721	0.1536	0.1200	Y
17 34.1631 0.2956 42.9584 34.1774 0.2547 42.8143 -0.0143 0.0409 0.1441 0.1505 0.1441 18 33.5286 6.2684 42.876 33.6289 6.2684 42.7059 -0.0045 0.1001 -0.0440 0.1917 0.2163 0.1917 20 31.1678 17.3983 42.5472 31.2549 42.3665 -0.0376 -0.0082 0.1762 0.1844 0.1807 21 23.9012 6.1360 46.3854 23.9337 6.0155 46.2887 -0.0325 0.1205 0.1467 0.1846 0.1762 22 24.3543 -0.2128 46.3046 24.4254 -0.3341 44.119 -0.0111 -0.1213 0.1627 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380 0.1997 0.2380		16	34 0372	5 0018	-43 0528	33 9973	4 9580	-42 9492	0.0399	0.0438	0.1036	0 1193	0.1036	7
18 33.5288 -6.2644 -42.8976 33.6289 -6.2684 -42.7059 -0.1001 -0.0420 0.1917 0.2163 0.1917 19 32.4830 12.4984 -42.7376 32.5197 -12.5469 -42.3665 -0.0376 -0.0485 0.1762 0.1844 0.1762 21 23.9012 6.1380 -46.3854 23.3937 6.0155 +42.3676 -0.0325 0.1205 0.1467 0.1986 0.1867 22 24.3543 -0.2128 +46.3046 24.4254 -0.3341 +46.1419 -0.0711 -0.1213 0.1627 0.2150 0.1627 24 24.3476 -10.3012 +45.9301 24.4739 +10.3455 +45.7344 -0.1263 -0.0443 0.1907 0.2330 0.1907 25 24.1382 +44.8484 +45.631 +42.9267 +0.0200 0.1246 0.1231 0.1752 0.1231 26 9.9818 5.9860 +7.2072 9.9888 5.8614 +47.0614 -0.0607 0.16		17	34 1631	0.2956	-42 9584	34 1774	0 2547	-42 8143	-0.0143	0.0409	0.1000	0.1505	0 1441	7
19 32,4830 -12,4984 42,7376 32,5197 -12,5489 -42,5614 -0.0387 -0.0485 0.1762 0.1864 0.1762 20 31,1678 -17,3893 -42,5472 31,2054 -17,3895 -42,3665 -0.0376 -0.0092 0.1807 0.1864 0.1467 21 23,9012 61,380 -46,3354 23,9337 0.0155 46,2387 -0.0325 0.1205 0.1467 0.1467 22 24,3476 -10.3012 -45,9301 24,4739 -10.3455 -45,7394 -0.1263 -0.0443 0.1907 0.2330 0.1907 25 24,1382 -14,8803 -45,6031 24,2329 -14,808 -45,425 -0.0102 0.1263 0.1786 0.2288 0.1786 24 24,3476 -10.3012 -47,2130 9.8672 -0.0308 -47,0619 -0.0617 0.1576 0.1511 0.2289 0.1511 28 10.0386 -10.5979 -46,8817 10.4111 -10.7159 -0.0118 <		18	33,5288	-6.2644	-42.8976	33.6289	-6.2684	-42,7059	-0.1001	-0.0040	0.1917	0.2163	0.1917	z
20 31.1678 -17.3893 42.5472 31.2054 -17.3895 42.3665 -0.0376 -0.0092 0.1807 0.1848 0.1807 21 23.9012 6.360 46.3884 23.9337 6.0155 -46.2887 -0.0326 0.1205 0.1467 0.1926 0.1467 22 24.3543 -0.2128 46.3044 24.4506 -5.4517 -45.9984 0.0099 0.1669 0.1588 0.1569 24 24.3476 -10.3012 45.9301 24.4506 -5.4517 -45.9394 -0.1633 0.0097 0.2300 0.1907 25 24.1382 -14.9434 45.6031 24.2392 -14.8608 45.4245 -0.1010 0.1026 0.1786 0.2298 0.1786 26 9.9818 5.9860 -47.2072 9.9938 5.8614 -47.0841 -0.0020 0.1245 0.1774 0.1762 0.1231 28 10.0330 -4.8152 -47.1161 10.0448 -4.9025 -46.9507 -0.0147 0.1607		19	32,4830	-12,4984	-42.7376	32.5197	-12.5469	-42.5614	-0.0367	-0.0485	0.1762	0.1864	0.1762	z
Q 21 23.9012 6.1360 46.3854 23.9337 6.0155 46.2387 -0.0325 0.1205 0.1467 0.1926 0.1467 22 24.3543 -0.2128 48.3046 24.4254 -0.3341 46.1419 -0.0711 -0.1213 0.1627 0.1627 0.1627 23 24.4740 -5.45817 45.9086 0.0234 0.0090 0.1568 0.1586 0.1586 0.1586 0.1586 0.1586 0.1586 0.1586 0.1298 0.1786 24 24.3476 -10.3012 45.9301 24.4739 -10.3455 45.7394 -0.1283 -0.0443 0.1907 0.2330 0.1907 25 24.1382 -14.9843 45.6011 24.2392 -14.8004 47.0641 -0.0020 0.1246 0.1771 0.1776 0.1786 0.1874 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674 0.1674		20	31.1678	-17.3893	-42.5472	31.2054	-17.3985	-42.3665	-0.0376	-0.0092	0.1807	0.1848	0.1807	Z
Q 22 24.3643 -0.2128 -46.3046 24.4254 -0.3341 -46.149 -0.0711 -0.1213 0.1627 0.2160 0.1682 23 24.4740 -5.4566 -46.1537 24.4506 -5.4517 -45.9968 0.0214 0.01690 0.1568 0.1569 24 24.3476 -10.3012 -45.9301 24.4739 -10.3455 -45.7394 -0.1263 -0.0443 0.1907 0.2330 0.1907 25 24.1382 -14.9843 -45.031 24.2323 -14.8808 45.4245 -0.1010 0.1035 0.1786 0.2298 0.1786 26 9.9818 5.9860 -47.2072 9.9838 5.8614 -47.0619 -0.0617 0.1576 0.1511 0.2269 0.1511 28 10.0330 -4.8152 -47.1161 10.04181 -4.9025 46.9627 -0.0118 0.0174 0.1624 0.1891 30 10.8870 -15.1470 -46.6073 10.8517 -15.3077 -46.4182 -0.0147	0	21	23.9012	6.1360	-46.3854	23.9337	6.0155	-46.2387	-0.0325	0.1205	0.1467	0.1926	0.1467	Z
Port 23 24.4740 -5.4586 -6.4517 -46.9988 0.0234 0.0069 0.1568 0.1588 0.1589 24 24.3476 -10.3012 -45.9301 24.4739 -10.3455 -45.7394 -0.1263 -0.0443 0.1907 0.2330 0.1907 25 24.1382 -14.8903 426.5031 24.2392 -14.8808 45.4245 -0.1010 0.1035 0.1786 0.2288 0.1786 26 9.9818 5.9860 -47.2072 9.9838 5.8614 -47.0619 -0.0617 0.1576 0.1511 0.2289 0.1511 28 10.0330 -4.8152 -47.1161 10.0448 -49.025 -0.0203 -0.1180 0.1774 0.2146 0.1874 0.1584 29 10.3868 -10.5977 46.7043 -0.0243 -0.1180 0.1744 0.2142 0.1692 N 30 10.8370 -51.470 -46.8177 -15.3077 46.4182 -0.0147 -0.1891 0.2466 0.1892		22	24.3543	-0.2128	-46.3046	24.4254	-0.3341	-46.1419	-0.0711	-0.1213	0.1627	0.2150	0.1627	Z
Q 24 24.3476 -10.3012 -45.9301 24.739 -10.3455 -45.7394 -0.10363 -0.0443 0.1907 0.2330 0.1907 25 24.1382 -14.9843 -45.6031 24.2392 -14.8808 45.4245 -0.1010 0.1035 0.1786 0.2298 0.1786 26 9.9818 5.9860 -47.2072 9.9838 5.8614 -47.0619 -0.0617 0.1576 0.1511 0.2296 0.1511 28 10.0330 -4.8152 -47.1161 10.0448 -4.9025 -46.5077 -0.0187 0.1654 0.1774 0.1774 30 10.8370 -15.1470 -46.6073 10.8517 -15.3077 -46.4182 -0.0147 -0.1607 0.1891 0.2486 0.1891 31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1069 0.1990 0.1294 0.2012 0.1992 Y 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 </td <td>5</td> <td>23</td> <td>24.4740</td> <td>-5.4586</td> <td>-46.1537</td> <td>24.4506</td> <td>-5.4517</td> <td>-45.9968</td> <td>0.0234</td> <td>0.0069</td> <td>0.1569</td> <td>0.1588</td> <td>0.1569</td> <td>Z</td>	5	23	24.4740	-5.4586	-46.1537	24.4506	-5.4517	-45.9968	0.0234	0.0069	0.1569	0.1588	0.1569	Z
C 25 24,1382 -14,8803 -45,6031 24,2392 -14,8808 -45,4245 -0.0101 0.1035 0.1786 0.2288 0.1786 26 9,9818 5,9860 -47,2130 9,8672 -0.0308 -47,0811 -0.0020 0.1266 0.1511 0.1269 0.1511 28 10.0330 -4.8152 -47,1161 10.0448 -4.9025 -46,9507 -0.0118 0.0673 0.1654 0.1874 0.1654 29 10.3868 -10.5979 -46.8817 10.517 15.5077 -46.7128 -0.0147 -0.1080 0.1990 0.1294 0.2124 0.1891 30 10.8370 -15.1470 -46.8073 10.8517 -15.5077 -25.6074 -29.7473 -0.1089 0.1990 0.1294 0.2012 0.1892 N 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0766 0.1366 0.21174 0.1552 N 34 38.9986	ğ [24	24.3476	-10.3012	-45.9301	24.4739	-10.3455	-45.7394	-0.1263	-0.0443	0.1907	0.2330	0.1907	Z
26 9.8818 5.9860 -47.2072 9.9838 5.8614 -47.0841 -0.0020 0.1226 0.1231 0.1752 0.1231 27 9.8055 0.1268 -47.2130 9.8672 -0.0308 -47.0619 -0.0617 0.1576 0.1511 0.2269 0.1511 0.2269 0.1511 0.2269 0.1511 0.2269 0.1654 0.1874 0.1654 0.1874 0.1654 0.1874 0.1654 0.1874 0.1654 0.1874 0.1654 0.1891 0.2486 <td>œ [</td> <td>25</td> <td>24.1382</td> <td>-14.9843</td> <td>-45.6031</td> <td>24.2392</td> <td>-14.8808</td> <td>-45.4245</td> <td>-0.1010</td> <td>0.1035</td> <td>0.1786</td> <td>0.2298</td> <td>0.1786</td> <td>Z</td>	œ [25	24.1382	-14.9843	-45.6031	24.2392	-14.8808	-45.4245	-0.1010	0.1035	0.1786	0.2298	0.1786	Z
27 9.8055 0.1268 -47.2130 9.8672 -0.0308 -47.0619 -0.0617 0.1576 0.1511 0.2269 0.1511 28 10.0330 -48152 -47.1161 10.0448 -4.9025 -46.507 -0.0118 -0.0873 0.1654 0.1874 0.1654 29 10.3868 -10.579 -46.817 10.8111 -0.0243 -0.0147 -0.1807 0.1891 0.2486 0.1891 30 10.8370 -15.1470 -46.6073 10.8517 -15.3077 -46.4182 -0.0147 -0.1607 0.1994 0.2144 0.1774 31 45.6407 -25.7164 -29.8767 42.25.3097 -30.1438 0.0766 0.1450 0.2174 0.1681 N 33 42.1968 -24.8757 -32.5073 42.3406 -24.801 -32.3623 -0.1472 0.0666 0.1368 0.2117 0.1522 N 34 38.9986 -24.8767 -32.6767 -39.8678 -0.1472 0.0666 0.1368		26	9.9818	5.9860	-47.2072	9.9838	5.8614	-47.0841	-0.0020	0.1246	0.1231	0.1752	0.1231	Z
28 10.0330 -4.8152 -47.1161 10.0448 -4.9027 -0.0118 -0.0873 0.1654 0.1874 0.1654 29 10.3868 -10.5979 -46.8817 10.4111 -10.7159 -46.7043 -0.0147 -0.1607 0.1891 0.2486 0.1891 30 10.8370 -15.1470 -46.6073 10.8517 -15.3077 -46.4182 -0.0147 -0.1690 0.1294 0.2012 0.1692 N 31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1089 0.1090 0.1294 0.2012 0.1692 N 33 42.1968 -24.8757 -32.6073 42.3406 -24.8011 -32.623 -0.1438 0.0746 0.1450 0.2174 0.1631 N 34 38.9986 -24.1896 -34.739 39.1458 -24.1230 -34.6371 -0.1472 0.0666 0.1368 0.2117 0.1522 N 35 35.3881 -23.5093 -37.2879		27	9.8055	0.1268	-47.2130	9.8672	-0.0308	-47.0619	-0.0617	0.1576	0.1511	0.2269	0.1511	Z
29 10.3886 -10.5979 -46.8817 10.4111 -10.7159 -46.7043 -0.0243 -0.1180 0.1774 0.21486 0.1774 30 10.8370 -15.1470 -46.6073 10.8517 -15.3077 -46.4182 -0.0147 -0.1607 0.1891 0.2486 0.1891 31 45.6407 -25.7164 -29.7473 -0.1089 0.1090 0.1294 0.2174 0.1631 N 32 44.1371 -25.4046 -31.0885 44.2832 -25.3097 -30.9141 -0.1438 0.0746 0.1450 0.2174 0.1631 N 33 42.1968 -24.8757 -32.5073 42.1230 -34.6371 -0.1438 0.0775 0.1547 0.2319 0.1730 N 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1641 0.0775 0.1547 0.2319 0.1730 N 31 45.6407 -25.1046 -31.0885 44.2832 -25.3097 -30.184	-	28	10.0330	-4.8152	-47.1161	10.0448	-4.9025	-46.9507	-0.0118	-0.0873	0.1654	0.1874	0.1654	Z
30 10.8370 -15.1470 446.6073 10.8371 -15.307 446.4182 -0.0147 -0.1807 0.1891 0.2486 0.1891 31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1689 0.1090 0.1294 0.2012 0.1692 N 32 44.1371 -25.4046 -31.0885 44.2832 -25.3097 -30.9141 -0.1461 0.0949 0.1744 0.2465 0.1692 N 33 42.1968 -24.8757 -32.5073 42.3406 -24.1200 -34.6371 -0.1472 0.0666 0.1368 0.2117 0.1522 N 35 35.3881 -23.5093 -37.2879 35.4288 -23.3987 -37.1758 -0.0407 0.1106 0.1121 0.1627 0.1730 N 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1438 0.0746 0.1450 0.2174 0.0746 31 45.6407 -25.4046	-	29	10.3868	-10.5979	-46.8817	10.4111	-10.7159	-46.7043	-0.0243	-0.1180	0.1774	0.2144	0.1774	Z
31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1089 0.1090 0.1294 0.2012 0.1692 N 32 44.1371 -25.4046 -31.0885 44.2832 -25.3097 -30.9141 -0.1461 0.0949 0.1744 0.2465 0.1885 N 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0746 0.1450 0.2174 0.1522 N 34 38.9986 -24.8757 -32.5073 42.3408 -23.9877 -37.1758 -0.0407 0.1106 0.1121 0.1627 0.1575 N 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2174 0.1730 N 32 44.1371 -25.7164 -29.8773 -25.3097 -30.9141 -0.1481 0.0775 0.1547 0.2174 0.0746 32 44.1371 -25.7644 -29.7473 -0.1481 0.0999 0.1744 0.2465 0.0949 0.1730		30	10.8370	-15.1470	-46.6073	10.8517	-15.3077	-46.4182	-0.0147	-0.1607	0.1891	0.2486	0.1891	<u> </u>
32 44.1371 -22.4046 -31.0885 44.2832 -22.309 -30.9141 -0.1461 0.0949 0.1744 0.2465 0.1985 1 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0746 0.1450 0.2174 0.1631 Y 34 38.9986 -24.8903 -37.2879 35.4288 -23.3987 -37.1758 -0.0407 0.1106 0.1121 0.1627 0.1575 Y 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2319 0.1730 Y 31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1689 0.1990 0.1294 0.2012 0.1090 32 44.1371 -25.4046 -31.0885 44.2832 -22.53097 -30.9141 -0.1461 0.0949 0.1744 0.2465 0.9494 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0746 0.	~ ~	31	45.6407	-25.7164	-29.8767	45.7496	-25.6074	-29.7473	-0.1089	0.1090	0.1294	0.2012	0.1692	Y, Z
Image: 1 3.3 42.1986 -24.8757 -32.5073 42.3406 -24.8101 -32.3623 -0.1438 0.0746 0.1450 0.2174 0.1631 1 Mode: 2 34 38.9986 -24.1896 -34.7739 39.1458 -24.1230 -34.6371 -0.1472 0.0666 0.1160 0.1121 0.1627 0.1575 N 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2319 0.1730 N 31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1089 0.1090 0.1294 0.2012 0.1090 32 44.1371 -25.4046 -31.0885 44.2832 -25.3097 -30.1438 0.0746 0.1450 0.2174 0.0746 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0746 0.1450 0.2174 0.0746 34 38.9966 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1472	H H H	32	44.13/1	-25.4046	-31.0885	44.2832	-25.3097	-30.9141	-0.1461	0.0949	0.1/44	0.2465	0.1985	Y,Z
A mer 35 35,3881 -23,5993 -37,775 -0.1472 0.0000 0.1306 0.2117 0.1522 1 A mer 35 35,3881 -23,5093 -37,2879 354,288 -23,3987 -37,7758 -0.0407 0.1106 0.1121 0.1627 0.1575 N 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2319 0.1730 N 31 45.6407 -25.7164 -29.8767 45.7496 -25.6074 -29.7473 -0.1089 0.1090 0.1744 0.2012 0.1090 32 44.1371 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0746 0.1450 0.2174 0.0746 33 42.1968 -24.877 -32.5073 42.3406 -24.8130 -34.6371 -0.1472 0.0666 0.1368 0.2174 0.0746 34 38.9986 -24.7522 -40.0225 31.1187	글통거나	34	38 0000	-24.0/0/	-32.00/3	42.3406	-24.8011	-34 6274	-0.1438	0.0/46	0.1260	0.21/4	0.1631	Y, Z
36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2319 0.1730 N 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2319 0.1730 N 31 45.6407 -22.7644 -29.8767 45.7496 -22.6707 -39.8678 -0.1684 0.0775 0.1547 0.2319 0.1730 N 32 44.1371 -25.4046 -31.0885 44.2832 -25.3097 -30.9141 -0.1461 0.0949 0.1744 0.2465 0.0949 33 42.1966 -24.877 -32.5073 42.3406 -24.8371 -3.1438 0.0746 0.1450 0.2174 0.0746 35 35.888 -23.5983 -37.1758 -0.0407 0.1106 0.1121 0.1627 0.1106 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.0407	A as	35	35 3881	-24.1090	-37 2879	35 / 288	-24.1230	-37 1758	-0.1472	0.1106	0.1300	0.2117	0.1522	Y 7
1 1	-	36	30,9643	-22 7542	-40 0225	31,1187	-22 6767	-39.8678	-0.1544	0.0775	0.1547	0.2319	0.1730	Y 7
32 44.1371 -25.4046 -25.3097 -25.3097 -20.1035 0.1034 0.1234 0.2012 0.10949 33 42.1371 -25.4046 -31.0885 44.2832 -25.3097 -30.9141 -0.1461 0.0949 0.1474 0.2465 0.0949 33 42.1968 -24.8757 -32.5073 42.3406 -24.8011 -32.3623 -0.1438 0.0746 0.1450 0.2174 0.0746 34 38.9966 -24.8956 -34.7739 39.1458 -24.1230 -34.6371 -0.1472 0.0666 0.1368 0.2117 0.0666 35 35.3881 -23.5093 -37.2879 35.4288 -23.3987 -0.1472 0.0666 0.1368 0.2117 0.0666 36 30.9643 -22.7542 -40.0225 31.1187 -22.6767 -39.8678 -0.1544 0.0775 0.1547 0.2319 0.0775 37 6.4496 -24.5877 -36.2592 6.4471 -24.4975 -36.1022 0.0025 0.0902 0.1570 0.1811 0.1811 X, 39 8.6498 <t< td=""><td></td><td>31</td><td>45 6407</td><td>-25 7164</td><td>-29 8767</td><td>45 7496</td><td>-25 6074</td><td>-29 7472</td><td>-0 1089</td><td>0 1000</td><td>0.1294</td><td>0 2012</td><td>0.1000</td><td>V</td></t<>		31	45 6407	-25 7164	-29 8767	45 7496	-25 6074	-29 7472	-0 1089	0 1000	0.1294	0 2012	0.1000	V
C C <thc< th=""> C <thc< th=""> <thc< th=""></thc<></thc<></thc<>	ms 1	32	44 1371	-25 4046	-31 0885	44 2832	-25 3097	-30 9141	-0.1461	0.0949	0.1234	0.2012	0.0949	V
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	PLO I	33	42,1968	-24.8757	-32,5073	42,3406	-24.8011	-32,3623	-0.1438	0.0746	0.1450	0.2174	0.0746	Y
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	era	34	38,9986	-24,1896	-34,7739	39,1458	-24,1230	-34,6371	-0.1472	0.0666	0.1368	0.2117	0.0666	Ý
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Lat	35	35,3881	-23.5093	-37.2879	35,4288	-23.3987	-37,1758	-0.0407	0.1106	0.1121	0.1627	0.1106	Y
X 37 6.4496 -24.5877 -36.2592 6.4471 -24.4975 -36.1022 0.0025 0.0902 0.1570 0.1811 0.1811 X, 38 4.2047 -27.5121 -23.7134 4.3044 -27.4138 -23.5763 -0.0997 0.0983 0.1371 0.1960 0.1687 N 39 8.6498 -27.6698 -19.6973 8.7277 -27.5675 -19.6103 -0.0779 0.1023 0.0870 0.1553 0.1343 N 40 4.8321 -27.8480 -14.7507 4.8897 -27.7408 -14.6389 -0.0576 0.1072 0.1118 0.1653 0.1549 N 40 4.8321 -27.8480 -14.7507 -36.2592 6.4471 -24.4975 -36.1022 0.0025 0.0902 0.1570 0.1811 0.0902 5 37 6.4496 -24.5877 -36.2592 6.4471 -24.4975 -36.1022 0.0025 0.0902 0.1570 0.1811 0.0902 5		36	30.9643	-22.7542	-40.0225	31.1187	-22.6767	-39.8678	-0.1544	0.0775	0.1547	0.2319	0.0775	Y
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Ύεαί	37	6.4496	-24.5877	-36.2592	6.4471	-24.4975	-36.1022	0.0025	0.0902	0.1570	0.1811	0.1811	X, Y. Z
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		38	4.2047	-27.5121	-23.7134	4.3044	-27.4138	-23.5763	-0.0997	0.0983	0.1371	0.1960	0.1687	Y,Z
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	l S si l	39	8.6498	-27.6698	-19.6973	8.7277	-27.5675	-19.6103	-0.0779	0.1023	0.0870	0.1553	0.1343	Y, Z
37 6.4496 -24.5877 -36.2592 6.4471 -24.4975 -36.1022 0.0025 0.0902 0.1570 0.1811 0.0902 38 4.2047 -27.5121 -23.7134 4.3044 -27.4138 -23.5763 -0.0997 0.0983 0.1371 0.1960 0.0983 39 8.6498 -27.6698 -19.6973 8.7277 -27.5675 -19.6103 -0.0779 0.1023 0.0870 0.1553 0.1023 40 4.8321 -27.8480 -14.7507 -27.7408 -14.6389 -0.0576 0.1072 0.1118 0.1653 0.1072	₩ã⊖	40	4.8321	-27.8480	-14.7507	4.8897	-27.7408	-14.6389	-0.0576	0.1072	0.1118	0.1653	0.1549	Y, Z
Single 38 4.2047 -27.5121 -23.7134 4.3044 -27.4138 -23.5763 -0.0997 0.0983 0.1371 0.1960 0.0983 39 8.6498 -27.6698 -19.6973 8.7277 -27.5675 -19.6103 -0.0779 0.1023 0.0870 0.1553 0.1023 40 4.8321 -27.8480 -14.7507 4.8897 -27.7408 -14.6389 -0.0576 0.1072 0.1118 0.1653 0.1072	¥	37	6.4496	-24.5877	-36.2592	6.4471	-24.4975	-36.1022	0.0025	0.0902	0.1570	0.1811	0.0902	Y
a t 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2) era	38	4.2047	-27.5121	-23.7134	4.3044	-27.4138	-23.5763	-0.0997	0.0983	0.1371	0.1960	0.0983	Y
	O at a	39	8.6498	-27.6698	-19.6973	8.7277	-27.5675	-19.6103	-0.0779	0.1023	0.0870	0.1553	0.1023	Y
	mi –	40	4.8321	-27.8480	-14.7507	4.8897	-27.7408	-14.6389	-0.0576	0.1072	0.1118	0.1653	0.1072	Y

deforming inward toward the occupant compartment. ^c Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure C-3. Left Interior Crush Data – Set 1, Test No. WZNP-2

IMPACI SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y)	POINT 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Pretest X (in) 44.8609 44.1037 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435	Pretest Y (in.) -14.2196 -26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	Pretest Z (in.) -32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577 -24.334	VE DRIVER S Posttest X (in.) 44.1167 43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.4036	HICLE DE DE INTEF Posttest Y (in.) -12.7395 -24.5478 -36.4011 -12.8564 -44.6757 -43.6364 -44.8762	FORMATI RIOR CRUS Posttest Z (in.) -32.6325 -33.1503 -21.3143 -20.1354	ON SH - SET 2 ΔX ^A (in.) 0.7442 0.3346 -0.0632 0.9481	ΔΥ ^A (in.) 1.4801 1.5117 1.5154 1.2866	ΔΖ ^A (in.) 0.1947 0.1255 0.0265 0.1494	Total Δ (in.) 1.6681 1.5534 1.5169 1.6052	Crush ^B (in.) 1.6681 1.5534 1.5169 1.6052	Direction for Crush ^C X, Y, Z X, Y, Z X, Y, Z
IMPACI SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y) (X, Y, Z)	POINT 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Pretest X (in.) 44.8609 44.1037 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	Pretest Y (in.) -14.2196 -26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	Pretest Z (in.) -32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577 -24.3344	VE DRIVER S Posttest X (in.) 44.1167 43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.7277 co.4465	Posttest Y (in.) -12.7395 -24.5478 -36.4011 -12.8564 -24.6757 -43.6364 -44.8762	Posttest Z (in.) -31.9402 -32.6325 -33.1503 -21.3143 -20.1354	ON SH - SET 2 ΔX ^A (in.) 0.7442 0.3346 -0.0632 0.9481	ΔΥ ^A (in.) 1.4801 1.5117 1.5154 1.2866	ΔZ ^A (in.) 0.1947 0.1255 0.0265 0.1494	Total Δ (in.) 1.6681 1.5534 1.5169 1.6052	Crush ^B (in.) 1.6681 1.5534 1.5169 1.6052	Direction for Crush ^C X, Y, Z X, Y, Z
IMPACT SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y) (Y)	POINT 1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15	Pretest X (in.) 44.8609 44.1037 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	Pretest Y (in.) -26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.0017 -46.0866 -46.0117 -48.3103 -48.5283	Pretest Z (in.) -32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577 -7.23344	DRIVER S Posttest X (in.) 44.1167 43.7691 44.3320 39.5892 42.1676 50.4036 50.7277 c6.4465	Posttest Y (in.) -12.7395 -24.5478 -36.4011 -12.8564 -34.6757 -43.6364 -44.8762	Posttest Z (in.) -31.9402 -32.6325 -33.1503 -21.3143 -20.1354	ΔX ^A (in.) 0.7442 0.3346 -0.0632 0.9481	ΔY ^A (in.) 1.4801 1.5117 1.5154 1.2866	ΔZ ^A (in.) 0.1947 0.1255 0.0265 0.1494	Total ∆ (in.) 1.6681 1.5534 1.5169 1.6052	Crush ^B (in.) 1.6681 1.5534 1.5169 1.6052	Direction for Crush ^C X, Y, Z X, Y, Z X, Y, Z
IMPACT SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y) (Y)	POINT 1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15	Pretest X (in.) 44.8609 44.1037 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	Pretest Y (in.) -14.2196 -26.0595 -37.9165 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	Pretest Z (in.) -32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577 -24.3344	Posttest X (in.) 44.1167 43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.4036 50.7277	Posttest Y (in.) -12.7395 -24.5478 -36.4011 -12.8564 -24.6757 -43.6364 -44.8762	Posttest Z (in.) -31.9402 -32.6325 -33.1503 -21.3143 -20.1354	ΔX ^A (in.) 0.7442 0.3346 -0.0632 0.9481	ΔΥ ^A (in.) 1.4801 1.5117 1.5154 1.2866	ΔZ ^A (in.) 0.1947 0.1255 0.0265 0.1494	Total ∆ (in.) 1.6681 1.5534 1.5169 1.6052	Crush ^B (in.) 1.6681 1.5534 1.5169 1.6052	Direction for Crush ^c X, Y, Z X, Y, Z X, Y, Z
IMPACT SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y) (Y)	POINT 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	44.8609 44.8609 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	Y (in.) -14.2196 -26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	2 (in.) -32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577	Posttest X (in.) 44.1167 43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.7277 50.4465	Posttest Y (in.) -12.7395 -24.5478 -36.4011 -12.8564 -24.6757 -43.6364 -44.8762	Posttest Z (in.) -31.9402 -32.6325 -33.1503 -21.3143 -20.1354	ΔX ^A (in.) 0.7442 0.3346 -0.0632 0.9481	ΔΥ ^A (in.) 1.4801 1.5117 1.5154 1.2866	ΔZ ^A (in.) 0.1947 0.1255 0.0265 0.1494	Total ∆ (in.) 1.6681 1.5534 1.5169 1.6052	Crush ^B (in.) 1.6681 1.5534 1.5169 1.6052	for Crush ^c X, Y, Z X, Y, Z X, Y, Z
IMPACI SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y)	POINT 1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15	(in.) 44.8609 44.1037 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	(in.) -14.2196 -26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.0866 -46.0866 -46.0117 -48.3103 -48.5283	2 (in.) -32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577 -24.3344	(in.) 44.1167 43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.7277 50.4462	(in.) -12.7395 -24.5478 -36.4011 -12.8564 -24.6757 -43.6364 -44.8762	(in.) -31.9402 -32.6325 -33.1503 -21.3143 -20.1354	(in.) 0.7442 0.3346 -0.0632 0.9481	(in.) 1.4801 1.5117 1.5154 1.2866	(in.) 0.1947 0.1255 0.0265 0.1494	(in.) 1.6681 1.5534 1.5169 1.6052	(in.) 1.6681 1.5534 1.5169 1.6052	Crush ^C X, Y, Z X, Y, Z X, Y, Z
IMPACT SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y)	1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15	44.8609 44.1037 44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-14.2196 -26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-32.1349 -32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577	44.1167 43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.7277	-12.7395 -24.5478 -36.4011 -12.8564 -24.6757 -43.6364 -44.8762	-31.9402 -32.6325 -33.1503 -21.3143 -20.1354	0.7442 0.3346 -0.0632 0.9481	1.4801 1.5117 1.5154 1.2866	0.1947 0.1255 0.0265 0.1494	1.6681 1.5534 1.5169 1.6052	1.6681 1.5534 1.5169 1.6052	X, Y, Z X, Y, Z X, Y, Z
IMPACT SIDE SIDE DASH DOOR PANEL (X, Y, Z) (Y) (Y)	2 3 4 5 6 7 8 9 10 11 11 12 13 14 15	44.1037 44.2688 37.8990 40.0917 41.9406 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-26.0595 -37.9165 -14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-32.7580 -33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577	43.7691 44.3320 36.9509 39.5892 42.1676 50.4036 50.7277	-24.5478 -36.4011 -12.8564 -24.6757 -43.6364 -44.8762	-32.6325 -33.1503 -21.3143 -20.1354	0.3346 -0.0632 0.9481	1.5117 1.5154 1.2866	0.1255	1.5534 1.5169 1.6052	1.5534 1.5169	X, Y, Z X, Y, Z X, Y, Z
IMPACT SIDE SIDE DASH DOOR PANEL (X, Y, Z (Y) (Y)	3 4 5 6 7 8 9 10 11 12 13 14 15	44.2688 37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-37.9165 -14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-33.1768 -21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577 24.3344	44.3320 36.9509 39.5892 42.1676 50.4036 50.7277	-36.4011 -12.8564 -24.6757 -43.6364 -44.8762	-33.1503 -21.3143 -20.1354	-0.0632 0.9481	1.5154	0.0265	1.5169	1.5169	X, Y, Z
IMPACI SIDE SIDE DA: DOOR PANEL (X, Y (Y) (Y)	4 5 6 7 8 9 10 11 12 13 14 15	37.8990 40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-14.1430 -26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-21.4637 -20.2049 -20.1722 -9.1002 -5.4469 -7.0577	36.9509 39.5892 42.1676 50.4036 50.7277	-12.8564 -24.6757 -43.6364 -44.8762	-21.3143 -20.1354	0.9481	1,2866	0 1/0/	1.6052	1 6052	VV7
IMPACI SIDE SIDE I DOOR PANEL () (Y) (Y) (2)	5 6 7 8 9 10 11 12 13 14 15	40.0917 41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-26.0335 -45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-20.2049 -20.1722 -9.1002 -5.4469 -7.0577	39.5892 42.1676 50.4036 50.7277	-24.6757 -43.6364 -44.8762	-20.1354			0.1434		1.0002	A, T, Z
IMPACT SIDE SIDE DOOR PANEL (Y) (Y)	6 7 8 9 10 11 12 13 14 15	41.9406 50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-45.0494 -46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-20.1722 -9.1002 -5.4469 -7.0577	42.1676 50.4036 50.7277	-43.6364	00 1000	0.5025	1.3578	0.0695	1.4495	1.4495	X, Y, Z
IMPACT SIDE SIDE DOOR PANEL (Y) (Y)	7 8 9 10 11 12 13 14 15	50.3336 50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-46.1077 -46.0866 -46.0117 -48.3103 -48.5283	-9.1002 -5.4469 -7.0577	50.4036 50.7277	-44.8762	-20.1696	-0.2270	1.4130	0.0026	1.4311	1.4311	X, Y, Z
IMPACT SIDE SID DOOR PAN (Y) (Y) (Y)	8 9 10 11 12 13 14 15	50.6836 53.3140 40.3612 30.0831 19.6435 40.4730	-46.0866 -46.0117 -48.3103 -48.5283	-5.4469 -7.0577	50.7277		-9.0362	-0.0700	1.2315	0.0640	1.2351	1.2315	Y
	9 10 11 12 13 14 15	53.3140 40.3612 30.0831 19.6435 40.4730	-46.0117 -48.3103 -48.5283	-7.0577	EO 4400	-44.8713	-5.4460	-0.0441	1.2153	0.0009	1.2161	1.2153	Y
IMPACT SIDE DOOR (Y)	10 11 12 13 14 15	40.3612 30.0831 19.6435 40.4730	-48.3103 -48.5283	24 3344	53.1468	-45.8905	-6.9314	0.1672	0.1212	0.1263	0.2421	0.1212	Y
IMPACT SIC DOOR (Y)	11 12 13 14 15	30.0831 19.6435 40.4730	-48.5283	-24.5544	40.2606	-48.1259	-24.2916	0.1006	0.1844	0.0428	0.2144	0.1844	Y
IMPACT DOO (Y)	12 13 14 15	19.6435 40.4730	10 0	-23.8665	29.9820	-48.3093	-23.8066	0.1011	0.2190	0.0599	0.2485	0.2190	Y Y
	13 14 15	40.4730	-48.8884	-23.8336	19.5159	-48.6856	-23.8240	0.1276	0.2028	0.0096	0.2398	0.2028	Y
	14	20.0054	-47.2758	-10.5298	40.2594	-4/.19/6	-10.5545	0.2136	0.0782	-0.0247	0.2288	0.0782	Y
	10	32.9031	49.0039	-0.3100	32.0224	49.7214	-0.3035	0.1027	0.1425	-0.0669	0.2204	0.1372	r V
	10	26.2790	-43.2700	47.0074	26.2446	43.1410	46.9420	0.0264	0.10/2	-0.1000	0.2004	0.1072	7
_	17	36 5884	-18 6392	-46.8997	36,5980	-18 4424	-46.7229	-0.0304	0.1941	0.1035	0.2504	0.1035	7
-	18	36 0724	-25 2094	-46.8234	36 1561	-24 9740	-46 6411	-0.0837	0.1300	0.1700	0.3093	0.1700	7
-	19	35 1386	-31 4608	-46 6503	35 1494	-31 2703	-46 5272	-0.0108	0.1905	0.1231	0.2271	0.1020	7
	20	33.9111	-36.3742	-46.4516	33,9136	-36,1435	-46.3601	-0.0025	0.2307	0.0915	0.2482	0.0915	Z
	21	26.2361	-12.9942	-50.3817	26.2912	-12.8391	-50.2188	-0.0551	0.1551	0.1629	0.2316	0.1629	Z
₿ F	22	26.8034	-19.3335	-50.2818	26.8866	-19.1800	-50.1388	-0.0832	0.1535	0.1430	0.2257	0.1430	Z
ц.	23	27.0172	-24.5759	-50.1162	26.9950	-24.2971	-50.0104	0.0222	0.2788	0.1058	0.2990	0.1058	Z
8	24	26.9774	-29.4194	-49.8799	27.0966	-29.1907	-49.7691	-0.1192	0.2287	0.1108	0.2807	0.1108	Z
<u>د</u>	25	26.8512	-34.1046	-49.5409	26.9340	-33.7302	-49.4713	-0.0828	0.3744	0.0696	0.3897	0.0696	Z
	26	12.3251	-13.3976	-51.2562	12.3537	-13.2198	-51.1883	-0.0286	0.1778	0.0679	0.1925	0.0679	Z
_	27	12.2545	-19.2590	-51.2467	12.3341	-19.1132	-51.1866	-0.0796	0.1458	0.0601	0.1767	0.0601	Z
	28	12.5707	-24.1959	-51.1355	12.5910	-23.9816	-51.0900	-0.0203	0.2143	0.0455	0.2200	0.0455	Z
	29	13.0279	-29.9705	-50.8840	13.0509	-29.7891	-50.8597	-0.0230	0.1814	0.0243	0.1845	0.0243	Z
	30	13.5590	-34.5101	-50.5954	13.5646	-34.3739	-50.5849	-0.0056	0.1362	0.0105	0.1367	0.0105	<u> </u>
~	31	48.4829	-44.4049	-33.7034	48.4795	-44.1557	-33.6399	0.0034	0.2492	0.0635	0.2572	0.2572	X, Y, Z
수 별 (?) ㅡ	32	46.9786	-44.1236	-34.9218	47.0187	-43.8781	-34.8186	-0.0401	0.2455	0.1032	0.2693	0.2663	Y,Z
티 흔 거 누	33	40.0340	-43.0335	-30.3494	45.0606	-43.3900	-30.2023	-0.0462	0.2370	0.0671	0.2506	0.2403	1, Z
A Rain	35	38 2200	-42 4030	-41 1596	38 1895	-42.7032	-41 1521	0.0314	0.2401	0.0471	0.2001	0.2020	X V 7
`- -	36	33,7948	-41,7352	-43 9131	33 8919	-41 4311	-43,8797	-0.0971	0.3041	0.0334	0.3210	0.3059	Y 7
	31	48 4820	-44 4040	-33 7034	48 4705	-44 1557	-33 6300	0.0034	0.2492	0.0635	0.2572	0.2492	V V
mc -	32	46 9786	-44 1236	-34 9218	47 0187	-43 8781	-34 8186	-0.0401	0.2452	0.1032	0.2693	0.2452	v v
AC -	33	45.0346	-43.6335	-36.3494	45.0808	-43.3965	-36,2823	-0.0462	0.2370	0.0671	0.2506	0.2370	Y
era	34	41.8333	-43.0113	-38.6301	41.8954	-42,7632	-38,5830	-0.0621	0.2481	0.0471	0.2601	0.2481	Ý
Lat	35	38.2209	-42.4030	-41.1596	38.1895	-42.0913	-41.1521	0.0314	0.3117	0.0075	0.3134	0.3117	Y
	36	33.7948	-41.7352	-43.9131	33.8919	-41.4311	-43.8797	-0.0971	0.3041	0.0334	0.3210	0.3041	Y
¥ EΩ	37	9.3028	-44.0010	-40.2384	9.2215	-43.6706	-40.3388	0.0813	0.3304	-0.1004	0.3548	0.3403	X, Y
A nu Z	38	7.0625	-46.9321	-27.6934	7.0170	-46.6652	-27.8422	0.0455	0.2669	-0.1488	0.3089	0.2708	X, Y
L Sail	39	11.4942	-46.9988	-23.6600	11.4072	-46.7598	-23.8377	0.0870	0.2390	-0.1777	0.3103	0.2543	X, Y
ah ≌ ⊂	40	7.6613	-47.2327	-18.7274	7.5290	-47.0134	-18.9011	0.1323	0.2193	-0.1737	0.3095	0.2561	X, Y
¥_	37	9.3028	-44.0010	-40.2384	9.2215	-43.6706	-40.3388	0.0813	0.3304	-0.1004	0.3548	0.3304	Y
	38	7.0625	-46.9321	-27.6934	7.0170	-46.6652	-27.8422	0.0455	0.2669	-0.1488	0.3089	0.2669	Y
	39	11.4942	-46.9988	-23.6600	11.4072	-46.7598	-23.8377	0.0870	0.2390	-0.1777	0.3103	0.2390	Y
mi –	40	7.6613	-47.2327	-18.7274	7.5290	-47.0134	-18.9011	0.1323	0.2193	-0.1737	0.3095	0.2193	Y

deforming inward toward the occupant components will disregard components that are negative and only include positive values where the or ^c Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure C-4. Left Interior Crush Data – Set 2, Test No. WZNP-2

Date: Year:	3/14/ 20	/2019 111			Test Name: Make:	WZ Do	NP-2 dge			VIN: Model:	1D7R	B1GP6BS6 Ram 1500	34520
					VE	HICLE DE GER SIDE	FORMATIC	ON N - SET 1					
	POINT	Pretest X (in.)	Pretest Y (in.)	Pretest Z (in.)	Posttest X (in.)	Posttest Y (in.)	Posttest Z (in.)	∆X ^A (in.)	ΔΥ ^Α (in.)	∆Z ^A (in.)	Total ∆ (in.)	Crush ^B (in.)	Directions for Crush ^C
	1	55.2346	32.0113	-1.5403	55.2220	32.0556	-1.3620	0.0126	-0.0443	-0.1783	0.1842	0.0126	X
	2	56.0127	29.1949	-0.2558	56.0140	29.2546	-0.1220	-0.0013	-0.0597	-0.1338	0.1465	0.0000	NA
	3	55.7108	25.9067	0.0439	55.6973	25.9444	0.1734	0.0135	-0.0377	-0.1295	0.1355	0.0135	Х
żΨ	4	55.4657	23.3568	-0.0348	55.4549	23.4429	0.0786	0.0108	-0.0861	-0.1134	0.1428	0.0108	Х
R ≥ Q	5	54.2642	21.6627	-1.5696	54.2668	21.8255	-1.3988	-0.0026	-0.1628	-0.1708	0.2360	0.0000	NA
ж Ш	6	50.8912	32.6256	2.7549	50.9063	32.7508	2.8586	-0.0151	-0.1252	-0.1037	0.1633	0.0000	NA
은 뿐	7	50.8806	28.6701	2.7721	50.9231	28.8273	2.8624	-0.0425	-0.1572	-0.0903	0.1862	0.0000	NA
· >	8	51.0141	25.6962	2.7273	51.0467	25.8328	2.8224	-0.0326	-0.1366	-0.0951	0.1696	0.0000	NA
	9	50.8971	23.1290	2.5518	50.9127	23.2613	2.6733	-0.0156	-0.1323	-0.1215	0.1803	0.0000	NA
	10	50.0692	21.1014	0.2794	50.0565	21.2626	0.4505	0.0127	-0.1612	-0.1711	0.2354	0.0127	Х
	11	45.2116	34.2453	5.0508	45.2639	34.3217	5.1505	-0.0523	-0.0764	-0.0997	0.1361	-0.0997	Z
	12	44.9768	29.8539	5.0172	45.0207	29.9183	5.1155	-0.0439	-0.0644	-0.0983	0.1254	-0.0983	Z
	13	44.7672	26.3345	5.0305	44.8177	26,4063	5.1287	-0.0505	-0.0718	-0.0982	0.1317	-0.0982	Z
	14	44,7369	23.2152	5.0178	44,7441	23.3043	5.1172	-0.0072	-0.0891	-0.0994	0.1337	-0.0994	Z
	15	44.5559	20.3186	4.7805	44.5602	20.3955	4.8803	-0.0043	-0.0769	-0.0998	0.1261	-0.0998	Z
	16	40.5707	34.4791	5.1106	40.6098	34.5679	5.2072	-0.0391	-0.0888	-0.0966	0.1369	-0.0966	Z
	17	40,1689	30.3747	5.0711	40.2249	30,4823	5.1670	-0.0560	-0.1076	-0.0959	0.1546	-0.0959	Z
7	18	39.6967	26.0647	5.0719	39.7652	26.1659	5.1673	-0.0685	-0.1012	-0.0954	0.1550	-0.0954	Z
AP	19	39.2462	22.9082	5.0733	39.2909	22.9482	5.1683	-0.0447	-0.0400	-0.0950	0.1124	-0.0950	Z
а с ()	20	39.1815	17.8692	5.0741	39.2358	17.9557	5.1698	-0.0543	-0.0865	-0.0957	0.1400	-0.0957	Z
ΫŅ	21	34.6625	34.3302	5.1387	34.7189	34,4115	5.2302	-0.0564	-0.0813	-0.0915	0.1348	-0.0915	Z
P	22	34.6595	30.7932	5.1376	34.6915	30.8611	5.2287	-0.0320	-0.0679	-0.0911	0.1180	-0.0911	Z
ш	23	34.9819	25.4563	5.1017	35.0209	25.5320	5.1938	-0.0390	-0.0757	-0.0921	0.1254	-0.0921	Z
	24	34.8232	21.6166	5.1091	34.8772	21.6812	5.2006	-0.0540	-0.0646	-0.0915	0.1243	-0.0915	Z
	25	35.0005	17.2748	5.1075	35.0093	17.3250	5.1997	-0.0088	-0.0502	-0.0922	0.1053	-0.0922	Z
	26	30.6182	33.8089	4.1514	30.6254	33.8889	4.2399	-0.0072	-0.0800	-0.0885	0.1195	-0.0885	Z
	27	30.7718	30.0524	4.3797	30.8101	30.1038	4.4667	-0.0383	-0.0514	-0.0870	0.1081	-0.0870	Z
	28	31.0939	25.0769	4.3685	31.1283	25.1438	4.4550	-0.0344	-0.0669	-0.0865	0.1146	-0.0865	Z
	29	31.1409	20.8643	4.3656	31.2175	20.9748	4.4565	-0.0766	-0.1105	-0.0909	0.1623	-0.0909	Z
	30	31.1655	16.6633	4.3721	31.2053	16.6826	4.4605	-0.0398	-0.0193	-0.0884	0.0988	-0.0884	Z

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



Figure C-5. Right Floor Pan Deformation Data – Set 1, Test No. WZNP-2

Date: Year:	3/14.	/2019 011			Test Name: Make:	WZ Do	NP-2 dge	i i		VIN: Model:	1D7R	B1GP6BS6 Ram 1500	34520
					VE	EHICLE DE GER SIDE	FORMATIC	ON AN - SET 2					
	POINT	Pretest X (in.)	Pretest Y (in.)	Pretest Z (in.)	Posttest X (in.)	Posttest Y (in.)	Posttest Z (in.)	∆X ^A (in.)	ΔΥ ^Α (in.)	∆Z ^A (in.)	Total ∆ (in.)	Crush ^B (in.)	Directions for Crush ^C
	1	56.9506	13.5389	-5.4618	56.7813	13.5184	-5.0272	0.1693	0.0205	-0.4346	0.4669	0.1693	Х
	2	57.7727	10.7397	-4.1671	57.6069	10.7264	-3.7886	0.1658	0.0133	-0.3785	0.4134	0.1658	Х
. H	3	57.5274	7.4474	-3.8606	57.3396	7.4108	-3.5052	0.1878	0.0366	-0.3554	0.4036	0.1878	Х
żΨ	4	57.3275	4.8934	-3.9341	57.1372	4.9062	-3.6090	0.1903	-0.0128	-0.3251	0.3769	0.1903	Х
Z Z A	5	56.1624	3.1747	-5.4698	55.9867	3.2747	-5.1007	0.1757	-0.1000	-0.3691	0.4208	0.1757	Х
ШШ×	6	52.5790	14.0869	-1.1863	52.4209	14.1336	-0.8402	0.1581	-0.0467	-0.3461	0.3834	0.1581	х
은뿔	7	52.6378	10.1319	-1.1594	52.4991	10.2108	-0.8473	0.1387	-0.0789	-0.3121	0.3505	0.1387	Х
3	8	52.8237	7.1607	-1.1964	52.6699	7.2187	-0.8947	0.1538	-0.0580	-0.3017	0.3436	0.1538	Х
	9	52.7527	4.5914	-1.3661	52.5774	4.6459	-1.0522	0.1753	-0.0545	-0.3139	0.3636	0.1753	Х
	10	51.9701	2.5443	-3.6370	51.7708	2.6406	-3.2876	0.1993	-0.0963	-0.3494	0.4136	0.1993	Х
	11	46.8621	15.6120	1.0818	46.7361	15.6093	1.4098	0.1260	0.0027	-0.3280	0.3514	-0.3280	Z
	12	46.7047	11.2171	1.0579	46.5622	11.2027	1.3603	0.1425	0.0144	-0.3024	0.3346	-0.3024	Z
	13	46.5569	7.6946	1.0790	46.4141	7.6880	1.3620	0.1428	0.0066	-0.2830	0.3171	-0.2830	Z
	14	46.5815	4.5752	1.0738	46.3891	4.5852	1.3411	0.1924	-0.0100	-0.2673	0.3295	-0.2673	Z
	15	46.4524	1.6753	0.8428	46.2528	1.6746	1.0945	0.1996	0.0007	-0.2517	0.3212	-0.2517	Z
	16	42.2177	15.7643	1.1215	42.0784	15.7825	1.4290	0.1393	-0.0182	-0.3075	0.3381	-0.3075	Z
	17	41.8881	11.6534	1.0904	41.7578	11.6915	1.3741	0.1303	-0.0381	-0.2837	0.3145	-0.2837	Z
7	18	41.4918	7.3357	1.0998	41.3658	7.3685	1.3584	0.1260	-0.0328	-0.2586	0.2895	-0.2586	Z
A	19	41.0968	4.1718	1.1071	40.9420	4.1438	1.3465	0.1548	0.0280	-0.2394	0.2865	-0.2394	Z
н К ()	20	41.1207	-0.8675	1.1200	40.9650	-0.8489	1.3334	0.1557	0.0186	-0.2134	0.2648	-0.2134	Z
DO 10	21	36.3129	15.5117	1.1253	36.1907	15.5340	1.4032	0.1222	-0.0223	-0.2779	0.3044	-0.2779	Z
LC LC	22	36.3721	11.9751	1.1327	36.2189	11.9836	1.3914	0.1532	-0.0085	-0.2587	0.3008	-0.2587	Z
ш	23	36.7883	6.6446	1.1113	36.6320	6.6604	1.3442	0.1563	-0.0158	-0.2329	0.2809	-0.2329	Z
	24	36.6971	2.8028	1.1275	36.5485	2.8078	1.3389	0.1486	-0.0050	-0.2114	0.2585	-0.2114	Z
	25	36.9507	-1.5353	1.1373	36.7488	-1.5458	1.3268	0.2019	-0.0105	-0.1895	0.2771	-0.1895	Z
	26	32.2826	14.9169	0.1223	32.1141	14.9503	0.3779	0.1685	-0.0334	-0.2556	0.3080	-0.2556	Z
	27	32.5012	11.1643	0.3604	32.3561	11.1680	0.5955	0.1451	-0.0037	-0.2351	0.2763	-0.2351	Z
	28	32.9107	6.1952	0.3628	32.7521	6.2136	0.5724	0.1586	-0.0184	-0.2096	0.2635	-0.2096	Z
	29	33.0318	1.9841	0.3704	32.9065	2.0465	0.5629	0.1253	-0.0624	-0.1925	0.2380	-0.1925	Z
	30	33.1301	-2.2158	0.3873	32.9616	-2.2454	0.5547	0.1685	-0.0296	-0.1674	0.2394	-0.1674	Z

^B Crush calculations that use multiple directional components will disregard components that are negative and only include positive values where the component is deforming inward toward the occupant compartment.

^C Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.



Figure C-6. Right Floor Pan Deformation Data – Set 2, Test No. WZNP-2

Year:	20	011	9 8		Make:	Do	dge			Model:		Ram 1500	
					VE		CODMATU						
				PA	SSENGER	R SIDE INT		USH - SE	T 1				
ſ		Pretest	Pretest	Pretest		-		٨				Р	Direction
		Х	Y	Z	Posttest X	Posttest Y	Posttest Z	ΔX ^A	ΔY ^A	ΔZ ^Δ	lotal∆ (in.)	Crush	for
	POINT	(in.)	(in.)	(in.)	(111.)	(111.)	(111.)	(in.)	(in.)	(in.)	(m.)	(in.)	Crush
	1	42.5805	4.4646	-28.2357	42.2176	4.8593	-28.1835	0.3629	-0.3947	0.0522	0.5387	0.5387	X, Y, Z
$-\overline{N}$	2	42.1795	16.4458	-27.7750	41.7185	16.8600	-27.6837	0.4610	-0.4142	0.0913	0.6264	0.6264	X, Y, Z
ASt. ∕	3	43.5913	32.7279	-27.1442	42.9760	33.1676	-27.0547	0.6153	-0.4397	0.0895	0.7615	0.7615	X, Y, Z
0×	4	35.6580	4.6833	-17.4948	35.2623	4.9981	-17.3774	0.3957	-0.3148	0.0003	0.5191	0.5191	X, Y, Z
	6	38.3435	33 1453	-16.3397	37 6990	33,5380	-16,2161	0.4972	-0.3334	0.0993	0.0079	0.0079	X Y 2
	7	47 6294	37 0809	-5.0823	47 0114	37 4463	-4.9683	0.6180	-0.3654	0.1140	0.7269	-0.3654	Y
ΞΪЯ	8	47.7156	37.0587	-0.3821	47.0999	37.4223	-0.2615	0.6157	-0.3636	0.1206	0.7251	-0.3636	Ý
D A C	9	49.6820	37.0614	-2.5690	49.0159	37.4433	-2.4376	0.6661	-0.3819	0.1314	0.7790	-0.3819	Y
ш	10	38.0588	38.9786	-19.3935	37.4222	39.2742	-19.2810	0.6366	-0.2956	0.1125	0.7108	-0.2956	Y
	11	26.2088	38.8460	-18.3675	25.5596	39.0287	-18.2752	0.6492	-0.1827	0.0923	0.6807	-0.1827	Y
- Ö 🖓	12	15.6850	39.5418	-17.7652	15.0435	39.6241	-17.6065	0.6415	-0.0823	0.1587	0.6659	-0.0823	Y
A D C	13	37.4303	37.6034	-6.8585	36.8095	37.9271	-6.8258	0.6208	-0.3237	0.0327	0.7009	-0.3237	Y
Ę	14	28.4348	40.1436	-3.6056	27.7637	40.3459	-3.4959	0.6711	-0.2023	0.1097	0.7095	-0.2023	Y
-	15	16.0051	39.2685	-2.9015	15.3206	39.3644	-2.7729	0.6845	-0.0959	0.1286	0.7030	-0.0959	Y
	16	34.0213	4.8882	-43.0854	33.6278	5.1938	-42.9189	0.3935	-0.3056	0.1665	0.5253	0.1665	Z 7
	18	33 3036	15 7737	42 8007	33.4704	16.0228	42.0404	0.3639	-0.3202	0.1955	0.5550	0.1955	7
	10	32 4106	20.8193	-42.0307	31 9143	21 1067	-42.5706	0.4963	-0.2431	0.1700	0.6043	0.1700	7
	20	30.9663	26.3807	-42.4575	30.4283	26.7114	-42.2454	0.5380	-0.3307	0.2121	0.6662	0.2121	Z
0	21	23.8955	5.9450	-46.4042	23.5442	6.1664	-46.2193	0.3513	-0.2214	0.1849	0.4546	0.1849	Z
N I	22	23.9585	11.1828	-46.2978	23.5277	11.3361	-46.1171	0.4308	-0.1533	0.1807	0.4917	0.1807	Z
ц.	23	23.8953	16.3896	-46.0906	23.3412	16.6121	-45.9195	0.5541	-0.2225	0.1711	0.6211	0.1711	Z
õ	24	23.3865	22.1010	-45.7694	22.8928	22.3236	-45.5752	0.4937	-0.2226	0.1942	0.5753	0.1942	Z
Ľ I	25	22.8205	27.0259	-45.3638	22.2982	27.2645	-45.1594	0.5223	-0.2386	0.2044	0.6095	0.2044	Z
	26	9.9701	5.9491	-47.2094	9.6094	6.0093	-47.0474	0.3607	-0.0602	0.1620	0.4000	0.1620	Z
	27	9.6380	11.1704	-47.1303	9.1472	11.2215	-46.9728	0.4908	-0.0511	0.1635	0.5198	0.1635	
	20	11 2036	20.9736	-46.9329	9.9094	21 0097	-40.7743	0.5231	-0.0361	0.1589	0.5491	0.1589	7
	30	11.8980	25.3162	-46.3502	11.3269	25.4388	-46 1856	0.5423	-0.0001	0.1509	0.0000	0.1509	7
	31	45 3664	35 5243	-30 4379	44.8803	35,9235	-30 2628	0.4861	-0.3992	0.1751	0.6529	0.5167	X 7
YEO	32	43 4673	35 0927	-31 8196	42 9247	35 4579	-31 6796	0.5426	-0.3652	0.1400	0.6689	0.5604	X Z
	33	41.3102	34.6061	-33.3831	40.7147	34.9308	-33.2486	0.5955	-0.3247	0.1345	0.6915	0.6105	X,Z
	34	39.2185	34.0691	-34.9434	38.6873	34.3951	-34.8236	0.5312	-0.3260	0.1198	0.6347	0.5445	X, Z
4 2 °	35	36.1268	33.4921	-37.1928	35.5284	33.7716	-37.0881	0.5984	-0.2795	0.1047	0.6687	0.6075	X, Z
	36	31.5301	32.4782	-39.9912	31.0119	32.7305	-39.8273	0.5182	-0.2523	0.1639	0.5992	0.5435	X, Z
	31	45.3664	35.5243	-30.4379	44.8803	35.9235	-30.2628	0.4861	-0.3992	0.1751	0.6529	-0.3992	Y
RA S	32	43.4673	35.0927	-31.8196	42.9247	35.4579	-31.6796	0.5426	-0.3652	0.1400	0.6689	-0.3652	Y
ilLL	33	41.3102	34.6061	-33.3831	40./14/	34.9308	-33.2486	0.5955	-0.3247	0.1345	0.6915	-0.3247	Y
A-P ate	35	36 1269	33 /001	-34.9434	35.528/	33 7716	-34.0230	0.5312	-0.3260	0.1198	0.6697	-0.3260	Y V
~ _	36	31 5301	32 4782	-39 9912	31 0119	32 7305	-39 8273	0.5364	-0.2523	0.1639	0.5992	-0.2523	Y
LE O	37	5 9475	33 7852	-35 5795	5 3917	33 7843	-35 4461	0.5558	0.0009	0.1334	0.5716	0.5716	XY
N I I	38	3.7464	36,3412	-24,4609	3,1336	36,3293	-24,2579	0.6128	0.0119	0.2030	0.6457	0.6457	XYZ
금눐강	39	8.2263	36.6378	-18.4434	7.6033	36.6596	-18.3177	0.6230	-0.0218	0.1257	0.6359	0.6356	X Z
μăς	40	4.3314	36.7277	-13.2758	3.7079	36.7138	-13.1541	0.6235	0.0139	0.1217	0.6354	0.6354	X, Y, Z
¥	37	5.9475	33.7852	-35.5795	5.3917	33.7843	-35.4461	0.5558	0.0009	0.1334	0.5716	0.0009	Y
Gera	38	3.7464	36.3412	-24.4609	3.1336	36.3293	-24.2579	0.6128	0.0119	0.2030	0.6457	0.0119	Y
	39	8.2263	36.6378	-18.4434	7.6033	36.6596	-18.3177	0.6230	-0.0218	0.1257	0.6359	-0.0218	Y
'n –	40	4.3314	36.7277	-13.2758	3.7079	36.7138	-13.1541	0.6235	0.0139	0.1217	0.6354	0.0139	Y

deforming inward toward the occupant compartment. ^c Direction for Crush column denotes which directions are included in the crush calculations. If "NA" then no intrusion is recorded, and Crush will be 0.

Figure C-7. Right Interior Crush Data – Set 1, Test No. WZNP-2

Year:	2011		Make:							Model:	10/6	Ram 1500	34520
					VE	HICLE DE	FORMATI	ON					
				PA	SSENGE	R SIDE INT	FERIOR CF	RUSH - SE	Т 2				
		Pretest	Pretest	Pretest	Posttest X	Posttest Y	Posttest Z	ΔX ^A	ΔY ^A	ΔZ ^A	Total ∆	Crush ^B	Direction
	POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	Crush ^C
DASH (X, Y, Z)	1	44.8857	-14.2855	-32.1464	44.9318	-14.0979	-32.0439	-0.0461	0.1876	0.1025	0.2187	0.2187	X, Y, Z
	2	44.2717	-2.3122	-31.7159	44.2666	-2.1068	-31.5096	0.0051	0.2054	0.2063	0.2912	0.2912	X, Y, Z
	3	45.3936	13.9937	-31.1183	45.2986	14.2141	-30.8182	0.0950	-0.2204	0.3001	0.3843	0.3843	X, Y, Z
	5	39.5141	-2.1641	-20.4113	39.4297	-2.0821	-20.2158	0.0844	0.0820	0.1955	0.2282	0.2282	X, Y, Z
	6	40.0958	14.3435	-20.3358	39.9307	14.4774	-20.0212	0.1651	-0.1339	0.3146	0.3797	0.3797	X, Y, Z
E SIDE PANEL (Y)	7	49.2654	18.4684	-9.0509	49.0994	18.4736	-8.6866	0.1660	-0.0052	0.3643	0.4004	-0.0052	Y
	8	49.3331	18.4585	-4.3504	49.1507	18.4352	-3.9793	0.1824	0.0233	0.3711	0.4142	0.0233	Y
	10	39,7206	20 1638	-23 4047	39 6009	20 2195	-23 0698	0.1197	-0.0557	0.3349	0.3600	-0.0557	Y
ST SIDE DOR Y)	11	27.8707	19.8245	-22.4256	27.7351	19.8108	-22.1601	0.1356	0.0137	0.2655	0.2984	0.0137	Ý
	12	17.3340	20.3359	-21.8669	17.2069	20.2620	-21.5739	0.1271	0.0739	0.2930	0.3278	0.0739	Y
DDD	13	39.0659	18.8067	-10.8691	38.9071	18.8230	-10.6244	0.1588	-0.0163	0.2447	0.2922	-0.0163	Y
IMI	15	17.5989	20.1027	-7.0014	17.3691	19.9569	-6.7394	0.2298	0.1458	0.2620	0.3756	0.1458	Y
	16	36.3802	-14.0473	-47.0311	36.4561	-13.8304	-46.8466	-0.0759	0.2169	0.1845	0.2947	0.1845	Z
ROOF - (Z)	17	36.1237	-8.6394	-47.0012	36.2309	-8.4071	-46.7579	-0.1072	0.2323	0.2433	0.3531	0.2433	Z
	18	35.5599	-3.1742	-46.8649	35.6079	-3.0126	-46.6105	-0.0480	0.1616	0.2544	0.3052	0.2544	Z
	20	34.4875	7 3893	-46.7512	34.5251	2.0566	-46.4610	-0.0375	-0.2030	0.2902	0.3561	0.2902	7
	21	26.2509	-13.1770	-50.3927	26.3870	-12.9829	-50.2247	-0.1361	0.1941	0.1680	0.2906	0.1680	Z
	22	26.2210	-7.9387	-50.2986	26.2998	-7.8143	-50.1060	-0.0788	0.1244	0.1926	0.2424	0.1926	Z
	23	26.0652	-2.7334	-50.1041	26.0404	-2.5420	-49.8931	0.0248	0.1914	0.2110	0.2860	0.2110	Z
	24	25.4545	2.9689	-49.7984	25.5122	3.1618	-49.5340	-0.0577	-0.1929	0.2644	0.3323	0.2644	7
	26	12.3309	-13.4204	-51.2534	12.4626	-13.3252	-51.1650	-0.1317	0.0952	0.0884	0.1850	0.0884	Z
	27	11.9065	-8.2057	-51.1941	11.9295	-8.1200	-51.0775	-0.0230	0.0857	0.1166	0.1465	0.1166	Z
	28	12.6861	-2.8651	-50.9999	12.6980	-2.7833	-50.8551	-0.0119	0.0818	0.1448	0.1667	0.1448	Z
	30	13.2971	5.9796	-50.7535	13.9105	6 1228	-50.5607	0.0030	-0.0615	0.1726	0.1637	0.1726	7
A-PILLAR Maximum (X, Y, Z)	31	47.1323	16.8134	-34.4116	47.1910	17.0061	-34.0021	-0.0587	-0.1927	0.4095	0.4564	0.4095	Z
	32	45.2468	16.3451	-35.7998	45.2533	16.5188	-35.4360	-0.0065	-0.1737	0.3638	0.4032	0.3638	Z
	33	43.1049	15.8169	-37.3707	43.0632	15.9672	-37.0244	0.0417	-0.1503	0.3463	0.3798	0.3488	X, Z
	35	37 9573	14 6028	-30.9360	37 9238	14 7509	-30.0174	0.0335	-0.1700	0.3206	0.3039	0.3208	X 7
	36	33.3904	13.5016	-44.0127	33.4438	13.6581	-43.6879	-0.0534	-0.1565	0.3248	0.3645	0.3248	Z
A-PILLAR Lateral (Y)	31	47.1323	16.8134	-34.4116	47.1910	17.0061	-34.0021	-0.0587	-0.1927	0.4095	0.4564	-0.1927	Y
	32	45.2468	16.3451	-35.7998	45.2533	16.5188	-35.4360	-0.0065	-0.1737	0.3638	0.4032	-0.1737	Y
	33	43.1049	15.2395	-37.3707	43.0632	15.9672	-37.0244	-0.0266	-0.1503	0.3463	0.3639	-0.1503	Y Y
	35	37.9573	14.6028	-41.1984	37.9238	14.7509	-40.9091	0.0335	-0.1481	0.2893	0.3267	-0.1481	Y
	36	33.3904	13.5016	-44.0127	33.4438	13.6581	-43.6879	-0.0534	-0.1565	0.3248	0.3645	-0.1565	Y
AR UM	37	7.7713	14.3671	-39.7060	7.7775	14.3518	-39.5090	-0.0062	0.0153	0.1970	0.1977	0.1976	Y,Z
Xim Y.	38	5.4807	16.9097	-28.6024	5.3960 9.8134	16.8290	-28.3311	0.0847	0.0807	0.2713	0.2954	0.2954	X, Y, Z
A-B-R X	40	6.0138	17.3323	-17.4161	5.8765	17.1844	-17.2220	0.1373	0.1479	0.1941	0.2800	0.2800	X, Y, Z
B-PILLAR Lateral (Y)	37	7.7713	14.3671	-39.7060	7.7775	14.3518	-39.5090	-0.0062	0.0153	0.1970	0.1977	0.0153	Y
	38	5.4807	16.9097	-28.6024	5.3960	16.8290	-28.3311	0.0847	0.0807	0.2713	0.2954	0.0807	Y
	39	9.9304	17.2991	-22.5679	9.8134	17 1998	-22.3543	0.1170	0.0993	0.2136	0.2630	0.0993	Y
Positive v ompartme Crush cal leforming i	ralues denot ent. culations that nward towa	e deformation at use multip	on as inward	I toward the al compone tment.	occupant c	ompartment	, negative va	ilues denote	e deformatio	ns outward a	away from t	he occupan ere the con	t nponent is
Direction	for Crush co	olumn denote	es which din	ections are	included in t	he crush ca	Iculations. If	"NA" then	no intrusion	is recorded,	and Crush	will be 0.	

Figure C-8. Right Interior Crush Data – Set 2, Test No. WZNP-2



Figure C-9. Exterior Vehicle Crush (NASS) - Front, Test No. WZNP-2



Figure C-10. Exterior Vehicle Crush (NASS) - Side, Test No. WZNP-2

Appendix D. Accelerometer and Rate Transducer Data Plots, Test No. WZNP-2



Figure D-1. 10-ms Average Longitudinal Deceleration System A (SLICE-1), Test No. WZNP-2



Figure D-2. Longitudinal Occupant Impact Velocity System A (SLICE-1), Test No. WZNP-2



Figure D-3. Longitudinal Occupant Displacement System A (SLICE-1), Test No. WZNP-2



Figure D-4. 10-ms Average Lateral Deceleration System A (SLICE-1), Test No. WZNP-2



Figure D-5. Lateral Occupant Impact Velocity System A (SLICE-1), Test No. WZNP-2



Figure D-6. Lateral Occupant Displacement System A (SLICE-1), Test No. WZNP-2



Figure D-7. Vehicle Angular Displacements System A (SLICE-1), Test No. WZNP-2

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Figure D-8. Acceleration Severity Index System A (SLICE-1), Test No. WZNP-2



Figure D-9. 10-ms Average Longitudinal Deceleration System A (SLICE-2), Test No. WZNP-2



Figure D-10. Longitudinal Occupant Impact Velocity System A (SLICE-2), Test No. WZNP-2



Figure D-11. Longitudinal Occupant Displacement System A (SLICE-2), Test No. WZNP-2



Figure D-12. 10-ms Average Lateral Deceleration System A (SLICE-2), Test No. WZNP-2



Figure D-13. Lateral Occupant Impact Velocity System A (SLICE-2), Test No. WZNP-2



Figure D-14. Lateral Occupant Displacement System A (SLICE-2), Test No. WZNP-2


Figure D-15. Vehicle Angular Displacements System A (SLICE-2), Test No. WZNP-2



Figure D-16. Acceleration Severity Index System A (SLICE-2), Test No. WZNP-2



Figure D-17. 10-ms Average Longitudinal Deceleration System B (SLICE-1), Test No. WZNP-2



Figure D-18. Longitudinal Occupant Impact Velocity System B (SLICE-1), Test No. WZNP-2



Figure D-19. Longitudinal Occupant Displacement System B (SLICE-1), Test No. WZNP-2



Figure D-20. 10-ms Average Lateral Deceleration System B (SLICE-1), Test No. WZNP-2



Figure D-21. Lateral Occupant Impact Velocity System B (SLICE-1), Test No. WZNP-2



Figure D-22. Lateral Occupant Displacement System B (SLICE-1), Test No. WZNP-2



Figure D-23. Vehicle Angular Displacements System B (SLICE-1), Test No. WZNP-2



Figure D-24. Acceleration Severity Index System B (SLICE-1), Test No. WZNP-2



Figure D-25. 10-ms Average Longitudinal Deceleration System B (SLICE-2), Test No. WZNP-2



Figure D-26. Longitudinal Occupant Impact Velocity System B (SLICE-2), Test No. WZNP-2



Figure D-27. Longitudinal Occupant Displacement System B (SLICE-2), Test No. WZNP-2



Figure D-28. 10-ms Average Lateral Deceleration System B (SLICE-2), Test No. WZNP-2



Figure D-29. Lateral Occupant Impact Velocity System B (SLICE-2), Test No. WZNP-2



Figure D-30. Lateral Occupant Displacement System B (SLICE-2, Test No. WZNP-2



Figure D-31. Vehicle Angular Displacements System B (SLICE-2), Test No. WZNP-2



Figure D-32. Acceleration Severity Index System B (SLICE-2), Test No. WZNP-2

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