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CONCRETE MEDIAN BARRIER RESEARCH

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16. Abstract A comprehensive research p		a
of concrete median but tests which evaluated performand and end treatments. Theore simulation program identifies to compare performance with criteria were determined from ternatives. Three crash test impacted at 45 and 55 mph to collected and analyzed for it barrier. State-of-the-art is and specimen CMB details. barrier construction. This bridge parapets. This volume is the second of the se	mance of barrier prestical investigations ed a new barrier shape the currently used prome experiments and sts examined performance of a 40,000-lb internservice performance cost factors are directly a considerations.	using mathematical crash ape which was crash tested ofiles. Load and stability used to analyze barrier almance of the CMB when city bus. Accident data were not of the concrete median de summary of state practice iscussed for concrete median are deplicable to concrete
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Stability. A reasonable math model was developed to evaluate CMB foundation restraint. Considerable difficulty was encountered in exercising this model due to boundary conditions which include complex interactions. Experimental results did not completely verify the model, but did give some confidence to the results in terms of judging acceptable values of barrier motion during simulated impacts. Results of experimental investigations were compared to establish validity of the model. A maximum roll angle of 7.5 deg indicated from the math model related to California Test 162 (see Table 20) was established as a threshold of barrier stability. No measurable roll angle in the reference test occurred; however, limitations of the math model preclude absolute correlation. Thus, the selection of the 7.5 deg angle is somewhat arbitrary, but should be on the conservative side. Since rolling of the barrier induces ramping, it is considered the least desirable when considering yawing or lateral displacements of the barrier. As shown in Figure 52 the roll angle of the barrier is related to embedment, but not in a direct sense. Due to the interaction of yaw and roll, and lateral displacements, it is difficult to predict barrier response without exercising the model.

For Soil 1, the deeper embedment provides the better restraint; however for Soil 2, the 4-in. (100 mm) embedment is adequate for all New Jersey shape barrier lengths greater than 20 ft (6.1 m) where the values converge. For Configuration F, the 6-in. (38 mm) embedment is recommended for 20-ft (6.1 m) barriers and 4 in. (25mm) for barriers 30 ft (3.2 m) and greater. An asphalt layer of 1 in. (25mm) is adequate for lengths of 30 ft (3.2 m) in length.

Concrete barriers are placed on new and existing paved medians. For new medians, the use of keyways is recommended in lieu of dowels except for the shoulder barrier detail as shown in Figure 53. It may be economically advantageous to use a full section barrier even on shoulders due to stability considerations. For existing concrete medians, dowels installed into the existing pavement can be used as shown in Figure 53. Deformed bars are recommended to take advantage of the bar tension load in reacting barrier overturning forces. For asphalt pavements, it is recommended that a 1-2-in. (25-50mm) course of asphalt be placed at the barrier base as presented in Figure 52. Precast barriers with adequate joint strength can be sufficiently anchored by 1-2 in. (25-50mm) of asphalt or 1-in. (25mm) grout bed discussed previously. Barriers placed on existing foundations (i.e., approximately the same width as the barrier) have the same requirements regarding foundation depth in soil as given in Figure 52. Shoulder barriers (half sections) are not recommended for placement on foundations of the same width. A full section barrier is considered necessary for shoulder barriers not placed on continuous pavements.

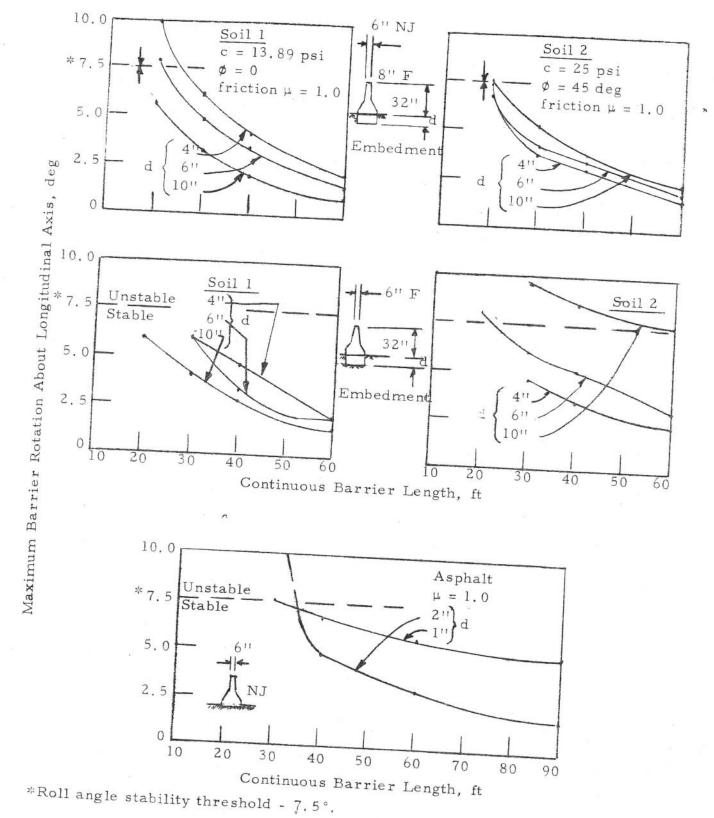


FIGURE 52. BARRIER STABILITY CURVES

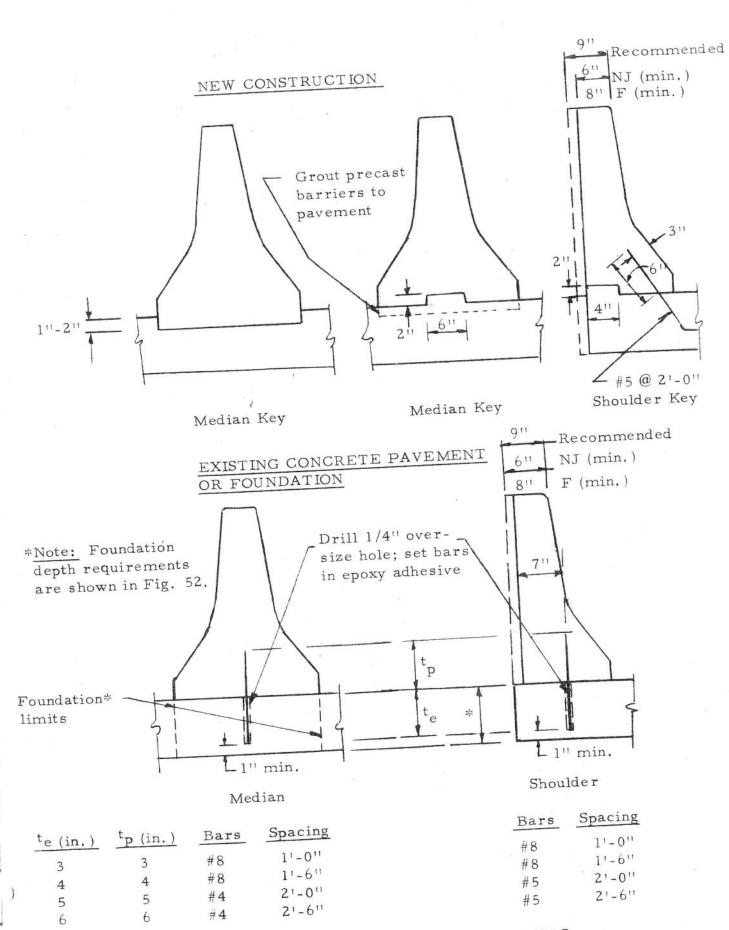
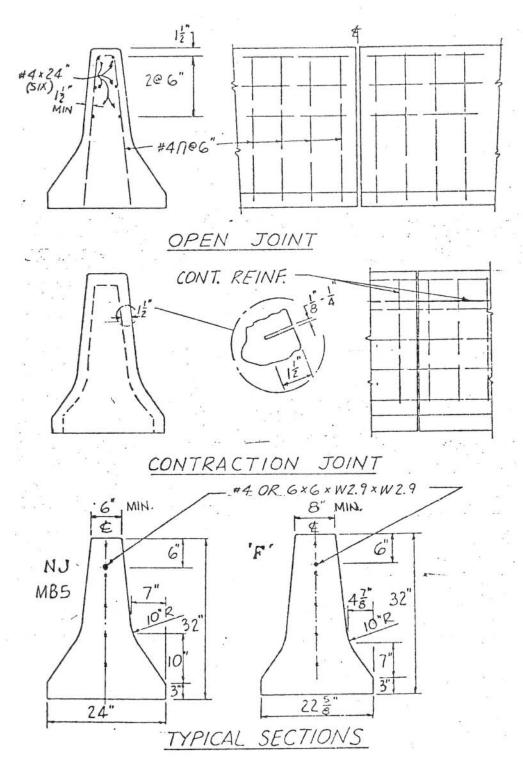


FIGURE 53. BARRIER STABILITY DETAILS



Notes: 1. Barrier reinforcement is for severe impacts where fracture of barrier occurs. Either one rebar or welded wire fabric is recommended to hold barrier together. Adequate splice length of reinforcement is required across construction joints.

- 2. Corner reinforcement at open joints is required for equivalent strength of typical section.
- 3. Barriers shown are structurally adequate for standard strength test conditions with concrete strength $f_c^1 = 3000 \text{ psi}$.
- 4. Foundation requirements are shown in Figure 52

FIGURE 55. RECOMMENDED MEDIAN BARRIER DESIGN, SLIPFORM AND CAST-IN-PLACE