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MIDWEST GUARDRAIL SYSTEM (MGS) WITH SOUTHERN YELLOW PINE POSTS

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16. Abstract (Limit: 200 words)

The Midwest Guardrail System (MGS) has previously been approved for use with various alternative species of wood posts. However, Southern Yellow Pine (SYP) is the most common wood guardrail post material in the United States. The goal of this research was to evaluate the MGS with rectangular SYP posts. In a previous test, the 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1,829-mm) rectangular White Pine post was found to have 39 percent lower capacity than the 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine post. This result indicated that the MGS with SYP posts would likely be successful, but full-scale crash testing was deemed useful to verify satisfactory safety performance and obtain dynamic deflection and working width data under Manual for Assessing Safety Hardware (MASH) TL-3 test conditions.

The MGS was crash tested with 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine posts. This system also used a 6-in. x 12-in. x 141/4-in. long (152-mm x 305-mm x 362-mm) blockout as well as 12-gauge (2.66-mm) guardrail sections. The design was evaluated using a small car (test no. 3-10) and a pickup truck (test no. 3-11) according to the testing standards established in the MASH. The MGS with Southern Yellow Pine posts met the MASH safety requirements for both full-scale crash tests. Following the full-scale crash testing, recommendations were given regarding the use of SYP posts in special MGS applications.

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UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority (IAA) for the data contained herein was Scott Rosenbaugh, Research Associate Engineer.

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1 INTRODUCTION

1.1 Problem Statement

The Midwest Guardrail System (MGS) is a non-proprietary, strong post, W-beam barrier composed of W6x9 or W6x8.5 steel posts or wood guardrail posts, 12-gauge (2.66-mm) W-beam rail, and a 12-in. (305-mm) deep blockout. The MGS has been evaluated under the safety criteria of both the National Cooperative Highway Research Program (NCHRP) Report No. 350 [1] and the *Manual for Assessing Safety Hardware (MASH)* [2] under Test Level 3 (TL-3) impact conditions. Subsequently, the Federal Highway Administration (FHWA) deemed the MGS eligible for reimbursement under the Federal-Aid Highway Program. However, the MGS had never been tested with rectangular Southern Yellow Pine (SYP) wood posts to evaluate the working width and dynamic deflection of the system. Being that rectangular SYP posts are the most commonly used wood guardrail posts in the United States, it was proposed that an evaluation of the MGS with SYP posts would prove beneficial for many State Departments of Transportation (DOTs).

The MGS was previously tested and approved for use with several wood post variations. The MGS has been successfully tested with both alternative wood species round posts [3] and 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1829-mm) rectangular White Pine (WP) posts [4]. WP posts have approximately 39 percent lower capacity than standard SYP wood posts [5]. The Midwest Roadside Safety Facility (MwRSF) performed a crash test under MASH test designation no. 3-11 on the MGS with WP posts. The 2270P vehicle was smoothly redirected in test no. MGSWP-1, and six posts fractured or split [5]. Although test no. MGSWP-1 was a good indicator that the MGS would perform well with SYP posts, the Midwest Pooled Fund Program members desired to obtain the actual system behavior (e.g., dynamic deflection and working width) for a SYP wood post MGS.

1.2 Objective

The objective of this research effort was to evaluate the safety performance of the MGS with 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1829-mm) SYP posts according to the TL-3 full-scale crash testing criteria set forth in MASH.

1.3 Scope

The research objective was achieved through the completion of several tasks. First, two full-scale crash tests were conducted on the MGS with SYP wood posts. The crash tests utilized a pickup truck and a small car, weighing approximately 5,000 lb (2,268 kg) and 2,425 lb (1,100 kg), respectively. The target impact conditions for both tests were an impact speed of 62 mph (100 km/hr) and an impact angle of 25 degrees. Next, the test results were analyzed, evaluated, and documented. Finally, conclusions and recommendations were made that pertain to the safety performance of the MGS with SYP posts.

2 DESIGN DETAILS

The test installation consisted of 181 ft - 3 in. (55.3 m) of standard 12-gauge (2.66-mm) W-beam supported by SYP wood posts, as shown in Figure 1. Anchorage systems similar to those used on tangent guardrail terminals were utilized on both the upstream and downstream ends of the guardrail system. Design details are shown in Figures 1 through 10. Photographs of the test installations are shown in Figures 11 and 12. Material specifications, mill certifications, and certificates of conformity for the component materials are shown in Appendix A.

The system was constructed with twenty-nine wood posts spaced at 75 in. (1,905 mm) on center, as shown in Figures 1 and 2. Post nos. 3 through 27 were 6-in. x 8-in. x 72-in. long (152mm x 203-mm x 1,829-mm) Grade 1 SYP wood posts with a soil embedment depth of 40 in. (1,016 mm). A 6-in. wide x 12-in. deep x 14¹/₄-in. long (152-mm x 305-mm x 362-mm) wood spacer blockout was used to block the rail away from the front face of each steel post. A 16D double head nail was also driven through a hole in the front flange of the post into the top of the blockout assembly to prevent rotation of the blockout. Post nos. 1, 2, 28, and 29 were breakaway cable terminal (BCT) timber posts measuring 5½ in. wide x 7½ in. deep x 46 in. long (140 mm x 191 mm x 1,168 mm) and were placed in 6-ft (1.8-m) long foundation tubes, as shown in Figure 6. A tangent anchorage system was utilized on the upstream and downstream ends of the guardrail system in order to develop the barrier's tensile capacity. The anchorage system consisted of timber posts, foundation tubes, anchor cables, bearing plates, rail brackets, and channel struts, which closely resembled the hardware used in the Modified BCT system. As such, this system is believed to be representative of existing guardrail terminal end anchorages. All posts were placed in a compacted coarse, crushed limestone material.

Standard 12-ft 6-in. (3.81-m) long 12-gauge (2.66-mm) W-beam rails with additional post bolt slots at half-post spacings were placed between post nos. 1 and 29, as shown in Figures

1, 2, and 9. Standard splice bolts, 5% x 22 in. (M16x559) long guardrail bolt and nuts, were used to attach the rail to the posts. The W-beam's top rail height for MGSSYP-1 was 31 in. (787 mm) with a 24%-in. (632-mm) center mounting height. The rail splices were placed at midspan locations, as shown in Figures 1 and 2. All lap-splice connections between the rail sections were configured with the upstream segment in front to minimize vehicle snag at the splice during the crash test.

The installation for test no. MGSSYP-2 was raised 1 in. (25 mm) such that the height to the top of the guardrail was 32 in. (813 mm), as shown in Figures 13 through 22. Photographs of the test installation for test no. MGSSYP-2 are shown in Figure 23.

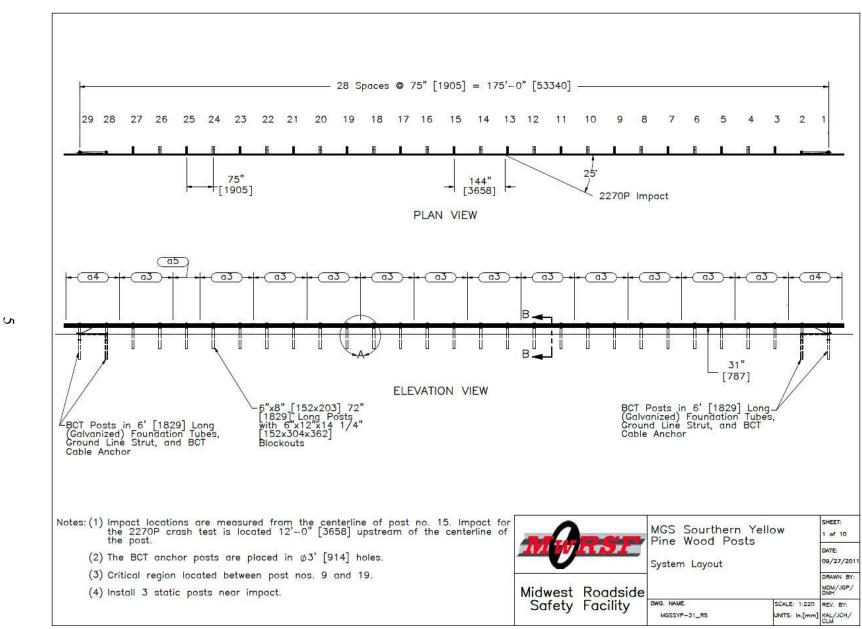


Figure 1. Test Installation Layout, Test No. MGSSYP-1

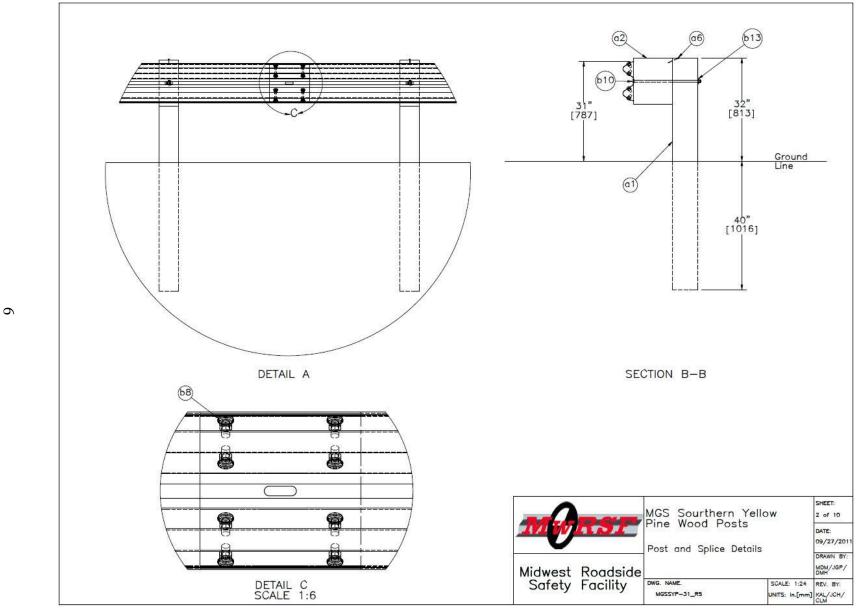


Figure 2. Post and Splice Details, Test No. MGSSYP-1

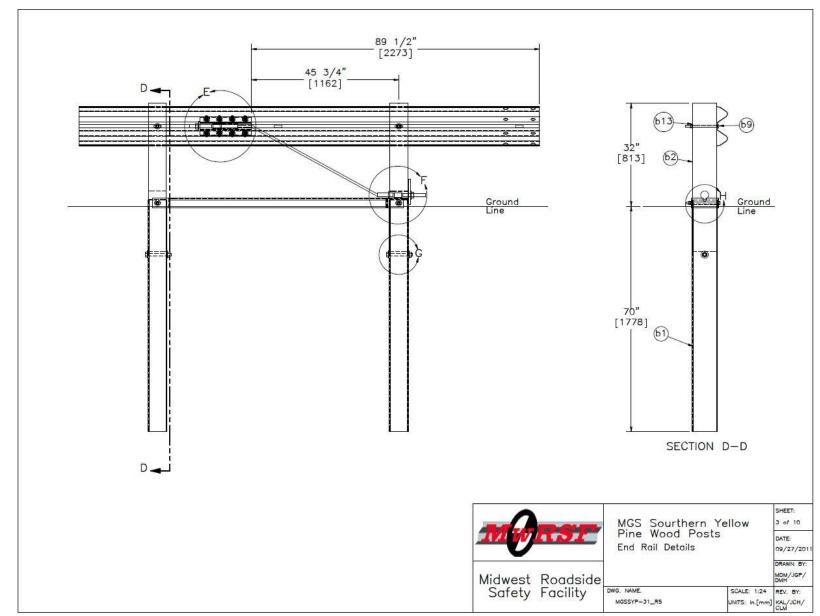


Figure 3. Anchorage Layout, Test No.MGSSYP-1

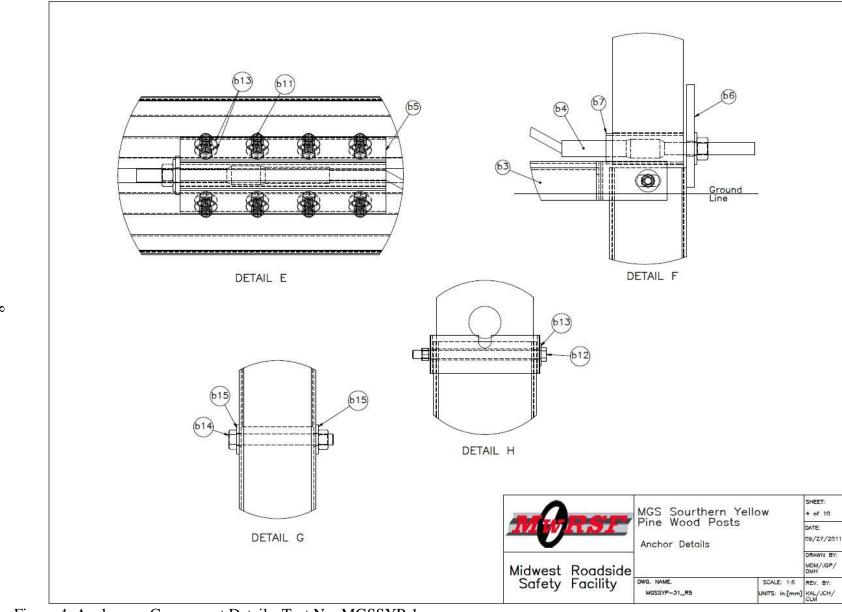


Figure 4. Anchorage Component Details, Test No. MGSSYP-1

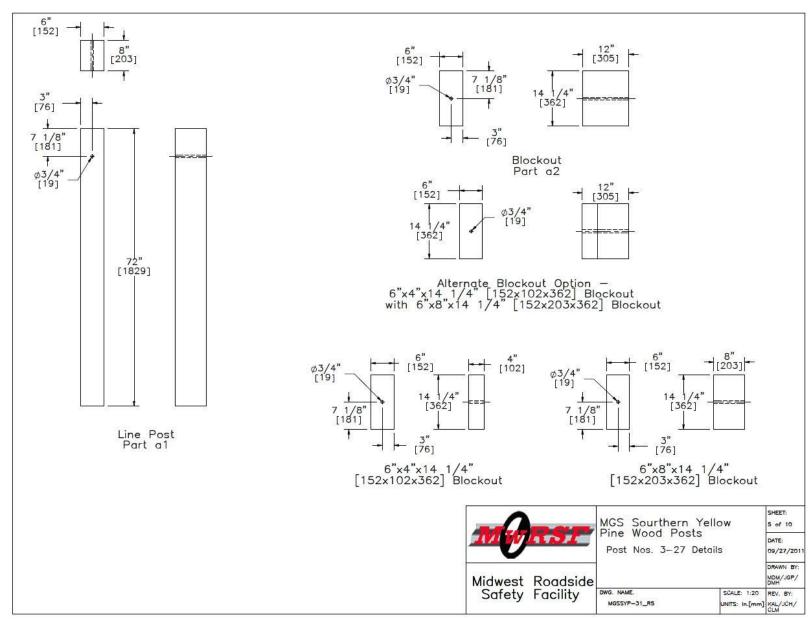


Figure 5. Post nos. 3 through 27 and Blockout Details, Test No. MGSSYP-1

9

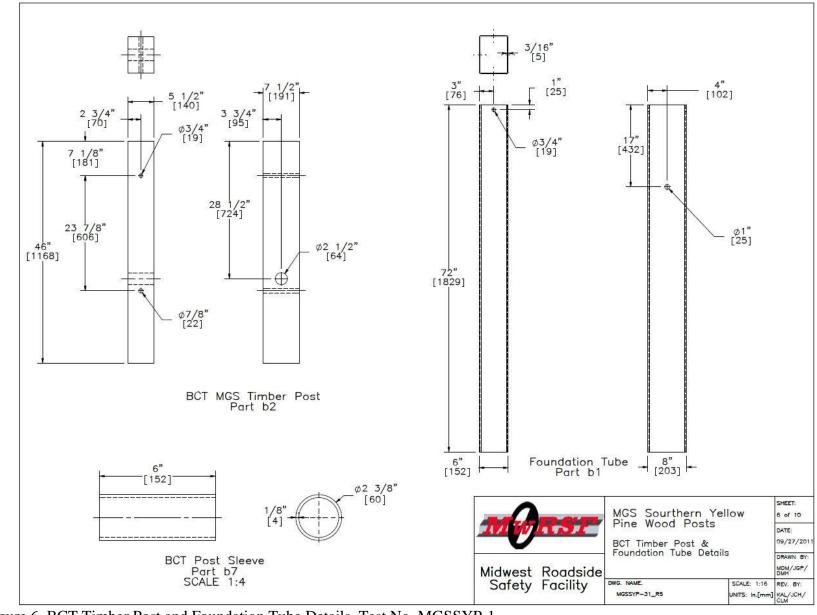


Figure 6. BCT Timber Post and Foundation Tube Details, Test No. MGSSYP-1

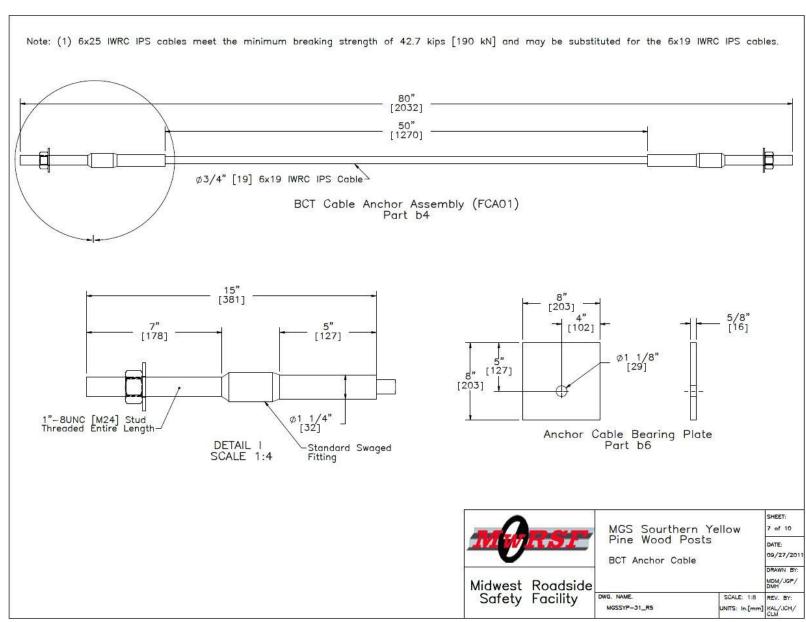


Figure 7. BCT Anchor Cable Details, Test No. MGSSYP-1

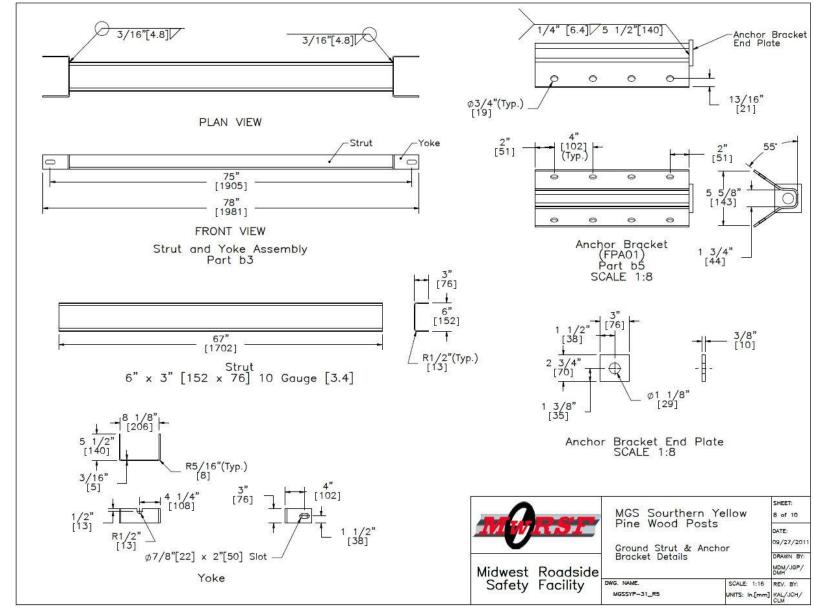


Figure 8. Ground Strut and Anchor Bracket Details, Test No. MGSSYP-1

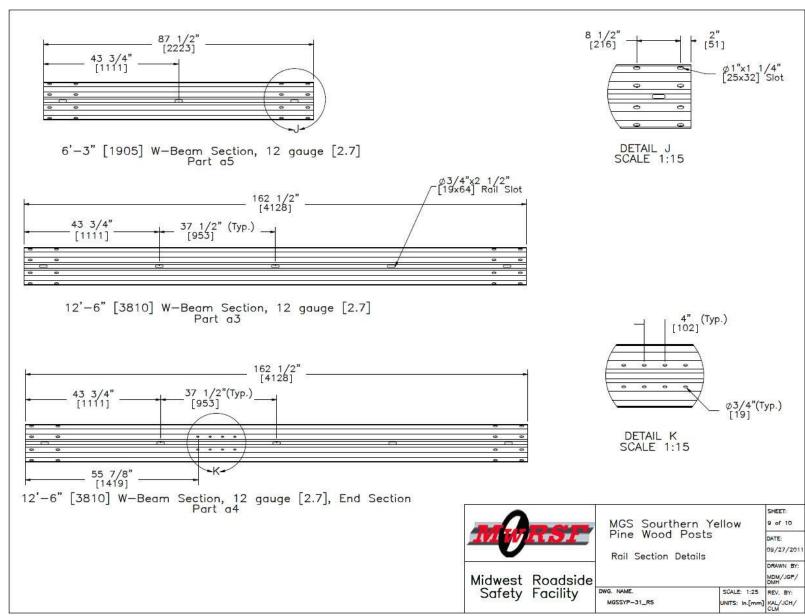


Figure 9. Rail Section Details, Test No. MGSSYP-1

tem No.	QTY.	Description	Material Specification	Hardware Guide
a 1	25	6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	PDE02
a2	25	6"x12"x14 1/4" [152x305x362] MGS Timber Blockout	SYP Grade No.1 or better	PDB11a
a3	12	12'-6" [3810] 4-Space W-Beam Guardrail	12 gauge [2.7] AASHTO M180	RWM04a
a4	2	12'-6" [3810] BCT Terminal Rail Section	12 gauge [2.7] AASHTO M180	-
a5	1	6'-3" [1905] W-Beam Spacer Guardrail	12 gauge [2.7] AASHTO M180	RWM01a
a6	25	16D Double Head Nail	200	12
b1	4	72" [1829] Long Foundation Tube	ASTM A500 Gr. B	PTE06
b2	4	T Timber Post-MGS Height SYP Grade No.1 or better		PDF01
b3	2	Strut and Yoke Assembly	ASTM A36 Steel Galvanized	
b4	2	BCT Cable Anchor Assembly	Ø3/4" 6x19 IWRC IPS Galvanized Wire Rope	FCA01-0
b5	2	Guardrail Anchor Bracket	ASTM A36 Steel	FPA01
b6	2	8"x8"x5/8" [203x203x16] BCT Bearing Plate	ASTM A36 Steel	FPB01
b7	2	2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	FMM02
b8	112	5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB01
b9	4	5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	
b10	25	5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB07
b11	16	5/8" Dia. x 1 1/2" [M16x38] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX16a
b12	4	5/8" Dia. x 9 1/2" [M16x241] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX16a
b13	69	5/8" [16] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC16a
b14	4	7/8" Dia. x 7 1/2" [M22x191] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX22a
b15	8	7/8" [22] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC22a
5.550			MGS Sourthern Yellow	91

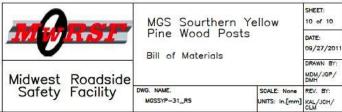


Figure 10. Bill of Materials, Test No. MGSSYP-1







Figure 11. Test Installation Photographs, Test No. MGSSYP-1





Figure 12. Test Installation Photographs, Test No. MGSSYP-1

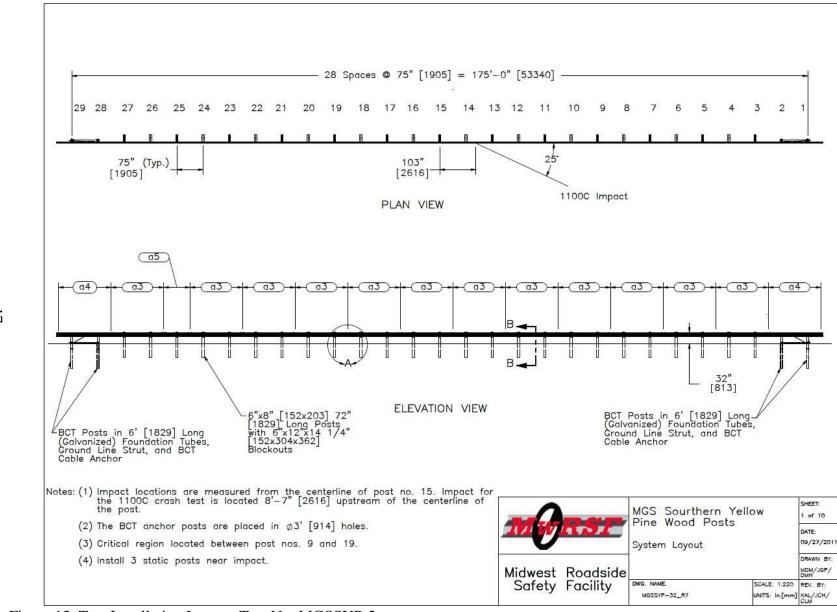


Figure 13. Test Installation Layout, Test No. MGSSYP-2

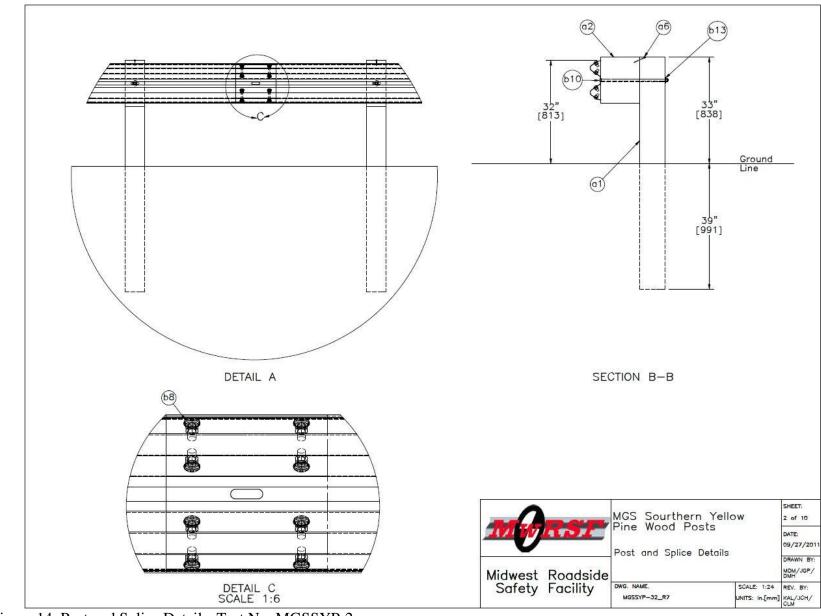


Figure 14. Post and Splice Details, Test No. MGSSYP-2

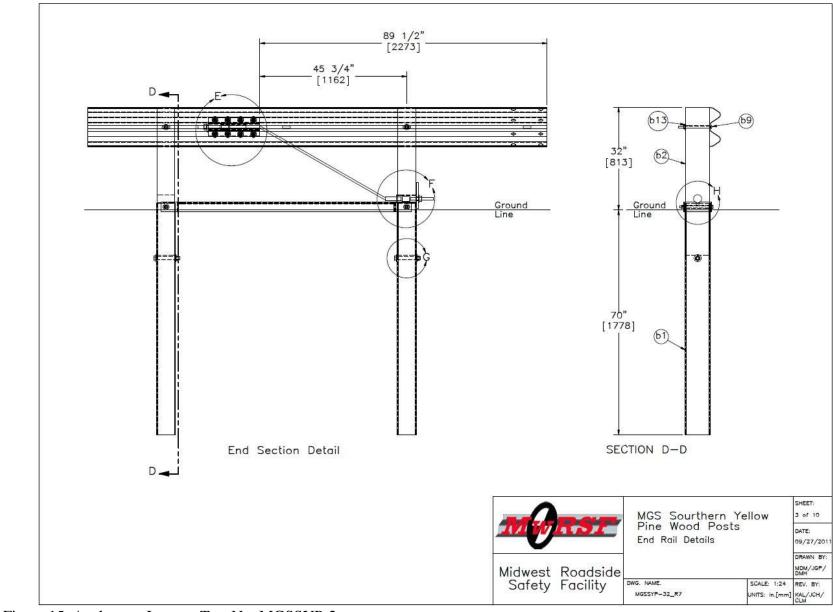


Figure 15. Anchorage Layout, Test No. MGSSYP-2

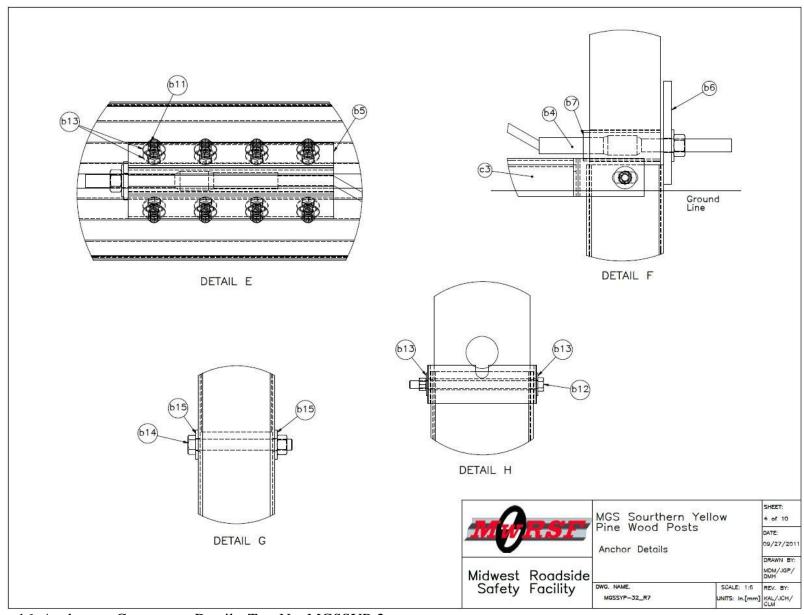


Figure 16. Anchorage Component Details, Test No. MGSSYP-2

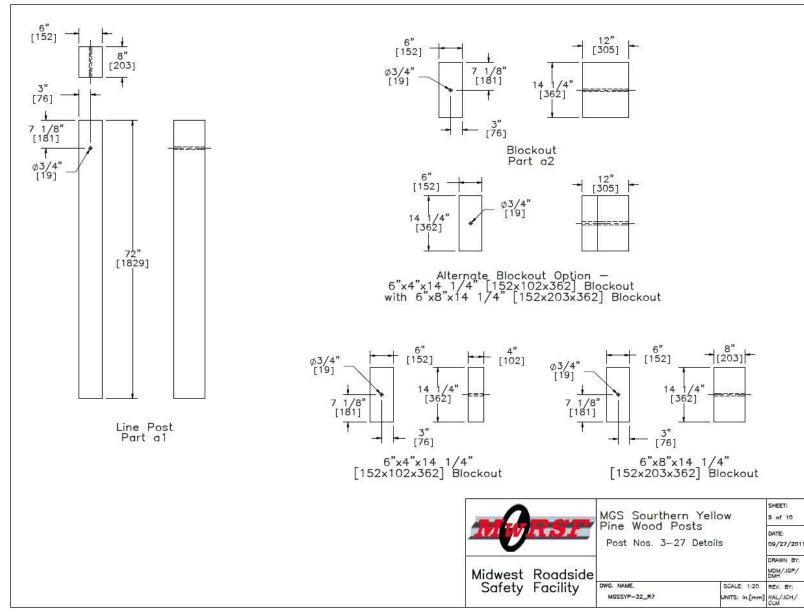


Figure 17. Post nos. 3 through 27 and Blockout Details, Test No. MGSSYP-2

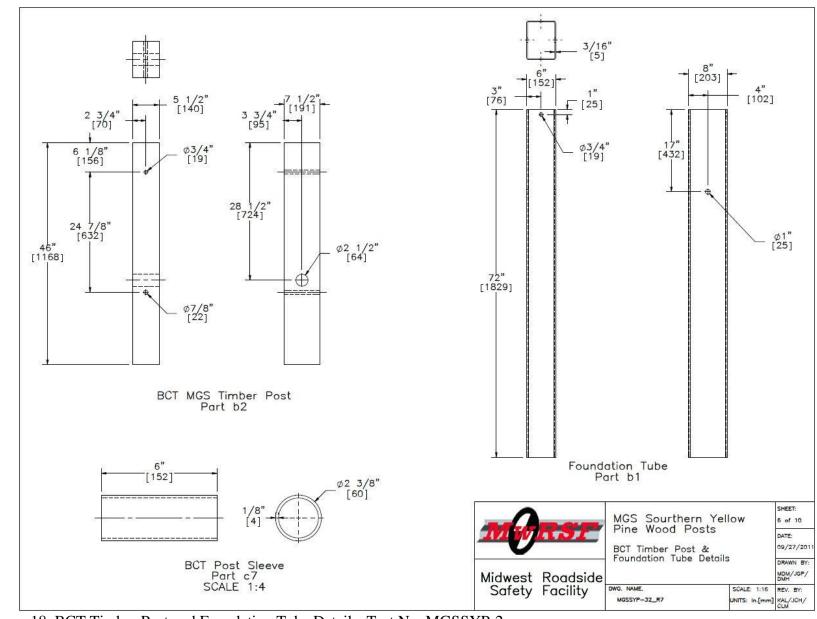


Figure 18. BCT Timber Post and Foundation Tube Details, Test No. MGSSYP-2

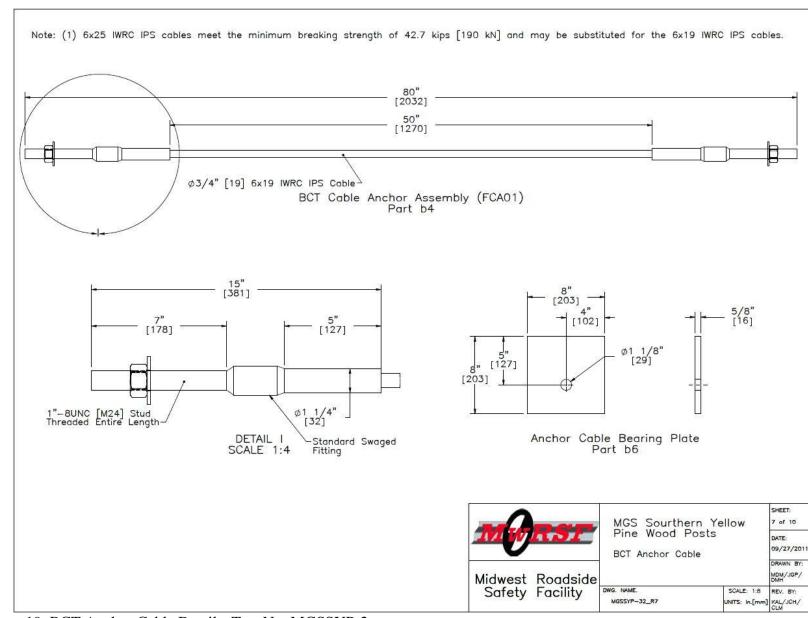


Figure 19. BCT Anchor Cable Details, Test No. MGSSYP-2

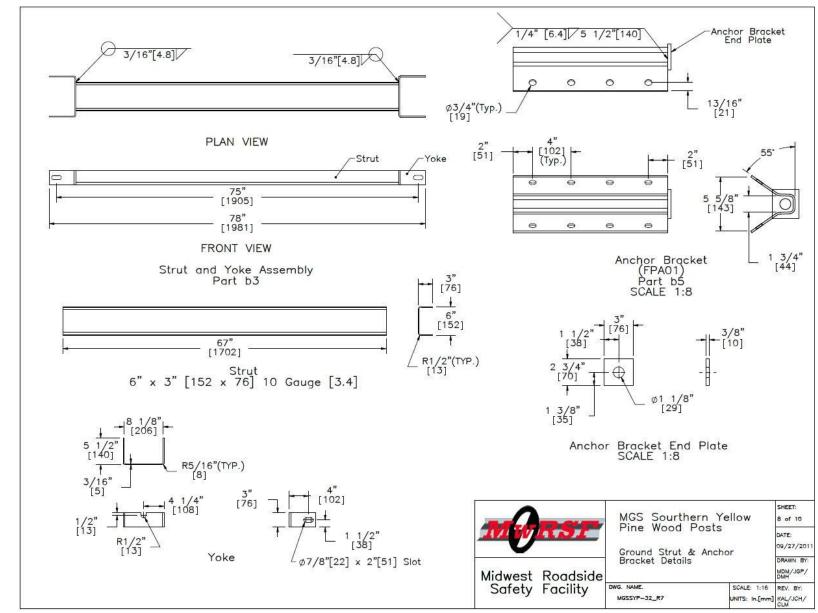


Figure 20. Ground Strut and Anchor Bracket Details, Test No. MGSSYP-2

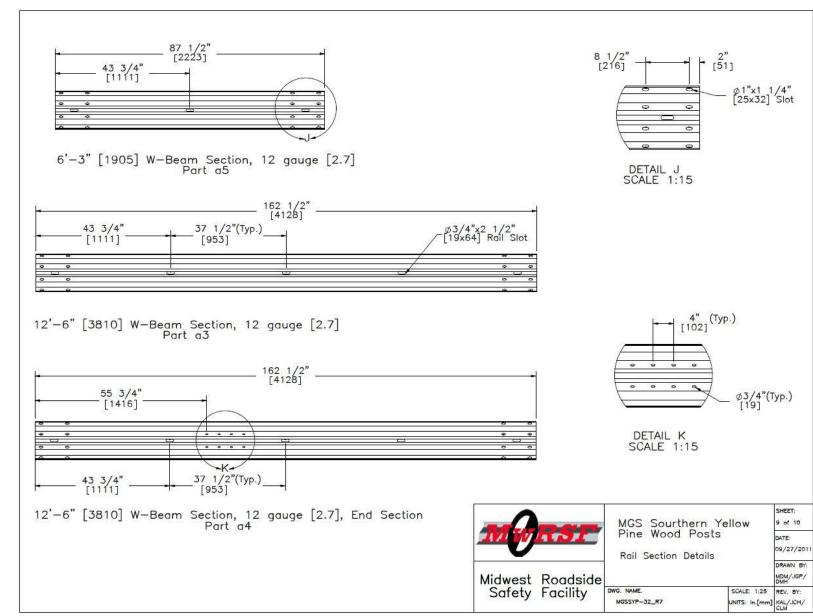


Figure 21. Rail Section Details, Test No. MGSSYP-2

Item No.	QTY.	Description	Material Specification	Hardware Guide	
a1	25	6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	PDE02	
a2	25	6"x12"x14 1/4" [152x305x362] MGS Timber Blockout	SYP Grade No.1 or better	PDB11a	
a3	12	12'-6" [3810] 4-Space W-Beam Guardrail	12 gauge [2.7] AASHTO M180	RWM04c	
a4	2	12'-6" [3810] BCT Terminal Rail Section	12 gauge [2.7] AASHTO M180	-	
a5	1	6'-3" [1905] W-Beam Spacer Guardrail	12 gauge [2.7] AASHTO M180	RWM01c	
a6	25	16D Double Head Nail	12	-	
b1	4	72" [1829] Long Foundation Tube	ASTM A500 Gr. B	PTE06	
b2	4	BCT Timber Post-MGS Height	SYP Grade No.1 or better	PDF01	
b3	2	Strut and Yoke Assembly	ASTM A36 Steel Galvanized	-	
b4	2	BCT Cable Anchor Assembly	φ3/4" 6x19 IWRC IPS Galvanized Wire Rope	FCA01-0	
b5	2	Guardrail Anchor Bracket	ASTM A36 Steel	FPA01	
b6	2	8"x8"x5/8" [203x203x16] BCT Bearing Plate	ASTM A36 Steel		
b7	2	2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40		
b8	112	5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB01	
b9	4	5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB03	
b10	25	5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB07	
b11	16	5/8" Dia. x 1 1/2" [M16x38] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX16d	
b12	4	5/8" Dia. x 9 1/2" [M16x241] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX16a	
b13	69	5/8" [16] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC16a	
b14	4	7/8" Dia. x 7 1/2" [M22x191] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX22a	
b15	8	7/8" [22] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC22d	

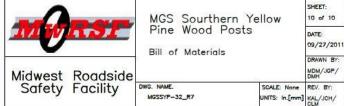


Figure 22. Bill of Materials, Test No. MGSSYP-2







Figure 23. Test Installation Photographs, Test No. MGSSYP-2

3 TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 Test Requirements

Longitudinal barriers, such as W-beam guardrails, must satisfy impact safety standards in order to be accepted by the Federal Highway Administration (FHWA) for use on the National Highway System (NHS). For new hardware, these safety standards consist of the guidelines and procedures published in MASH [2]. According to TL-3 of MASH, longitudinal barrier systems must be subjected to two full-scale vehicle crash tests. The two full-scale crash tests are noted below:

- 1. Test Designation No. 3-10 consists of a 2,425-lb (1,100-kg) passenger car impacting the system at a nominal speed and angle of 62 mph (100 km/h) and 25 degrees, respectively.
- 2. Test Designation No. 3-11 consists of a 5,000-lb (2,268-kg) pickup truck impacting the system at a nominal speed and angle of 62 mph (100 km/h) and 25 degrees, respectively.

The test conditions of TL-3 longitudinal barriers are summarized in Table 1.

Table 1. MASH TL-3 Crash Test Conditions

	Test		Imp	act Condit	Evaluation Criteria ¹	
Test Article	Designation	Test Vehicle	Speed			Angle
Article	No.	Venicie	mph	km/h	(deg)	Cincila
Longitudinal	3-10	1100C	62	100	25	A,D,F,H,I
Barrier	3-11	2270P	62	100	25	A,D,F,H,I

¹ Evaluation criteria explained in Table 2.

3.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas:
(1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the longitudinal barrier to contain and

redirect impacting vehicles. In addition, controlled lateral deflection of the test article is acceptable. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are summarized in Table 2 and defined in greater detail in MASH. The full-scale vehicle crash test was conducted and reported in accordance with the procedures provided in MASH.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported on the test summary sheet. Additional discussion on PHD, THIV and ASI is provided in MASH. Note that ASI values were calculated according to MASH as developed by TTI.

3.3 Soil Strength Requirements

In order to limit the variation of soil strength among testing agencies, foundation soil must satisfy the recommended performance characteristics set forth in Chapter 3 and Appendix B of MASH. Testing facilities must first subject the designated soil to a dynamic post test to demonstrate a minimum dynamic load of 7.5 kips (33.4 kN) at deflections between 5 and 20 in. (127 and 508 mm). If satisfactory results are observed, a static test is conducted using an identical test installation. The results from this static test become the baseline requirement for soil strength in future full-scale crash testing in which the designated soil is used. An additional post installed near the impact point is statically tested on the day of full-scale crash test in the same manner as used in the baseline static test. The full-scale crash test can be conducted only if the static test results show a soil resistance equal to or greater than 90 percent of the baseline static test at deflections of 5, 10, and 15 in. (127, 254, and 381 mm) or if a dynamic test shows a

soil resistance of at least 7.5 kips (33.4 kN) at deflections between 5 and 20 in. (127 and 508 mm). Otherwise, the crash test must be postponed until the soil demonstrates adequate post-soil strength.

Table 2. MASH Evaluation Criteria for Longitudinal Barrier

Structural Adequacy	A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.						
	D.	Detached elements, fragment should not penetrate or show compartment, or present a pedestrians, or personnel in intrusions into, the occupant set forth in Section 5.3 and Ap	potential for penetra an undue hazard a work zone. De compartment should	ating the occupant to other traffic, formations of, or not exceed limits				
	F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.						
Occupant	H.	Occupant Impact Velocity (OIV) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:						
Risk		Occupant Impact Velocity Limits						
		Component	Preferred	Maximum				
		Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)				
	I.	The Occupant Ridedown Acceleration (ORA) (see Appendix Section A5.3 of MASH for calculation procedure) should satisfy following limits:						
		Occupant Rideo	Occupant Ridedown Acceleration Limits					
		Component	Preferred	Maximum				
		Longitudinal and Lateral	15.0 g's	20.49 g's				

4 TEST CONDITIONS

4.1 Test Facility

The testing facility is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles (8.0 km) northwest of the University of Nebraska-Lincoln.

4.2 Vehicle Tow and Guidance System

A reverse cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [6] was used to steer the test vehicle. A guide flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the barrier system. The 3/8-in. (9.5-mm) diameter guide cable was tensioned to approximately 3,500 lb (15.6 kN) and supported both laterally and vertically every 100 ft (30.5 m) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

4.3 Test Vehicles

For test no. MGSSYP-1, a 2004 Dodge Ram Quad Cab 1500 pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 5,130 lb (2,327 kg), 5,029 lb (2,281 kg), and 5,199 lb (2,358 kg), respectively. The test vehicle is shown in Figure 24, and vehicle dimensions are shown in Figure 25.

For test no. MGSSYP-2, a 2004 Kia Rio sedan was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 2,402 lb (1,090 kg), 2,442 lb (1,108 kg), 2,612







Figure 24. Test Vehicle, Test No. MGSSYP-1

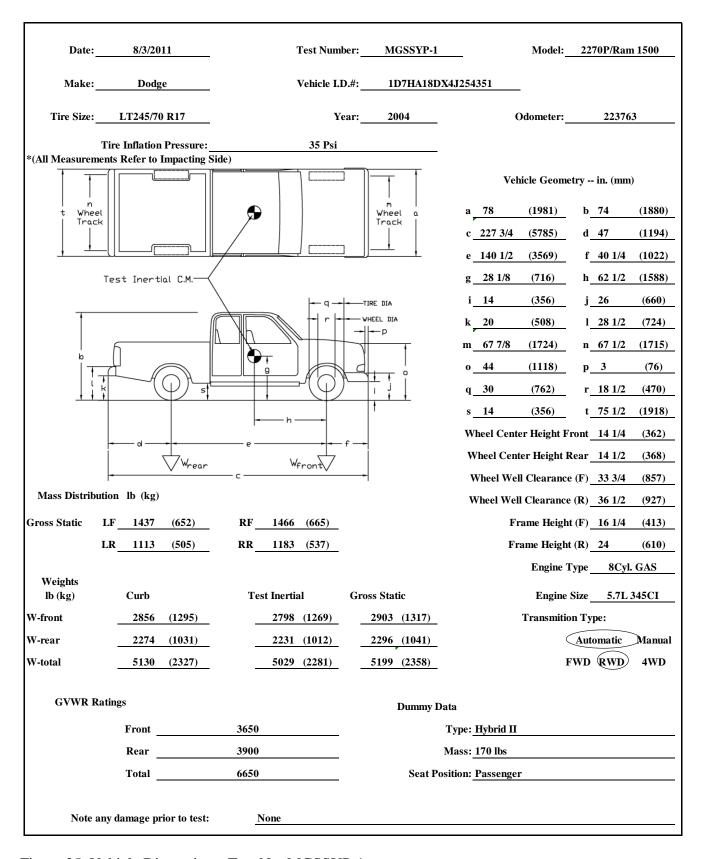


Figure 25. Vehicle Dimensions, Test No. MGSSYP-1

lb (1,185 kg) respectively. The test vehicle is shown in Figure 26, and the vehicle dimensions are shown in Figure 27.

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The Suspension Method [7] was used to determine the vertical component of the c.g. for the pickup truck. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The vertical component of the c.g. for the 1100C vehicle was based on historical c.g. height measurements. The location of the final c.g. is shown in Figures 25 through 29. Data used to calculate the location of the c.g. and ballast information are shown in Appendix B.

Square, black- and white-checkered targets were placed on the vehicles for reference to be viewed from the high-speed digital video cameras and aid in the video analysis, as shown in Figures 28 and 29. Round, checkered targets were placed on the center of gravity on the left-side door, the right-side door, and the roof of the vehicle.

The front wheels of the test vehicles were aligned to vehicle standards except the toe-in value was adjusted to zero so that the vehicles would track properly along the guide cable. A 5B flash bulb was mounted on the right side of the vehicle's dash for both tests and was fired by a pressure tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial impact with the test article to create a visual indicator of the precise time of impact on the high-speed videos. A remote controlled brake system was installed in the test vehicles so the vehicles could be brought safely to a stop after the test.







Figure 26. Test Vehicle, Test No. MGSSYP-2

Date:	9/13/20	11		Test Nun	nber:I	MGSSYP-2	Model: 1100C
Make:	Kia			Vehicle I	. D. #:	KNADC125	5046350879
Tire Size:	175/65 I	R14		Ŋ	Year: 2	004	Odometer: 85056
	Tire Inflation	Pressure:		30psi	i		
*(All Measuren	nents Refer to	Impacting S	Side)				_
<u> </u>	·		П		5	-	Vehicle Geometry in. (mm)
					1	1	a 65 1/4 (1657) b 55 (1397)
a m —		-			- Q vehicl	_ n t	c 167 (4242) d 38 1/2 (978)
					Venici		e 95 3/4 (2432) f 32 3/4 (832)
			// [_		<u></u>		g 17 (432) h 37 (942)
	. •						i 8 1/2 (216) j 21 (533)
							k 11 1/2 (292) l 22 (559)
	P q					+	m 56 1/8 (1426) n 56 3/4 (1441)
		4)		o 27 3/8 (695) p 3 (76)
1					<u> </u>	, b	q_22 1/2 (572) r_15 1/4 (387)
			15		<u>⊬</u>	9	s 11 (279) t 60 1/4 (1530)
	f	h	12		,	1 1 1	Wheel Center Height Front 10 3/4 (273)
		√front	e	Wre			Wheel Center Height Rear 10 7/8 (276)
	-	HOHE		1	201		Wheel Well Clearance (F) 23 7/8 (606)
Mass Distrib	oution lb (kg)						Wheel Well Clearance (R) 24 (610)
Gross Static	LF 783	(355)	RF_	797 (362)	-		Frame Height (F) 6 3/4 (171)
	LR 482	(219)	RR_	550 (249)	_		Frame Height (R) 16 1/2 (419)
							Engine Type 4cyl gas
Weights lb (kg)	Curb		Test	t Inertial	Gross Sta	ıtic	Engine Size1.4L
W-front	1517	(688)	_	1496 (679)	1580	(717)	Transmition Type:
W-rear	885	(401)	_	946 (429)	1032	(468)	Automatic Manual
W-total	2402	(1090)	_	2442 (1108)	2612	(1185)	FWD RWD 4WD
GVWR R	Ratings					Dummy Da	ata
	Front		1808				Type: Hybrid 1
	Rear		1742		-		Mass: <u>170 lbs.</u>
	Total		3399		-	Seat I	Position: Passenger
Note a	Note any damage prior to test: Minor Hail Damage						

Figure 27. Vehicle Dimensions, Test No. MGSSYP-2

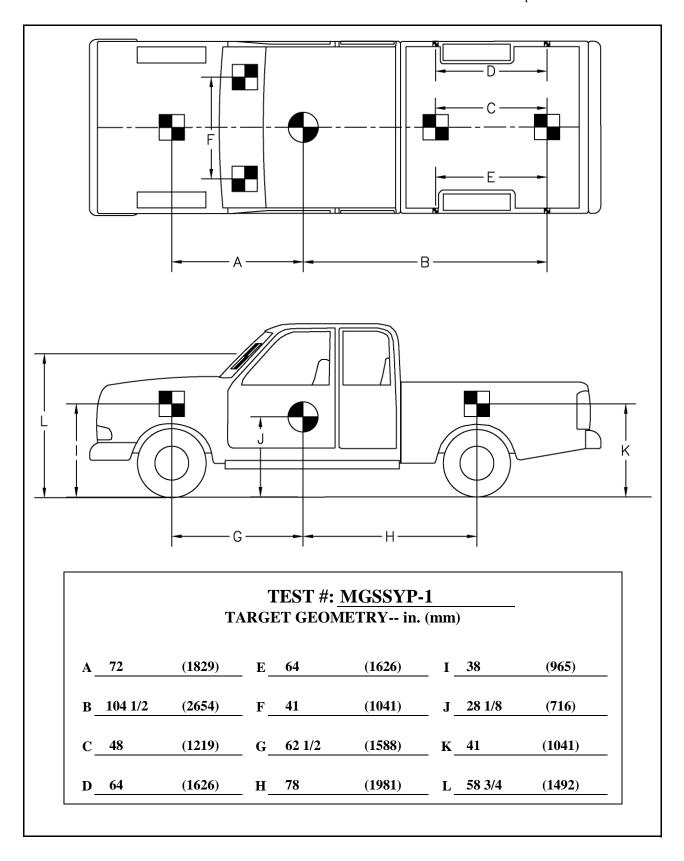


Figure 28. Target Geometry, Test No. MGSSYP-1

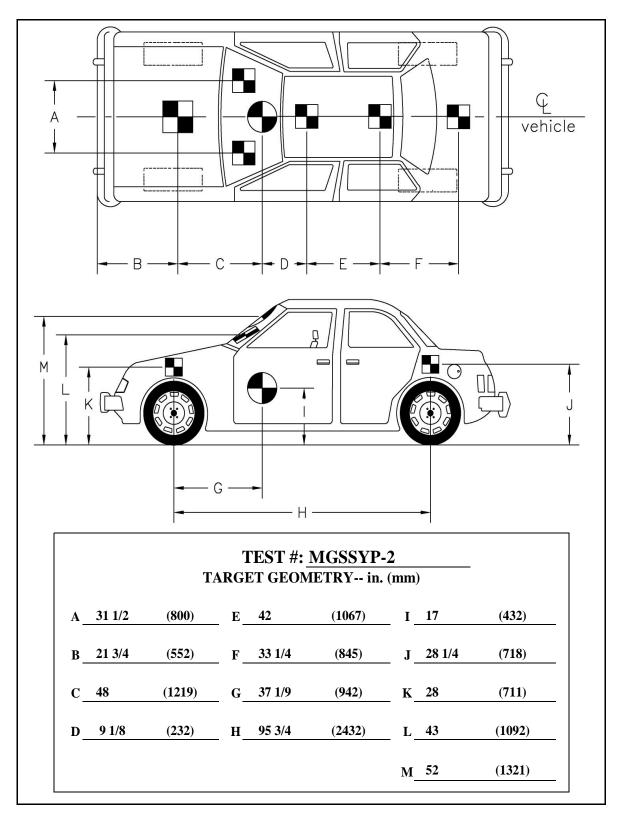


Figure 29. Target Geometry, Test No. MGSSYP-2

4.4 Simulated Occupant

For test nos. MGSSYP-1 and MGSSYP-2, a Hybrid II 50th-Percentile, Adult Male Dummy, equipped with clothing and footwear, was placed in the right-front seat of the test vehicle with the seat belt fastened. The dummy, which had a final weight of 170 lb (77 kg), was represented by model no. 572, serial no. 451, and was manufactured by Android Systems of Carson, California. As recommended by MASH, the dummy was not included in calculating the c.g. location.

4.5 Data Acquisition Systems

4.5.1 Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. All of the accelerometers were mounted near the center of gravity of the test vehicles. The electronic accelerometer data obtained in dynamic testing was filtered using the SAE Class 60 and the SAE Class 180 Butterworth filter conforming to SAE J211/1 specifications [8].

The first accelerometer system was a two-arm piezoresistive accelerometer system manufactured by Endevco of San Juan Capistrano, California. Three accelerometers were used to measure each of the longitudinal, lateral, and vertical accelerations independently at a sample rate of 10,000 Hz. Two additional accelerometers were used to measure longitudinal and lateral accelerations independently at the same rate. The accelerometers were configured and controlled using a system developed and manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. More specifically, data was collected using a DTS Sensor Input Module (SIM), Model TDAS3-SIM-16M. The SIM was configured with 16 MB SRAM and 8 sensor input channels with 250 kB SRAM/channel. The SIM was mounted on a TDAS3-R4 module rack. The module rack was configured with isolated power/event/communications, 10BaseT

Ethernet and RS232 communication, and an internal backup battery. Both the SIM and module rack were crashworthy. The "DTS TDAS Control" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

The second system, Model EDR-3, was a triaxial piezoresistive accelerometer system manufactured by IST of Okemos, Michigan. The EDR-3 was configured with 256 kB of RAM, a range of ±200 g's, a sample rate of 3,200 Hz, and a 1,120 Hz low-pass filter. The "DynaMax 1 (DM-1)" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

4.5.2 Rate Transducers

An angular rate sensor, the ARS-1500, with a range of 1,500 degrees/sec in each of the three directions (roll, pitch, and yaw) was used to measure the rates of rotation of the test vehicles. The angular rate sensor was mounted on an aluminum block inside the test vehicle near the center of gravity and recorded data at 10,000 Hz to the SIM. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The "DTS TDAS Control" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

4.5.3 Pressure Tape Switches

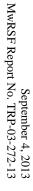
For test nos. MGSSYP-1 and MGSSYP-2, five pressure-activated tape switches, spaced at approximately 6.56-ft (2-m) intervals, were used to determine the speed of the vehicle before impact. Each tape switch fired a strobe light which sent an electronic timing signal to the data acquisition system as the right-front tire of the test vehicle passed over it. Test vehicle speeds were determined from electronic timing mark data recorded using TestPoint and LabVIEW computer software programs. Strobe lights and high-speed video analysis are used only as a backup in the event that vehicle speed cannot be determined from the electronic data.

4.5.4 Digital Photography

Two AOS VITcam high-speed digital video cameras, three AOS X-PRI high-speed digital video cameras, four JVC digital video cameras, and two Canon digital video cameras were utilized to film test no. MGSSYP-1. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 30.

Three AOS VITcam high-speed digital video cameras, three AOS X-PRI high-speed digital video cameras, four JVC digital video cameras, and two Canon digital video cameras were utilized to film test no. MGSSYP-2. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 31.

The high-speed videos were analyzed using ImageExpress, MotionPlus, and RedLake MotionScope software programs. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed videos. A Nikon D50 digital still camera was also used to document pre- and post-test conditions for all tests.



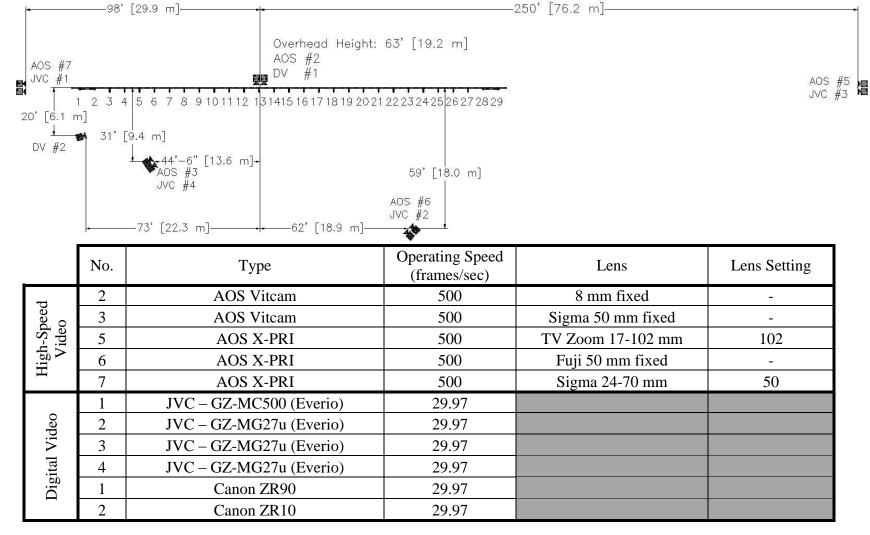
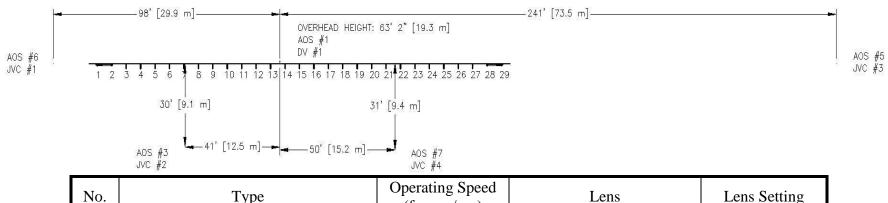


Figure 30. Camera Locations, Speeds, and Lens Settings, Test No. MGSSYP-1



-	No.	Туре	(frames/sec)	Lens	Lens Setting
.eo	1	AOS Vitcam CTM	500	Cosmicar 12.5 mm fixed	-
Video	3	AOS Vitcam	500	Sigma 24-70 mm	35
eq	4	AOS Vitcam	500	-	-
High-Speed	5	AOS X-PRI	500	Canon 17-102 mm	102
gh-,	6	AOS X-PRI	500	Fujinon 50 mm fixed	-
Hig	7	AOS X-PRI	500	Sigma 50 mm fixed	-
	1	JVC – GZ-MC500 (Everio)	29.97		
Video	2	JVC – GZ-MG27u (Everio)	29.97		
	3	JVC – GZ-MG27u (Everio)	29.97		
ital	4	JVC – GZ-MG27u (Everio)	29.97		
Digital	1	Canon ZR90	29.97		
	2	Canon ZR10	29.97		

Figure 31. Camera Locations, Speeds, and Lens Settings, Test No. MGSSYP-2

5 FULL-SCALE CRASH TEST NO. MGSSYP-1

5.1 Dynamic Soil Test

Before full-scale crash test no. MGSSYP-1 was conducted, the strength of the foundation soil was evaluated with a dynamic test, as described in MASH [2]. The dynamic test results are shown in Appendix C. The force vs. deflection curve for the dynamic soil test was determined using the acceleration data from the bogie vehicle to determine both the load and deflection of the post in the soil. While Appendix B of MASH requires the use of load cells for determination of post-soil forces, MwRSF has demonstrated through previous bogie tests of posts in soil that the load versus deflection as determined by accelerometers on the bogie vehicle compares well with data obtained from load cells mounted on an impacted post. There are minor differences in the load and deflection as measured by the accelerometer versus a dedicated transducer. First, loads measured by the load cell are expected to be slightly higher than those measured by the accelerometer due to the accelerometer only capturing the longitudinal component of the impact force as the post rotates backward. The vertical component of the impact load, which increases in magnitude as the rotation angle increases, is not reflected in the accelerometer data. Thus, utilizing accelerometers to obtain force data would be a conservative estimate of soil strength.

The soil strength test conducted prior to test no. MGSSYP-1 demonstrated that the soil for the test generated relatively high initial force levels, but the force level between 19 and 20 in. (483 and 508 mm) was slightly lower than the MASH requirement of 7,500 lb (33.4 kN). It was reasoned that the soil strength was sufficient even though the end of the post-soil force vs. deflection curve dipped slightly below the required threshold. First, the initial loading of the soil was significantly higher than the 7,500 lb (33.4 kN) force limit for the initial 10 in. (254 mm) of deflection. This indicated that the soil stiffness was high and that the soil was absorbing a significant amount of energy. Second, as noted above, the force data measured by the

accelerometer is conservative and was likely underestimating the soil resistance near the end of the post deflection. Third, the post-soil forces were only below the threshold for a limited deflection near the end of the 20 in. (508 mm) deflection limit. As such, the effect on overall post behavior was determined to be negligible.

5.2 Test No. MGSSYP-1

The 5,199-lb (2,358-kg) pickup truck impacted the MGS with SYP wood posts at a speed of 62.2 mph (100.1 km/h) and at an angle of 24.9 degrees. A summary of the test results and sequential photographs are shown in Figure 32. Additional sequential photographs are shown in Figures 33 and 34.

5.3 Weather Conditions

Test no. MGSSYP-1 was conducted on August 3, 2011 at approximately 4:45 pm. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported and are shown in Table 3 [9].

Table 3. Weather Conditions, Test No. MGSSYP-1

Temperature	85° F
Humidity	55 %
Wind Speed	11 mph
Wind Direction	30° from True North
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0.00 in.
Previous 7-Day Precipitation	0.14 in.

5.4 Test Description

Initial vehicle impact was to occur 12 ft (3.7 m) upstream of the center line of post no. 15, as shown in Figure 35, which was selected using the CIP plots found in Section 2.3 of MASH to maximize pocketing and the propensity of wheel snag. The actual point of impact was 12 ft - 6 in. (3.8 m) upstream of post no. 15. A sequential description of the impact event is

contained in Table 4. The vehicle came to rest 209 ft (63.7 m) downstream of the impact point and 56 ft - 10 in. (17.3 m) laterally behind the barrier system, and its trajectory did not violate the bounds of the exit box. The vehicle trajectory and final position are shown in Figures 32 and 36.

Table 4. Sequential Description of Impact Events, Test No. MGSSYP-1

TIME	EVENT
(sec)	
0.000	The right-front corner of vehicle impacted rail $12 \text{ ft} - 6 \text{ in.}$ (3.8 m) upstream from post no. 15.
0.004	Post no. 13 deflected backward.
0.022	The right-front fender of vehicle deformed, post no. 14 deflected backward, and rail kinked downstream of post no. 14.
0.030	The upstream terminal deflected downstream, post no. 1 was moved upward, and post no. 12 deflected backward.
0.038	The right-front headlight shattered, downstream terminal rail deflected upstream, post no. 15 deflected backward, and rail kinked upstream of post no. 15.
0.060	The rail kinked downstream of post no. 15, and vehicle began to yaw counterclockwise.
0.066	The rail released from post no. 14.
0.074	Post no. 16 deflected backward.
0.080	Post no. 14 began to fracture.
0.095	The posts upstream of impact rotated toward impact point, and right-front wheel snagged on post no. 14 and disengaged from vehicle.
0.100	Post no. 15 fractured.
0.112	The rail released from post no. 15.
0.118	A kink formed in rail downstream of post no. 16, post no. 16 fractured approximately 1 ft (305 mm) above ground level, and right-front door of vehicle became slightly ajar.
0.136	Post nos. 17 and 18 deflected backward, and the vehicle rolled away from system.
0.144	The rail released from post no. 16.
0.154	The rail kinked at post no. 18.
0.228	The vehicle rolled slightly toward system.
0.238	The undercarriage of vehicle impacted remaining 1 ft (305 mm) of post no. 16.
0.290	The vehicle was parallel to system with a speed of 46.8 mph (75.3 km/h).
0.300	The upstream terminal was at maximum deflection, post no. 19 deflected backward, and post no. 17 fractured.

0.308	The rail released from post no. 17.
0.652	The vehicle exited system with a speed of 37.8 mph (60.8 km/h) and at an angle of 15.7 degrees.
0.892	The right-front brake disk contacted ground.
0.966	The right-front bumper contacted ground.

5.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 37 through 38. Barrier damage consisted of deformed guardrail, fractured posts, and contact marks on the front face of the W-beam guardrail. The length of vehicle contact along the barrier was approximately 34 ft -4 in. (10.5 m) which spanned from 4 in. (102 mm) upstream of the centerline of post no. 13 and extended to 33 in. (838 mm) downstream of post no. 18.

The rail disengaged from several posts both upstream and downstream of impact. The guardrail bolt pulled through the rail at post nos. 3 through 5, 7 through 9, and 14 through 17. A ¹/₄-in. (6-mm) tear was found in the rail on the upstream end of the slot at post no 3. A ¹/₄-in. (6-mm) tear also occurred at the bottom center of the slot at post no. 7. A ¹/₂-in. (13-mm) tear occurred on the bottom downstream edge of the slot at post no. 14.

Deformations in the rail occurred from post no. 12 to post no. 18. The top of the rail kinked at post no. 12. The rail buckled $2\frac{1}{2}$ in. (64 mm) downstream of the downstream side of the slot at post no. 13. The bottom corrugation began to fold at post no. 13. Folding of the bottom corrugation also occurred from 52 in. (1,321 mm) downstream of post no. 13 and extended to 33 in. (838 mm) downstream of post no. 14. The rail kinked 4 in. (102 mm) upstream of post no. 13. Flattening of the rail began 1 in. (25 mm) downstream of post no. 13 and extended to 52 in. (1,321 mm) downstream of post no. 13. Flattening occurred again from 33 in. (838 mm) downstream of post no. 14 and extended to 5 in. (127 mm) upstream of post no. 17. Flattening also occurred from 23 in. (584 mm) upstream of post no. 18 and extended to 10 in. (254 mm)

downstream of post no. 18. The bottom corrugation of the rail kinked at 31 in. (787 mm) downstream of post no. 18. The rail also buckled at post no. 18.

The top of the blockouts of post nos. 3 through 5 were twisted upstream. The top of the blockouts of post nos. 6 and 7 were twisted downstream. The front of the blockouts for post nos. 6 and 10 were rotated downstream. The top of the blockouts for post nos. 9 and 11 were twisted downstream.

Damage to the posts began at post no. 6, which split on the front face downstream corner. Post no. 10 split at the center of the top of the post from the front to the back. This split started at the top of the post and extended $8\frac{1}{2}$ in. (216 mm) down the post. Post no. 11 split at the center of the post from the front to the back. The split started at the top of the post and extended to the groundline. Post nos. 12 and 13 rotated backwards and split at the center of the post from the front of the post to the back of the post. The splits on both posts started at the top of the post and continued to the groundline. Post nos. 14 through 17 were fractured at the groundline. Post no. 14 came to rest 9 ft – 6 in. (2,896 mm) behind the barrier. Post no. 15 came to rest 9 ft – 3 in. (2,819 mm) behind the barrier. Post no. 16 came to rest 14 ft – 6 in. (4,420 mm) behind the barrier. Post no. 17 came to rest 1 ft – 1 in. (330 mm) behind the barrier. Tire contact marks were found 21 in. (533 mm) down from the top of the front face of post no. 14. Post no. 16 was split into 3 pieces due to contact with the vehicle, and contact marks were also found on the front face of the post. Soil gaps, heaves, and craters can be found in Table 5.

The maximum permanent set of the barrier system was 30¼ in. (768 mm) at the midspan between post nos. 15 and 16, as measured in the field. The maximum lateral dynamic rail and post deflections were 40.0 in. (1,016 mm) at post no. 15 and 28.1 in. (714 mm) at post no. 17, respectively, as determined from high-speed digital video analysis. The working width of the

system was found to be 53.8 in. (1,367 mm), also determined from high-speed digital video analysis.

Table 5. Soil Gap, Soil Heave, and Soil Crater Measurements, Test No. MGSSYP-1

	S	oil Gap Location in. (mm)	on ¹ ,	Soil He in. (n	/	Soil Cra in. (m	,	
Post No.	Upstream	Downstream	Front	Back	Diameter	Height	Diameter	Depth
1	1½ (38)	0	0	0	28 (711)	3 (76)	0	0
2	1/4 (6)	¹ / ₄ (6)	0	0	0	0	0	0
12	½ (13)	0	1/2 (13)	0	0	0	0	0
13	³ / ₄ (19)	0	21/4 (57)	³ / ₄ (19)	27 (686)	3 (76)	0	0
14	0	0	1¾ (44)	2 (51)	17 (432)	2 (51)	13 (330)	4 (102)
15	0	0	0	0	0	0	42 (1,067)	3 (76)
16	0	0	0	0	24 (610)	3 (76)	0	0
17	0	0	4 (102)	0	20 (508)	4 (102)	0	0
18	0	0	11/4 (32)	2½ (64)	18 (457)	4 (102)	0	0
19	0	0	1/4 (6)	1/4 (6)	0	0	0	0
29	0	¹ / ₄ (6)	0	0	0	0	0	0

¹ If a post is omitted in the table, there were no soil disturbances at that post location

5.6 Vehicle Damage

The damage to the vehicle was minimal, as shown in Figures 47 and 48. The maximum occupant compartment deformations are listed in Table 6 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix D.

Table 6. Maximum Occupant Compartment Deformations by Location

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	1/2 (13)	≤9 (229)
Floor Pan & Transmission Tunnel	1/2 (13)	≤ 12 (305)
Side Front Panel (in Front of A-Pillar)	³ ⁄ ₄ (19)	≤ 12 (305)
Side Door (Above Seat)	3/4 (19)	≤9 (229)
Side Door (Below Seat)	1 (25)	≤ 12 (305)
Roof	0	≤4 (102)
Windshield	0	≤3 (76)

The majority of the damage was concentrated on the right-front corner and right side of the vehicle where the impact occurred. The front bumper was bent on the right lower side approximately 8 in. (203 mm) from the centerline of the vehicle. There was also a kink on the top of the front bumper approximately 19 in. (483 mm) from the centerline of the vehicle. There were contact marks on the right side of the front bumper cover. The front bumper cover also had a 5-in. (127-mm) tear along the right quarter panel. The grill of the vehicle was deformed backward 2½ in. (64 mm) on the bottom right side. The right quarter panel was folded inward 7 in. (178 mm). The right headlight fractured, and the right-front tire detached from the vehicle at the wheel bearing. The right-front upper control arm and disc brake assembly detached. Contact marks extended the entire length of the right side of the vehicle. Both of the doors on the right side were slightly ajar. The top of the right-front door separated 1 in. (25 mm) from the cab of the vehicle, while the bottom of the right rear door separated \(^3\)/4 in. (19 mm) from the cab. The right-front door also had flattening that extended the entire length of the door 17 in. (432 mm) up from the bottom of the door. The right-rear door had contact marks that extended the length of the door. Flattening occurred at the bottom of the door and at the rear corner of the cab. The right

side of the rear bumper was flattened and had a kink 12 in. (305 mm) from the right fender. The right-rear taillight separated approximately 2½ in. (64) mm from the fender. A 35 in. (889 mm) long crack was found down the center of the windshield.

5.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec average occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 7. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 7.

The results of the occupant risk analysis, as determined from the accelerometer data, are summarized in Figure 32. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix E.

Table 7. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MGSSYP-1

Evaluation Criteria		Tran	sducer	MASH
		EDR-3	DTS	Limits
OIV	Longitudinal	-14.20 (-4.33)	-13.25 (-4.04)	≤ 40 (12.2)
ft/s (m/s)	Lateral	-14.77 (-4.50)	-14.74 (-4.50)	≤40 (12.2)
ORA	Longitudinal	8.39 -7.56	-8.14	≤ 20.49
g's	Lateral	-7.65	-8.51	≤ 20.49
	THIV s (m/s)	NA	19.82 (6.04)	not required
PHD g's		NA	11.36	not required
ASI ¹		0.70	0.70	not required

¹ASI procedures based on MASH Appendix F

5.8 Discussion

The analysis of the test results for test no. MGSSYP-1 showed that the system adequately contained and redirected the 2270P vehicle with controlled lateral displacements of the barrier. There were no detached elements nor fragments which showed potential for penetrating the occupant compartment nor presented undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix E, were deemed acceptable because they did not adversely influence occupant risk safety criteria nor cause rollover. After impact, the vehicle exited the barrier at an angle of 15.7 degrees. Therefore, test no. MGSSYP-1 was determined to be acceptable according to the MASH safety performance criteria for test designation no. 3-11.

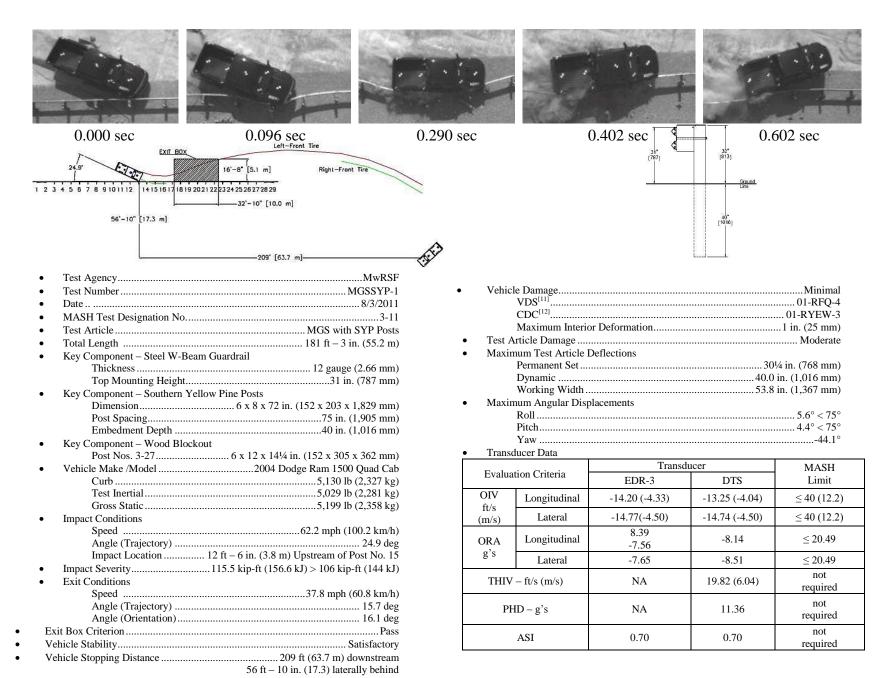


Figure 32. Summary of Test Results and Sequential Photographs, Test No. MGSSYP-1

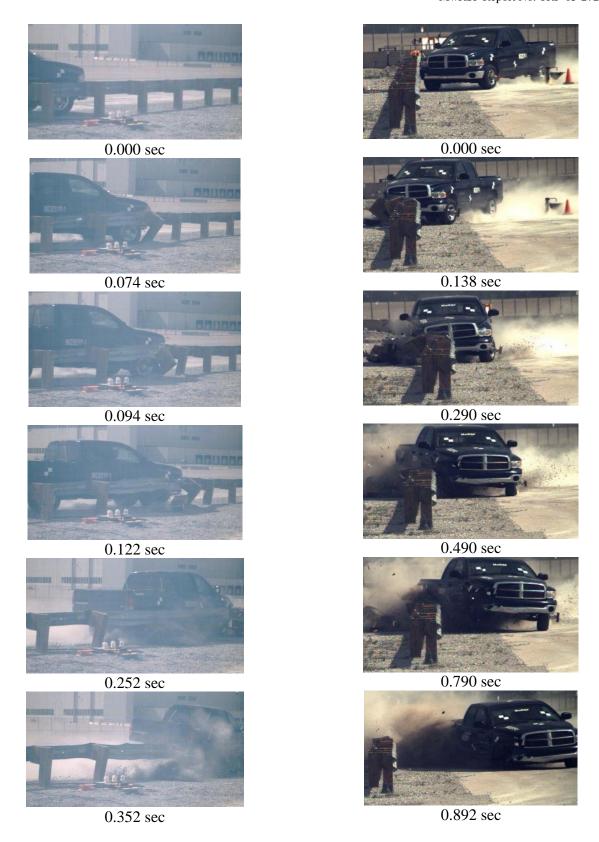


Figure 33. Additional Sequential Photographs, Test No. MGSSYP-1



Figure 34. Additional Sequential Photographs, Test No. MGSSYP-1







Figure 35. Impact Location, Test No. MGSSYP-1





Figure 36. Vehicle Final Position and Trajectory Marks, Test No. MGSSYP-1









Figure 37. System Damage, Test No. MGSSYP-1

Figure 38. Rail Damage Between Post Nos. 13 and 18, Test No. MGSSYP-1

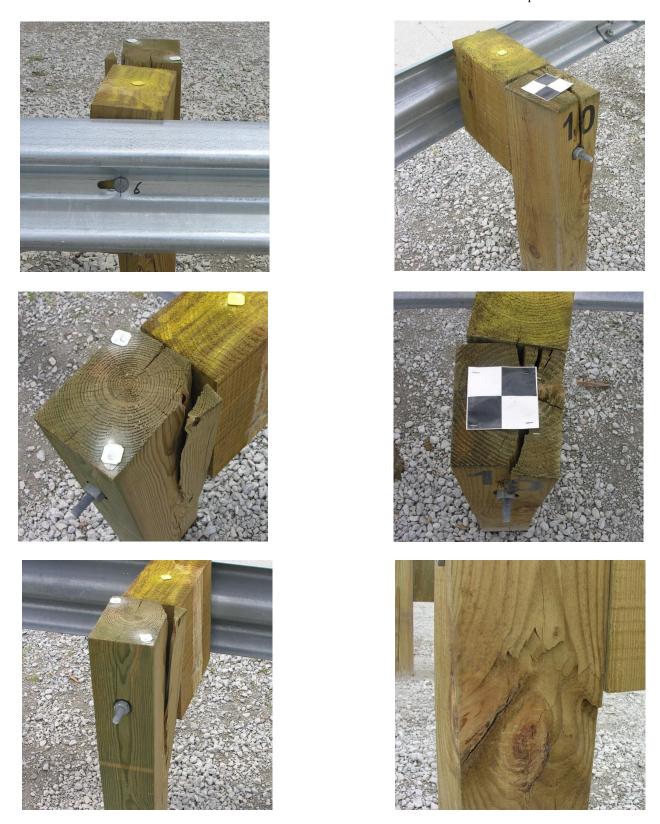


Figure 39. Post Nos. 6 and 10 Damage, Test No. MGSSYP-1

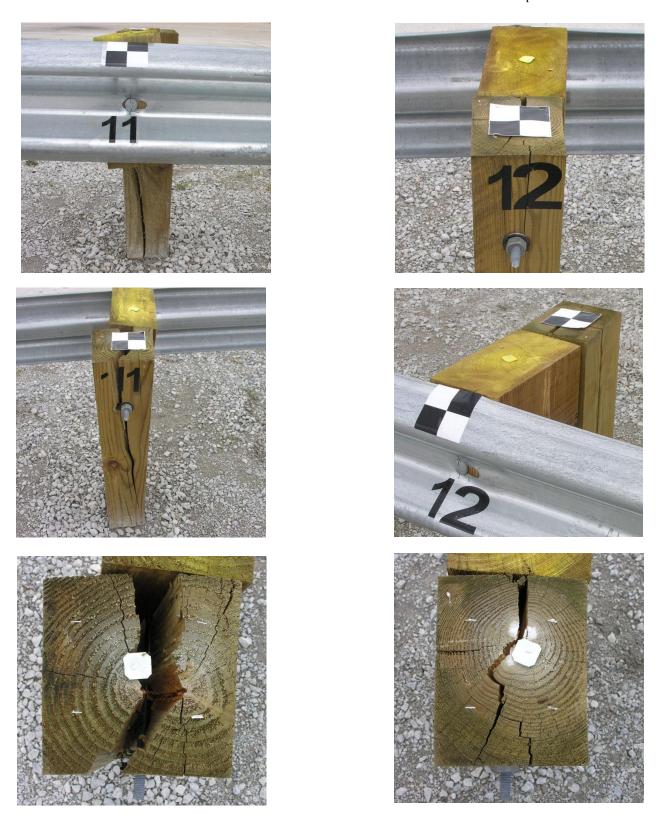


Figure 40. Post Nos. 11 and 12 Damage, Test No. MGSSYP-1.

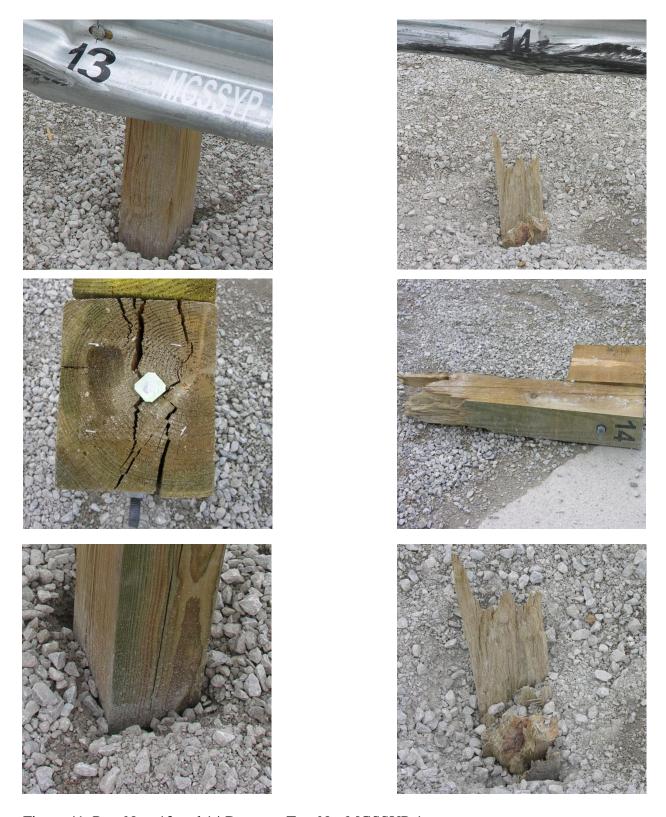


Figure 41. Post Nos. 13 and 14 Damage, Test No. MGSSYP-1



Figure 42. Post Nos. 15 and 16 Damage, Test No. MGSSYP-1

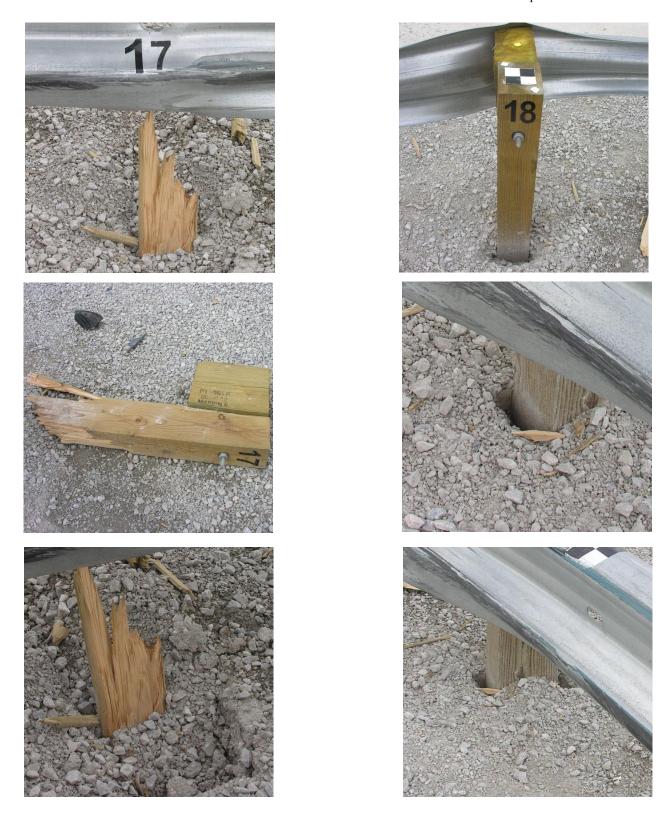


Figure 43. Post Nos. 17 and 18 Damage, Test No. MGSSYP-1







Figure 44. Local Rail Tearing at Post Nos. 3, 7, and 14, Test No. MGSSYP-1

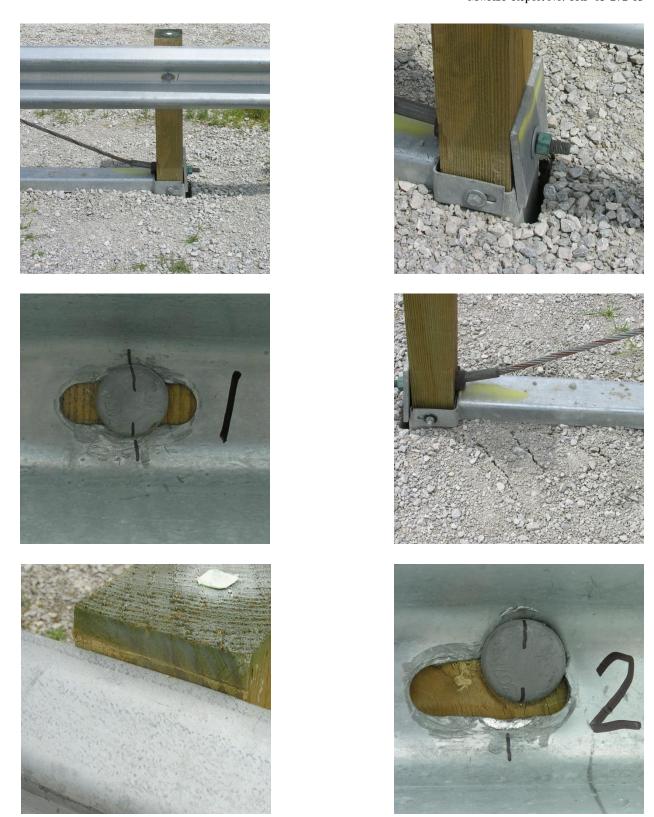


Figure 45. Upstream Anchor Damage, Test No. MGSSYP-1

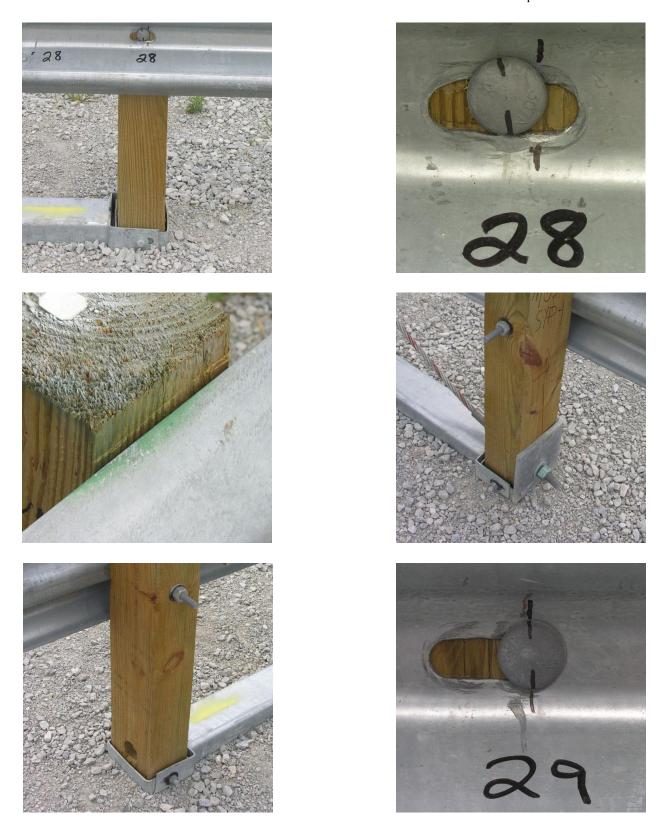


Figure 46. Downstream Anchor Damage, Test No. MGSSYP-1

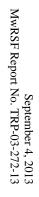










Figure 47. Vehicle Damage, Test No. MGSSYP-1









Figure 48. Vehicle Damage, Test No. MGSSYP-1

6 FULL-SCALE CRASH TEST NO. MGSSYP-2

6.1 Static Soil Test

Before full-scale crash test no. MGSSYP-2 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The post-soil resistance was measured at deflections of 5 in., 10 in., and 15 in. (127 mm, 254 mm, and 381 mm) using load cells during a static test, as shown in Table 8. The complete force versus deflection curves for the static post test are shown in Appendix C.

Table 8. Soil Resistance

Displacement		•	Minimum Load	
in. [mm]	Load Cell #1	(90% Base lb [kg] (90% Base lb [kg] 134.8] 7,899 [35.1] 5,547 [24] 35.1] 8,013 [35.6] 6,650 [29]	lb [kg]	
5 [127]	7,814 [34.8]	7,899 [35.1]	5,547 [24.7]	
10 [254]	7,899 [35.1]	8,013 [35.6]	6,650 [29.6]	
15 [381]	6,852 [30.5]	6,845 [30.4]	6,973 [31.0]	

At 5 in. (127 mm) of deflection, the static post-soil resistance was approximately 41 percent higher than the baseline minimum. As the post rotated through the 10 in. (254 mm) was approximately 19 percent greater than the baseline minimum. At 15 in. (381 mm) of deflection, the post-soil resistance was less than 2 percent lower than the baseline minimum value. However, it should be noted that the static baseline capacity was excessively high, as shown in Figure C-2, and it corresponded to a soil strength with significant dynamic post-soil resistance, ranging between 10,000 lb (44.5 kN) and 11,000 lb (48.9 kN). As such, the test day dynamic soil strength would have easily surpassed the 7,500-lb (33.4-kN) limit. Therefore, the soil was determined to provide adequate strength for embedded wood guardrail posts, and full-scale crash testing was then conducted on the barrier system.

6.2 Test No. MGSSYP-2

The 2,612-lb (1,185-kg) small car impacted the MGS with SYP wood posts at a speed of 61.5 mph (99.0 km/h) and at an angle of 25.3 degrees. A summary of the test results and sequential photographs are shown in Figure 49. Additional sequential photographs are shown in Figures 50 and 51.

6.3 Weather Conditions

Test no. MGSSYP-2 was conducted on September 13, 2011 at approximately 4:30 pm. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported and are shown in Table 9 [9].

Table 9. Weather Conditions, Test No. MGSSYP-2

Temperature	70° F
Humidity	53 %
Wind Speed	10 mph
Wind Direction	10° from True North
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0.00 in.
Previous 7-Day Precipitation	0.00 in.

6.4 Test Description

Initial vehicle impact was to occur 8 ft - 7 in. (2.6 m) upstream of the center line of post no. 15, as shown in Figure 52, which was selected using the CIP plots found in Section 2.3 of MASH to maximize pocketing and the propensity of wheel snag. The actual point of impact was 8 ft - 4 in. (2.5 m) upstream of post no. 15. A sequential description of the impact events is contained in Table 10. The vehicle came to a rest 168 ft - 2 in. (51.3 m) downstream of the impact location and 17 ft - 11 in. (5.5 m) laterally in front of the barrier system, and its trajectory

did not violate the bounds of the exit box. The vehicle trajectory and final position are shown in Figure 53.

Table 10. Sequential Description of Impact Events, Test No. MGSSYP-2

TIME (sec)	EVENT
0.000	The right-front corner of vehicle impacted rail 8 ft – 4 in. (2.5 m) upstream of post no. 15.
0.008	The hood of vehicle separated and began to override rail.
0.030	Post nos. 14 and 15 rotated backward.
0.062	The rail penetrated front of vehicle to center point.
0.082	The blockout of post no. 15 twisted.
0.084	The vehicle impacted post no. 15.
0.088	The front bumper of vehicle started detaching.
0.090	Post no. 16 rotated backward.
0.096	The right-front door became ajar.
0.112	The rail detached from post no. 15.
0.120	The surrogate occupant's head impacted right-front window and shattered it.
0.136	Post no. 15 fractured near groundline.
0.150	The right side of front bumper detached from vehicle.
0.164	Post no. 15 became airborne, and vehicle impacted blockout of post no. 16, causing it to twist.
0.166	The vehicle impacted post no. 16.
0.186	The maximum deflection of system occurred.
0.194	The right-front tire impacted post no. 16, causing it to split vertically and fracture near groundline.
0.222	The blockout of post no. 16 detached from post no. 16
0.258	The detached portion of front bumper impacted ground.
0.260	The vehicle was parallel with system at a speed of 41.2 mph (66.3 km/h).
0.262	The vehicle impacted blockout of post no. 17.
0.280	The vehicle redirected away from system.
0.290	The right-front tire impacted post no. 17.
0.320	Post no. 17 rotated slightly back toward traffic.
0.370	The front of vehicle lost contact with rail.
0.484	The vehicle exited system at a speed of 35.7 mph (57.4 km/h) and at an angle of 13.6 degrees.

6.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 54 through 56. Barrier damage consisted of deformed guardrail, rotated and fractured posts, and contact marks on the guardrail and posts. The length of vehicle contact along the barrier was approximately 23 ft – 1 in. (7.0 m) which spanned from 2 ft – $6\frac{1}{2}$ in. (775 mm) upstream of post no. 14 to 1 ft – $9\frac{1}{2}$ in. (546 mm) downstream of post no. 17.

The guardrail bolt pulled through the rail at post nos. 15 through 17. A 1-in. (25-mm) tear was found in the bolt slot of the rail at post no. 15. The rail kinked at the downstream edge of post no. 13. The rail kinked at the top of the rail at the midspan between post nos. 13 and 14. The rail buckled at the downstream edge of the blockout at post no. 14. Flattening occurred from post no. 14 and extended to the splice downstream from post no. 16. The rail buckled at post no. 17 and kinked at post no. 18.

Post no. 15 fractured at the groundline and splintered on the upstream corner of the front face. Contact marks were found on the front of post no. 15. Post no. 16 fractured at the groundline, and tire gouging was found on the front face of the post. Post no. 17 deflected backwards. The top of post no. 17 split at the nail location, and a 6½-in. (165-mm) gouge was found on the upstream side of the front face. Soil gaps, heaves, and craters can be found in Table 11.

The maximum permanent set of the barrier system measured from the back of the posts was 11 in. (279 mm) at post no. 17, as measured in the field. The maximum permanent set of the rail was 16¼ in. (413 mm) at the midspan between post nos. 15 and 16, as measured in the field. The maximum lateral dynamic barrier deflection was 22.2 in. (564 mm) at the midspan between post nos. 15 and 16, as determined from high-speed digital video analysis. The working width of

the system was found to be 39.7 in. (1,008 mm), also determined from high-speed digital video analysis.

Table 11. Soil Gap, Soil Heave, Soil Crater Measurements, Test No. MGSSYP-2

	S	oil Gap Location in. (mm)	Soil Hoin. (n	,		Soil Crater, in. (mm)		
Post No.	Upstream	Downstream	Front	Back	Diameter	Height	Diameter	Depth
13	0	0	1/2 (13)	0	0	0	0	0
14	0	0	2½ (64)	1 (25)	13 (330)	3 (76)	0	0
15	0	0	2 (51)	0	0	0	20 (508)	3½ (89)
16	0	0	0	0	22 (559)	2 (51)	19 (483)	3 (76)
17	1½ (38)	0	4 (102)	0	22 (559)	4 (102)	0	0
18	0	0	³ / ₄ (19)	0	0	0	0	0
29	0	1/2 (13)	0	0	0	0	0	0

¹ If a post is omitted in the table, there were no soil disturbances at that post location

6.6 Vehicle Damage

The damage to the vehicle was moderate, as shown in Figures 61 and 62. The maximum occupant compartment deformations are listed in Table 12 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix D.

Table 12. Maximum Occupant Compartment Deformations by Location

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	1/2 (13)	≤9 (229)
Floor Pan & Transmission Tunnel	1/4 (6)	≤ 12 (305)
Side Front Panel (in Front of A-Pillar)	³ / ₄ (19)	≤ 12 (305)
Side Door (Above Seat)	1 1/4 (32)	≤9 (229)
Side Door (Below Seat)	1/4 (6)	≤ 12 (305)
Roof	0	≤ 4 (102)
Windshield	0	≤ 3 (76)

The majority of the damage was concentrated on the right-front corner and right side of the vehicle where the impact occurred. The right-front of the vehicle was folded under. The right-front quarter panel crushed inward 13 in. (330 mm) and into the shock absorber. Contact marks and gouging were found on the right-front fender. The right-front wheel dented and crushed severely. The right-front tire was punctured and deflated. The tie-rod on the right-front side fractured. The right-front control arm bent and disengaged from the vehicle. The door on the right-front of the vehicle was dented, ajar from the vehicle, and crushed inward. The mirror on the right side disengaged from the vehicle. The windshield cracked on the right side from the right A – pillar and extended 21 in. (533 mm) toward the center and the entire height of the windshield. Tears were found along the bottom of the right-front fender behind the wheel well. The bottom of the door frame crushed inward for 1 ft (305 mm) behind the right-front wheel well. The front bumper disengaged from the vehicle and had contact marks and dents on the right side. The radiator fan disengaged from the vehicle, and brake fluid leaked from the front-left of the vehicle. Contact marks extended the entire length of the right side of the vehicle.

6.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 13. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 13.

The results of the occupant risk analysis, as determined from the accelerometer data, are summarized in Figure 49. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix F.

Table 13. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MGSSYP-2

Evaluation Criteria		Transo	MASH		
Evaluat	ion Criteria	EDR-3	DTS	Limits	
OIV	Longitudinal	-17.13 (-5.22)	-15.70 (-4.79)	≤ 40 (12.2)	
ft/s (m/s)	Lateral	-19.52 (-5.95)	-20.92 (-6.38)	≤40 (12.2)	
ORA	Longitudinal	-13.05	-13.34	≤ 20.49	
g's	Lateral	-7.42	-9.30	≤ 20.49	
	HIV s (m/s)	NA	27.92 (8.51)	not required	
PHD g's		NA	14.38	not required	
I	ASI ¹	0.91	0.99	not required	

¹ASI procedures based on MASH Appendix F

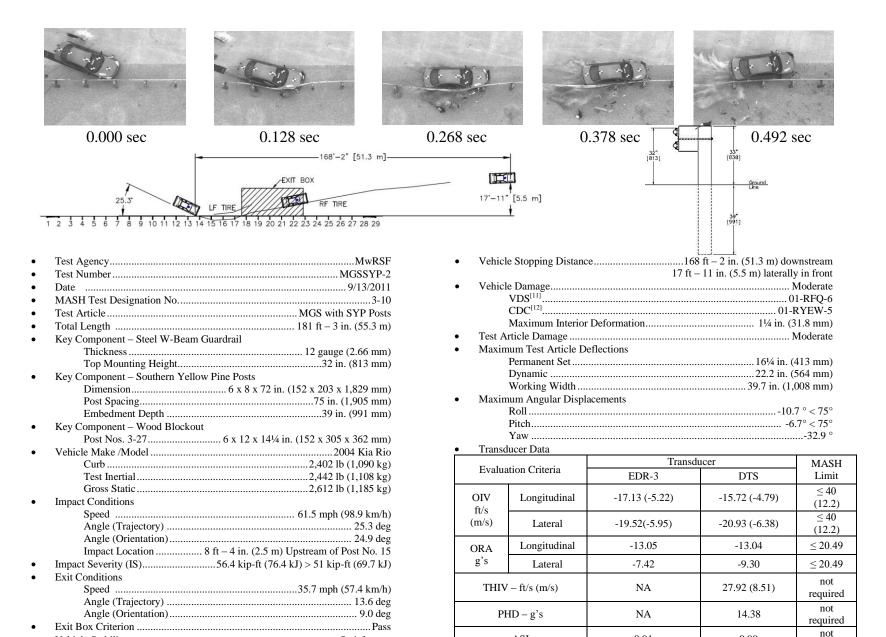
6.8 Discussion

The analysis of the test results for test no. MGSSYP-2 showed that the system adequately contained and redirected the 1100C vehicle with controlled lateral displacements of the barrier. There were no detached elements or fragments which showed potential for penetrating the occupant compartment nor presented undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix F, were deemed acceptable because they did not adversely influence occupant risk safety criteria nor cause rollover. After impact, the vehicle exited the barrier at an angle of 13.6 degrees. Therefore, test no. MGSSYP-2 was determined to be acceptable according to the MASH safety performance criteria for test designation no. 3-10.

required

0.99

0.91



ASI

Figure 49. Summary of Test Results and Sequential Photographs, Test No. MGSSYP-2

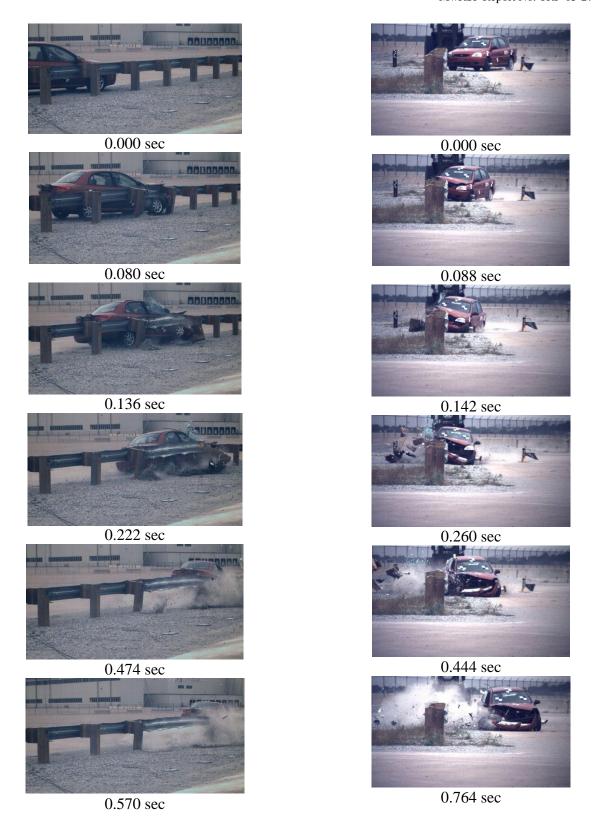


Figure 50. Additional Sequential Photographs, Test No. MGSSYP-2

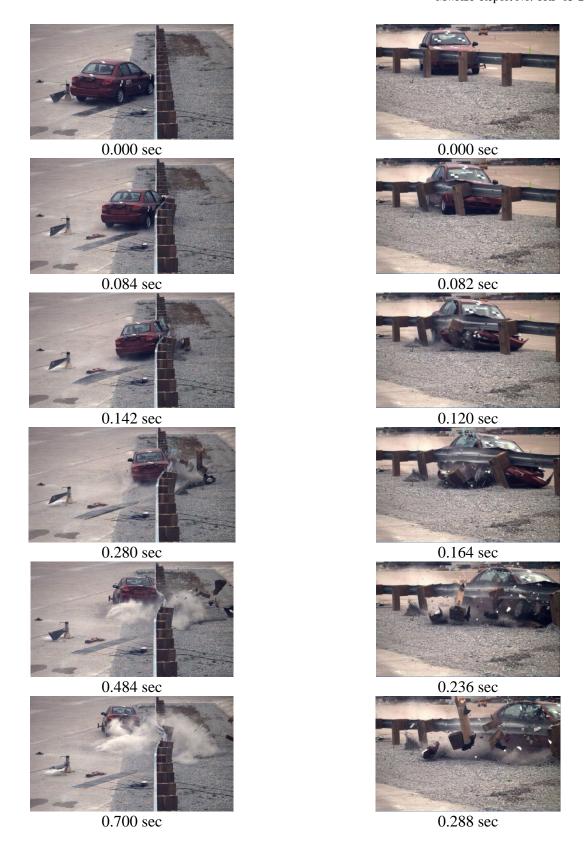


Figure 51. Additional Sequential Photographs, Test No. MGSSYP-2







Figure 52. Impact Location, Test No. MGSSYP-2





Figure 53. Vehicle Final Position and Trajectory Marks, Test No. MGSSYP-2

Figure 54. System Damage, Test No. MGSSYP-2

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Figure 55. Rail Damage Between Post Nos. 13 and 15, Test No. MGSSYP-2



Figure 56. Rail Damage Between Post Nos. 16 and 18, Test No. MGSSYP-2



Figure 57. Post Nos. 13 and 14 Damage, Test No. MGSSYP-2



Figure 58. Post Nos. 15 and 16 Damage, Test No. MGSSYP-2

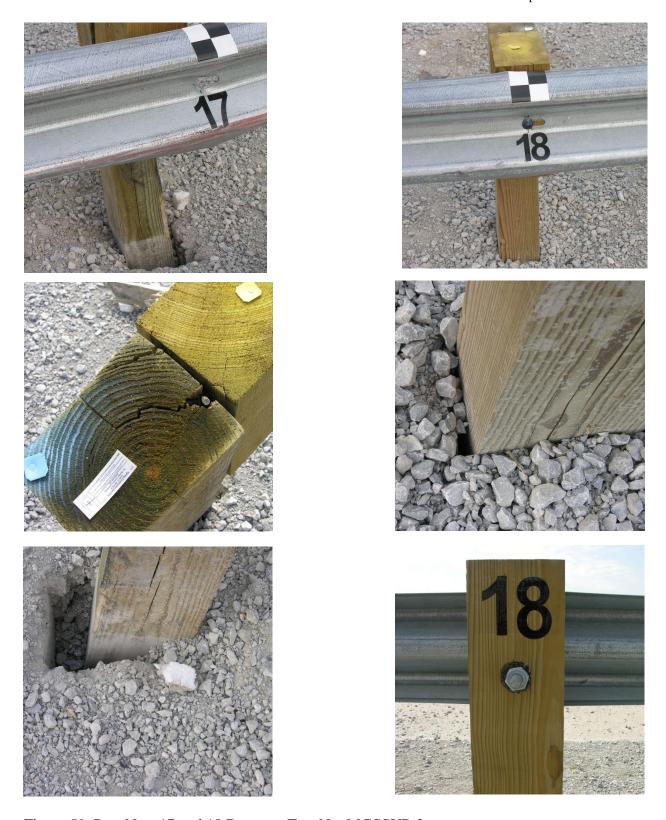


Figure 59. Post Nos. 17 and 18 Damage, Test No. MGSSYP-2

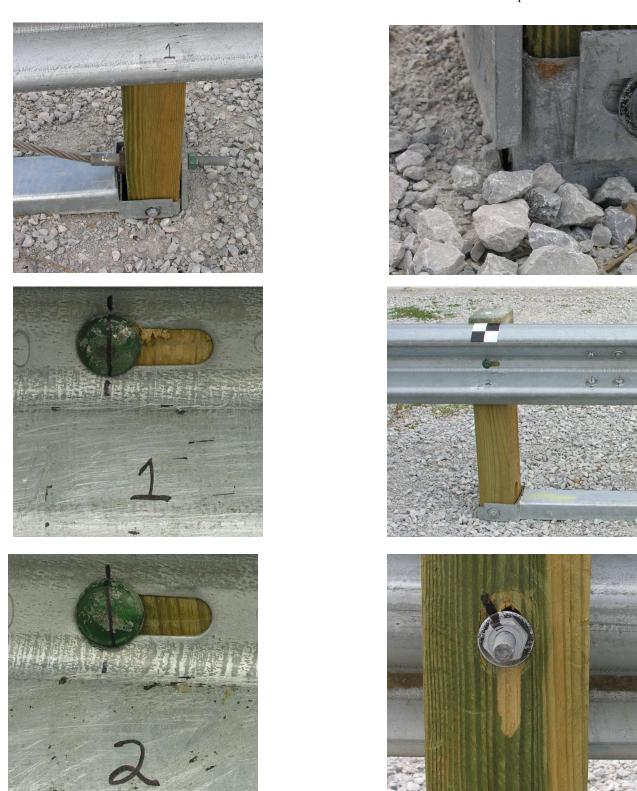


Figure 60. Upstream Anchor Damage, Test No. MGSSYP-2



Figure 61. Vehicle Damage, Test No. MGSSYP-2

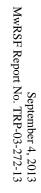










Figure 62. Vehicle Damage, Test No. MGSSYP-2

7 SUMMARY AND CONCLUSIONS

A non-proprietary, Southern Yellow Pine wood post, W-beam guardrail system was developed and crash tested according to MASH. The wood post MGS utilized 6-in. x 8-in. x 72in. (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine posts instead of the standard W6x8.5x72 in. (W152x216x1,829 mm) steel posts. Two full-scale crash tests were performed according to the TL-3 safety performance criteria, as defined in MASH. Test no. MGSSYP-1 (test designation no. 3-11) consisted of a 5,199-lb (2,358-kg) pickup truck impacting the MGS with Southern Yellow Pine posts at a speed of 62.2 mph (100.1 km/h) and at an angle of 24.9 degrees. The vehicle was contained and smoothly redirected. Test no. MGSSYP-2 (test designation no. 3-10) consisted of a 2,612-lb (1,185-kg) small car impacting the wood post MGS at a speed of 61.5 mph (99.0 km/h) and at an angle of 25.3 degrees. The vehicle was contained and smoothly redirected. Thus, the MGS with Southern Yellow Pine posts was judged to be acceptable according to the safety performance criteria presented in MASH. A summary of the safety performance evaluation is provided in Table 14. The successful evaluation of the MGS with Southern Yellow Pine posts as a non-proprietary system may prevent State DOTs that already have an inventory of Southern Yellow Pine posts from having to invest in an inventory of specialized components for use in other systems.

The standard MGS has demonstrated acceptable safety performance when configured with either standard W6x9 (W152x13.4) or W6x8.5 (W152x12.6) steel posts [13-15], round wood posts [3], 6-in. x 8-in. (152-mm x 203-mm) White Pine wood posts [4], and now 6-in. x 8-in. (152-mm x 203-mm) Southern Yellow Pine wood posts. The different configurations have exhibited similar performance, as shown in Table 15. Therefore, the MGS configured with standard-sized, Southern Yellow Pine wood posts is an acceptable alternative to the previously-

recommended, steel post, round wood post, and rectangular White Pine wood post configurations.

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Table 14. Summary of Safety Performance Evaluation Results

Evaluation Factors		Eva		Test No. MGSSYP-1	Test No. MGSSYP-2	
Structural Adequacy	A.	Test article should contain and controlled stop; the vehicle shinstallation although controlled la	erride, or override the	S	S	
	D.	Detached elements, fragments of penetrate or show potential for an undue hazard to other traff Deformations of, or intrusions in limits set forth in Section 5.3 and	compartment, or present onnel in a work zone.	S	S	
	F.	The vehicle should remain uprig and pitch angles are not to exceed	S	S		
Occupant	H.	Occupant Impact Velocity (OIV calculation procedure) should sat				
Risk		Occupa	S	S		
		Component	Preferred	Maximum		
		Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)		
	I.	The Occupant Ridedown Accele MASH for calculation procedure				
		Occupant F	nits	S	S	
		Component	Preferred	Maximum		
		Longitudinal and Lateral	15.0 g's	20.49 g's		
		3-11	3-10			
		Pass	Pass			

S – Satisfactory U – Unsatisfactory NA - Not Applicable

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Table 15. Comparison of MGS with Steel and Wood Post

							M	GS					
Performance Criteria		71/4-in. Diameter Douglas Fir Posts		8-in. Diameter Ponderosa Pine Posts		W6x9 Steel Posts		W6x9 Steel Posts		6-in. x 8-in. White Pine Posts		6-in. x 8-in. Southern Yellow Pine Posts	
Те	est Criteria	NCHR	P 350	NCHR	P 350	NCHRP 350		MASH		MASH		MASH	
Test D	esignation No.	3-11	3-10	3-11	3-10	3-11	3-10	3-11	3-10	3-11	3-10	3-11	3-10
Te	est Vehicle	2000P [3]	820C ¹	2000P [3]	820C ¹	2000P [13]	820C [13]	2270P [14]	1100C [15]	2270P [4]	1100C ¹	2270P	1100C
_	eact Severity cip-ft (kJ)	106.4 (144.3)	-	107.2 (145.3)	-	101.5 (137.7)	31.2 (42.3)	122.3 (165.8)	58.8 (79.7)	131.5 (178.3)	-	115.5 (156.6)	56.4 (76.4)
D	rmanent Set eflections in. (mm)	35.5 (902)	-	27.8 (705)	-	26.0 (652)	9.4 (238)	315/8 (803)	19.9 (505)	33¾ (857) - 30¼ (768)		16 ¹ / ₄ (413)	
_	nic Deflections in. (mm)	60.2 (1,529)	-	37.6 (956)	-	43.1 (1,094)	17.4 (443)	43.9 (1,115)	35.9 (913)	46.3 (1,176)	-	40.0 (1,016)	22.2 (564)
	rking Width in. (mm)	60.3 (1,531)	-	48.6 (1,234)	-	49.6 (1,260)	40.3 (1,023)	48.6 (1,234)	48.3 (1,227)	58.4 (1,483)	-	53.8 (1,367)	39.7 (1,008)
OIV ft/s	Longitudinal	13.22 (4.03)	-	22.47 (6.85)	-	18.32 (5.58)	11.55 (3.52)	15.32 (4.67)	14.83 (4.52)	-15.27 (-4.65)	-	-13.25 (-4.04)	-15.72 (-4.79)
(m/s)	Lateral	13.22 (4.03)	-	23.56 (7.18)	-	12.87 (3.89)	18.64 (5.68)	15.62 (4.76)	17.13 (5.22)	-16.14 (-4.92)	ı	-14.74 (-4.50)	-20.93 (-6.38)
ORA	Longitudinal	8.76	-	5.90	-	9.50	6.13	8.23	16.14	-8.25	-	-8.14	-13.04
g's	Lateral	5.69	-	4.09	-	6.94	7.97	6.93	8.37	-10.13	-	-8.51	-9.30

This test was not conducted.

8 IMPLEMENTATION GUIDANCE

8.1 Background

As previously noted, the research detailed herein demonstrated that the MGS utilizing 6-in. x 8-in. x 72-in. (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine posts, performed in an acceptable manner according to test designation nos. 3-10 and 3-11 of the MASH impact safety standards. However, several variations of the MGS system have been developed for special applications, which may be more sensitive to the use of wood posts. These special applications would include the MGS long-span system, MGS adjacent to 2:1 fill slopes, MGS on 8:1 approach slopes, MGS adjacent to a curb, MGS stiffness transition to approach guardrail transitions, MGS with reduced post spacing, and MGS without blockouts. Since several MGS variations are available, recommendations regarding the use SYP wood posts will likely vary depending on the nature and behavior of the special applications listed above. Implementation guidance and/or recommendations regarding the use SYP wood posts in these special applications are discussed below.

8.2 MGS Long-Span Guardrail

The MGS long-span guardrail system was successfully full-scale crash tested using an unsupported length of 25 ft (7.62 m) and three CRT posts with 12-in. (305-mm) deep blockouts adjacent to each end of the unsupported span [16]. These CRT posts were incorporated into the system in order to mitigate concerns for wheel snag on posts adjacent to the unsupported span when traversing from the unsupported span to the downstream standard guardrail. Adjacent to the CRT posts, the standard MGS utilized 12-in. (305-mm) deep blockouts. The MGS long-span guardrail system was installed with the back of the CRT posts positioned flush with the front face of the culvert headwall. The posts upstream and downstream from the culvert were installed 2 ft (610 mm) away from the slope break point of a 3:1 fill slope.

Occasionally, it may be desirable to attach a SYP wood post version of the MGS to the MGS long-span guardrail system. There are no concerns regarding the use of SYP wood posts in the MGS long-span guardrail system. The SYP wood-post version of the MGS performed in an acceptable manner when using the standard post spacing on level terrain and full-scale crash tested under the MASH TL-3 safety performance criteria using both the 1100C and 2270P vehicles. The maximum dynamic deflections of the MGS with W6x8.5 (W152x12.6) steel posts and SYP wood posts under MASH designation no. 3-11 were found to be 43.9 in. (1,115 mm) and 40.0 in. (1,016 mm), respectively. These results indicate that the relative deflection and stiffness of the wood and steel post versions of the MGS are very similar. As such, the SYP wood post version of the MGS system would not be expected to significantly alter the safety performance of the MGS long-span guardrail system when attached to guardrail beyond the upstream and downstream CRT wood posts. Therefore, it would seem reasonable to allow for the SYP wood post MGS to be attached to the MGS long-span guardrail system, as shown in Figure 63.

8.3 MGS Adjacent to 2:1 Fill Slopes

Previously, the 31-in. (787-mm) tall Midwest Guardrail System with 9-ft (2.74-m) long W6x8.5 (W152x12.6) steel posts was successfully crash tested under the MASH TL-3 criteria when installed at the slope break point of a 2:1 fill slope using standard post spacing and blockouts [17]. However, similar crash testing was not successful for the minimum recommended MGS mounting height of 27¾ in. (705 mm). As such, the minimum recommended top mounting height is unknown for the MGS adjacent to 2:1 fill slopes. Later and based on dynamic component testing, a wood post version of the MGS system was configured with 7.5-ft (2,286-mm) long, SYP posts and for use in shielding a 2:1 fill slope, as shown in Figure 64. For the SYP wood post variation, the embedment depth was 58 in. (1,473 mm). Based on this

previous research, it is highly recommended that the MGS with 7.5-ft (2,286-mm) long SYP wood posts adjacent to 2:1 fill slopes utilize a minimum top mounting height of 31 in. (787 mm).

8.4 MGS on 8:1 Approach Slopes

Previously, full-scale crash testing was successfully performed on the steel-post version of the MGS installed on an 8:1 approach slope with the W-beam positioned 5 ft (1.52 m) laterally behind the slope break point [18]. This testing program was conducted according to the NCHRP Report No. 350 impact safety standards using both an 820C small car and a 2000P pickup truck. From the crash testing program, the mounting height of the blocked MGS relative to the airborne trajectory of the front bumper and impact-side wheels was deemed critical for satisfactorily containing the 2000P pickup truck. Arguably, the test results may have also demonstrated that the 31-in. (787-mm) top railing height greatly contributed to adequate vehicle containment and stable redirection.

Based on the similar performance of the steel and wood post versions of the MGS system when tested on level terrain, there is little concern that the use of SYP wood posts would adversely affect the performance of the MGS on 8:1 approach slopes. Therefore, it is believed to be acceptable to install SYP wood posts with the MGS on an 8:1 approach slope using the previously-evaluated offset values, as shown in Figure 65.

8.5 MGS Adjacent to Curb

The steel post MGS was successfully crash tested and evaluated with the front face of the W-beam rail placed 6 in. (152 mm) behind the front face of a 6-in. (152-mm) tall concrete curb according to the NCHRP Report No. 350 TL-3 criteria using a 2000P pickup truck [19]. Based on the similar performance of the steel and wood post versions of the MGS system when tested on level terrain, there is little concern that the use of SYP wood posts would adversely affect the performance of the MGS installed adjacent to a curb. Therefore, it is believed to be acceptable to

install a SYP wood post MGS with the front face of the W-beam rail placed 6 in. (152 mm) behind the front face of a 6-in. (152-mm) tall concrete curb, as shown in Figure 66.

8.6 MGS Stiffness Transition to Approach Guardrail Transitions

Several options for approach guardrail transitions for the MGS system have been developed. As part of those efforts, a research project was conducted with the objective of identifying a wood-post MGS approach transition system that was equivalent to a previouslydesigned and full-scale crash tested steel-post MGS stiffness transition that utilized W6x9 and W6x15 steel posts [10]. A literature study on previous bogie testing and comparisons between wood and steel guardrail posts suggested that 6-ft (1.8-m) long, 6-in. x 8-in. (152-mm x 203mm) wood posts and W6x9 (W152x13.4) steel posts have similar force versus displacement characteristics. However, very little component testing had been previously conducted on larger transition posts. Thus, a bogie testing program was undertaken to determine the behavior of W6x15 (W152x22.3) steel posts and wood posts of various cross sections and embedment depths. Early in this bogie-testing program, the propensity for wood-post fracture in stiff soil was observed. As a result, the wood-post replacements were conservatively selected such that the cross section had excess strength capacity to minimize the risk of post fracture. Ultimately, 6.5 ft (2.0 m) long 8-in. x 10-in. (203-mm x 254-mm) wood posts provided similar resistance to rotation and were selected as the replacement for the 7-ft (2.1-m) long W6x15 (W152x22.3) steel transition posts.

The steel-post MGS stiffness transition was found to satisfy all of the TL-3 safety performance criteria of MASH through a full-scale crash testing program. Since BARRIER VII analysis showed the proposed wood-post transition system behaved similarly and without increases in deflections, pocketing, or snag, it was believed that the wood-post transition system would also satisfy the TL-3 performance criteria of MASH. Therefore, the wood-post MGS

stiffness transition was recommended for use as a TL-3 safety barrier. Full details on the wood post approach transition and recommendations for its use can be found in MwRSF research report no. TRP-03-243-11. In addition, it is believed that the use of the MGS with SYP wood posts in standard MGS guardrail upstream of the approach guardrail transition would be acceptable as well.

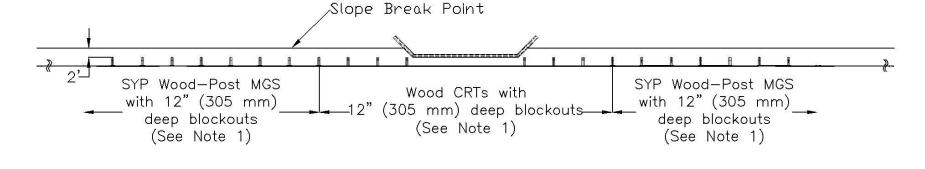
8.7 MGS with Reduced Post Spacing

A steel-post version of the MGS with quarter-post spacing was successfully full-scale crash tested and evaluated using a 2000P pickup truck according to the TL-3 criteria found in NCHRP Report No. 350 [19]. Subsequent analysis of the barrier system with BARRIER VII was used to develop details for a half-post spacing version of the MGS as well. As noted previously, the performance of the steel and wood post versions of the MGS system were found to be very similar in terms of stiffness and dynamic deflection. Thus, it is reasonable to assume that a SYP wood post MGS with reduced post spacing would provide similar performance to the previously evaluated steel post system.

8.8 MGS without Blockouts

Over the years, MwRSF has crash tested several wood-post MGS systems with blockouts, including the rectangular, SYP wood posts evaluation detailed herein. These wood-post MGS systems provided acceptable safety performance without concerns for vehicular instabilities, excessive occupant ridedown decelerations, or critical occupant impact velocities. Based on the similar performance observed for the wood- and steel-post MGS systems with blockouts, there may be a desire for end users to install a non-blocked, wood post MGS. Unfortunately, no crash tests have been performed on non-blocked versions of the wood-post MGS.

Wood and steel guardrail posts can provide slightly different behaviors when loaded through the W-beam rail and about the strong and weak axis of bending. Typical steel guardrail posts may rotate in soil, bend about one of the strong and weak axes near the ground line, or plastically deform from a combination of eccentric loading and/or lateral torsional buckling. Typical wood posts may also rotate in soil or fracture near the ground line. Based on these slight differences in post-soil behavior, there are some concerns that the removal of the blockout from the wood-post MGS may potentially lead to: (1) increased propensity for wheel snag on wood posts; (2) increased vehicle decelerations; and/or (3) greater risk of vehicular instabilities upon redirection. Thus, these outcomes could potentially result in degraded barrier performance. As such, it is not recommended to remove the blockouts from the wood-post MGS without further analysis and crash testing.

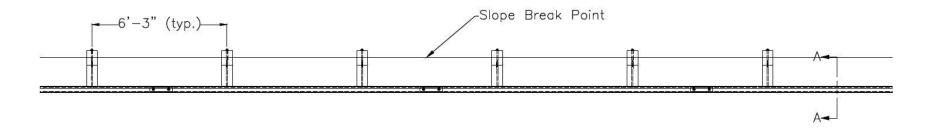


Note: (1) Back of post must be installed on level or mostly level soil grading 2 ft (0.6 m) away from the slope break point of a 3:1 or steeper fill slope. The back of the CRT posts can be flush with the headwall. The headwall cannot extend higher than 2 in. (51mm) above the ground line. The wingwall must match the fill slope.

Figure 63. MGS Long-Span System with SYP Wood Post MGS

101





PLAN VIEW

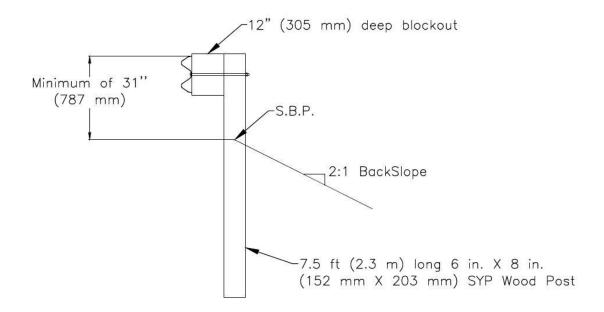


Figure 64. SYP Wood Post MGS Adjacent to 2:1 Fill-Slope

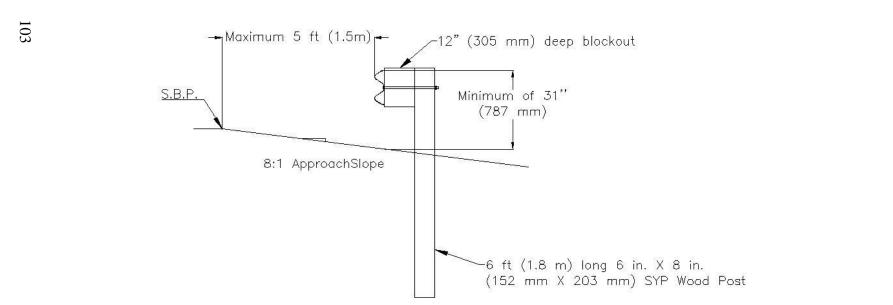


Figure 65. Use of SYP Wood Post MGS on 8:1 Approach Slope

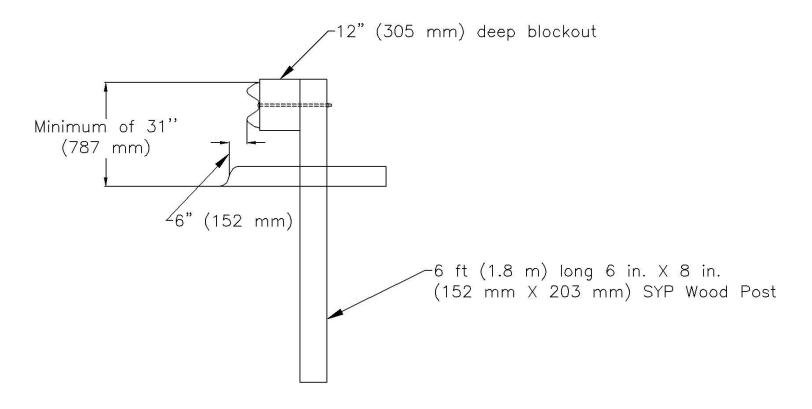


Figure 66. SYP Wood Post MGS Adjacent to Curb Cross-Section

9 REFERENCES

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10 APPENDICES

Appendix A. Material Specifications

MGSSYP-1		
Description	Material Specification	Reference
6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	White Tag
6"x12"x14 1/4" [152x305x362] Blockout	SYP Grade No.1 or better	Yellow Tag
12'-6" [3810] W-Beam MGS Section	12 gauge [2.7] AASHTO M180	4614
12'-6" [3810] W-Beam MGS End Section	12 gauge [2.7] AASHTO M180	4614
6'-3" [1905] W-Beam MGS Section	12 gauge [2.7] AASHTO M180	10-0142-5
16D Double Head Nail	-	N/A
72" [1829] Long Foundation Tube	ASTM A500 Gr. B	090458-7
BCT Timber Post-MGS Height	SYP Grade No.1 or better	10-0282
Strut and Yoke Assembly	ASTM A36 Steel Galvanized	090453-8
BCT Cable Anchor Assembly	Ø 3/4" 6x19 IWRC IPS Galvanized Wire Rope	Black Paint "A1"
Anchor Bracket Assembly	ASTM A36 Steel	090453-10
8"x8"x5/8" [203x203x16] Anchor Cable Bearing Plate	ASTM A36 Steel	090453-9
2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	90458
5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	100144-1,3
5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	Black Paint
5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	Black Paint
5/8" Dia. x 1 1/2" [M16x38] Long Hex Head Bolt	ASTM A307 Steel/ Nut ASTM A563 DH	11-0006-3
5/8" Dia. x 9 1/2" [M16x241] Long Hex Head Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	090453-11
5/8" [16] Dia. Flat Washer	ASTM A307 Steel	N/A
7/8" Dia. x 7 1/2" [M22x191] Long Hex Head Bolt and Nut	ASTM A307 Steel / Nut ASTM A563 DH	N/A
7/8" [22] Dia. Flat Washer	ASTM A307 Steel	N/A

Figure A-1. Bill of Materials, Test No. MGSSYP-1

MGSSYP-2		
Description	Material Specification	Reference
6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	(TAGGED SPA BLUE PAINT) / (TAGGED WHITE PAINT)
6"x12"x14 1/4" [152x305x362] MGS Timber Blockout	SYP Grade No.1 or better	TAGGED GLOSS SUN YELLOW PAINT
12'-6" [3810] 4-Space W-Beam Guardrail	12 gauge [2.7] AASHTO M180	4614
12'-6" [3810] BCT Terminal Rail Section	12 gauge [2.7] AASHTO M180	4614 AND 3390
6'-3" [1905] W-Beam Spacer Guardrail	12 gauge [2.7] AASHTO M180	10-0142-5
16D Double Head Nail	-	SCAN 16d-1
72" [1829] Long Foundation Tube	ASTM A500 Gr. B	090453-7 AND 09-0458
BCT Timber Post—MGS Height	SYP Grade No.1 or better	TAGGED WHITE PAINT
Strut and Yoke Assembly	ASTM A36 Steel Galvanized	09-0453-8
BCT Cable Anchor Assembly	ø 3/4"6x19 IWRC IPS Galvanized Wire Rope	STAMPED "A1" AND BLACK PAINT
Guardrail Anchor Bracket	ASTM A36 Steel	090453-10
8"x8"x5/8" [203x203x16] BCT Bearing Plate	ASTM A36 Steel	090453-9
2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	09-0458
5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	100144-1 (BOLTS)/ 10-0144-3 (NUTS) AND 12-0033 (NUTS)
5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	09-0453-2 (Green Paint) / 12-0033 (NUTS)
5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	10-0143(GLOSS NAVY BLUE PAINT) and 11 0490 (BLACK PAINT)/12-0033 (NUTS)
5/8" Dia. x 1 1/2" [M16x38] Long Hex Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	11-0006-3 (HEX BOLTS)/ 12-0030 (nuts)
5/8" Dia. x 9 1/2" [M16x241] Long Hex Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	BLACK PAINT (bolt)/12-0030 (nut)
5/8" [16] Dia. Plain Round Washer	ASTM A307 or Grade 2 Steel	09-0453-15/ N/A
7/8" Dia. x 7 1/2" [M22x191] Long Hex Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	11——0492 (bolts and nuts)/12— 0037(BOLT) and (NUT)12—0030
7/8" [22] Dia. Plain Round Washer	ASTM A307 or Grade 2 Steel	1JY82/12-0037
SOIL	350 SOIL	6222011

Figure A-2. Bill of Materials, Test No. MGSSYP-2



CERTIFICATE OF COMPLIANCE

JULY 20, 2010

MIDWEST MACHINERY & SUPPLY MILFORD, NE

The following material delivered on 7/20/10 on bill of lading number 20254 has been inspected before and after treatment and is in full compliance with applicable Nebraska Department of Roads requirements for southern yellow pine Timber Guardrail Components, preservative treated with Chromated-Copper-Arsenate (CCA-C) to a minimum retention of .60 lbs/cu.ft. The acceptance of each piece by company quality control is indicated by a hammer brand on the end of each piece.

MAT	ΓERIAL	CHARGE #	DATE	RETENTION	QUANTITY
6x8x6'	Line Post	10-342	7/1/10	0.62	105

This certificate applies to material ordered for your order no.: 2333

FOR ANY INQUIRIES, PLEASE RETAIN THIS DOCUMENT FOR FUTURE REFERENCE.

THANK YOU FOR YOUR ORDER.

SINCERELY

Karen Storey

SIGNED BEFORE ME THIS 20 DAY OF JULY 2010.

Notary: SCAMP South Georgia
My Commission Expires Oct. 19, 2010

Out 19

Out 1

Phone: 706-234-1605

P.O. Box 99, Armuchee, GA 30105

Fax: 706-235-8132

Figure A-3. Southern Yellow Pine Posts, Test Nos. MGSSYP-1 and MGSSYP-2



SEP 17 2010

CERTIFICATE OF COMPLIANCE

SEPTEMBER 10, 2010

MIDWEST MACHINERY & SUPPLY MILFORD, NE

The following material delivered on 9/10/10 on bill of lading number 20374 has been inspected before and after treatment and is in full compliance with applicable Nebraska Department of Roads requirements for southern yellow pine Timber Guardrail Components, preservative treated with Chromated-Copper-Arsenate (CCA-C) to a minimum retention of .60 lbs/cu.ft. The acceptance of each piece by company quality control is indicated by a Hammer brand on the end of each piece.

MAT	MATERIAL		DATE	RETENTION	QUANTITY
6x8x14"	OCD Blockout	10-456	8/31/10	0.75	280
51/2X71/2X421/2"	BCT Post	10-192	4/15/10	0.64	48
6x8x18"	Blockout	10-456	8/31/10	0.75	70
6x8x22"	Blockout	10-456	8/31/10	0.75	140

THIS CERTIFICATE APPLIES TO MATERIAL ORDERED FOR your order no.: 2355

FOR ANY INQUIRIES, PLEASE RETAIN THIS DOCUMENT FOR FUTURE REFERENCE.

THANK YOU FOR YOUR ORDER.

SINCERELY,

Karen Storey

Signed before me this $10\ \mathrm{DAY}\ \mathrm{OF}\ \mathrm{September}\ 2010.$

Notary: Notary Public Floyd Coloniy Georgia
My Commission Expires Oct. 19, 2010

Oct. 19, 2010

COUNTY

Phone: 706-234-1605

P.O. Box 99, Armuchee, GA 30105

Fax: 706-235-8132

Figure A-4. Southern Yellow Pine Posts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

PERMA-TREAT OF ILLINOIS, INC.

MARION, IL 62959 PH# 800.572.7384 FAX# 618.993.8680

This is to certify that the guardrail material has been treated and inspected according to the Iowa Department of Transportation Specification requirements and IM 462. Also, conforms to State of Illinois specification.

This material has been processed from Rough Sawn #1 Southern Yellow Pine.

Company:

Bill of Lading:

Quantity	Description	Charge #	Date of Treatment	Treatment	MC prior to Treatment
30	6X8X7 aH	4835	4.4.11	.60 CCA-C	20%
30	6X8X7 2H	4800	12-6-10	.60 CCA-C	20%
30	HE PXBXD	4843	4-8-11	.60 CCA-C	20%
(00)	GX8X6' CRT	4850	4-19-11	.60 CCA-C	20%
90	6X8X6 CRT	4845	4-15-11	.60 CCA-C	20%
25a	6x12x14" 1H	4844	4-12-11	.60 CCA-C	20%
288	6X8X18 DHTRANE	4851	4-19-11	.60 CCA-C	20%
144	6×8×18 attimes		4-12-11	.60 CCA-C	20%
				.60 CCA-C	20%
9				.60 CCA-C	20%
				.60 CCA-C	20%
				.60 CCA-C	20%

Perma-Treat of Illinois, Inc

Date: 5/10/11

NOTARIZED

Sworn to and described Before me this 10 day of

2011

Official Seal

Figure A-5. Wood Blockouts, Test Nos. MGSSYP-1 and MGSSYP-2

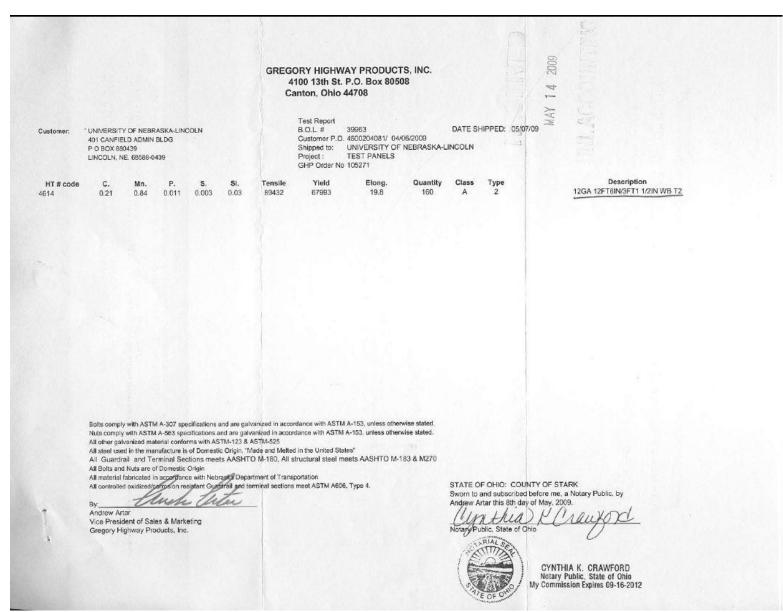


Figure A-6. 12-ft 6-in. Long W-Beam, Test Nos. MGSSYP-1 and MGSSYP-2

14:21

RECEIVED GREGORY HIGHWAY PRODUCTS, INC. OCT 0 5 2005 4100 13th St. P.O. Box 80508 Canton, Ohio 44708 UNLFMP Test Report UNIVERSITY OF NEBRASKA-LINCOLN B.O.L.# DATE SHIPPED: 09/27/05 401 CANFIELD ADMIN BLDG Customer P.O.: VERBAL JOHN ROHDE P O BOX 880439 Shipped to: UNIVERSITY OF NEBRASKA-LINCOLN LINCOLN, NE. 68588-0439 Project: STOCK GHP Order No.: 44822 Tensile Yield Description Elang. Type: 3390 0.013 0.007 0.01 81660 62520 20.76 180 12GA 12FT6IN/3FT1 1/2IN WB T2 Bolts comply with ASTM A-307 specifications and are getvanized in accordance with ASTM A-153, unless otherwise stated. Nuts comply with ASTM A-563 specifications and are gavantzed in accordance with ASTM A-153, unless otherwise stated. All other galvantzed material conforms with ASTM-123 & ASTM-526 All steel used in the manufacture is of Domestic Origin, "Mixing and Mixing and Interest ASHTO M-183 & M270 All Buts and Nuts are of Domestic Origin All Buts and Nuts are of Domestic Origin [[7]] All Bolts and Nuts are of Domestic Origin

STATE OF OHIO: COUNTY OF STARK Sworn to and subscribed before me, a Notary Public, by

Notary Public, State of Ohio My Commission Expires February 24, 2006

Figure A-7. Figure A-10. 12-ft 6-in. Long W-Beam, Test No. MGSSYP-2

Vice President of Sales and Marketing Gregory Highway Products, inc.

September 4, 2013 MwRSF Test No. TRP-03-272-13

Trinity Highw roducts, LLC 25-18 N.E. 28th St.

Ft Worth, TX

Customer: MIDWEST MACH.& SUPPLY CO.

P. O. BOX 81097

Sales Order: 1112249 Customer PO: 2188 BOL # 28104 Document # 1 Print Date: 8/4/09 Project: RESALE

Shipped To: NE Use State: KS

LINCOLN, NE 68501-1097

Trinity Highway Products, LLC
Certificate Of Compliance For Trinity Industries, Inc.
NCHRP Report 350 Compliant

	Pieces	Description
X	40	12/6'3/S

Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36
ALL OTHER GALVANIZED MATERIAL CONFORMS WITH ASTM-123.
BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.
NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.
3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING

STRENGTH - 49 100 LB State of Texas, County of T

Notary Public: Commission Expires My Commission Expires

July 13, 2013

Trinity Highway Products, LLC
Certified By: Telfamil Ingle
Quality Assurance

1 of 1

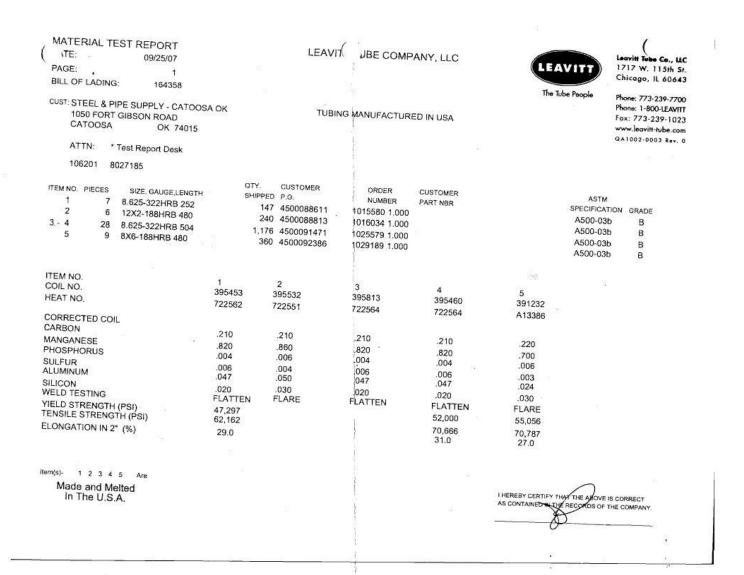


Figure A-9. Foundation Tube, Test Nos. MGSSYP-1 and MGSSYP-2

Trinity Highway Products, LLC

425 E. O'Connor

Order Number: 1108107

Lima, OH

Customer PO: 2132

Customer: MIDWEST MACH & SUPPLY CO.

BOL Number: 48341

P. O. BOX 81097

Document #: 1

Shipped To: NE

LINCOLN, NE 68501-1097

Use State: KS

Project; STOCK

MIDWEST MACHINERY Qty

Si Cu Ch Part# Description TV Heat Code/ Beat# **Vicld** TS 21.2 0.210 0.880 0.010 0.000 0.030 0.080 0.000 0.060 0.010 4 M-180 A C49037 64,600 88,600 25 37.0 0.210 0.770 0.009 0.006 0.016 0.010 0.00 0.020 0.001 736G 57TUBE \$1/.188"X6"X8"FLA A-500 Y85912 56,500 72,980 742G 60 TUBE SL/.188X8X6 Y85912 56,500 72,980 37.0 0.210 0.770 0.009 0.006 0.016 0.010 0.08 0.020 0.081 € A-508 26.9 0.190 0.520 0.012 0.003 0.020 0.090 0.00 0.040 0.000 4 26 764G 1/4"X24"X24"SOIL PLATE A-36 120039 46,660 73,630 32 923G BRONSTAD 98" W/O 26.6 0.190 0.230 0.015 0.004 0.020 0.110 0.00 0.040 0.000 4 122209 63,590 82,010 M-180 A

59,770

78,641

86/84/2889

Upon delivery, all materials subject to Trinity Highway Products , LLC Storage Stain Policy No. LG-002.

M-180 B

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT.

ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHERWISE STATED.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA. ASTM 4/9 AASHTO M30, TYPE II BREAKING

A314375

STRENOTH -49100 LB

State of Ohio, County of Allen. Sworn and subscribed before me this 22nd day of May, 2009

Notary Public: \ Commission Expires // 28 12014

927G 10/END SHOE/EXT

Trinity High Certified By:

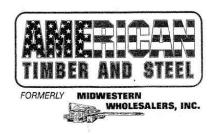
4 of 7

As of: 5/22/09

27.4 0.210 0.750 0.017 0.005 0.030 0.090 0.00 0.030 0.002 4

Figure A-10. Foundation Tube, Test No. MGSSYP-2

September 4, 2013 MwRSF Test No. TRP-03-272-13



QUANTITY	DESCRIPTION	CHARGE NO.	TREATMENT	TREATER
50	6x8-46" DSS SYP S4S BCT Pos	st 38040	CCA	MWT
4. 8.				
		eas .		
56 56				
	MWT - MIDWEST WOOD TO MWT-OK - MIDWEST WOOD In the USA. Meets AASHTO Specific Action of the USA.	TREATING, INC	C., CHICKASHA,	
	MBER AND STEEL	NOTARI		
By Heather I	PI VO		and subscribed be	707 20 20 20 20
Title Sales Ass		this 13	th day of Ap	ril 2010
Date April 1			/ / /	6 // \

Figure A-11. BCT Timber Post, Test Nos. MGSSYP-1 and MGSSYP-2 $\,$

2 of 4

#25 E. O'Connor
Lima, OH

Customer: MIDWEST MACH & SUPPLY CO. Sales Order: 1093497 Print Date: 6/30/08
P. O. BOX 81097 Customer PO: 2030 Project: RESALE
BOL # 43073 Shipped To: NE
LINCOLN, NE 68501-1097

Trinity Highway Products, LLC

Certificate Of Compliance For Trinity Industries, Inc. ** SLOTTED RAIL TERMINAL **

NCHRP Report 350 Compliant

989 1021 1021 1021 1021
MGSBR
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Ground Strut
Ground Strut
090453-8

Jpon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

2 LL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT
LL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36
LL OTHER GALVANIZED MATERIAL CONFORMS WITH ASTM-123.

3 JULIS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

3 JULIS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

4 DA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA. ASTM 449 AASHTO M30, TYTE II BREAKING

5 TRENGTH - 49100 LB

6 Citary Public:

6 Clary Public:

7 Certified By:

Figure A-12. Strut and Yoke Assembly, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-13. BCT Cable Anchor Assembly, Test Nos. MGSSYP-1 and MGSSYP-2

September 4, 2013 MwRSF Test No. TRP-03-272-13

Certified Analysis Trinity Highway Products, LLC 2548 N.B. 28th St. Order Number: 1095199 Oustomer PO: 2041 Pt Worth, TX Asof: 6/20/08 Customer: MIDWEST MACHL& SUPPLY CO. BOL Number: 24481 Document #: 1 P. O. BOX 81097 Shipped To: NE Use State: KS LINCOLN, NE 68501-1097 RESALE Project: MACHINERY TV Heat Code/ Heat# Yield Part# Description Spec CL 81,300 64,230 6G 12/6/3/S M-180 A MIDWEST 701A -25X11.75X16 CAB ANC 4153095 44,900 60,800 34.0 0.240 0.750 0.012 0.093 0.020 0.020 0.000 0.040 0.002 4 A8P8160 74,000 87,000 25.2 0.050 0.670 0.013 0.005 0.030 0.220 0.000 0.060 0.021 4 742G 60 TUBE SL/.188X8X6 6106195 46,700 69,900 23.5 0.120 0.230 0.010 0.005 0.020 0.230 0.000 0.070 0.006 4 782G 5/8"X8"X8" HEAR PL/OF L0049 73,500 25.0 0.160 0.760 0.011 0.008 0.020 0.200 0.000 0.100 0.000 4 907G 12/BUFFER/ROLLED M-180 A 402-761-3288 Upon delivery, all materials subject to Trinity Highway Products , LLC Storage Stain Policy No. LG-002. ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT. ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36 ALL OTHER GALVANIZED MATERIAL CONFORMS WITH ASTM-123. BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISH STATED. 15: 344° DIA CABLE 6K19 ZENC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD I!" DIA ASTM 449 AASHTO M30, TYPE II BREAKING 84/2889 STRENGTH-49100 LB State of Texas, County of Tarrage. Sworn and subscribed before me this 20th day of June, 2008 Notary Public: Trinity Highway Products, LLC Commission Expires

Certified By:

Figure A-14. Anchor Bracket Assembly, Test Nos. MGSSYP-1 and MGSSYP-2

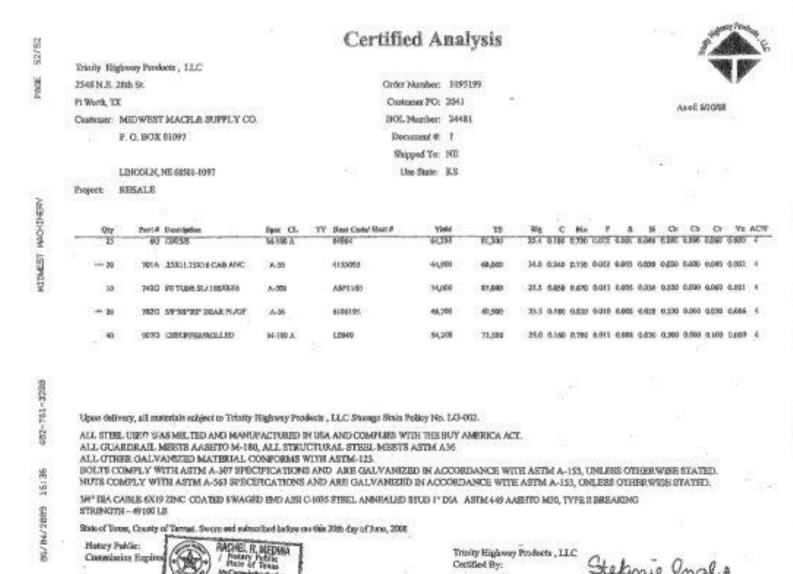


Figure A-15. Anchor Cable Bearing Plate, Test Nos. MGSSYP-1 and MGSSYP-2

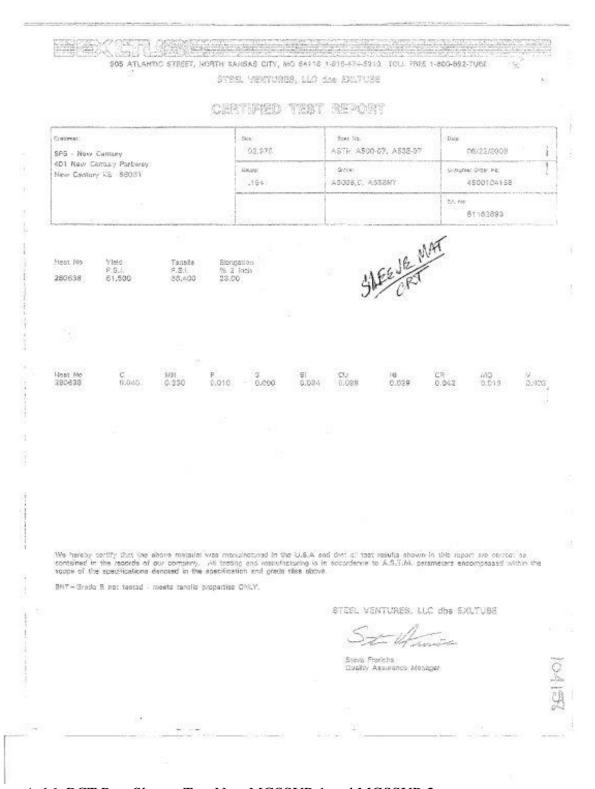


Figure A-16. BCT Post Sleeve, Test Nos. MGSSYP-1 and MGSSYP-2

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MIDWEST MACHINERY

11/04/2009 05:10 402-761-3288

Figure A-17. 5%-in. x 11/4-in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

402-761-3288 11/04/2009 05:10

MIDWEST MACHINERY

PAGE 02/10

TRINITY HIGHWAY PRODUCTS, LCC. Plant #55 425 E. O' CONNOR AVENUE Lima, OH 45801 419-227-1296



1	STOM	ER:	STO	CK					Y29, 20	0.9				-	
								MCE#	FD. 00	2020					
-				-					ER: 09						-
	5000 ON	MBER	0.5						: 110,7	103					
DE	SCRIP	TION:	2/8/2	1 %" G	KBOL	1	DATI	s san	PED:						
SP	ECIPIO	CATIO	NS: AS	TM A3	07-A/A	153	HEAT	rw: 50	72014		-				
-						M	ATERL	IT CH	EMISTI	RY					
ċ	. MN	P	s	SI	NI	CR	мо	cu	SN	v	AL	N	В	тз	,
15	A7	.006	.003	.09	.06	.05	.02	.05	.005	.009	.046	.0063	.000	.000	.0
		1	1	PLAT	ING	AND	OR I	PRO	FECT	TVE C	OAT	ING			-
HC	OT DIP	GALV	ANTZE	D (OZ.	PER S	Q. FT.	,				1	1.25	vg.	-	-
								- 4			-1				
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	T W	HE MA	REBY C	CERTIE O, COU	D IN T	HIS PR	ODUCTOR REINED H	T WAS U.S.A ST OF	OUR K	NOWLJ RRECA	MANUT	LL INFO	RED IN	THE	

Figure A-18. 5/8-in. x 11/4-in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

PAGE 09/10

BUFFALO, HY 14219 FAX: 330-438-5695 2049 LEXESHORE-GATE 6 PHORE: 330-438-5694 REPUBLIC ENGINEERED PRODUCTS June 3, 2009 PAGE 1 PURCHASE ORD: 130969M PART MUMBER: 100944B ORDER NUMBER: 1409650 - 01 4/15/2009 5550-3007-01 5877-68 PURCHASE ORDER DATE: ACCOUNT NUMBER: REVISION: TRINITY INTOSTRISS INC HIGHWAY SAGETY PRODUCTS INC 2 O BOX 568887 4TH PLOOR DALLAS, TX 75356-8887 TRINITY INDOSTRIES INC C/O BCS METALS PREP 5800 STEELING AVE NOT ROLLED STEEL COLLS CARROW MIRITAGES AN AU KILLED FINE BRAIN COLD WORKING QUALITY VEST REPORTS OF MESCRAPICAL PROPERTIES FOR INTO ONLY EXTRA TESTING SIEE: RDS 1.2190 DIAM X COIL ROS 30,9626000 DIAM X COIL - LADUE CHEMISTRY & -----MM 0.45 NI 0.05 CR. 0.07 0.003 0.14 0.14 0.013 0.05 CB 0.900 MO 0.02 AL-0.037 0.004 0.0060 0.002 CALCULATED TESTS REDUCTION RATIO 39.1 TO 1 AUSTRAITIC GRAIN SIRE 5 OR FINER BASED ON A TOTAL ALAMINON CONTENT EQUAL TO OR GREATER TEAM . 8564 PER TENSILS THAT SIMBARD PORMAT TENSILS YIRLD(0.24) RA 9 E 64.2 33.0 30930 ASTM B10/ASYM A170 HBW A9-RED/CD HWW KARDWASS TEST MID-RADIUS 112 REPOBLIC PROGINEERED PRODUCTS HEREBY CRITIPY THAT THE MATERIAL LISTED HERRIN HAS BEEN INSPECTED AND TESTED IN ACCORDANCE WITH THE METHOUS PRESCRIED IN THE GOVERNING SPECIFICATIONS AND BASED UPON THE RESCRITS OF RUCH INSPECTION AND TESTING HAS BEEN APPROVED FOR CONFORMANCE TO THE SPECIFICATIONS. CERTIFICATE OF TESTS SHALL NOT HE REPRODUCED EXCEPT IN FULL. ALL TESTING HAS BEEN PERFORMED USING THE CURRENT REVISION OF THE TESTING SPECIFICATIONS. RECORDING OF PALSE, FICTITIOUS OR FRANDULENT STATEMENTS OR SWIRIES ON THIS DOCUMENT MAY BE PUNISHED AS A PELCHY UNDER PED STATUES TITLE 10 CHAPTER 47. THE MATERIAL WAS NOT REPOSED TO MERCURY OR MAY METAL ALLOY THAT IS LIQUID AT AMBIENT TEMPERATURE DURING PROCESSING OR WHILE IN OUR POSSESSION. NO WELD OR WELD REPAIR WAS PERFORMED ON THIS MATERIAL. THE RESULTS REPORTED RELATE ONLY TO THE ITEMS TESTED MELTUD AND MANUFACTURED IN THE U.S.A. BY WILDA MECUE R. A. BULLLOCK DIRECTOR DUAL, ASSURANCE Y' G Bullet

MIDWEST MACHINERY

11/04/2009 06:10 402-761-3288

Figure A-19. % in. Nut, Test Nos. MGSSYP-1 and MGSSYP-2

11/04/2009 06:18 402-761-3288

MIDWEST MACHINERY

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Trinity Metals Laboratory

A DIVISION OF TRINITY INDUSTRIES 4001 IRVING BLVD, 78247 - P.O. BOX 568887 DALLAS, TX 75368-8887 Phone: 214,589,7501 FAX; 214,589,7594

Lab No: 9080059F

SUE HENLINE TRINITY HWY PRODUCTS, LLC #55 ROLLFORM LIMA, OH 45801

Heat Code: Heat Code: Heat Nambor: 5072060
PO or Work Order: 55-50083
Test Spac: F606 ASTM METHODS
Other Information: Lot # 090717N2

Completion Date: 08/10/2009 Weld Spec: Material Type: A 563 A Material Size: 5/8" GR Nuts 33408

HARDNESS TEST:

Hardness Type: HARDNESS ROCKWELL BW Hardness Location; SURFACE of WRIENCH FLAT - A Herdness Average: 88.5

Measured Value	Measured Amt
Massured Value	89
Mossured Value	88

PASSED

Hardness Type: HARDNESS ROCKWELL BW Hardness Location: SURFACE of WRENCH FLAT - B Herdress Average: 92

Measured Value	Measured Amt
Measured Value	92
Measured Value	92

PASSED

Hardness Type: HARONESS ROCKWELL BW Herdness Location: SURFACE of WRENCH FLAT - C Hardness Average: 87,5

Measured Value	Measured Amt
Messured Value	88
Messured Vakre	67

PASSED

Hordness Type: HARDNESS ROCKWELL BW ans Location: SURFACE of WRENCH FLAT - D Hardness Average: 89.5

Measured Value	_ Measured Amt _
Measured Value	90
Measured Value	89

Pege 1 of 2

11/04/2009 05:10 402-761-3288 MIDWEST MACHINERY

Trinity Metals Laboratory

A DIVISION OF TRINITY INDUSTRIES 4001 RVING BLVD. 75247 - P.O. BOX 568887 DALLAS, TX 75356-8867 Phono: 214,589,7591 FAX: 214,589,7594



Lab No: 9080059F

SUE HENLINE TRINITY HWY PRODUCTS, LLC #55 ROLLFORM LTMA, OH 45801 Received Date: 09/07/2009 Heat Code: Heat Number: 5072080, or Work Order: 55-50083 Tect Spoc: F606 ASTM METHODS

ptetion Date: 08/10/2008 Wald Spec: aterial Type: A 583 A faterial Size: 5/6* GR Nuts 33408

Herdness Type: HARDNESS ROCKWELL BW Hardness Location: SURFACE of WRENCH FLAT - E

Measured Value	Measured Amt
Measured Value	88
Measured Value	88

PASSED

OTHER TEST:

Type: NUT PROOF LOAD

Samples PASSED proof loads of 16,950 LBS.

Quantity amount: 5

Type: HEAD MARKINGS

TRN L

Quantity amount 1

We certify the above results to be a true and accurate representation of the complete), submitted. Attaction report will void certification. NVLAP Certificate of Acceptitation effective fixough 12-31-09. This report may certification, approval, or endorsement by NVLAP, NIST, or any agency of the federal government.

11/04/2009 06:10

402-761-3288

MIDWEST MACHINERY

PAGE 06/10

TRINITY HIGHWAY PRODUCTS, LLC. 425 E. O'CONNOR AVENUE LIMA, OHIO 45801 419-227-1296



MATERIAL CERTIFICATION

CUSTOMER: STOCK	DATE: JULY 27, 2009
	INVOICE#:
	LOT#: 090717N2
PART NUMBER: 3340G	QUANTITY: 62,000
DESCRIPTION: 5/8" GR NUT	DATE SHIPPED
SPECIFICATIONS: ASTM A563-A/A153	HEAT 5072080

MATERIAL CHEMISTY

C	MIN	P	9	SI	CU	NI	CR	v	MO	SN	AL	СВ	N	
.14	.45	.013	.003	.14	.05	.05	.07	-002	.02	.006	.037	.000	.006	-

PLATING AND/OR PROTECTIVE COATING

HOT DIP GALVANIZING (OZ. PER SQ. FT.) 2.81 AVG.

****THIS PRODUCT WAS MANUFACTURED IN THE UNITED STATES OF AMERICA***

THE MATERIAL USED IN THIS PRODUCT WAS MELTED AND MANUFACTURED IN THE U.A.A.

WE HEREBY CERTIFY THAT TO THE BEST OF OUR KNOWLEDGE AND INFORMATION CONTAINED HEREIN IS CORRECT.

DENITY HIGHWAY, RODUCTS, LLC.

STATE OF OHIO, COUNTY OF ALLEN SWORN AND SUBSCRIBED BEFORE ME

THIS 277 DAY OF JULY, 2009

_NOTARY PUBLIC

425 E. O'CONNOR AVENUE

LIMA, OHIO 45801

419-227-1296

Figure A-22. 5/8 in. Nut, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

			100	TRIN	As	LIN	1A, OH 119-227-	O 4580 1296)1	s, LLC	3 Ha		K	10	7
		CU	STOME	R: SI		MATE	RIAL C	DATE	-	CH 31, 2	:011	- 3			
		PART NUMBER: 3MSG				LOT #: 110318N2									
							QUANTITY: 106,000								
		Di	SCRIP	ION:	5/8** (GR NU	т	DAT	E SHIP	PED					
		SF	AST	ATION M A56	NS: 3-A/A	153		HEA	T# 20	131470 8	£ 201314	60	24	8	
						M	ATERL	AL CH	EMIST	Y					_
c	MN	P	5	SI	NI	CR	мо	CU	SN	v	AL	N	В	TT.	N
.68 09	.35	.007	.004	.07	.05	.05	.02	.09	.007	.004	.023	.008	.0001	.001	.00
Ī	HOT I	m cu	LVANIZ					PROTE	CTIVE	COATI	2.52 AV	207			
L		**THIS	PRODI	D IN	AS M	ANUF.	ACTUR	AS ME		NITED S	STATES NUFAG	OF AM	ERICA* IN THE	U.S.A.	
		HERE	BY CER	TIFY	CO	NTAR	VED HE	DEIN	DUR KE	OWLE	7				
		HERE	BY CER	TIFY	CO	NTAL	NED HE	REIN	OUR KE	RINIT	1/h.	huy WAY IS	RODUCT	S, LLC.	
- 5		F OHIO	D, COUN	CTY O	FALL	NTAL	NED HE	REIN	OUR K?	RECT	1/h.		RODUCT	S, LLC.	
- 5	TATE O	F OHIO	D, COUN	CTY O BED B RCH,	FALL	EN EME	_NOTA	REIN	Is COR	RECT	1/h.		RODUCT	S, LLC.	
- 5	TATE O	of Ohio	D, COUNT DISCRIES OF MA	TY O BED B RCH,	FALL EFOR 2011	EN E MR	_NOTA	REIN	Is COR	RECT/ PRINTY	Angr			S, LLC.	

Figure A-23. 5/8 in. Nut, Test No. MGSSYP-2

rrinity Metals Laboratory A DIVISION OF TRINITY INCUSTRIES 4001 IRVING BLVD. 75247 - P.O. BOX 568867 DALLAS, TX 75356-8887 Phone: 214.589.7591 FAX: 214.589.7594 Lab No: 11040021F KEITH HAMBURG TRINTY HWY PRODUCTS, LLC #55 ROLLFORM LIMA, OH 45601 HARDNESS TEST:

athrips MSB &

Paceived Onte: 04/04/2011 Healt Code: Healt Number: 2013/1460 8, 2013/1470 PO or Work Order: 1103/18N2 Test Spec: P609 ASTM METHODS Other Information: 65-61387

Completion Date: 04/04/2011 Weld Spac: Material Type: A 563 A Material Size: 5/8° GR Nuts

Hardness Type: HARDNESS ROCKWELL BW Hardness Location: Surface of Whench Flat A Hardness Average: 86.5

Measured Value	Measured Amt				
Measured Value	86				
Measured Value	87				

PASSED

Hardness Typic HARDNESS ROCKWELL BW Hardness Location: Surface of Wrench Flat B Hardness Average: 84

Measured Value	Measured Amt
Measured Value	34
Measured Value	84

PASSED

Hardness Type: HARONESS ROCKWELL BW Hardness Location: Surface of Wiends Flet C

Measured Value	Measured Amt
Measured Value	87
Measured Value	87

PASSED

Hardness Average: 87

modeling raise	monoured yant
Measured Value	87
Measured Value	87

Hardress Type: HARDNESS ROCKWELL BW Hardness Location: Gurlace of Wisnoh Flat D Hardness Average: 87.5

Measured Value	Measured Amt
Measured Value	67
Measured Value	85

PASSED

4.04-1

We certify the above results to be a true and accurate representation of the sample(s) submitted. Alteration or partial reproduction of this report will valid certification. NVLAP Certificate of Accreditation effective through 12-31-11. This report may not be used to claim product certification, approval, or endorsement by NVLAP, NIST, or any agency of the federal government.

rrinity Metals Laboratory

A DWISION OF TRUNITY INDUSTRIES 4001 RVING BLVD. 75347 - P. C. BOX 568887 DALLAS, TX 75956-8887 Phone: 214,569,7591 FAX: 214,569,7594



MA(VÕ

Lab No: 11040021F

KEITH HAMBURG TRINITY HWY PRODUCTS, LLC #55 ROLLFORM LIMA, OH 45801 Received Date: 04/64/2011 Heat October Heat Number: 20131469 8:20131470 PO or Work Order: 110318N2 Test Spec: P606 ASTM METHODS Other Information: 55-61507

Completion Date: 04/04/2811 Weld Spec: Material Type: A 563 A Material Star; 5/8* GR Nuts

Hardness Type: HARDNESS ROCKWELL RW Hardness Location: Surface of Wrench Flat E Hardness Average: 96.5

Measured Value	Measured Amt
Measured Value	87
Measured Value	86

PASSED

OTHER TEST:

Type: NUT PROOF LOAD (to 30K)
Samples PASSED proof loads of 16,950 lbs.

Quantity amount: 5

Type: HEAD MARKINGS TRN N Quantity amount: 1

We certify the above results to be a true and accurate representation of the sample(s) submitted. Attention or partial reproduction of this separt will void peritication NNLAP Certificate of Acceptation effective through 12-31-11. This report may not be used to dain product certification, approval, or endormanter by NNLAP, NST, or any approxy of the federal queryment.

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Page 2 of 2

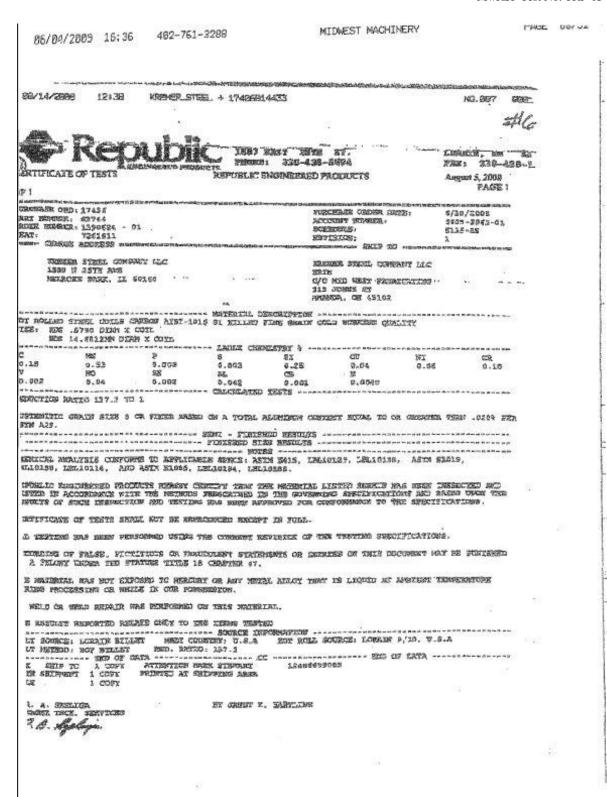


Figure A-26. % in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2

MIDWEST MACHINERY 402-761-3288 06/04/2009 15:36 Mld West Fabricating Company Rockmill Division 3115 West Fair Avenue Lab Test Report Lancaster, OH 43130 (740) 681-4411 Data Results Semple 1: Date: 24-Sep-08 Sample 2: 2.84 Part Number: 10-5 Sample 3: 2,63 Description: 10" POST BOLT W/6" THRD 2.95 Sample 4: Lot Number: 85217 3,28 Sample 5: Customer: Trinity Szympia 6: 2.13 Sample 7: 3.12 Test Type: Permiscope Sample 8: 2.64 Heat Number: 7261613 Sample 9: 3.50 Processor: Columbus Sample 10: 3.72 Testing Standard: ASTM=A183-A153/98 Sample 1.1: 2.15 Requirement: 1.77 Mil Sumple 12: 2.73 Sample Qty: 20 3.01 Sample 13t Semple 141 2,70 Disposition: Ship Sample 15: 2.86 Ship ID: XB9 Sample 15: 3,28 Sample 17: 3,12 Sample 18: 2,39 2.44 Sample 29: Sampla 20: 2.58 Average: 2.84 Conformance : Non-Conformance Performed By: D.Smith This report shall not be reproduced, except in full, without the written approval of Mid West Fabricating Company's Quality Department.

Figure A-27. 5% in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

COMPANY PROPERTY

MIDWEST MACHINERY

3115 West Felt Avenue **Lab Test Report** Lançaster, OH 43130 (740) 681-4411 Data Results Sample 1: 85,20 Dates 24-Sep-08 86.80 Satuple 2: Part Number: 10-6 Sample It 85.40 Description: 10" POST BOLT W/6" THRO 85.00 Symple 4: Lot Mumber: 85217 25,53 Sample St Customer: Trinity 0,00 Sample 61 Test Type: Rockwell Sample 7: 0.00 Spouple 8: 0.06 Heat Number: 7261611 0.00 Sumple 9s Processor: Columbus 0.00 Sample 10: Testing Standard: ASTM=E18-98 0.00 Sample 11: Requirement: 69-100 "S" Sample 12: 0,00 Sample 13: Sample Qty: 5 09.0 Sarapia 14: 0.00 Disposition: Screp Sample 18: 0.00 Ship 7D: Sumple 16: 9,99 0.00 . Sample 17: Sample 28: 0.00

Mid West Fabricating Company

Rockmill Division

Conformance

Non-Conformance

Performed By: D.Smith

Sample 19:

Sample 20:

Averageu

0.00

0.00

85.80

This report shall not be repreduced, except in full, without the written approval of bild West Fabricating Company's Quality Department.

Figure A-28. % in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

1 PENSE

-- - service many - record

Mid West Fabricating Company Rockmill Division 3115 West Pair Avenue Lab Test Report Lancaster, OH 43130 (740) 681-4411 Data Results Sumple 1: 16,850,00 Date: 24-Sep-08 Sample 2r 17,370.00 Part Number: 16-6 Sample 3: 17,190.00 Description: 10" POST BOLT W/6" THRD Semple 4: 17,900.00 Lot Number: 8823.7 Sample 5: 17,300.00 Customer: Trinity Semple 6: 5.00 Test Type: Rockwell Sample 7s 0.00 0.00 Sample 8: Heat Number: 7251611. Sample 9: 0.00 Processor: Columbus 00,00 Sample 10: Testing Standard: ASTM=F606-958 Sample 11: 0,00 Requirement: 13,590 lof Santple 12: 0.00 Sample Qtyr: 5 Sample 23: 0.00 0,00 Sample 14: Disposition: Screp Sample 15t 0.00 Ship ID: 0.00 Sample 15: Sample 17: 0.60 Sample 18: 0.00 0.00 Sample 19: 0.00 Sample 20: Average: 17,242.00 Conformance Non-Conformance Performed By: 0.9mith This report shall not be reproduced, except in full, without the written approval of Mid West Febricating Company's Quality Department.

Figure A-29. % in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

-	W. *						
			1522				
		INSPECTION	ON CERTIFICATE				
		ROCKFORD	BOLT & STEEL CO.				
			MILL STREET				
			ORD, IL 61101				
		815-968-0514	FAX#815-968-3111				
	OUGTONED NAME.	DENNETT DOLT WORKS					
	CUSTOMER NAME:	BENNETT BOLT WORKS					
	CUSTOMER P.O. :	6008015					
	INVOICE #: 945	5308	DATE SHIPPED:	2/3/11			
12	LOT#: 21	1306					
	SPECIFICATION:	ASTM A307, GRADE A M	IILD CARBON STEEL B	OLTS			
		TENSILE RESULTS:	SPECIFICATION	ACTUAL			
			60,000 min.	77,730			
				77,787	10,301		
		HARDNESS RESULTS:	SPECIFICATION	88.80	85,46		
			100 MAX	90.83	86,83		
	COATING: ASTMS	SPECIFICATION F2329 HOT D	IP GALVANIZE				
			GALVANIEL			52	
	STEEL SUPPLIER:	NUCOR, NUCOR	00		90		9
	HEAT NO. NF10102	253801, NF1020257001					
	QUANTITY AND DES	CRIPTION:		V 44.5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
	500 PCS 5/8	"X 22" GUARD RAIL BOLT					
		OVE BOLTS HAVE BEEN MANUFACTURE					
		U.S.A., WE FURTHER CERTIFY THAT TO AND THAT OUR PROCEDURES FOR TO					
		WEET OR EXCEED ALL APPLICABLE TES	STS, PROCESS, AND INSPECTIO	N-REQUIREMEN	ITS PER ABOVE		01.01.00.01.01.01.01.01.01.01.01.01.01.0
	SPECIFICATION.						
	STATE OF ILLINOIS COUNTY OF WINNEBAGO		885.000			(6)	
	SIGNED BEFORE ME ON THIS	1/	Denda M	1 toma	1 1/1	de	
	DAY OF FEEDE	ung 2011	APPROVED SIGNAT	ORY	DATE	1111	
	Sina Aus	niner					

| Figure A-30. 5/8 in. x 22 in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

Mill Certification Details	i				
NUCOR					
NUCOR CORPORATION					
NUCOR STEEL NEBRASKA					
Mill Certification	on Details - 8/19/20	10 8:47 AM			
Customer: KING STEEL CO	RP - GRAND BLANC				
Bill of Lading #: 178801 Chief Metallurgist : Jim Hill	Date: 7/13/2010				
Heat # : NF1010253801 Product : WIRE					
Grade: :010	Division : Norfolk, NE	rire Rou			
Comments :		Billet Heat	#: NF10102538		
C+1 0.58 0.20 0.000 0.015 0.27 0.09 0.09	0 02 0 032 0 000 0 000 0 000	9 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
0 0000 0.001					
Physical Properties	CONTRACTOR OF THE PARTY OF THE				
Tensile:	CALL THE PARTY.				
Yield:					
Elongation (in 8 inches):					
Elongation (in 2 inches):					
The testing was conducted in accordance with manufacturing processes were performed in	ith the requirements of the the United States of Ame	is specification. All me erica.	iting and		
The testing was conducted in accordance with manufacturing processes were performed to Jim Hill Division Metal orgist.	the United States of Ame	erica.	iting and		8
Jim Hill	the United States of Ame	erica.	iting and		* .
Jim Hill	the United States of Ame	erica.	iting and		86 (4)
Jim Hill D vision Melal big st	the United States of Ame	erica.	iting and		H
Jim Hill	the United States of Ame	erica.	iting and		*
Jim Hill D vision Melal big st	the United States of Ame	erica.	iting and		8
Jim Hill D vision Melal big st	the United States of Ame	erica.	iting and		*
Jim Hill D vision Melal big st	the United States of Ame	erica.	iting and		3K (1)
Jim Hill D vision Melal big st	the United States of Ame	erica.	iting and		26 S
Jim Hill D vision Melal big st	the United States of Ame	erica.	iting and		28 (3)
Jim Hill D vision Melal big st	n the United States of Ame	rrica.			
Jim Hill D vision Melal big st	n the United States of Ame	rrica.	iting and		
Jim Hill D vision Melal big st	n the United States of Ame	rrica.			
Jim Hill D vison Melal ong st	n the United States of Ame	rrica.			
Jim Hill D vision Melal big st	n the United States of Ame	rrica.			
Jim Hill D vison Melal ong st	n the United States of Ame	rrica.			
Jim Hill D vison Melal ong st	n the United States of Ame	rrica.			
Jim Hill D vison Melal ong st	n the United States of Ame	rrica.			
Jim Hill D vison Melal ong st	n the United States of Ame	rrica.			
Jim Hill D vison Melal ong st	n the United States of Ame	rrica.		3	

Figure A-31. 5/8 in. x 22 in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

The testing was conducted in accordance with the requirements of this specification. All melting and manufacturing processes were performed in the United States of America. AmHO) Jim Hill

Division Metallurgist

Figure A-32. 5/8 in. x 22 in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

Midwest Machinery :3156893999

5/10

INSPECTION CERTIFICATE

ROCKFORD BOLT & STEEL CO. 126 MILL STREET ROCKFORD, IL 61101 815-968-0514 FAX# 815-968-3111

CUSTOMER NAME:

BENNETT BOLT WORKS

CUSTOMER P.O. :

6005874

INVOICE #:

941845

DATE SHIPPED:

LOT#:

19934

SPECIFICATION:

ASTM A307, GRADE A MILD CARBON STEEL BOLTS

TENSILE RESULTS:

SPECIFICATION 60,000 min.

ACTUAL

76,513 75,053 77,617 76,876

76,796 74,699 77,628 76,938

HARDNESS RESULTS:

SPECIFICATION 100 MAX

81.22 88.80 81.62 86.98

81.80 85.25 87.10 81.00

COATING: ASTM SPECIFICATION F2329 HOT DIP GALVANIZE

STEEL SUPPLIER:

NUCOR, NUCOR, NUCOR, NUCOR

HEAT NO. 848853, 749237, 849289, 848872

QUANTITY AND DESCRIPTION:

PCS 5/8" X 22" GUARD RAIL BOLT

PATE N WE HEREBY CERTIFY THE ABOVE BOLTS HAVE BEEN MANUFACTURED BY ROCKFORD BOLT AND STEEL. THE MATCRIAL USED WAS MELTED AND MANUFACTURED IN THE U.S.A. WE HURTHER CERTIFY THAT THIS DATA IS A TRUE REPRESENTATION OF INFORMATION PROVIDED. BY THE MATERIALS SUPPLIER AND THAT OUR PROCEDURES FOR THE CONTROL OF PRODUCT QUALITY ASSURE THAT ALL ITEMS FURNISHED ON THIS ORDER MEET OR EXCEED ALL APPLICABLE TESTS, PROCESS, AND INSPECTION REQUIREMENTS PER ADOVE SPECIFICATION

STATE OF ILUNOIS COUNTY OF WIMNEBAGO SIGNED BEFORE ME ON THIS DAY OF JULY

OFFICIAL SEAL USA A, BERG Notacy Public - State of Illinois unission Expires Dec 11, 2011 PROVED SIGNATORY DATE

BALLEY STAL GRED BY ROCK CHO. THIS CATA'S A TELL t april mark . I t

Figure A-33. 5/8 in. x 22 in. Bolts, Test No. MGSSYP-2

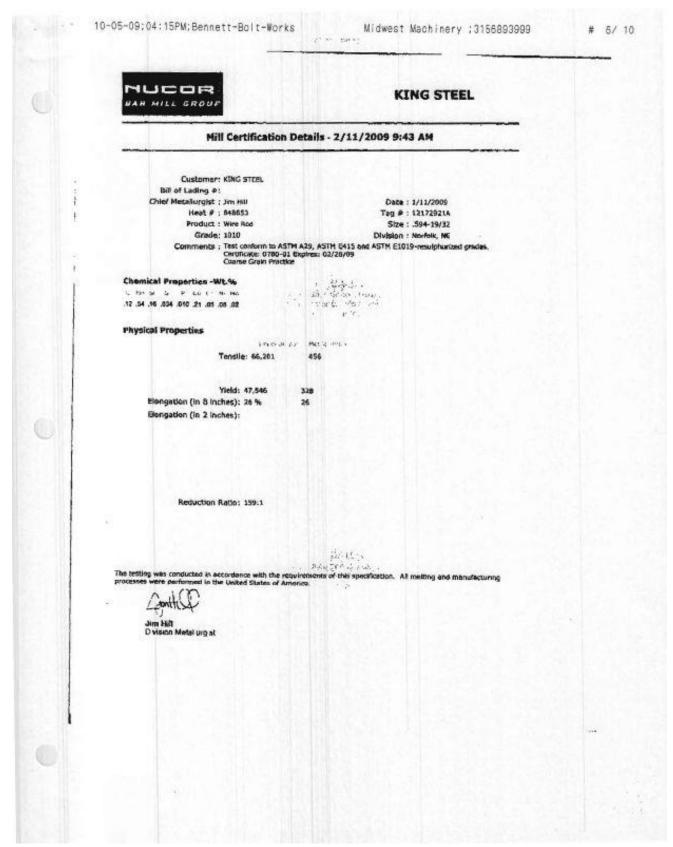


Figure A-34. % in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)

10-05-09;04:15PN	(;Bennett-Boit-W	orks Midwest Machinery ;3158893999	# 7/ 10
wure, king	gateelcorp.com		
Sent: Wednesday To: Sutherland, D	, January 14, 2009 2:23	port@nucorber.com] > PN	
PAR MILL O		KING STEEL	
	Mill Certification	n Detnils - 1/14/2009 2:23 PM	
0	estomer: KING STELL		
	ading #:		
	durgist : Jim Hiš	Date : 8/13/2008	
	Heat # : 749237 Product : Wire Rod	Tag # : 12116840 Size : .594-19/32	
	Grade: 1010	Division : Norfolk, Nr	
Com	sments : Test conform to A	STM A29, ASTM E415 and ASTM E1019-resulphurtzed grades. DI Expires: 12/31/08	
Chomical Proper			
C Ph S S P		(a.t. ofter.com)	
35-27-32-7-37-7-37		Chipmone of this space in	
Physical Propert	ties		
	Imperia	-pad Metric -mpa	
	10000000000		
	Tensile: 64,790	447 S18	
Connection	Yield: 46,264	25	
1000077000	n (in 8 Inches): 25 % n (in 2 arches):		
ppingassa	in the Taranage		
	CONTROL 1220		
	heduction Retio, 159:1		
		sharkwaj :	W
The taction was cure	further in accordance with th	a regularization of this epicification. All melting and manufacturing	
huckers were beign	ormed in the United States o	f America.	
Sulfor	(I)		
- Gun	34		
Jun Helt	letel service		
Chidwings Ma			
Citylaign M			
Chitalon M			
Chitakon M			
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CiMakon M			

Figure A-35. 5/8 in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)

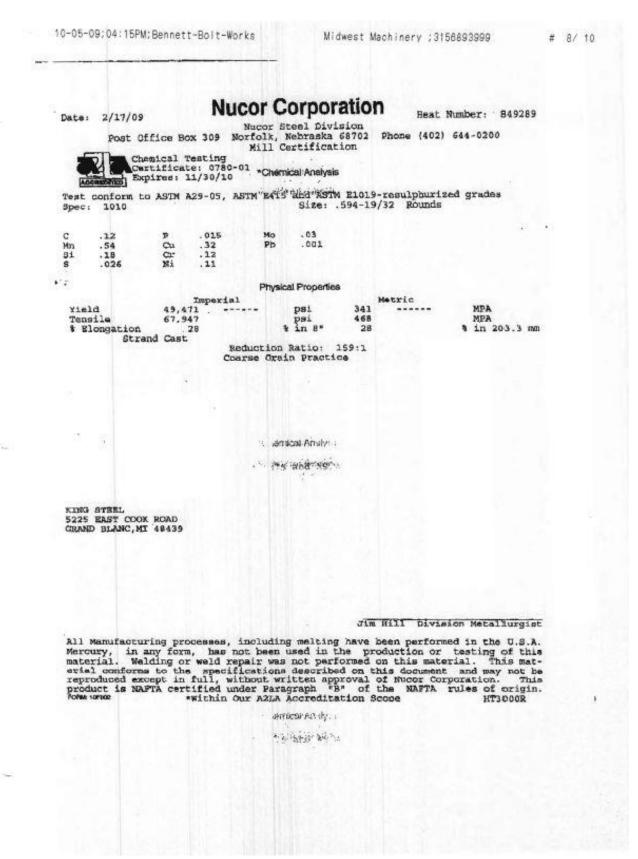


Figure A-36. % in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)

-05-09;04:15PM;Bennett-Bolt-Works	Midwest Machinery ;31568939	99 # 9/ 10
Nucor Bar Mill Group - Mill Certification	Details	Page 1 of 1
Mill Certification Details		
x Nucor Bai Mil Group		
	KRUEGER & CO.	
Mill Certification	n Details - 7/14/2008 5:02 PM	
	- N-1 11	
Customer: KRUEGER & CO	APPLE - ST. T.	
Bill of Lading #: 293611	393-5 AV	
Chiof Metallurgist : Jim Hill	Date : 7/1/2008	
Heat #: 846672	Tag #: 12095061	
Product : Wire Rod	Size : .594-19/32	
Grade: 1010	Division : Norfolk, NE	
	ASTM A29, ASTM E415 and ASTM E1019- ulca. Certificate: 0780-01 Expires: 11/30/08 actice	
Chemical Properties -Wt.%		
C Mn Si S P Cu Cr Ni Mo A .11 .53 .17 .026 .014 .23 .08 .08 .02 .00		
Tensile: 63,969 Yield: 41,456 Blongation (in 8 inches): 27 %	si Metric -mpa 441 286 27	
Blongation (in 2 inches):	CSuda with	
Reduction Ratio: 159:1	on Administration of the Administration of t	
The testing was conducted in accordance	with the requirements of this specification. All re performed in the United States of America.	
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<u>L</u> i		
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	nss/Local Sentings/Temp\Ht. #846672.htm	7/14/2008
	ass/Local Senings/Temp\Ht. #846672.htm	7/14/2008
		7/14/2008
	nas/Local Settings/Temp/Ht. #846672.htm	7/14/2008

Figure A-37. 5/8 in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)



TRINITY HIGHWAY PRODUCTS, LLC. 425 E. O'CONNOR AVENUE LIMA, OHIO 45801 419-227-1296

MATERIAL CERTIFICATION

CUSTOMER: STOCK	DATE: SEPTEMBER 29, 2009	
	INVOICE #:	
	LOT #: 090123B	
PART NUMBER: 3380G	QUANTITY: 119,201	
DESCRIPTION: 5/8" X 1 % HH BOLT	DATE SHIPPED:	
SPECIFICATIONS: ASTM A307-A/A153	HEAT #: 7367052, 7366484,7368369	

MATERIAL CHEMISTY

C	MN	P	S	SI	CU	NI	CR	МО	AL	v	N	CB	SN	В	TI	NB
.15	.49	.008	.002	.06	.03	.02	.05	.01	.029	.002	.005	.901	.001	.000	.000	.000
.13	.38	.007	.002	.10	.03	.04	.06	.02	.037	.002	.064	.001	.001	.000	.000	.000
.14	.43	.006	.008	.06	.04	.02	.06	.02	.034	.002	.005	.001	.001	.000	.000	.000

PLATING AND/OR PROTECTIVE COATING

HOT DIP GALVANIZING (OZ. PER SQ. FT.) 2.74 AVG.

****THIS PRODUCT WAS MANUFACTURED IN THE UNITED STATES OF AMERICA***

THE MATERIAL USED IN THIS PRODUCT WAS MELTED AND MANUFACTURED IN THE U.S.A.

WE HEREBY CERTIFY THAT TO THE BEST OF OUR KNOWLEDGE AND INFORMATION CONTAINED HEREIN IS CORRECT.

THINTY HIGHWAY PRODUCTS, LLC.

STATE OF OHIO, COUNTY OF ALLEN SWORN AND SUBSCRIBED BEFORE ME THIS 29TH BAY SEPTEMBER, 2009

NOTARY PUBLIC

425 E. O'CONNOR AVENUE

LIMA, OHIO 45801

419-227-1296

Figure A-38. 5/8 in. x 11/2 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

Trinity Metals Laboratory

A DIVISION OF TRINITY INDUSTRIES 4001 IRVING BLVD. 75247 - P.O. BOX 568887 DALLAS, TX 75356-8887

Phone: 214.589,7591 FAX: 214.589,7594

Lab No: 9010250F

SUE HENLINE TRINITY HWY PRODUCTS, LLC #55 ROLLFORM LIMA, OH 45801

Received Date: 01/27/2009

Heat Code: Word Spect Heat Number: 7367052, 7366464, and 7363369ana Type: A 307 A PO or Work Order: Lotti: 0901238 Material Size: 5/8" x 1-

Test Spec: F606 ASTM METHODS Other Information: SO#: 55-46502

Completion Date: 01/29/2009 Weld Speci

Quantity amount: 20

Material Size: 5/8" x 1-1/2" HHB

OTHER TEST:

Type: HARDNESS ROCKWELL BW

A) 90-91-90-89

B) 88-90-91-91

C) 89-91-91-91

D) 89-89-91-91

E) 91-91-90-88

Type: HEAD MARKINGS TRN 307A USA

Quantity amount: 0

We certify the above results to be a true and accurate representation of the sample[a] submitted. Attention or partial reproduction of this report will void certification. NVLAP Certificate of Accordington effective through 12-31-08. This report may not be used to claim product certification, approval, or endorsement by NVLAP, NIST, or any agency of the federal government.

Lan Director, Michael S. Beylon, PE

Figure A-39. \(\frac{5}{8} \) in. x 1\(\frac{1}{2} \) in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

PAGE 83/84 87/18/2008 11:19 338-678-3198 REPUBLIC ENGINEER ATTN CARINA SMITH 1807 EAST 28TH ST. LORAIN, OH 4405 PHONE: 330-438-5694 FAX: 330-438-565 REPUBLIC ENGINEERED PRODUCTS CERTIFICATE OF TESTS July 9, 2008 PAGE 1 OF 2 PURCHASE ORD: 127595M PURCHASE CRORR DATE: PART NUMBER: 1009418 ACCOUNT MIMBER: ORDHR STUMBER: 1379747 - 01 9CHEDULE: 4116-85 HEVISION: 2 C/O BCS METALA PRED TRINITY INDUSTRIES INC TRINITY INDUSTRIES INC MIGHNAY SAGETY PRODUCTS INC P O BOX 568887 47H FLOOR MAPLE HTS, OR 44137 DALLAS, TX 75356-8887 WATERIAL DESCRIPTION NOT ROLLED STREET COILS CARSON ALSI-1015 AK AL KILLED FIRE GRAIN COLD WORKING QUALITY TEST REPORTS OF MECHANICAL PROPERTIES FOR IMPO COULT EXTRA TESTING SIZE: RDS .6390 DIAM X COIL ROS 16.2306PM DIAM X COLL LANE CRIMISTRY \$ CU NI 0.03 0.04 N 0.0040 1430 9 8 SI 6.007 0.002 0.1,0 C **CS** 0.38 0.13 0.1.0 0.04 0.06 MO SN AL CB 0.027 0.051 0.0045 w 0.002 REDUCTION RATIO 112.3 TO 1 AUSTENTIC GRAIN SIZE 5 OR FINER BASED ON A TOTAL ALUMINUM CONTENT EQUAL TO OR GREATER TIME 5020 FER FINTSHED SIZE RESULTS TEMBLE TEST STANDARD FORMAT TENSILE YIELD(0.2%) RA
PST PST * 422000 72.4 49.0 PCE 10427 59700 HARDWESS TEST: ASTM E10/ASTM A370 HBW AS-RLD/CD HBW MID-WADIUS NOTES -----CHEMICAL AMALYSIS COMPORMS TO APPLICABLE SPECS: ASTM E415, DBL10129, LBL10130, ASTM E1019, LBL10158, 18510114, AND ASTM MIDES, IBL10184, 18510188, REDUBLIC REGISTERED CONCURS RESERV CENTURY THAT THE MATERIAL LISTED RESPONDENCE AND RESERVED AND TESTED IN ACCORDANCE NITH THE METHODS PRESCRIBED IN THE GOVERNING SPECIFICATIONS AND BASED UPON THE RESULTS OF SUCH IMSPECTION AND TESTING WAS BEEN APPROVED FOR COMPORMANCE TO THE SPECIFICATIONS. CERTIFICATE OF TESTS SHALL NOT BE REPRODUCED EXCEPT IN FULL. ALL TESTING WAS BEEN PERFORMED USING THE CURRENT REVISION OF THE TESTING SPECIFICATIONS. RECORDING OF FALSE, FICTITIOUS OR FRAUDOLEMS STATEMENTS OR ENTRIES ON THIS DOCUMENT MAY ME PUNISHED AS A PELONY UNDER PED STATUES TITLE 18 CHAPTER 47. THE MATERIAL WAS NOT EXPOSED TO MERCURY OR ANY METAL ALLOY THAT IS LIGHTED AT AMBIENT TEMPERATURE DURING PROCESSING OR WHILE IN OUR POSSESSION. NO WHLD OR MEED REPAIR WAS PERFORMED ON THIS MAYERIAL. R. A. SZELIGA MANAGER TROP. SERVICES BY JAWET K. HARTLINE P. A. Szeleja

Figure A-40. % in. x 1½ in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)



Figure A-41. 5% in. x 1½ in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

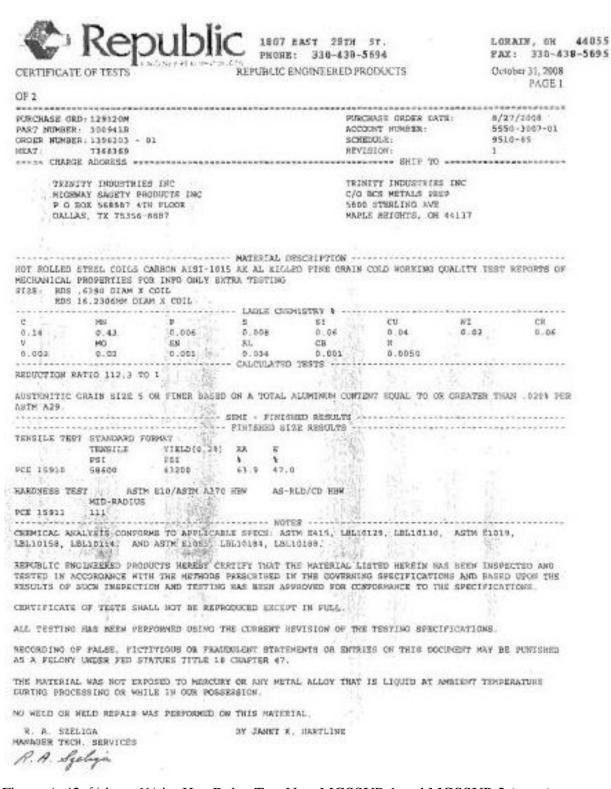


Figure A-42. % in. x 1½ in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

A25 E. O'Connor Lime, GH

Customer: MIDWEST MACH & SUPPLY CO.

P. O. BOX 81097

Sales Order: 1093497 Customer PO: 2030 BOL# 43073

Document# 1

Print Date: 6/30/08 Project: RESALE Shipped To: NE Use State: KS

LINCOLN, NE 68501-1097

Trinity Highway Products. LLC

Cartificate Of Compliance For Trinity Industries, Inc. ** SLOTTED RAIL TERMINAL **

NCHRP Report 350 Compliant

>	Pieces	Description	
MACHINERY	E reces		In the commence was priced on the price of the country was related
E	32	12/12/6/S SRT-1	
중	32	12/25'0/SPEC/S 8RT-2	
¥	32	3/16X12.5X16 CAB ANC BRKT	
		2" X 5 1/2" PIPE (LONG)	
83	64	60 TUBE SL/.188XSX6	
MIDWEST	64 32 32	5/8 X 6 X 8 BEARING PLATE	
E	32	12/BUTFER/ROLLED	
	32	CBL 3/4X6'6/DBL SWG/NOHWD	
	640	5/8" RD WASHER 1 3/4 OD	
	1,728	5/8" GR HEX NUT	
	1,152	5/8"X1.25" GR BOLT	
	256	5/8*X1.5* HEX BOLT A307	
	£54	5/6"X9.5" HEX BOLT A307	
0000	Upon delivery, a	, all materials subject to Trinity Highway Products , LLC Storage Stain Policy No. LG-002.	an an
	į.		
	AT I. STREET, US	USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT	
		RAIL MEETS AASHTO M-190. ALL STRUCTURAL STEEL MEETS ASTM A36	慰
		GALVANIZED MATERIAL CONFORMS WITH ASTM-123,	
		PLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERW	ISE STATED.
	ON ITS COMPLY	LY WITH ASTM A-363 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWIS	E STATED.
	M" DIA CABLE	LE 6X19 ZINC COATED SWAGED END AISI C 1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING	600 00 1000
	STRENGTH -49		
		Stimty of Allen. Syrom and Subscribed before merinis 30th day of June, 2008	la/
	MATE OF CHEO, CO.	Trinity Highway Products, LLC	a X
	ŷ.	Contified By:	COMB
	Stotary Public:	common by:	
	Samueleolen De	mine BLANCE	

Figure A-43. 5/8 in. x 91/2 in. Hex Bolt, Test No. MGSSYP-1

Southeastern Bolt & Screw, Inc. 1037 16th Avenue West Birmingham, AL 35204

Certification Of Compliance

DATE: September 28, 2010

CUSTOMER: Midwest Machinery & Supply RE: Purchase Order No. 2351

P.O. Box 703

SBS Shop Order No. 1093439

Milford, NE 68405

QTY	DESCRIPTION	SPECIFICATION	HEAT/LOT NO.
150	5/8-11 X 10 Hex Bolt	A307 Grade A	DL10101333405
100	5/8-11 X 12 Hex Bolt	A307 Grade A	1077688-1 DL10101383405 1077688-2
500	5/8-11 X 19 Hex Bolt	A307 Grade A	DL10101333405
150	3/4-10 X 8 Hex Bolt	A307 Grade A	1077688·3 11893810 1077688·4
500	7/8-9 X 14 Hex Bolt	A307 Grade A	DL1010333403
100	7/8-9 X 16 Hex Bolt	A807 Grade A	1077688-5 DL10103333403 1077688-6

Surface coating: A153 Grade C

We certify the materials listed meet or excess the latest ASTM specification as shown.

Jim Waddell Quality Assurance Manager

402 9101 3288

PAGE 01/10

POCCUNTING

0/87/2010 08:52 2052634851

80 0102/20/01

Figure A-44. $\frac{5}{8}$ in. x 10 in. Hex Bolt, Test No. MGSSYP-2

Mill Certification MUCCE 9/8/2010 NUCOR CORPORATION NUCOR STEEL SOUTH CAROLINA SOUTHEASTERN BOLT & SCREW INC 1037 167H AVE W PO BOX 788 BIRMINISHAM, AL 25201-0080 (205) 338-4551 Fax: (2005) 458-1627 Ship To: SCUTHEASTERN BOLT & SCHEWING 1937 ISTH AVE W PO BOX 759 BRMMINGHAM, AL 35201-0000 1205) 328-461 Fax: [205] 458-1827 Customer P.O. 95947 Sales Order | 120158 1 Product Group Merchant Bar Quality Part Number 300005624805740 Grade | ASTM A572/A572M-07 GR 50 TY2 / 30 Loc10 DL10103334 Size 5615 Round Heaf ID | DL 1010333405 Product .5815" Round 40" A572-55 B.L. Number | C1-537010 Description | A572-55 - ASTM A572-03 C1-223418 Load Number Photody cordly Matrix a material destinated hardining bean manufactured in accordance with the apportion one and example black status and that it satisfies those requirements Mn NI Mo Cu 0.007% 0.036% Yield 1: 83000psi (434MPa) Tensile 1: 91000psi (627MPa) Elengation: 18% in 8'(% in 203.3mm) Yield 2: 53000psi (434MPa) Elongation 19% in 6'(% in 203.3mm) Tensile 2: 9 (000psi (627MPa) WELDING OF WELD REPAIR WAS NOT PERFORMED ON THIS MATERIAL MELTED AND MANUFACTURED IN THE USA. MELTED AND MANUFACTURED IN THE USA. METHOD METHOD WELD IN THE PRODUCTION OF THIS MATERIAL MERCURY, RADITIAL, OR ALPHA SOURCE MATERIALS IN ANY FORM HAVE NOT BEEN USED IN THE PRODUCTION OF THIS MATERIAL James H. Blow JEMES 10 May 12, 2003 Page 2 of 3 Division Metalurgist 29:80 9792//9/91 DINT INCCOOM TORBERERE. 91/10 39Vd

Figure A-45. 5% in. x 10 in. Hex Bolt, Test No. MGSSYP-2 (cont.)



Figure A-46. 5% in. Hex Nut, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-47. 5% in. Flat Washer, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-48. 5% in. x 71/2 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-49. 7/8 in. x 8 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

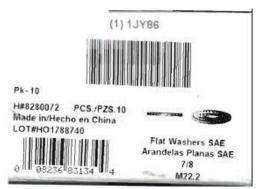


Figure A-50. 7/8 in. Flat Washer, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-51. Double Head Nail, Test Nos. MGSSYP-1 and MGSSYP-2

Appendix B. Vehicle Center of Gravity Determination

			Vehicle CG Determination		
		Weight	Vert CG		Vert M
VEHICLE	Equipment	(lb)	(in.)		(lb-in.)
+	Unbalasted Truck(Curb)	5130	28.14805	5	144399.5
+	Brake receivers/wires	6	49		294
+	Brake Frame	5	24		120
+	Brake Cylinder (Nitrogen)	22	26	6	572
+	Strobe/Brake Battery	6	31		186
+	Hub	26	14.4375	5	375.375
+	CG Plate (EDRs)	7.5	32	2	240
-	Battery	-37	41		-1517
-	Oil	-8	16	S	-128
-	Interior	-59	22	2	-1298
-	Fuel	-165	19		-3135
-	Coolant	-21	33.5	5	-703.5
-	Washer fluid	-3	34		-102
BALLAST	Water	100	19	9	1900
	Misc.				0
	Misc.				0
	·	· · · · · ·			•
				313208.5 496.125	141203.4
	TOTAL WEIGHT	5009.5	lb CG location (in.)	62.5229 0.099037	28.18712

Vehicle: 2270P/Ram 1500

Calculated Test Inertial Weight wheel base 140.5 CURRENT MASH Targets Difference Targets Test Inertial Weight (lb) 5000 ± 110 5009.5 9.5 Long CG (in.) 63 ± 4 62.52 -0.47710Lat CG (in.) NA 0.10 Vert CG (in.) ≥ 28 28.19

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

Left	Right
147	0 1386
109	7 1177
285	6 lb
227	<u>4</u> lb
513	0 lb
	Left 1470 109 2850 2270 5130

Test: MGSSYP-1

Actual test inertial weight (lb)							
(from scales)							
	Left	Right					
Front	1424	1374					
Rear	1090	1141					
FRONT	2798	lb					
REAR	2231	lb					
TOTAL	5029	lb					

Figure B-1. Vehicle Mass Distribution, Test No. MGSSYP-1

Test: MGSSYP-2 Vehicle: 1100C

Vehicle CG Determination

		Weight	Long CG	Lat CG	Long M	Lat M
VEHICLE	Equipment	(lb)	(in.)	(in.)	(lb-in.)	(lb-in.)
+	Unbalasted Car (curb)	2402	35.27841	0.211464	84738.75	507.9375
+	Brake receivers/wires	6	129.25	0	775.5	0
+	Brake Frame	5	27	-12	135	-60
+	Brake Cylinder	22	62.5	-15	1375	-330
+	Strobe Battery	6	56.75	0	340.5	0
+	Hub	20	0	-35.5	0	-710
+	CG Plate (EDRs)	7.5	39	0	292.5	0
+	DTS	18	63	9.5	1134	171
-	Battery	-29	-8.5	-15	246.5	435
-	Oil	-3	-6.5	10	19.5	-30
-	Interior	-38	40	0	-1520	0
-	Fuel	-6	81	-4	-486	24
-	Coolant	-8	-17	0	136	0
-	Washer fluid	-7	-14	22	98	-154
BALLAST	Water	25	81	-4	2025	-100
	Misc.				0	0
	Misc.				0	0

		TEMP	89310.25	-246.063
Estimated Total Weight	2420.5 lb	CG location	36.89744	

wheel base	95.75	in.
------------	-------	-----

MASH targets			
Test Inertial Wt (lb)	2420 (+/-)55	2442	22.0
Long CG (in.)	39 (+/-)4	37.09	-1.90766
Lateral CG (in.)	N/A	-0.02311	NA

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

CURB WEIGHT (lb)					
	Left Right				
Front		778		739	
Rear		414		471	
FRONT		1517	lh		
REAR		885			
TOTAL		2402	lb		

Dummy = 166lbs.

Dullilly - 100ibs.								
TEST INERTIAL WEIGHT (Ib)								
(from scales)								
	Left		Right					
Front		765		731				
Rear		457		489				
		•						
FRONT		1496	lb					
REAR		946	lb					
TOTAL		2442	lb					

Figure B-2. Vehicle Mass Distribution, Test No. MGSSYP-2

Appendix C. Dynamic and Static Soil Tests

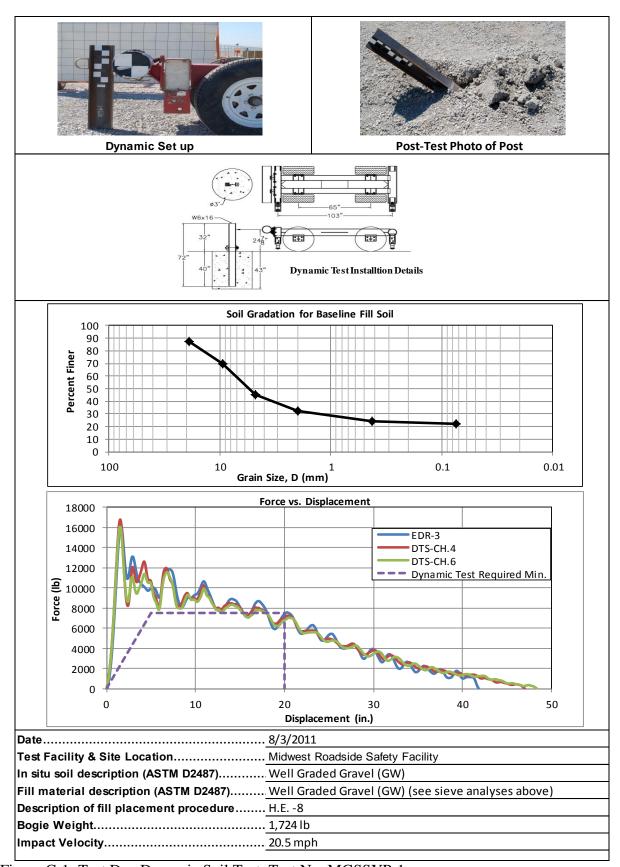


Figure C-1. Test Day Dynamic Soil Test, Test No. MGSSYP-1

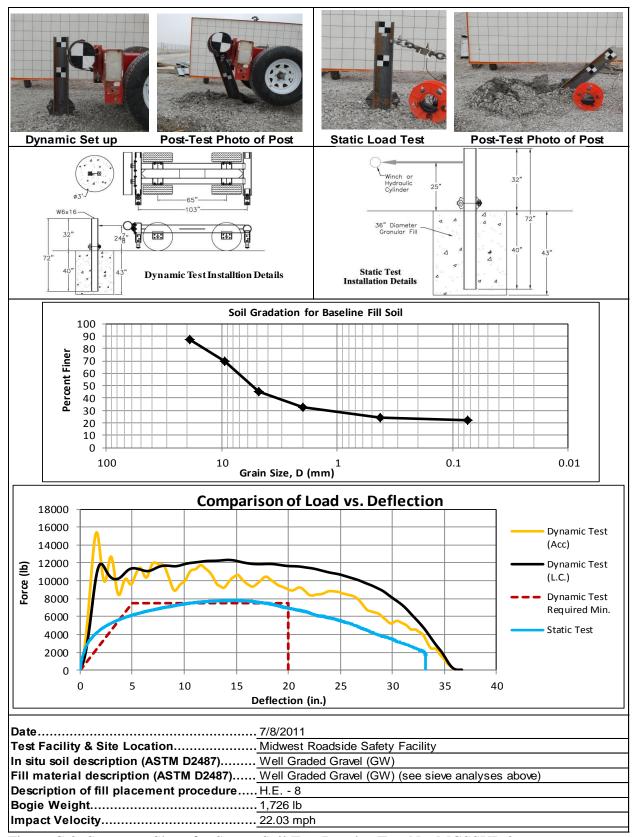


Figure C-2. Summary Sheet for Strong Soil Test Results, Test No. MGSSYP-2

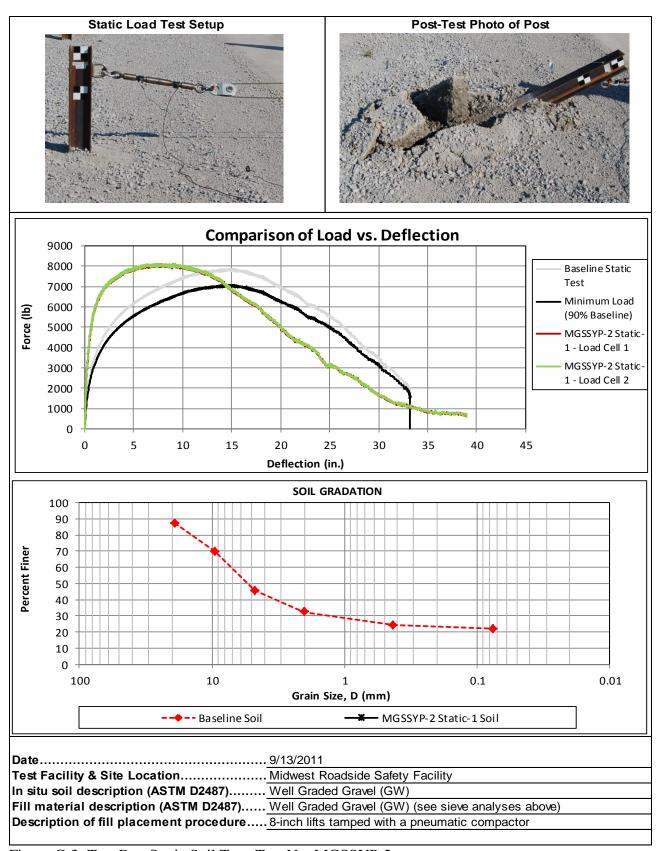


Figure C-3. Test Day Static Soil Test, Test No. MGSSYP-2

Appendix D. Vehicle Deformation Records

				PRE/POS ORPAN - S					
TEST: VEHICLE:	MGSSYP- 2270P/Ran					Note: If impenter nega		lriver side n	eed to
DOINT	X (in.)	Y	Z	X	Y'	Z'	ΔX	ΔY	ΔZ
POINT 1	(in.) 25	(in.) 12 3/4	(in.) -1	(in.) 25	(in.) 13	(in.) - 1/2	(in.) 0	(in.) 1/4	(in.) 1/2
2	30	19 1/4	-4	30	19 1/2	-3 3/4	0	1/4	1/4
3	30	25	-3	30	25	-2 1/2	0	0	1/2
5	28 3/4 21	29 10	-1 1/4 -1 1/4	28 1/2 21 1/4	29 10	-1 -1	- 1/4 1/4	0	1/4 1/4
6	22	14 1/2	-3 3/4	22	14 1/2	-3 1/2	0	0	1/4
7	23 1/2	21 1/2	-7	23 1/4	21 1/2	-7	- 1/4	0	0
8	23 3/4	29 1/4	-6 3/4	23 1/2	29 3/4	-6 1/2	- 1/4	1/2 0	1/4 1/4
10	12 1/2 18	3 3/4 9	-2 1/2 -2 3/4	12 1/2 18	3 3/4 9 1/4	-2 1/4 -2 3/4	0	1/4	0
11	19	13 3/4	-5 1/2	19	13 1/2	-5 1/4	0	- 1/4	1/4
12	20 1/2	18	-8 3/4	20 1/2	18	-8 1/2	0	0	1/4
13 14	20 3/4 20 3/4	24 1/4 28 3/4	-8 1/2 -8 1/2	20 1/2 20 3/4	24 28 3/4	-8 1/4 -8 1/4	- 1/4 0	- 1/4 0	1/4
15	11	28 3/4 6	-8 1/2 -2 3/4	20 3/4 11	28 3/4 6	-8 1/4 -2 1/2	0	0	1/4
16	16 3/4	15	-8 3/4	16 3/4	15	-8 3/4	0	0	0
17	16 3/4	21 1/2	-8 1/2	16 1/2	21 1/2	-8 1/2	- 1/4	0	0
18	17	29 1/4	-8 1/2	17	28 3/4	-8 1/4	0	- 1/2	1/4 1/4
19 20	8 11	6 1/2 13	-3 -8 3/4	8 11	6 1/4 12 3/4	-2 3/4 -8 1/2	0	- 1/4 - 1/4	1/4
21	11 3/4	19	-8 1/2	11 1/2	18	-8 1/4	- 1/4	-1	1/4
22	11 1/2	24 1/2	-8 1/4	11 1/4	24 1/4	-8	- 1/4	- 1/4	1/4
23	11 1/4	29 1/2	-8	11 1/4	29 1/4	-8	0	- 1/4	0
24 25	1 1/2 3/4	6 1/2 13 1/4	-2 1/2 -4 1/2	1 1/2 3/4	6 1/2 13 1/4	-2 1/4 -4 1/2	0	0	0
26	1	20 3/4	-4 1/4	1	20 1/2	-4	0	- 1/4	1/4
27	1	27 1/2	-4	1	27 3/4	-4	0	1/4	0
28							0	0	0
29 30							0	0	0
31							0	0	0
				DASH	BOARI)	2 3	4	
DOOR—					9 15 19 24 7	10 11 16	7 2 13 17 21 22 26 2	18	<u></u> D□□F

Figure D-1. Floor Pan Deformation Data – Set 1, Test No. MGSSYP-1

				PRE/POS ORPAN - S					
TEST: VEHICLE:	MGSSYP- 2270P/Rar		Note: If impact is on driver side need to enter negative number for Y						eed to
POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔΥ (in.)	ΔZ (in.)
1	40 3/4	19 1/4	- 1/4	40 1/2	19 3/4	0	- 1/4	1/2	1/4
2	46	25 1/2	-3 1/4	46	25 1/4	-3	0	- 1/4	1/4
3	46	31 3/4	-2	46	31 1/2	-1 1/2	0	- 1/4	1/2
5	44 1/2 37 1/4	35 3/4 16 3/4	0 - 3/4	44 37	35 1/2 16 1/4	1/4 - 1/2	- 1/2 - 1/4	- 1/4 - 1/2	1/4 1/4
6	38	21	-3	38	21	-2 3/4	0	0	1/4
7	39 1/2	28	-6 1/4	39 1/2	28	-6	0	0	1/4
8	39 3/4	35 1/2	-5 1/2	39 3/4	35 1/2	-5 1/2	0	0	0
9	28 1/2	10 1/2	-2 1/4	28 1/2	10 1/2	-2	0	0	1/4
10 11	34 35 1/4	16 20 1/4	-2 1/2 -4 3/4	34 35	16 20 1/4	-2 1/4 -4 1/2	0 - 1/4	0	1/4 1/4
12	36 3/4	24 1/4	-4 3/4 -8	36 1/2	24 1/2	- 4 1/2 -8	- 1/4	1/4	0
13	37	30 3/4	-7 1/2	36 3/4	30 3/4	-7 1/2	- 1/4	0	0
14	37	35 1/4	-7 1/4	37	35	-7	0	- 1/4	1/4
15	27	12 3/4	-2 1/4	27	12 3/4	-2 1/4	0	0	0
16 17	33 32 3/4	21 3/4 28 1/4	-8 1/4 -7 3/4	33 32 3/4	21 1/4 28	-8 1/4 -7 1/2	0	- 1/2 - 1/4	1/4
18	32 3/4	35 1/4	-7 3/4 -7 1/4	32 3/4	35	-7 1/2 -7	- 1/4	- 1/4	1/4
19	24 1/4	13 1/2	-2 1/2	24	13 1/2	-2 1/4	- 1/4	0	1/4
20	27 1/2	19 1/4	-8	27	18 3/4	-8	- 1/2	- 1/2	0
21	27 3/4	25 1/2	-7 3/4	27 1/2	25	-7 1/2	- 1/4	- 1/2	1/4
22	27 1/2	31 1/4	-7 1/4	27 1/2	31	-7	0	- 1/4 - 1/2	1/4 1/4
23 24	27 1/2 17 1/2	36 1/2 13 1/4	-7 -2	27 1/4 17 1/2	36 13 1/4	-6 3/4 -1 3/4	- 1/4 0	0	1/4
25	17 1/2	20 1/4	-4	16 3/4	20	-3 3/4	- 1/4	- 1/4	1/4
26	17	27 1/2	-3 1/4	17	27 1/2	-3 1/4	0	0	0
27	17	34 1/2	-3	17	34 1/4	-2 3/4	0	- 1/4	1/4
28							0	0	0
29 30							0	0	0
31							0	0	0
				DASH	HBOARI)	2		
DOOR—					× V		1 6 12 11 16 20 21) DOO
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Figure D-2. Floor Pan Deformation Data – Set 2, Test No. MGSSYP-1

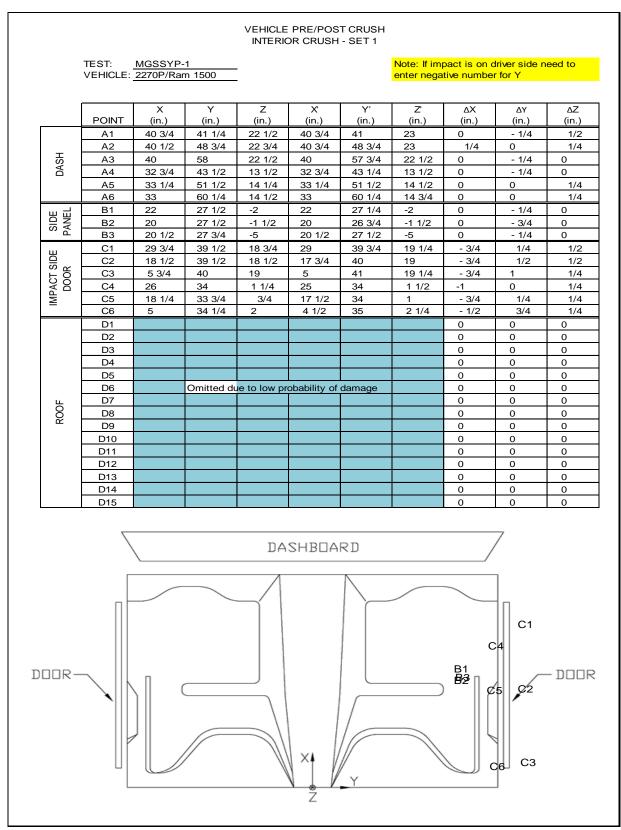


Figure D-3. Occupant Compartment Deformation Data – Set 1, Test No. MGSSYP-1

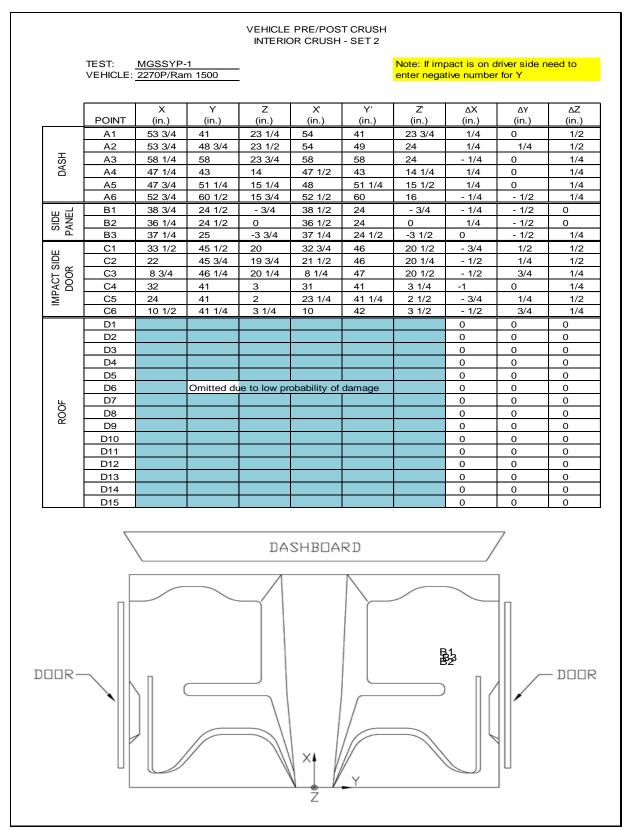


Figure D-4. Occupant Compartment Deformation Data – Set 2, Test No. MGSSYP-1

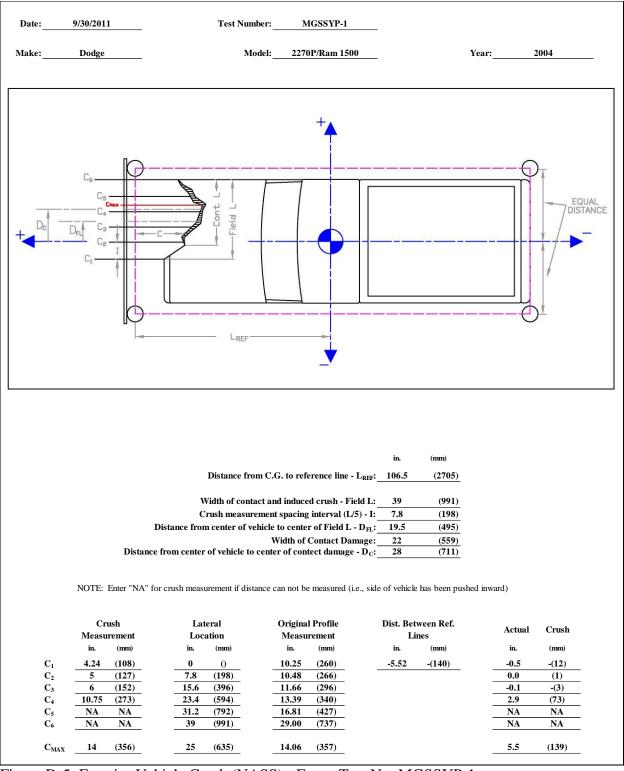


Figure D-5. Exterior Vehicle Crush (NASS) - Front, Test No. MGSSYP-1

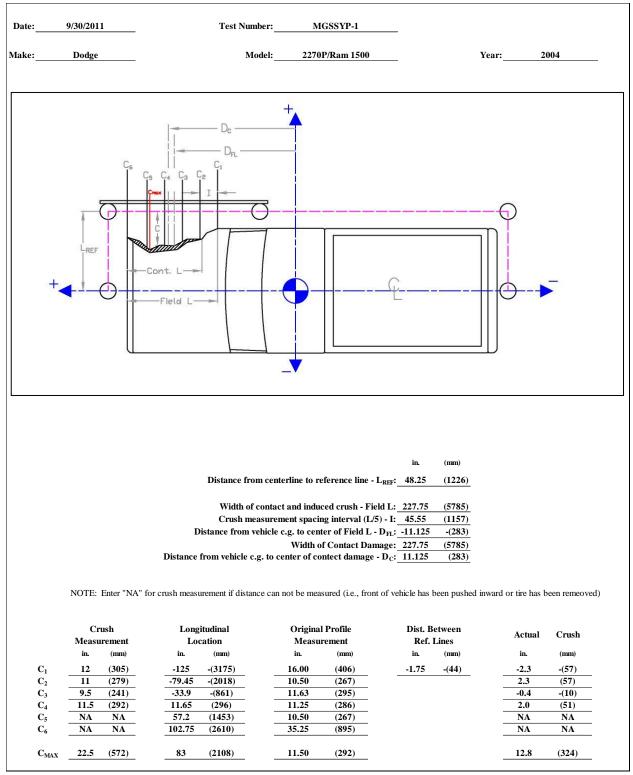


Figure D-6. Exterior Vehicle Crush (NASS) - Side, Test No. MGSSYP-1

			_	PRE/POS ORPAN - S						
TEST: MGSSYP-2						Note: If impact is on driver side need to				
VEHICLE:	1100C					enter nega	<mark>tive numbe</mark>	r for Y		
	Х	Y	Z	X	Y'	Z'	ΔΧ	ΔΥ	ΔΖ	
POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	
F1 2	28 3/4 30	3 3/4 11 1/4	- 1/4 -1	28 1/2 29 1/2	4 1/4 11	0 - 3/4	- 1/4 - 1/2	1/2 - 1/4	1/4 1/4	
3	28 1/2	16	-1 1/2	28 1/4	16	-1 1/2	- 1/4	0	0	
4	25 1/2	21 1/2	0	25 1/4	21 3/4	0	- 1/4	1/4	0	
5 6	24 3/4 27	8 3/4	-3 1/4 -3 3/4	24 3/4 27	4 1/4 8 3/4	-3 1/4 -3 1/2	0	1/4 0	1/4	
7	26 1/2	13	-3 3/4	26 1/2	13 1/4	-3 1/2	0	1/4	0	
8	24 3/4	19 1/4	-3	24 3/4	19 3/4	-3	0	1/2	0	
9	22	5 1/2	-6	22	5 1/2	-6 1/4	0	0	- 1/4	
10	22 1/2 22 1/4	11 16	-5 1/2 -5 1/2	22 1/2 22 1/2	11 1/4 16 1/4	-5 1/2 -5 1/2	0 1/4	1/4 1/4	0	
12	21 3/4	21	-5 1/2 -6	21 3/4	20 3/4	-5 1/2 -6	0	- 1/4	0	
13	17 1/2	5 1/4	-6 1/4	17 1/2	5 1/2	-6 1/4	0	1/4	0	
14	18	11 1/4	-5 3/4	18	11 1/2	-5 3/4	0	1/4	0	
15	19	15 3/4	-6	19	15 3/4	-6	0	0	0	
16 17	18 1/2 13	21 3	-6 -6	18 1/2 12 3/4	21 3	-6 -6	0 - 1/4	0	0	
18	14	9 3/4	-6	14	9 1/2	-6	0	- 1/4	0	
19	14 1/2	14 1/2	-5 3/4	14 1/2	14 1/2	-5 3/4	0	0	0	
20	15	20 3/4	-6	15	20 3/4	-6	0	0	0	
21 22	8 1/4 7 3/4	5 9 3/4	-6 1/4 -6 1/4	8 1/4 7 3/4	5 1/4 9 1/2	-6 1/4 -6 1/4	0	1/4 - 1/4	0	
23	7 1/4	14 1/2	-6	7 1/4	14 3/4	-6	0	1/4	0	
24	8 1/4	19 3/4	-6	8 1/4	20	-6 1/4	0	1/4	- 1/4	
25 26	1 1/2 1	3 3/4 8 1/2	-2 3/4 -3 1/2	1 1/2 1	3 3/4 8 1/2	-2 3/4 -3 1/2	0	0	0	
27	1	13 3/4	-3 1/2	1 1/4	13 3/4	-3 3/4	1/4	0	- 1/4	
28	1 1/2	20 1/2	-3 1/4	1 1/2	20 1/2	-3 1/4	0	0	0	
29							0	0	0	
30 31							0	0	0	
							0	0	0	
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Figure D-7. Floor Pan Deformation Data – Set 1, Test No. MGSSYP-2

				PRE/POS ORPAN - S						
TEST: MGSSYP-2 VEHICLE: 1100C			Note: If impact is on driver side need to enter negative number for Y							
POINT	X (in.)	Y (in.)	Z (in.)	X' (in.)	Y' (in.)	Z' (in.)	ΔX (in.)	ΔΥ (in.)	ΔZ (in.)	
1	37 1/4	9 3/4	0	37 1/4	9 3/4	0	0	0	0	
2	38 1/2	16 3/4	-1	38 1/4	16 1/2	- 3/4	- 1/4	- 1/4	1/4	
<u>3</u>	37 1/4 34	21 1/2 27 1/4	-1 3/4 - 1/4	36 3/4	21 1/2	-1 1/2 0	- 1/2	0 - 1/2	1/4 1/4	
5	33 1/4	8 3/4	- 1/4	33 3/4 33 1/2	26 3/4 9 1/2	-3	- 1/4 1/4	3/4	0	
6	35 3/4	14 1/4	-3 1/2	35 3/4	14 1/2	-3 1/2	0	1/4	0	
7	35 1/4	18 1/2	-4	35 1/4	19	-3 3/4	0	1/2	1/4	
8	33 1/2	25 1/4	-3 1/4	33 1/2	24 3/4	-3 1/2	0	- 1/2	- 1/4	
9	31 31 1/4	10 1/4 15 3/4	-6 -5 1/2	30 3/4 31 1/4	10 3/4 16 1/4	-6 -5 1/2	- 1/4 0	1/2 1/2	0	
11	31 1/4	21	-5 3/4	31 1/4	21 1/2	-5 3/4	0	1/2	0	
12	30 1/2	26 1/4	-6 1/4	30 1/2	26	-6 1/4	0	- 1/4	0	
13	26 1/4	10 1/4	-6	26 1/4	10 1/2	-6	0	1/4	0	
14 15	27	16 1/2	-5 3/4	26 3/4	16 3/4	-5 3/4	- 1/4	1/4	0	
16	28 27 1/4	20 3/4 26 1/2	-6 -6 1/4	28 27 1/4	21 1/4 26 1/2	-6 -6 1/4	0	1/2 0	0	
17	21 1/2	8	-6	21 1/2	8	-6	0	0	0	
18	22 3/4	14 3/4	-6 1/4	22 3/4	14 3/4	-6 1/4	0	0	0	
19	23 1/2	20	-6	23 1/2	20 1/2	-6	0	1/2	0	
20	23 3/4	26 1/4	-6 1/2	24	26	-6 1/2	1/4	- 1/4	0	
21 22	17 16 3/4	10 1/4 14 1/2	-6 1/4 -6 1/2	17 16 3/4	10 3/4 15	-6 1/4 -6 1/2	0	1/2 1/2	0	
23	16 3/4	19 1/2	-6 1/4	16 1/4	20	-6 1/4	1/4	1/2	0	
24	17 1/4	25 1/4	-6 1/2	17 1/4	25 1/2	-6 1/2	0	1/4	0	
25	10 1/4	9	-3	10 1/4	9	-2 3/4	0	0	1/4	
26	9 3/4	14	-3 3/4	10	13 3/4	-3 3/4	1/4	- 1/4	0	
27 28	10 10 1/4	19 1/4 25 3/4	-4 -3 1/2	10 10 1/2	19 1/4 26	-4 -3 1/2	1/4	0 1/4	0	
29	10 17 1	20 0/ 1	0 1/2	10 1/2	20	0 1/2	0	0	0	
30							0	0	0	
31							0	0	0	
DOOR—					1	1 6	3 8 4 11 12 15 16		DC DC)OR

Figure D-8. Floor Pan Deformation Data – Set 2, Test No. MGSSYP-2

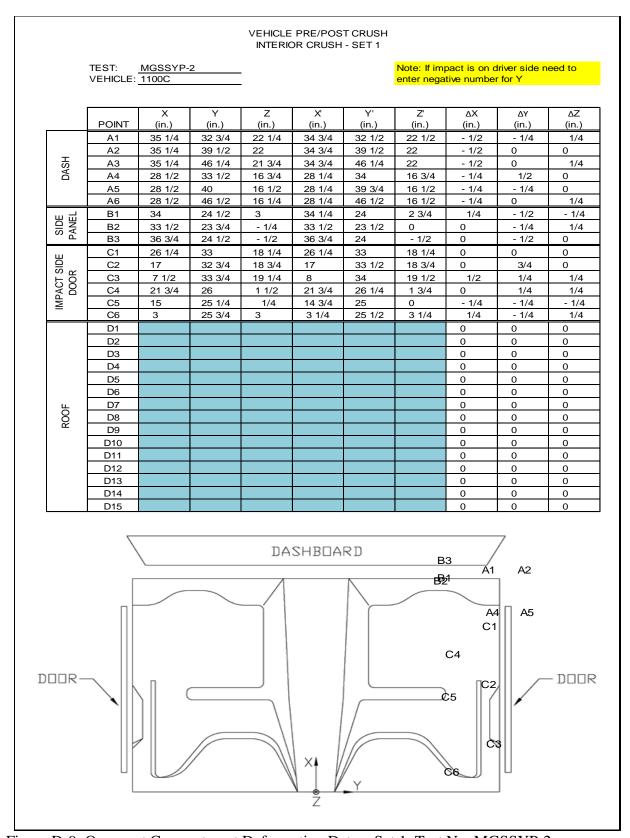


Figure D-9. Occupant Compartment Deformation Data – Set 1, Test No. MGSSYP-2

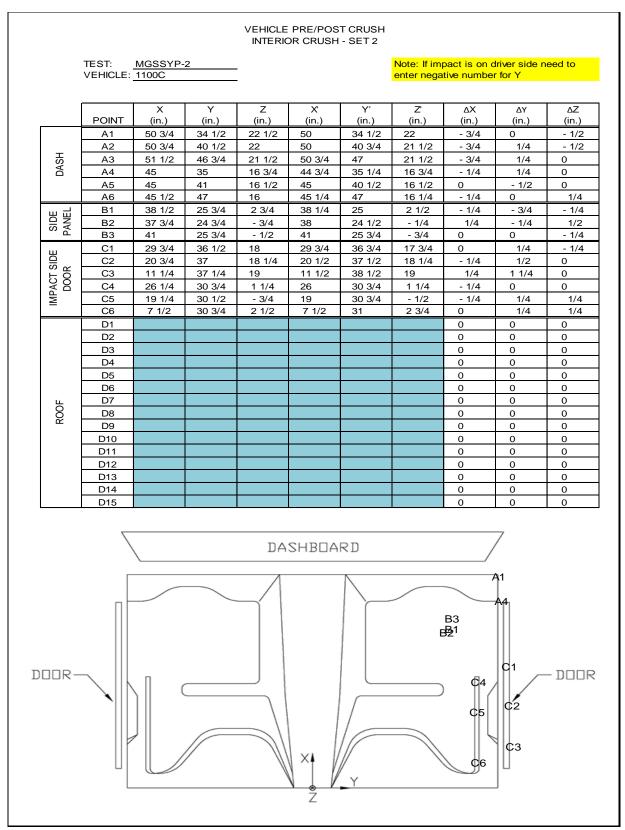


Figure D-10. Occupant Compartment Deformation Data – Set 2, Test No. MGSSYP-2

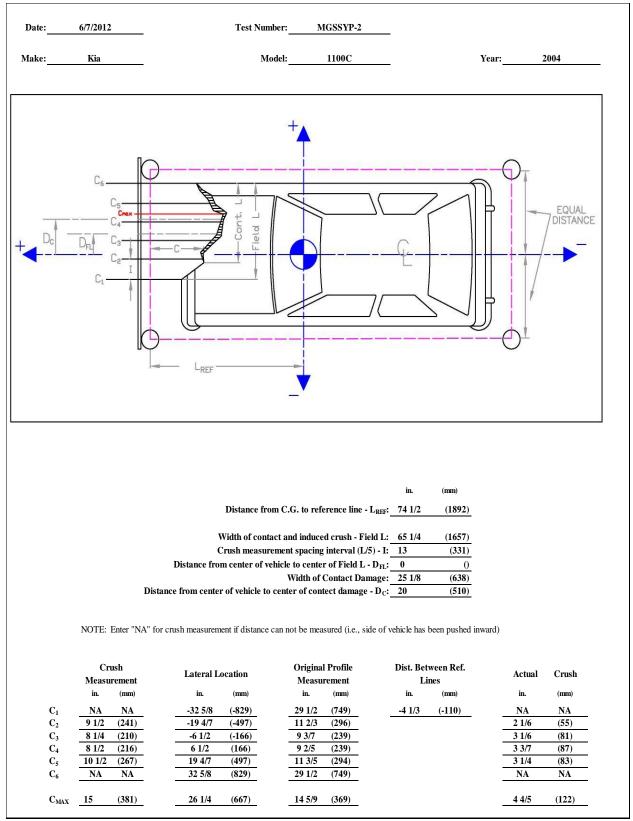


Figure D-11. Exterior Vehicle Crush (NASS) - Front, Test No. MGSSYP-2

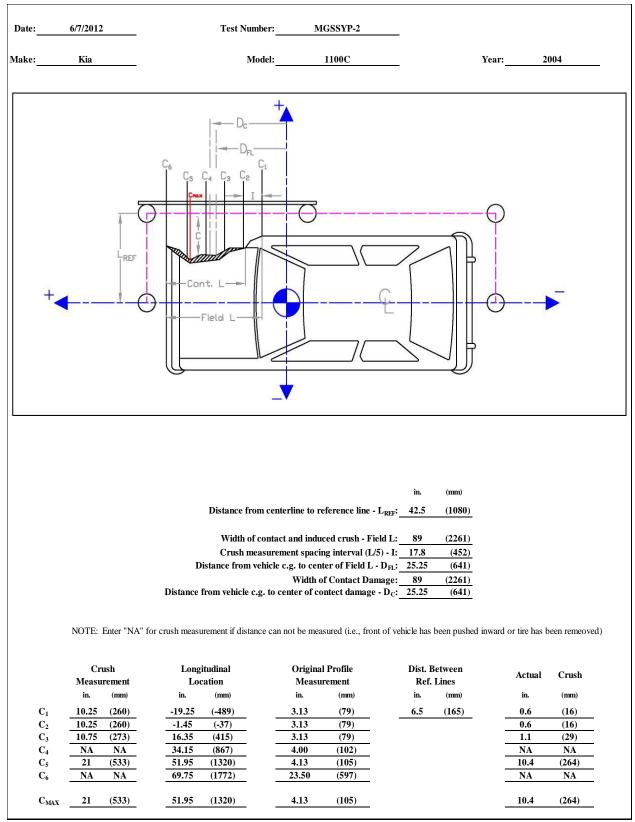


Figure D-12. Exterior Vehicle Crush (NASS) - Side, Test No. MGSSYP-2

Appendix E. Accelerometer and Rate Transducer Data Plots, Test No. MGSSYP-1

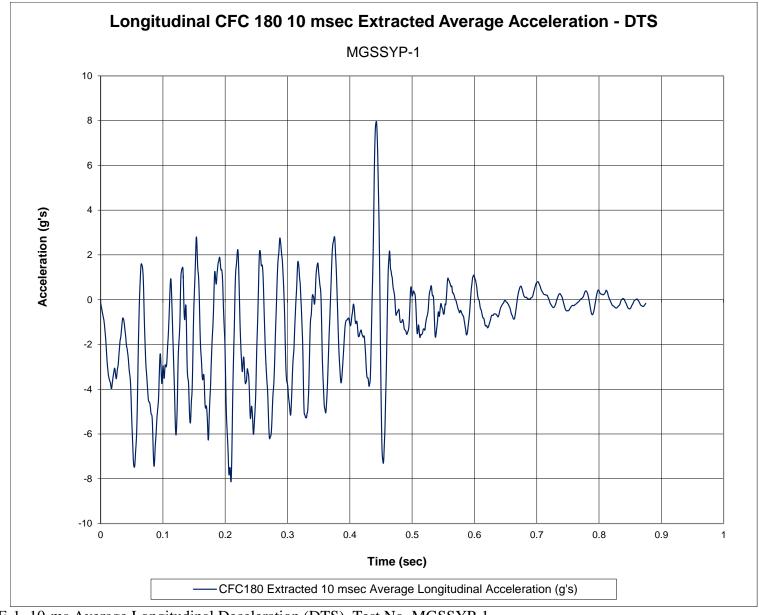


Figure E-1. 10-ms Average Longitudinal Deceleration (DTS), Test No. MGSSYP-1

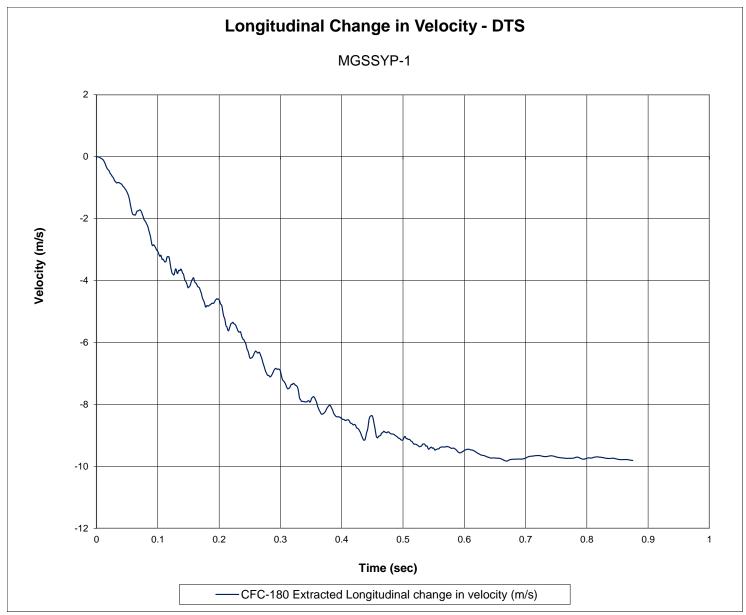


Figure E-2. Longitudinal Occupant Impact Velocity (DTS), Test No. MGSSYP-1

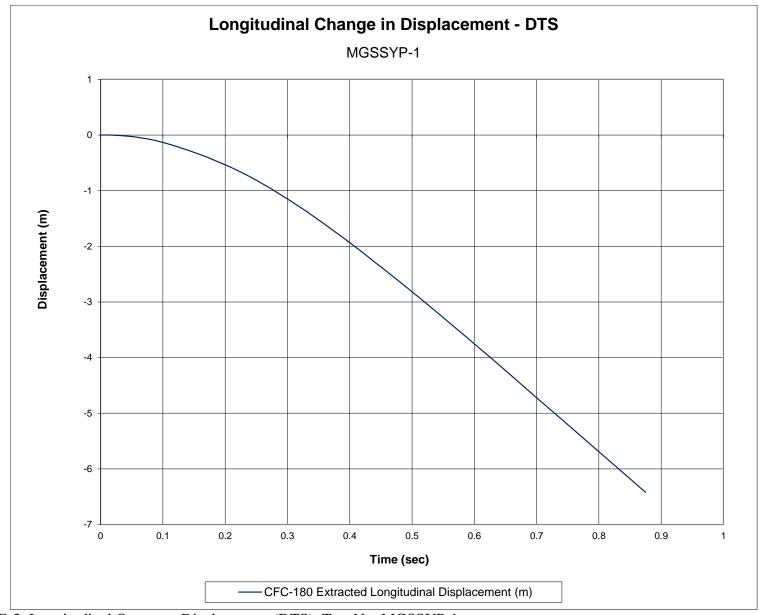


Figure E-3. Longitudinal Occupant Displacement (DTS), Test No. MGSSYP-1

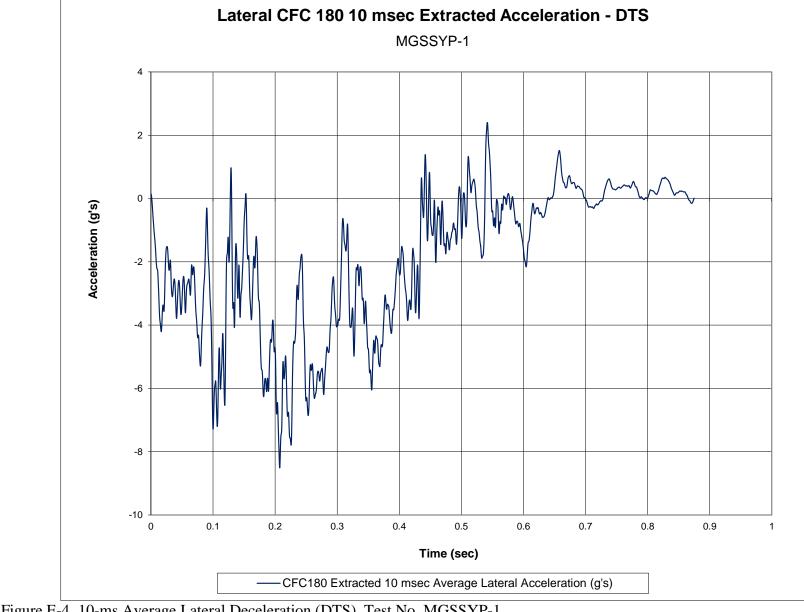


Figure E-4. 10-ms Average Lateral Deceleration (DTS), Test No. MGSSYP-1

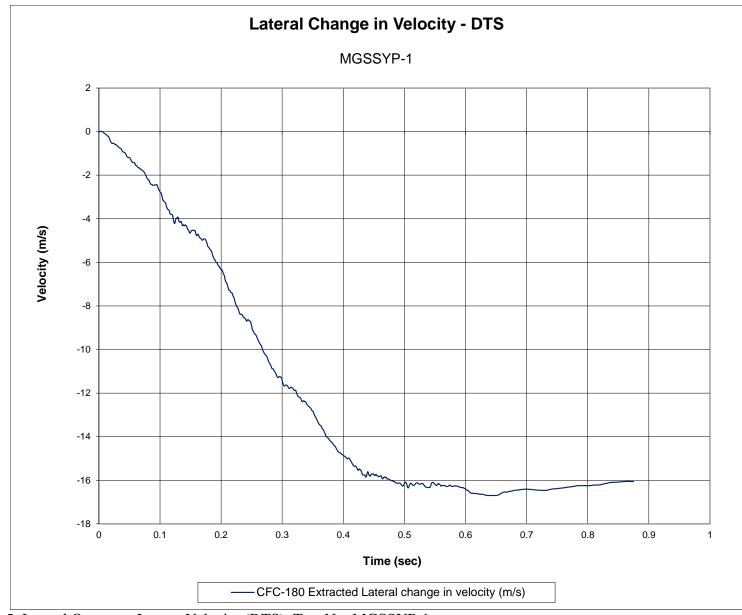


Figure E-5. Lateral Occupant Impact Velocity (DTS), Test No. MGSSYP-1

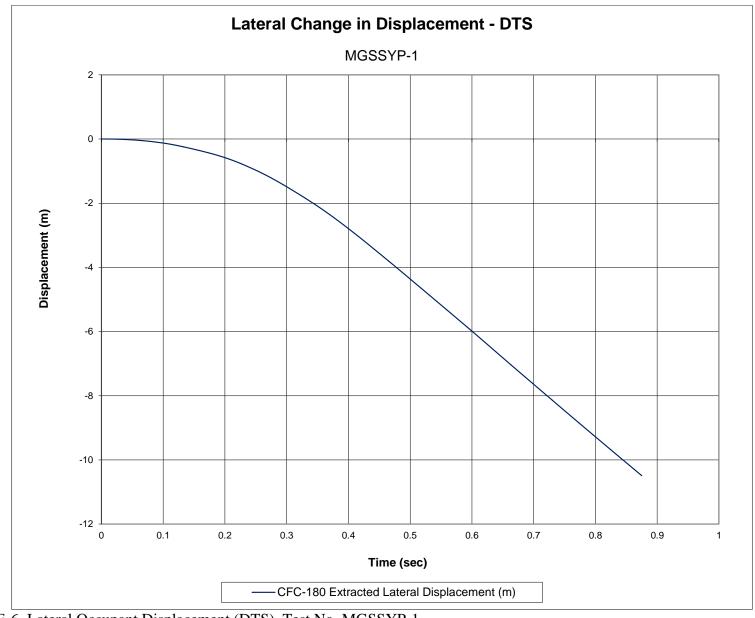
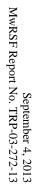


Figure E-6. Lateral Occupant Displacement (DTS), Test No. MGSSYP-1



Figure E-7. Vehicle Angular Displacements (DTS), Test No. MGSSYP-1



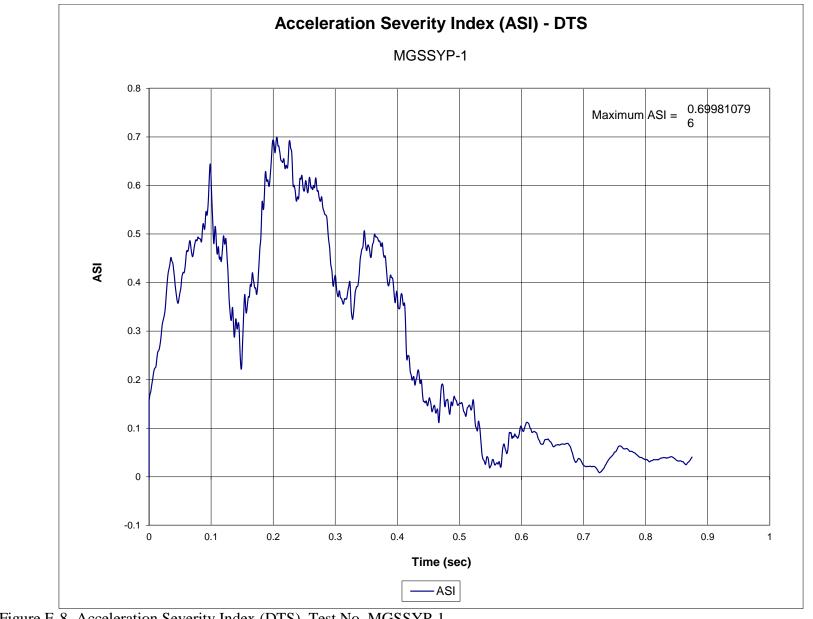


Figure E-8. Acceleration Severity Index (DTS), Test No. MGSSYP-1

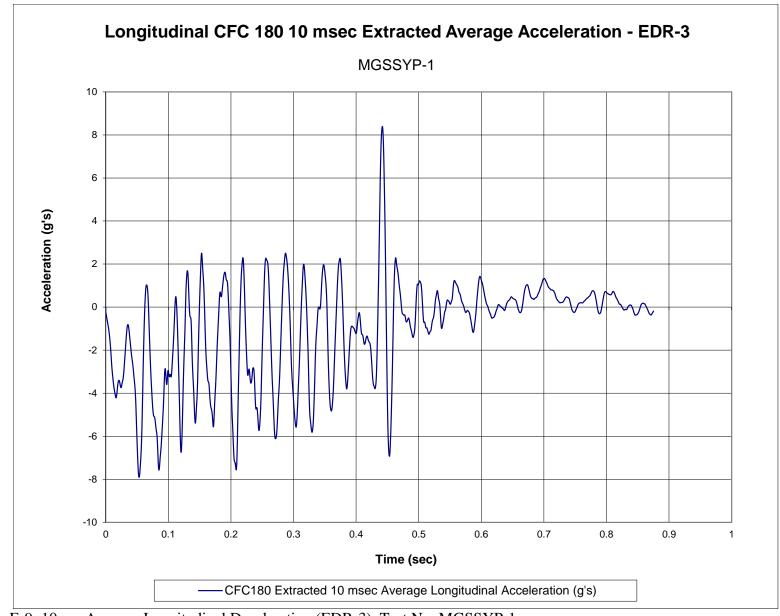


Figure E-9. 10-ms Average Longitudinal Deceleration (EDR-3), Test No. MGSSYP-1



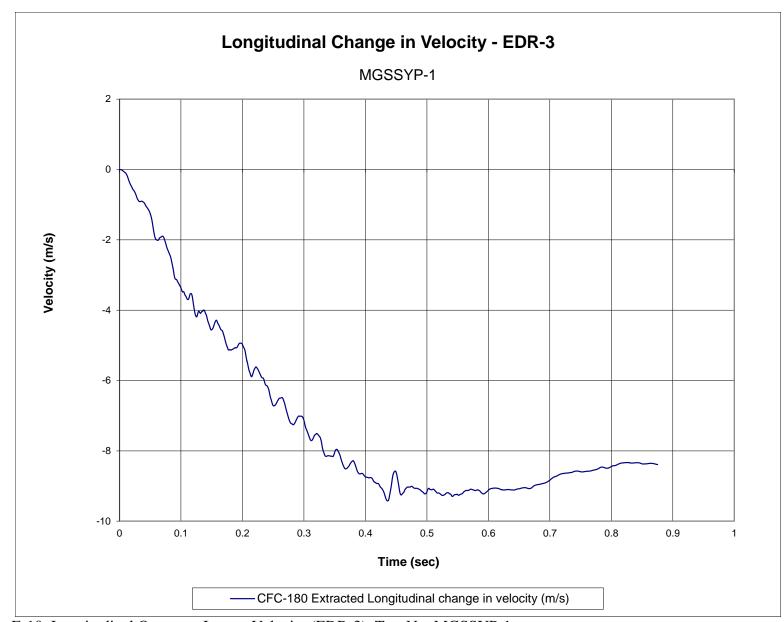


Figure E-10. Longitudinal Occupant Impact Velocity (EDR-3), Test No. MGSSYP-1

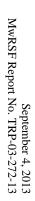




Figure E-11. Longitudinal Occupant Displacement (EDR-3), Test No. MGSSYP-1

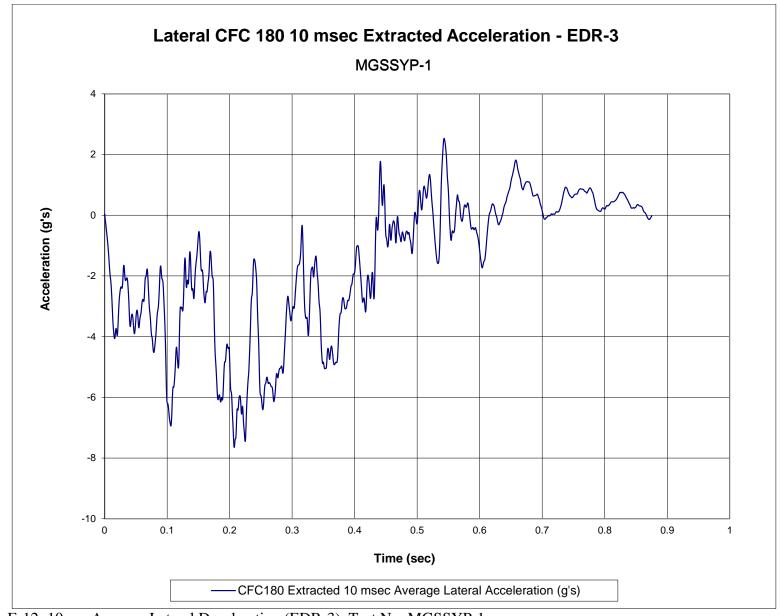
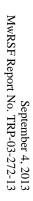


Figure E-12. 10-ms Average Lateral Deceleration (EDR-3), Test No. MGSSYP-1



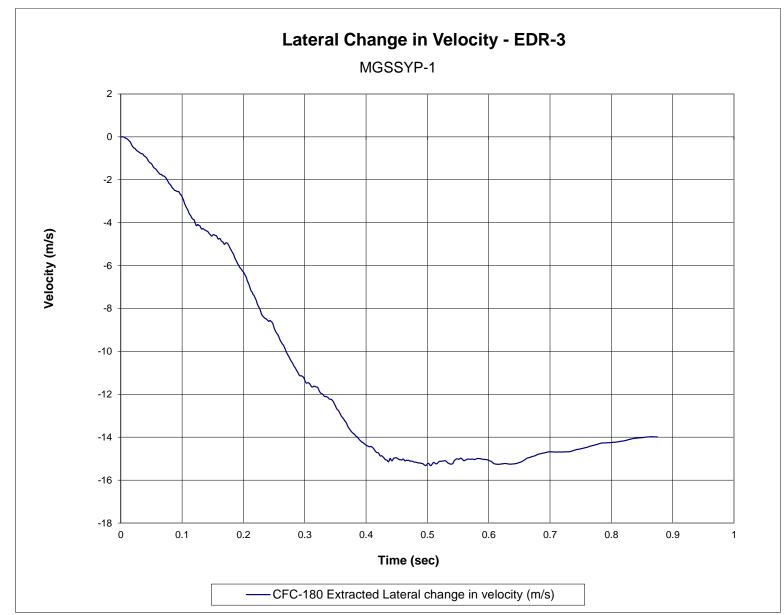


Figure E-13. Lateral Occupant Impact Velocity (EDR-3), Test No. MGSSYP-1





Figure E-14. Lateral Occupant Displacement (EDR-3), Test No. MGSSYP-1



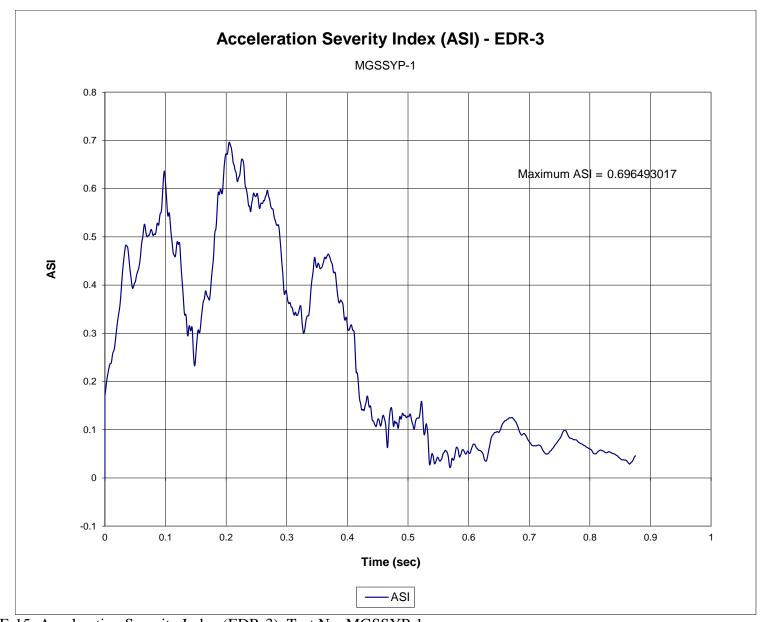
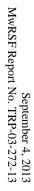


Figure E-15. Acceleration Severity Index (EDR-3), Test No. MGSSYP-1

Appendix F. Accelerometer and Rate Transducer Data Plots, Test No. MGSSYP-2



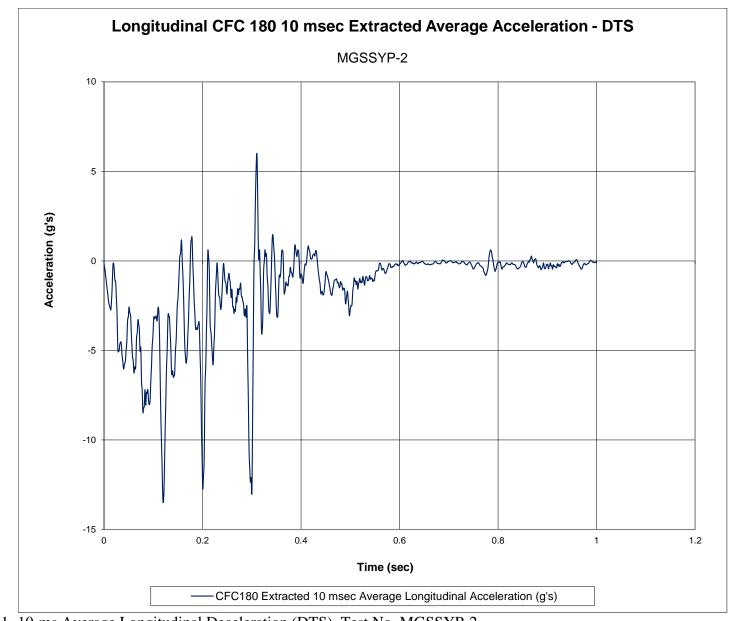


Figure F-1. 10-ms Average Longitudinal Deceleration (DTS), Test No. MGSSYP-2

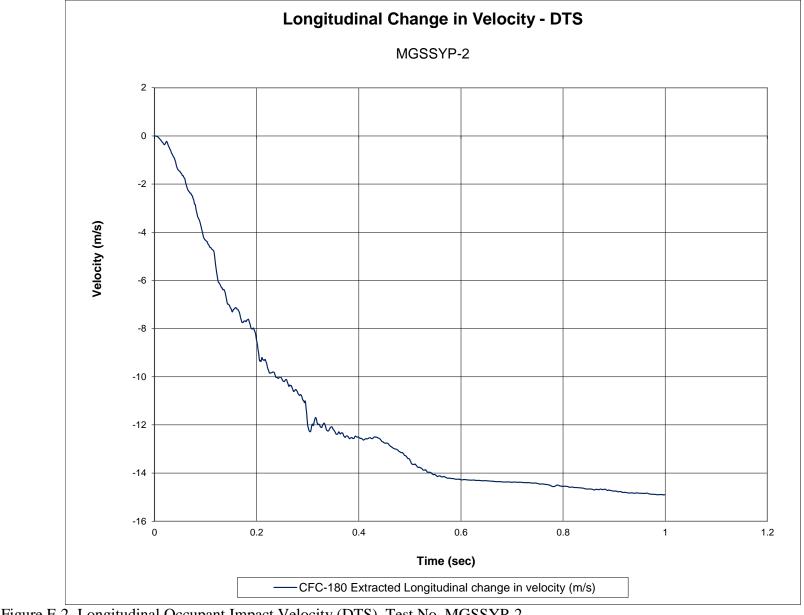


Figure F-2. Longitudinal Occupant Impact Velocity (DTS), Test No. MGSSYP-2

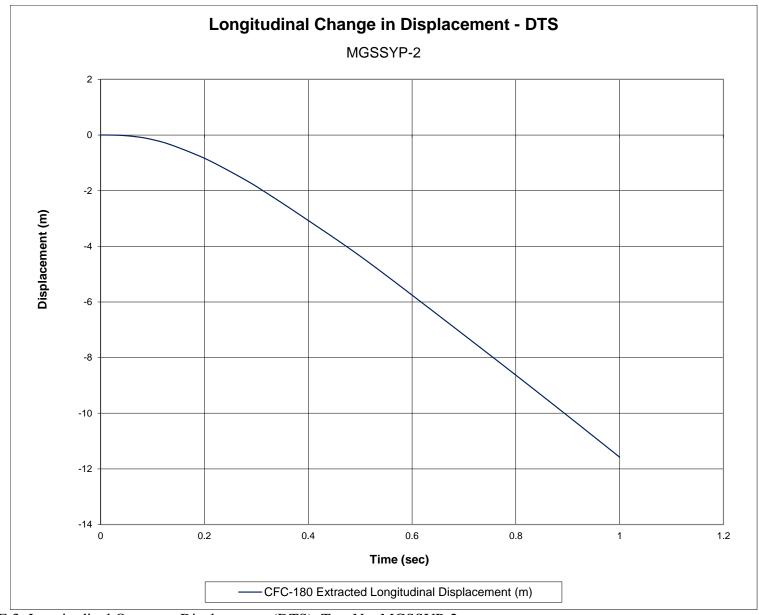


Figure F-3. Longitudinal Occupant Displacement (DTS), Test No. MGSSYP-2



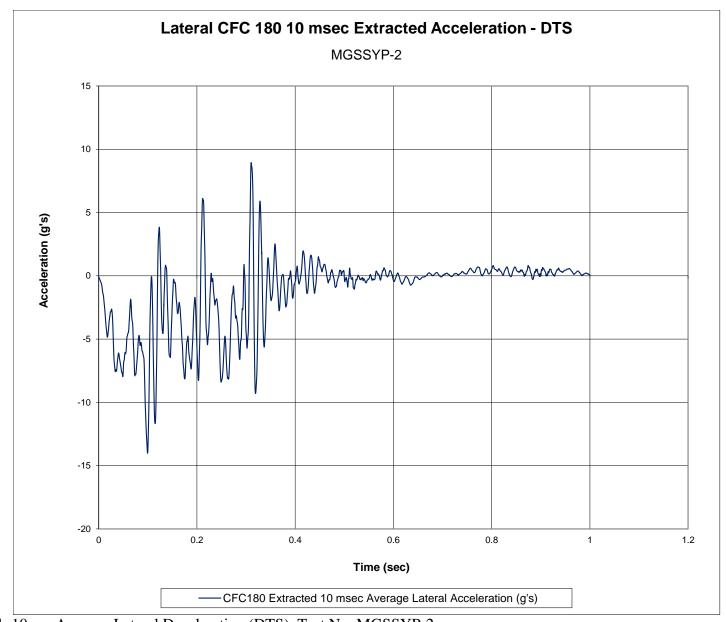
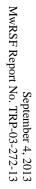


Figure F-4. 10-ms Average Lateral Deceleration (DTS), Test No. MGSSYP-2



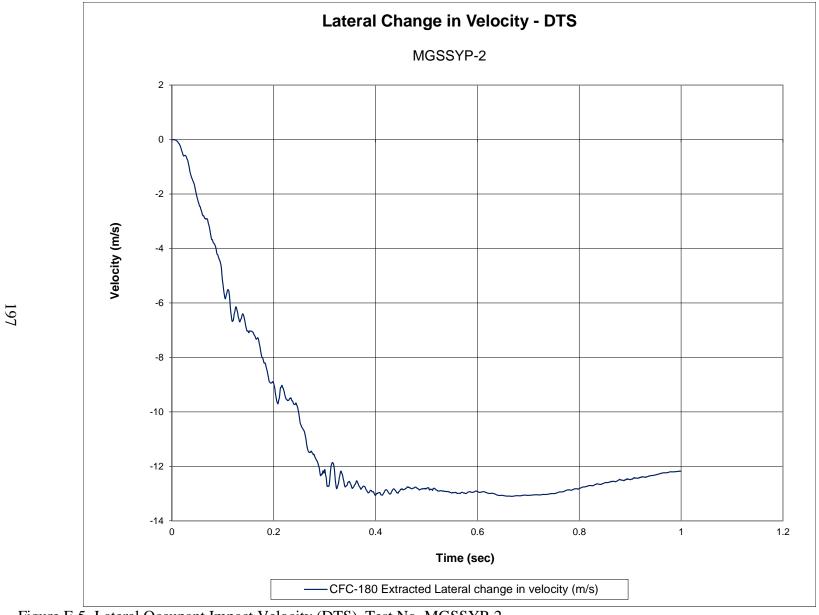


Figure F-5. Lateral Occupant Impact Velocity (DTS), Test No. MGSSYP-2



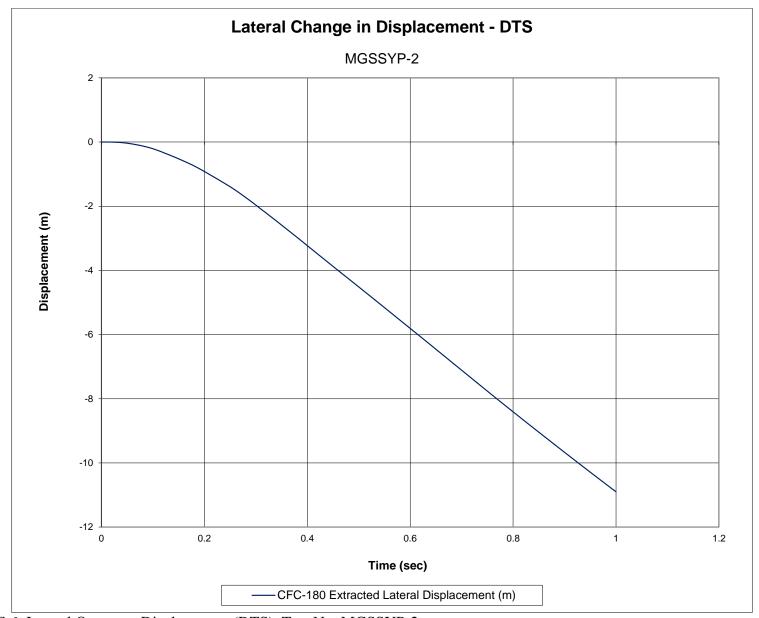
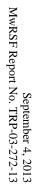


Figure F-6. Lateral Occupant Displacement (DTS), Test No. MGSSYP-2

Figure F-7. Vehicular Angular Displacement (DTS), Test No. MGSSYP-2



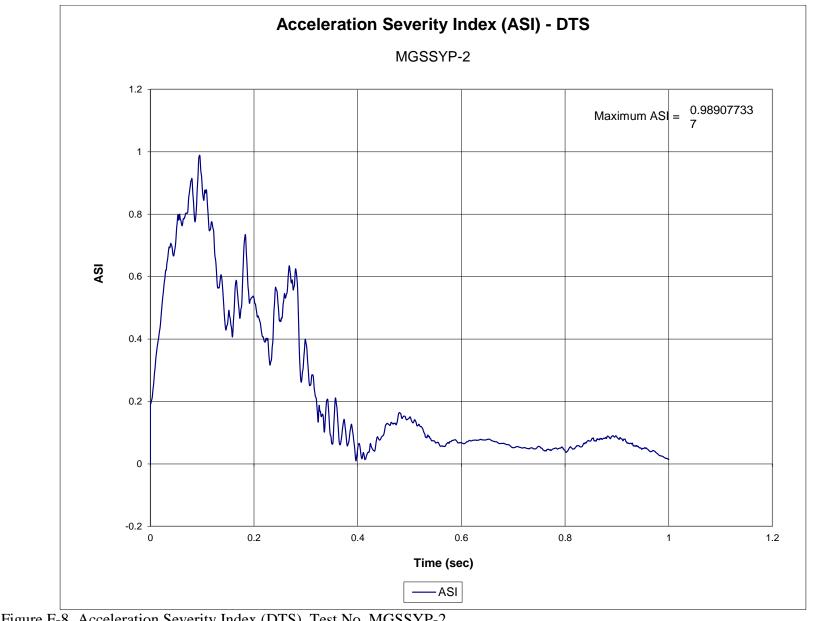


Figure F-8. Acceleration Severity Index (DTS), Test No. MGSSYP-2

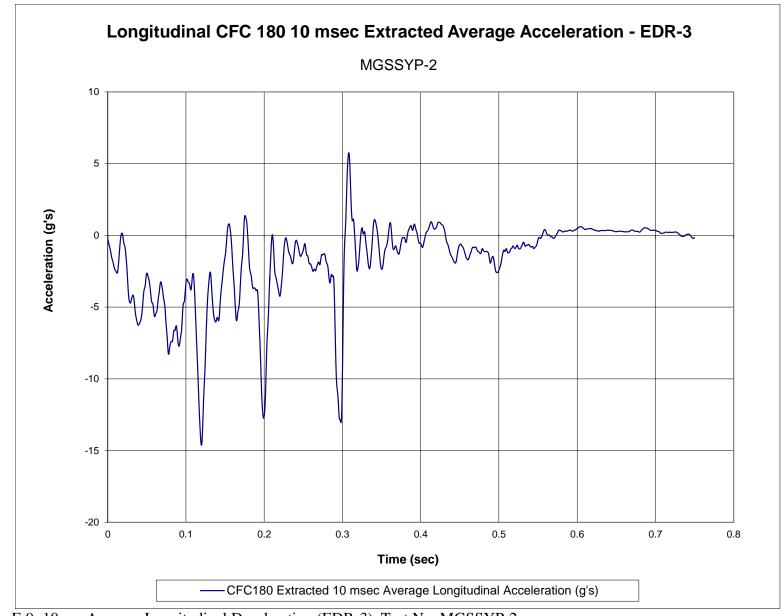


Figure F-9. 10-ms Average Longitudinal Deceleration (EDR-3), Test No. MGSSYP-2

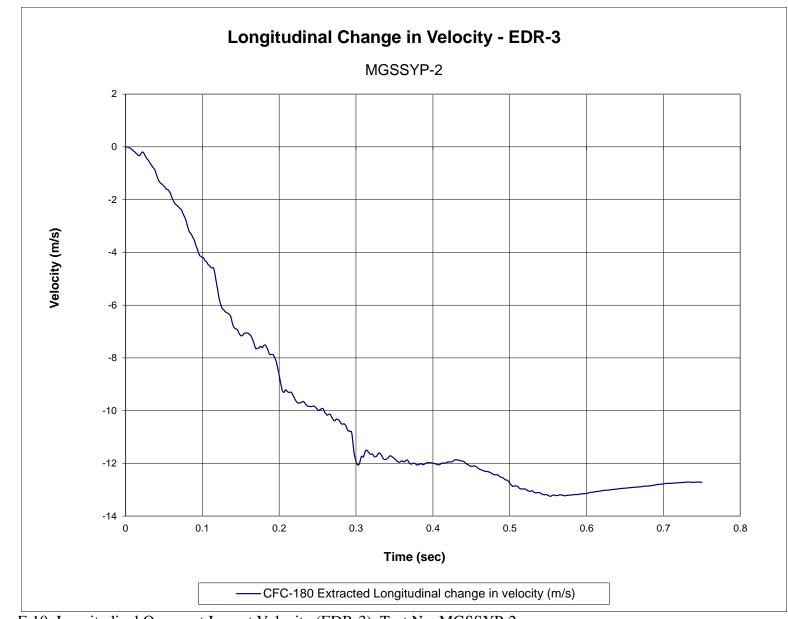


Figure F-10. Longitudinal Occupant Impact Velocity (EDR-3), Test No. MGSSYP-2

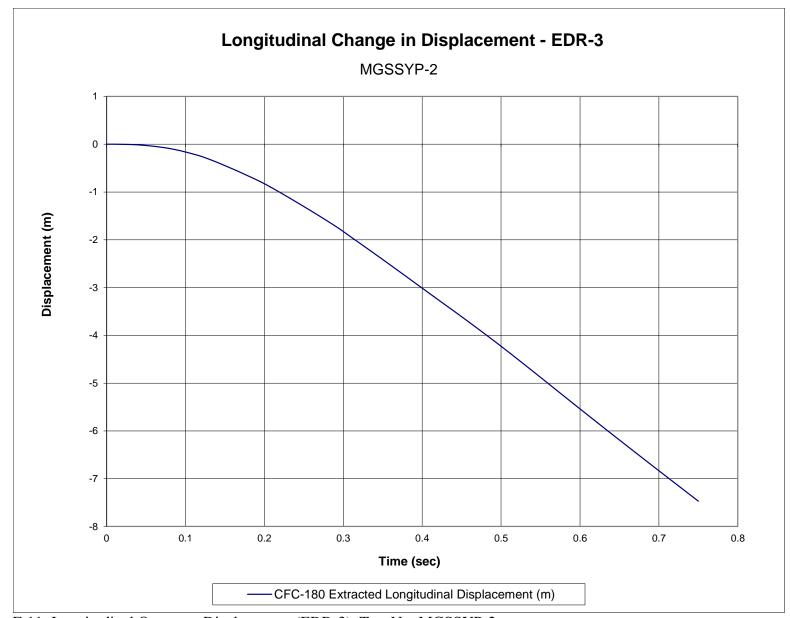


Figure F-11. Longitudinal Occupant Displacement (EDR-3), Test No. MGSSYP-2

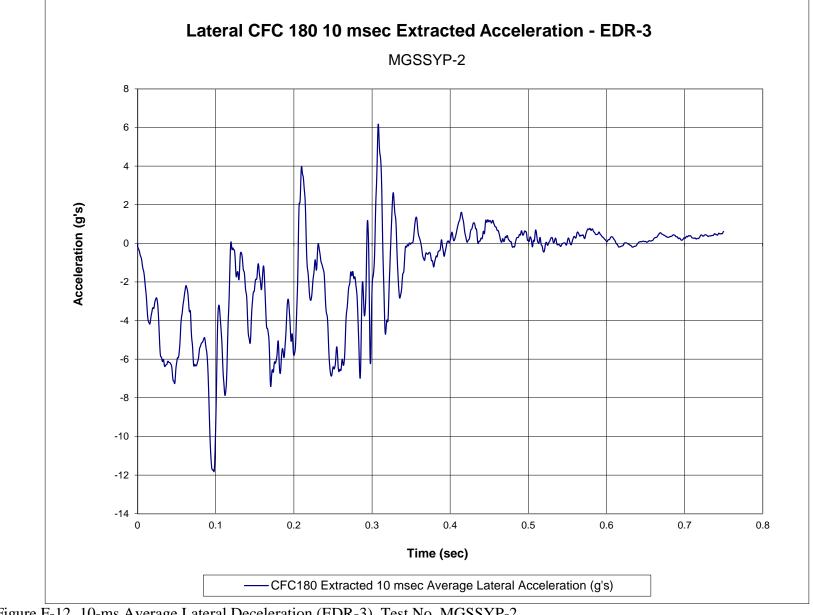


Figure F-12. 10-ms Average Lateral Deceleration (EDR-3), Test No. MGSSYP-2

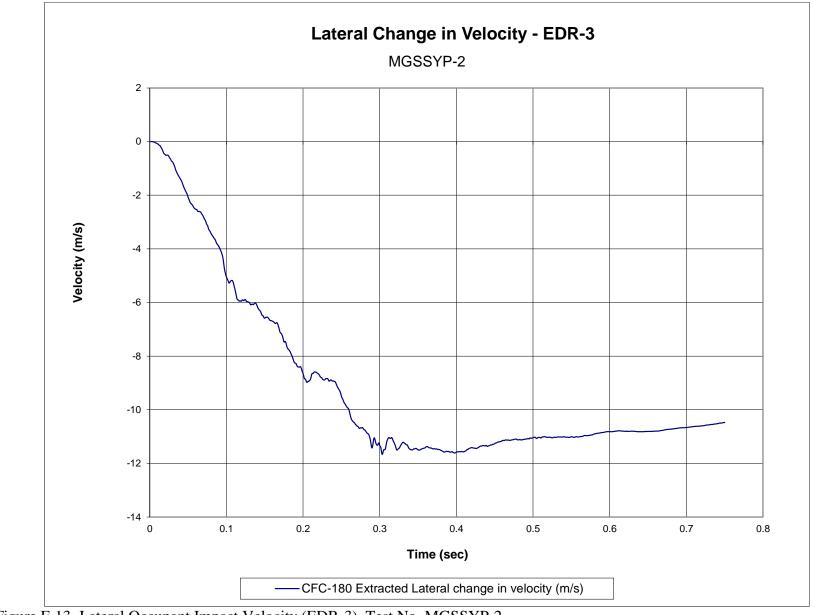


Figure F-13. Lateral Occupant Impact Velocity (EDR-3), Test No. MGSSYP-2



Figure F-14. Lateral Occupant Displacement (EDR-3), Test No. MGSSYP-2

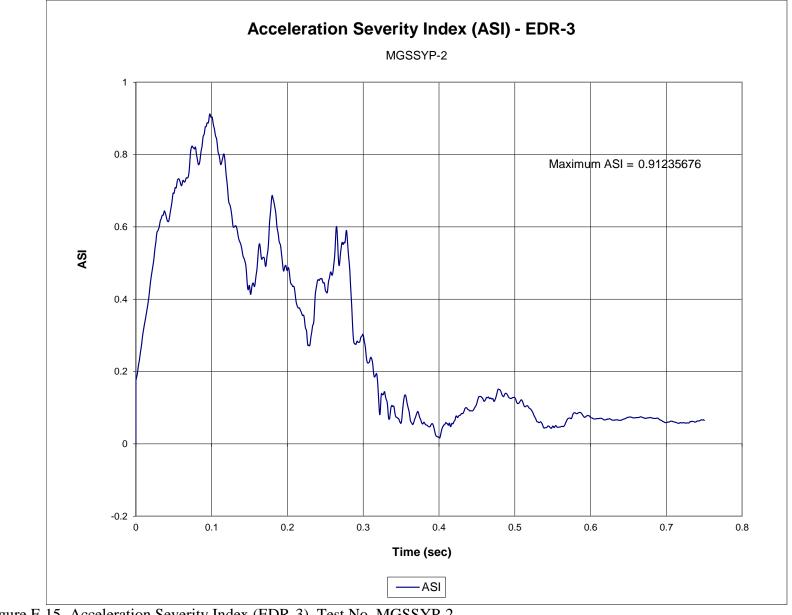


Figure F-15. Acceleration Severity Index (EDR-3), Test No. MGSSYP-2

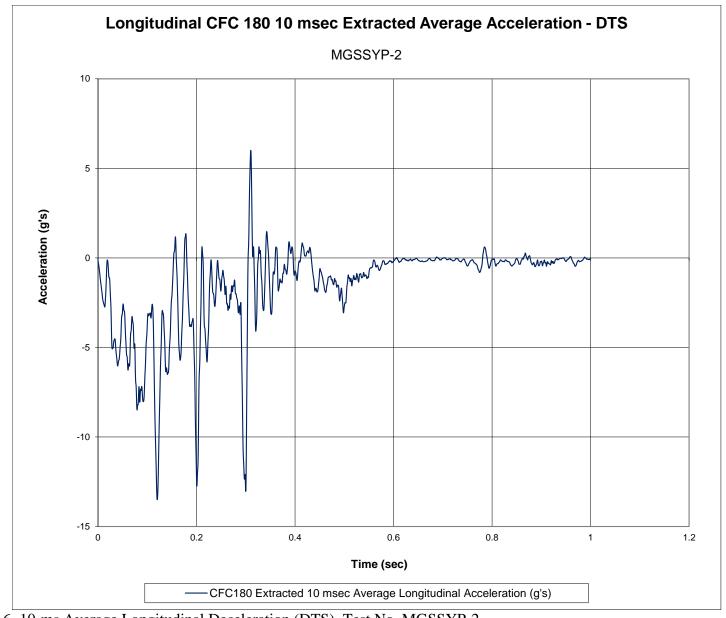


Figure F-16. 10-ms Average Longitudinal Deceleration (DTS), Test No. MGSSYP-2

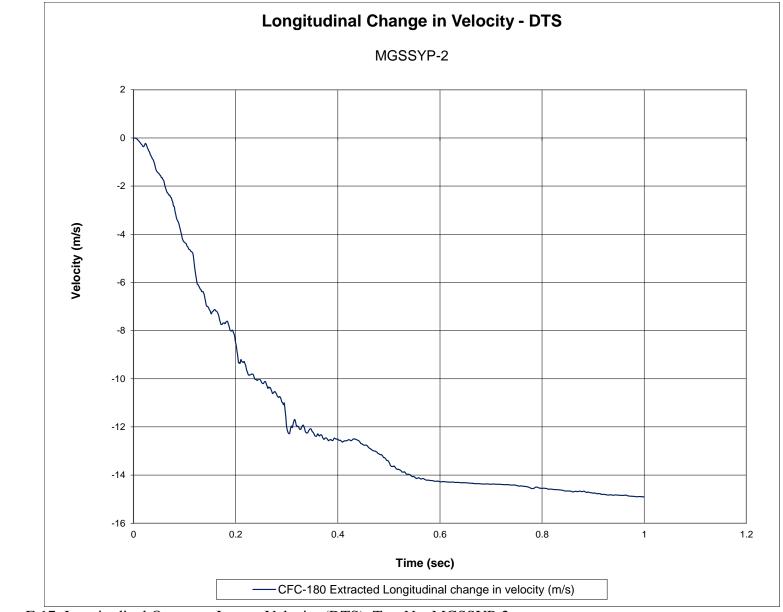


Figure F-17. Longitudinal Occupant Impact Velocity (DTS), Test No. MGSSYP-2

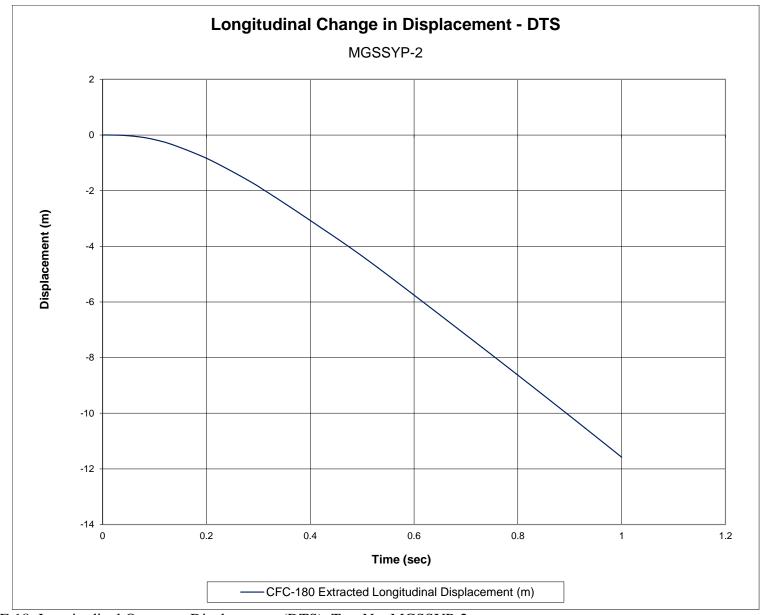


Figure F-18. Longitudinal Occupant Displacement (DTS), Test No. MGSSYP-2

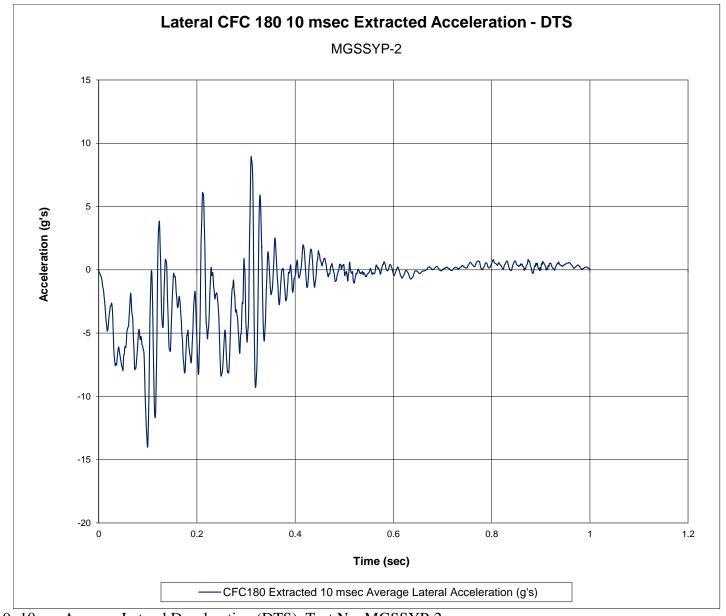


Figure F-19. 10-ms Average Lateral Deceleration (DTS), Test No. MGSSYP-2

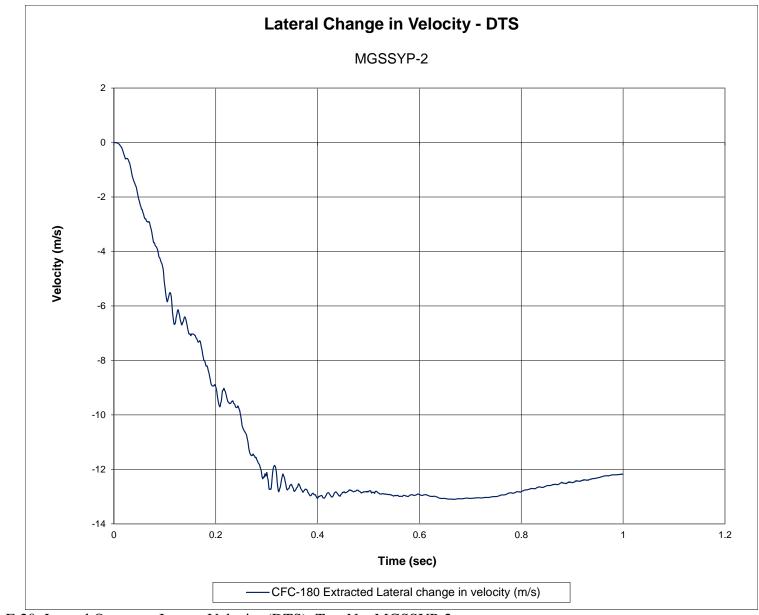


Figure F-20. Lateral Occupant Impact Velocity (DTS), Test No. MGSSYP-2

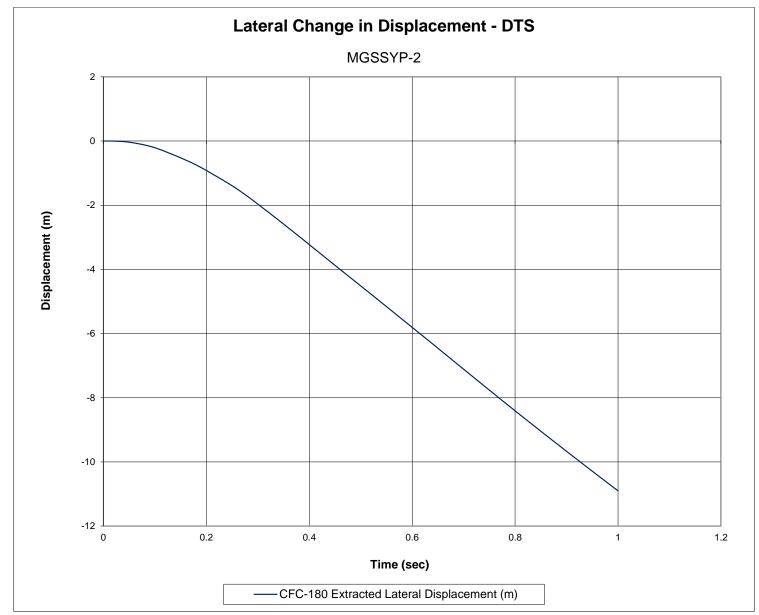


Figure F-21. Lateral Occupant Displacement (DTS), Test No. MGSSYP-2

Figure F-22. Vehicular Angular Displacement (DTS), Test No. MGSSYP-2



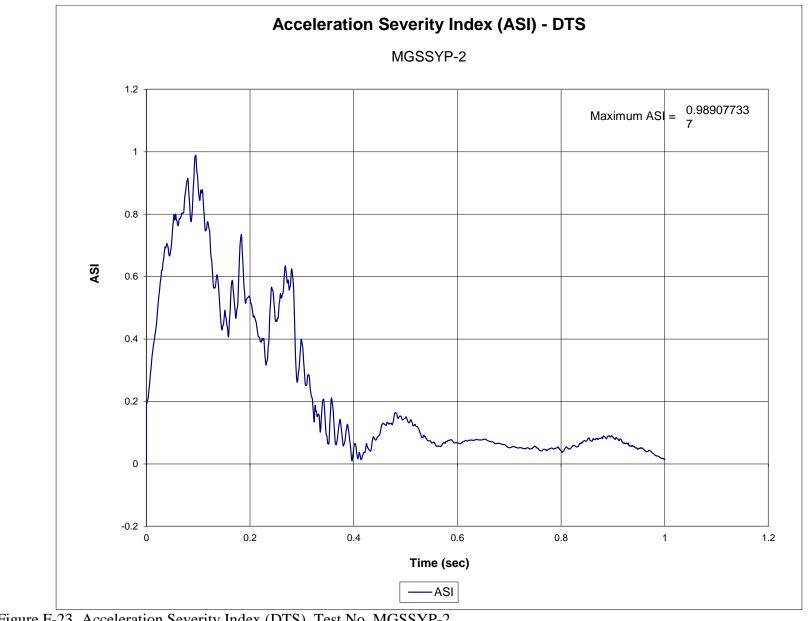


Figure F-23. Acceleration Severity Index (DTS), Test No. MGSSYP-2

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