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# PERFORMANCE LIMITS FOR 6-IN. (152-MM) HIGH CURBS PLACED IN ADVANCE OF THE MGS USING MASH VEHICLES PART III: FULL-SCALE CRASH TESTING (TL-2)

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A full-scale crash test utilizing the Test Level 2 (TL-2) safety performance criteria of the Manual for Assessing Safety Hardware (MASH) was performed on the Midwest Guardrail System (MGS) offset 6 ft (1.8 m) behind a 6-in. (152-mm) high AASHTO Type B curb with a top mounting height of 31 in. (787 mm) relative to the ground [37 in. (940 mm) relative to the roadway]. In the test, the 2270P vehicle was redirected by the guardrail, and all safety performance criteria were met. Thus, the MGS offset 6 ft (1.8 mm) behind a 6-in. (152-mm) high curb with a top mounting height of 31 in. (787 mm) was deemed to be acceptable according to TL-2 of MASH. Based on test results and prior research, preliminary guidelines were developed for use of the MGS when offset behind curbs.

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This report was completed with funding from the Federal Highway Administration, U.S. Department of Transportation. The contents of this report reflect the views and opinions of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the state highway departments participating in the Midwest States Regional Pooled Fund Program nor the Federal Highway Administration, U.S. Department of Transportation. This report does not constitute a standard, specification, regulation, product endorsement, or an endorsement of manufacturers.

#### UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

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#### 1 INTRODUCTION

#### 1.1 Problem Statement

Highway design policy typically discourages the use of 6- to 8-in. (152- to 203-mm) vertical curbs on high-speed roadways because of their potential to cause drivers to lose control in a crash [1]. Curbs can also affect the interaction of errant vehicles with roadside barriers by causing vaulting or underride of the barrier. However, the use of curbs is often required because of restricted right-of-way, drainage considerations, access control, and other functions. Often, there is a desire to offset the guardrail from the curb to reduce the propensity for snow plows to gouge and/or damage the W-beam rail sections or to allow for placement of sidewalks between the road and a barrier or other roadside features.

When curbs are required, the offset of the barrier from the curb has been shown to be critical in the performance of the system through modeling and crash testing. Previous work with steel-post, nested W-beam guardrail has shown that a 4-in. (102-mm) high sloped curb with the toe of the curb placed at the front face of the guardrail is capable of meeting National Cooperative Highway Research Program (NCHRP) Report No. 350 safety requirements [2-4]. Further research with standard wood-post W-beam guardrail has shown that a 4-in. (102-mm) high sloped curb with its toe set out 1 in. (25 mm) from the front face of the guardrail is also capable of meeting TL-3 requirements [5].

Investigation of curb-barrier combinations was reported in NCHRP Report No. 537, *Recommended Guidelines for Curbs and Curb-Barrier Combinations* [6]. This study developed guidelines for the use of curbs and curb-barrier combinations on roadways with operating speeds greater than 37.3 mph (60 km/h). The study recommended that guardrail be installed flush with the face of the sloped curb or offset more than 8.2 ft (2.5 m) behind the curb for operating speeds

in excess of 37.3 mph (60 km/h). In addition, the study recommended that guardrail should not be offset behind sloped curbs for speeds greater than 62.1 mph (100 km/h).

The recent development and testing of the Midwest Guardrail System (MGS) has demonstrated that this system can be used with a 6-in. (152-mm) tall, American Association of State Highway Transportation Officials (AASHTO) Type B curb positioned 6 in. (152 mm) in front of the face of the guardrail element [7-8]. Although this guardrail-to-curb configuration provides increased hydraulic flow for roadway runoff as well as reduced guardrail maintenance arising from snow plowing operations, state departments of transportation (DOTs) often desire to locate roadside curbs farther away from the front face of the guardrail. Thus, a research effort was begun with the goal of determining placement guidelines for the MGS in relation to curbs.

# 1.2 Background

In 2008, testing was performed with the small car and pickup truck vehicles specified in the *Manual for Assessing Safety Hardware (MASH)* [9]. The test vehicles impacted a 6-in. (152-mm) high AASTHO Type B curb under Test Level 3 (TL-3) conditions [i.e., 62 mph (100 km/h) and 25 degrees]. The main goal of the tests was to determine the vehicle behavior following the impact, with particular attention focused on the pitch angles and the bumper trajectories of the vehicles [10-11].

By comparing the critical bumper impact point trajectories against the MGS top/bottom corrugation heights, the critical override/underride offset for placing the MGS behind the curb was determined. Results of this analysis created offset guidelines for placement of the MGS with a 6-in. (152-mm) high curb [10-11].

To further investigate the critical offset distance for MGS placement behind an AASHTO Type B curb, finite element analysis was performed. The MGS was offset from a 6-in. (152-mm) high AASTHO Type B curb at various distances and impacted with the 2000P test vehicle.

Based on previous vehicle-curb simulation results and to ensure reliability of the model, the offset distance under investigation was limited to the range of 0.0 ft (0.0 m) to 7.35 ft (2.24 m) behind the curb. Simulation results indicated that the current pickup model (2000P) was fairly accurate in predicting the vehicle trajectory within 7.35 ft (2.24 m) behind the curb. Details of this research effort are documented in prior MwRSF research reports [10-11].

Based on the simulation results, a full-scale crash test was then performed on the MGS with a top mounting height of 37 in. (940 mm) above the roadway, offset 8 ft (2.44 m) behind a 6-in. (152-mm) high AASHTO Type B Curb [12]. In the test, the 2270P vehicle was contained by the guardrail, but it became unstable and rolled over. Analysis of the test revealed that the right-front tire snagged on a post and detached. The right-rear tire of the pickup traversed over the detached tire, causing the rear of the vehicle to pitch upward. The vehicle subsequently became unstable and rolled over. Thus, the MGS offset 8 ft (2.44 mm) behind a 6-in. (152-mm) high curb with a top mounting height of 37 in. (940 mm) relative to the roadway was deemed to be unacceptable according to TL-3 of MASH.

Simulation of this crash test was then performed with the newly released 2270P vehicle model. Simulation results also showed the 2270P rolling over in the same impact scenario as the first crash test.

## 1.3 Objective

Following the unsuccessful full-scale crash test, the original project was modified based on a survey of the states in the Midwest States Regional Pooled Fund Program. The new objective was to determine a range of distances for which the MGS could be offset behind a 6-in. (152-mm) high AASHTO Type B curb and satisfy the TL-2 safety performance criteria of MASH.

# 1.4 Scope

The research objective was achieved through the completion of several tasks. First, finite element simulations of the system were performed to determine the critical offset distance of the MGS relative to the curb. This configuration would represent the highest probability of system failure under TL-2 conditions for the range of offsets. Then, a full-scale vehicle crash test was performed on the MGS offset 6 ft (1.83 m) behind a 6-in. (152-mm) high AASHTO Type B curb. The MGS was raised 6 in. (152 mm) resulting in a top mounting height of 37 in. (940 mm) relative to the roadway. The crash test utilized a pickup truck, weighing approximately 5,000 lb (2,268 kg). Target impact conditions for the test were an impact speed of 44 mph (70 km/h) and an impact angle of 25 degrees. Next, the test results were analyzed, evaluated, and documented. Finally, conclusions and recommendations were made that pertain to the safety performance of the MGS and curb system relative to the test performed.

#### 2 BARRIER DESIGN AND ANALYSIS

Researchers concluded that the critical offset distance for the MGS behind the curb was the distance which would provide the most probable conditions for override of the pickup truck test vehicle. It was believed that the worst-case placement for the MGS relative to the curb would be at the location where the front bumper of the truck reached the apex of its trajectory following impact with the curb. The truck would be at its maximum height at this location, and its momentum would not yet be going downward. It was believed an acceptable range for placing the MGS behind the curb could be achieved by testing the worst-case location for the MGS with the pickup truck and using previous knowledge concerning the small car.

Finite element analysis was performed using LS-DYNA to determine the critical offset of the MGS relative to the curb [13]. The vehicle model used for the simulation was the National Crash Analysis Center (NCAC) Silverado V2 model released in March 2009, while the MGS model used in the simulations was developed by MwRSF in previous studies [11].

To determine the critical offset distance for TL-2 conditions, simulations with only the pickup truck and the curb were initially conducted. Results from this study showed the apex of the trajectory of the front bumper occurred at a distance of approximately 6 ft (1.83 m) behind the toe of the curb.

Further simulations were then performed in which the Silverado impacted the MGS at various offsets from the curb. These offsets ranged from 4 ft (1.22 m) to 10 ft (3.05 m) at 1-ft (0.30-m) increments. Results from the 6-ft (1.83-m) and 8-ft (2.44-m) offset simulations, which are shown in Figure 1, clearly indicated that the 6-ft (1.83-m) offset produced the worst-case impact. However, in this scenario, the truck was smoothly redirected by the MGS. Therefore, the system was expected to perform successfully in full-scale crash testing.

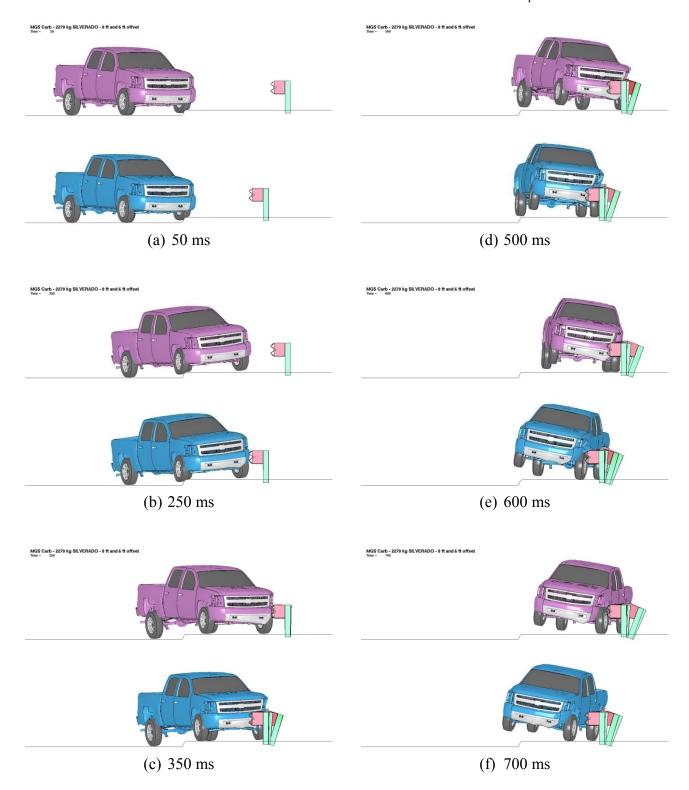


Figure 1. 8-ft Offset (Top Vehicle in Each Frame) vs. 6-ft Offset (Bottom Vehicle in Each Frame)

#### 3 DESIGN DETAILS

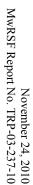
The barrier system test installation was comprised of 175 ft (53.34 m) of MGS guardrail supported by steel posts and positioned 6 ft (1.83 m) behind a 6-in. (152-mm) tall, AASHTO Type B curb, as shown in Figures 2 through 11. Photographs of the test installation are shown in Figures 12 through 14. Material specifications, mill certifications, and certificates of conformity for the system materials are shown in Appendix A.

The MGS was constructed with twenty-nine guardrail posts. Post nos. 3 through 27 were galvanized ASTM A36 steel W6x8.5 (W152x12.6) sections measuring 72 in. (1,829 mm) long and embedded in 40 in. (1016 mm) of soil, as shown in Figures 3 and 6. Post nos. 1, 2, 28, and 29 were timber posts measuring 5½ in. wide x 7½ in. deep x 46 in. long (140 mm x 190 mm x 1,168 mm) and were placed in 72-in. (1,829-mm) long steel foundation tubes, as shown in Figures 4 and 7. The timber posts and foundation tubes were part of the anchor system designed to replicate the capacity of a tangent guardrail terminal.

Post nos. 1 through 29 were spaced 75 in. (1,905 mm) on center, as shown in Figure 2. The posts were placed in a compacted, coarse, crushed limestone material that met Grading B of AASHTO M147-65 (1990) as described in MASH. For post nos. 3 through 27, 6-in. wide x 12-in. deep x 14½-in. long (152-mm x 305-mm x 362-mm) wood spacer blockouts were used to block the rail away from the front face of the steel posts, as shown in Figures 3 and 6.

Standard 12-gauge (2.66-mm thick) W-beam rails were placed between post nos. 1 and 29, as shown in Figures 2, 4, and 10. The top mounting height of the W-beam rail was 31 in. (787 mm) above the ground surface with a 24½-in. (632-mm) center mounting height, or 37 in. (940 mm) above the roadway surface. Rail splices were placed at midspan locations between guardrail posts, as shown in Figures 2 and 4. All lap splice connections between the rail sections were configured to reduce vehicle snag at the splice during the crash test.

A 6-in. (152-mm) tall, AASHTO Type B curb was placed in front of the MGS. The concrete curb was 73 ft - 6 in. (22.40 m) long, beginning at the midspan between post nos. 8 and 9 to post no. 20, as shown in Figure 2. The toe of the curb was offset 6 ft (1.83 m) in front of the front face of the guardrail. The concrete mix had a minimum 28-day compressive strength of 4,000 psi (27.6 MPa). All steel reinforcement was specified as ASTM A615 Grade 40 rebar and consisted of No. 4 longitudinal and vertical bars, as shown in Figure 3.



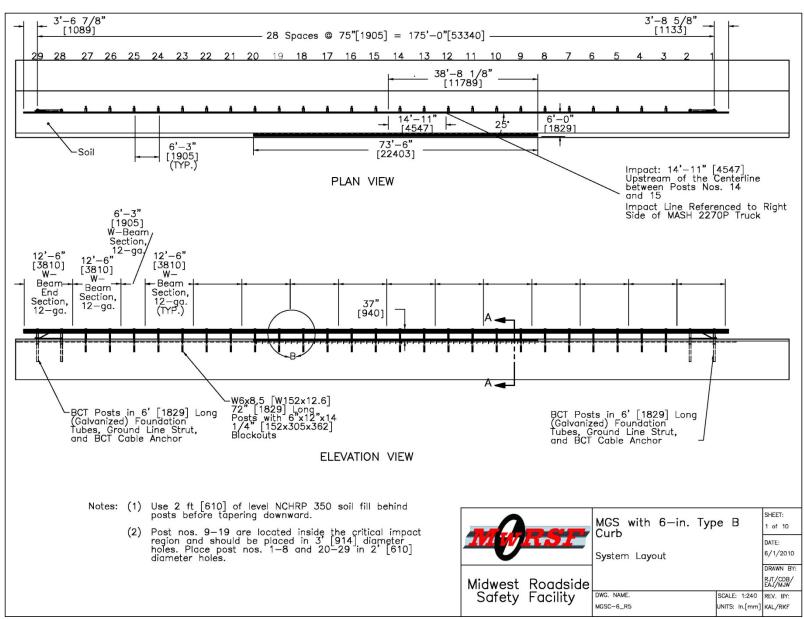


Figure 2. Test Installation Layout, Test No. MGSC-6

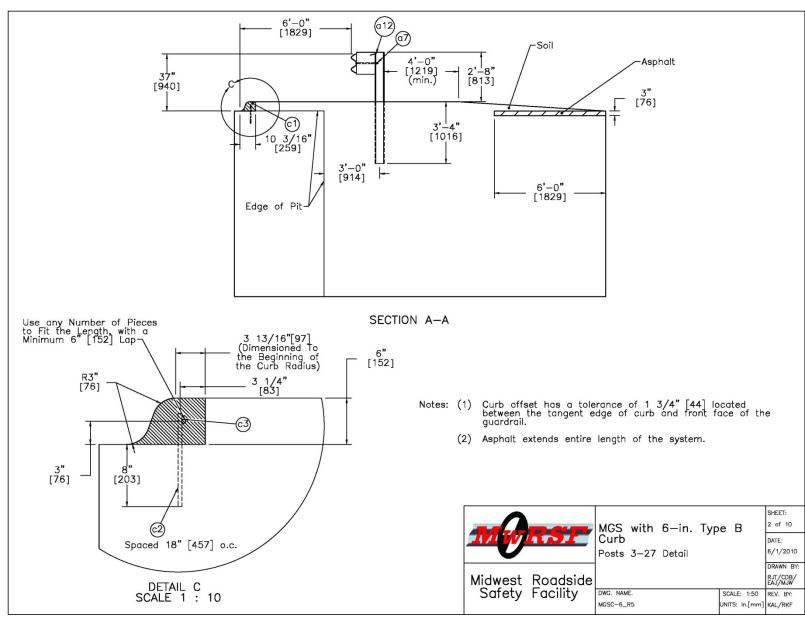
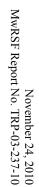


Figure 3. Post and Curb Details, Test No. MGSC-6



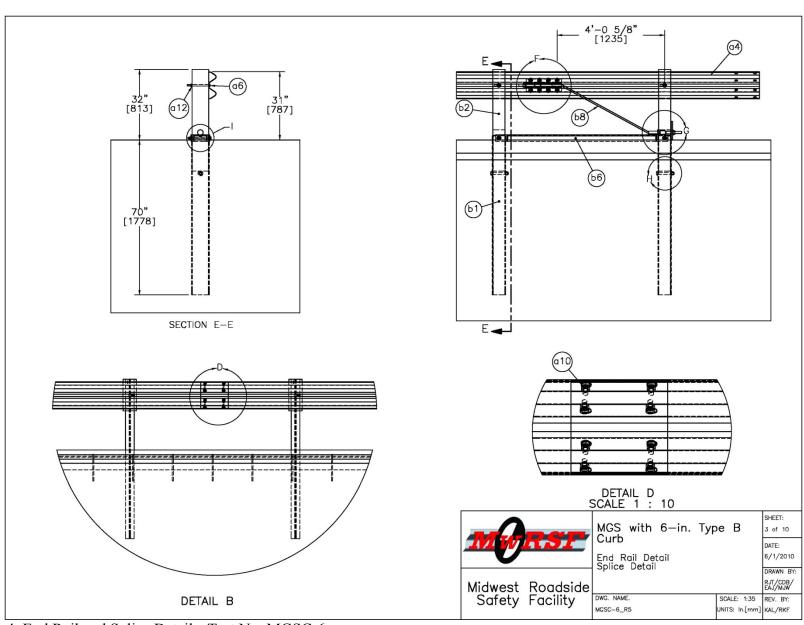


Figure 4. End Rail and Splice Details, Test No. MGSC-6

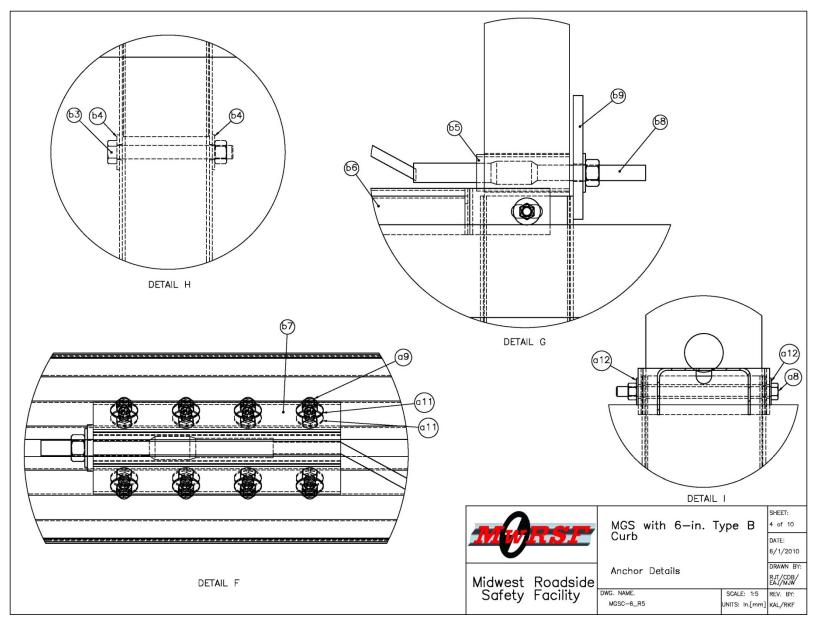


Figure 5. Anchor Details, Test No. MGSC-6

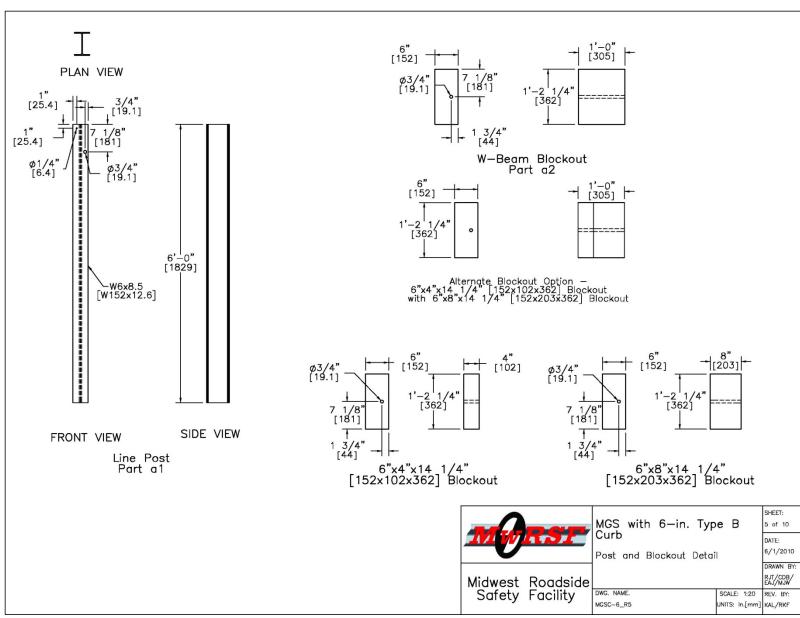


Figure 6. Post and Blockout Details, Test No. MGSC-6

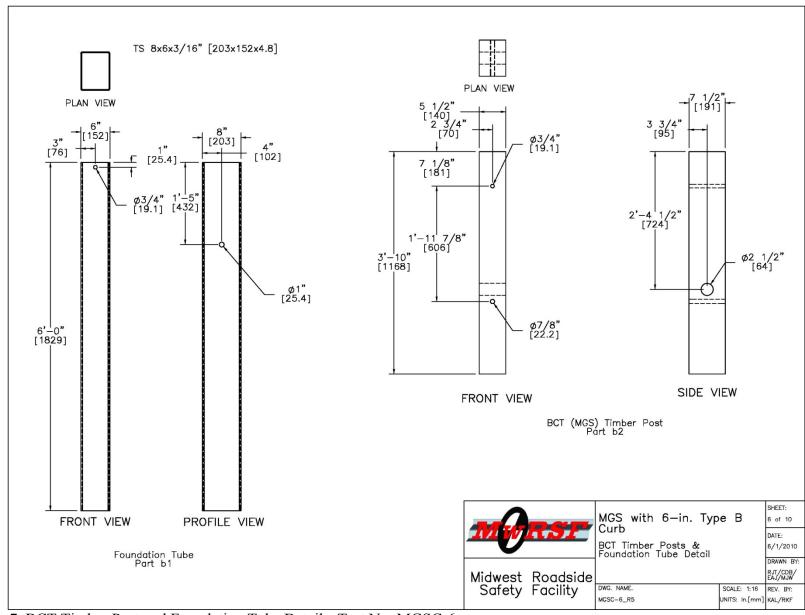


Figure 7. BCT Timber Post and Foundation Tube Details, Test No. MGSC-6

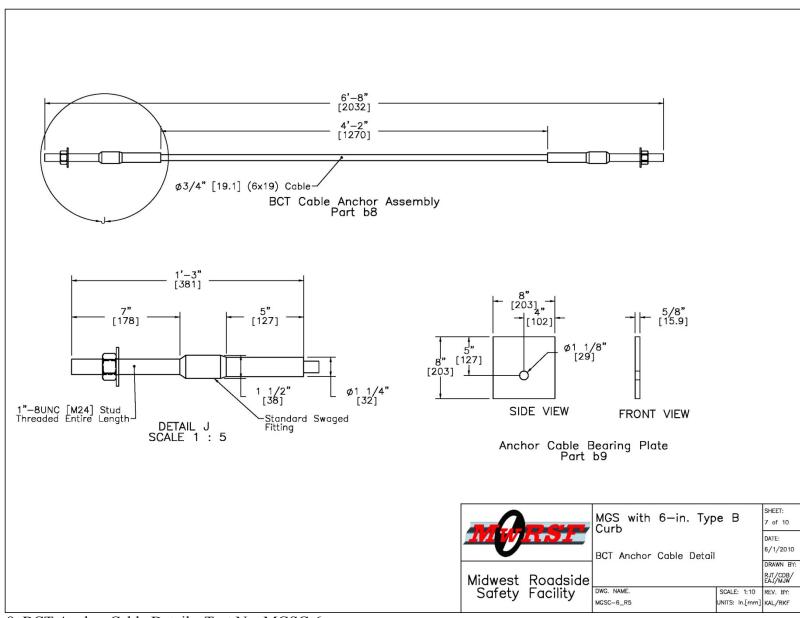


Figure 8. BCT Anchor Cable Details, Test No. MGSC-6

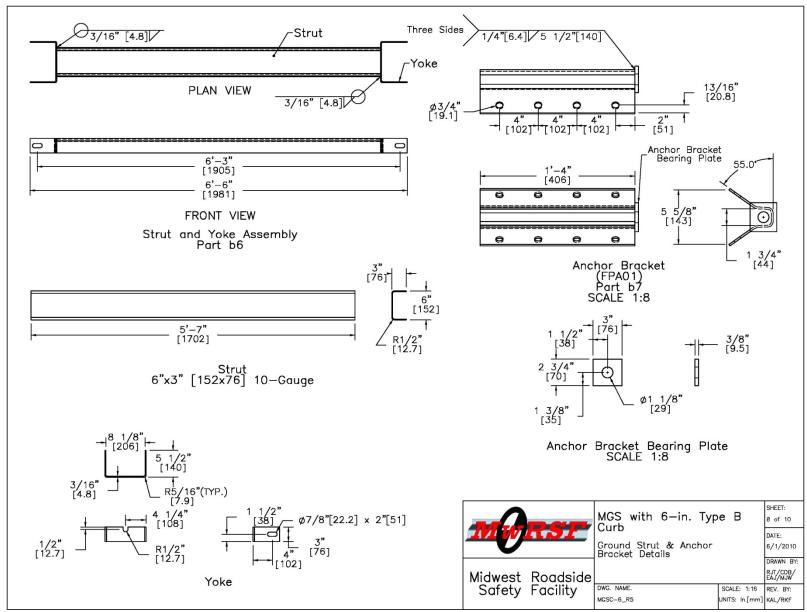


Figure 9. Ground Strut and Anchor Bracket Details, Test No. MGSC-6

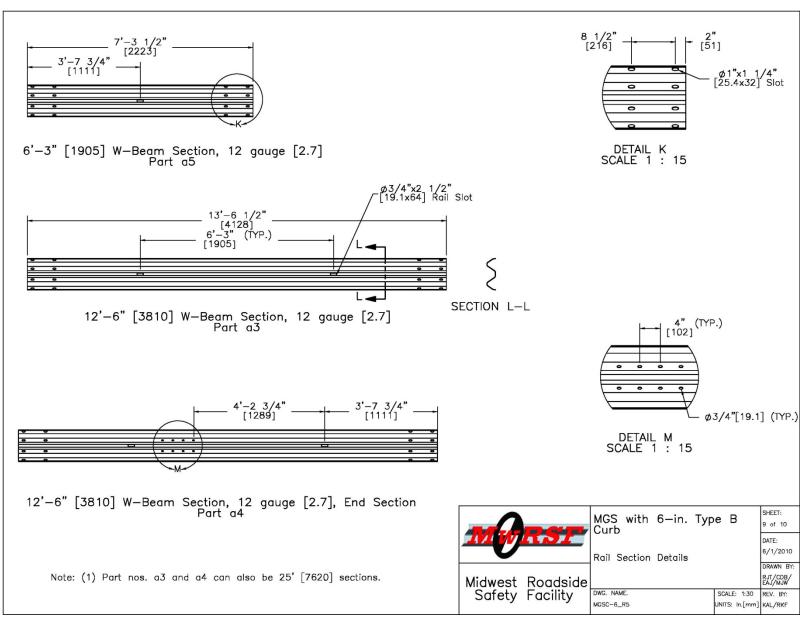


Figure 10. Rail Section Details, Test No. MGSC-6

Item No.	QTY.	Description	Material Specifications	Hardware Guide
a1	25	W6x8.5 [W152x12.6] 72" [1829] long	ASTM A36 Steel	_
a2	25	6x12x14 1/4" [152x305x362] Blockout	SYP Grade No.1 or better	PDB10a-b
а3	12	12'-6" [3810] W-Beam MGS Section	12 gauge [2.7] AASHTO M180	RWM04a
a4	2	12'-6" [3810] W-Beam MGS End Section	12 gauge [2.7] AASHTO M180	RWM14a
a5	1	6'-3" [1905] W-Beam MGS Section	12 gauge [2.7] AASHTO M180	RWMO1a
a6	4	5/8" [15.9] Dia. x 10" [254] long Guardrail Bolt and Nut	ASTM A307	FBB03
a7	25	5/8" [15.9] Dia. x 14" [356] long Guardrail Bolt and Nut	ASTM A307	FBB06
a8	4	5/8" [15.9] Dia. x 10" [254] long Hex Head Bolt and Nut	ASTM A307	FBX16a
a9	16	5/8" [15.9] Dia. x 1 1/2" [38] long Hex Head Bolt and Nut	ASTM A307	FBX16a
a10	112	5/8" [15.9] Dia. x 1 1/2" [38] long Guardrail Bolt and Nut	ASTM A307	FBB01
a11	44	5/8" [15.9] Dia. Flat Washer	ASTM F436 Grade 1	FWC16a
a12	25	16D Double Head Nail	-	-
ь1	4	72" [1829] Foundation Tube	ASTM A500 Gr. B	PTE06
b2	4	BCT Timber Post	SYP Grade No. 1 or better (No knots, 18" [457] above or below ground tension face)	PDF01
b3	4	7/8" [22.2] Dia. x 7 1/2" [191] long Hex Head Bolt and Nut	ASTM A307	FBX22a
b <b>4</b>	8	7/8" [22.2] Dia. Flat Washer	ASTM F436 Grade 1	FWC22a
b5	2	2 3/8" [60] O.D.x 6" [152] long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	FMM02
b6	2	Strut and Yoke Assembly	ASTM A36 Steel Galvanized	-
b7	2	Anchor Bracket Assembly	ASTM A36 Steel Galvanized	FPA01
b8	2	BCT Cable Anchor Assembly	ø3/4" [19] 6x19 IWRC IPS Galvanized Wire Rope	FCA01-02
b <b>9</b>	2	8"x8"x5/8" [203x203x16] Anchor Bearing Plate	ASTM A36 Steel Galvanized	FPB01
c1	1	Curb	Concrete (s/g mix) — Min. 4000 psi [27.6 MPa] Comp. Strength	-
c2	49	#4 Rebar 12" [305] Long	ASTM A615 Grade 40	-
с3	1	#4 Rebar 73' [22.3 m] Long	ASTM A615 Grade 40	_

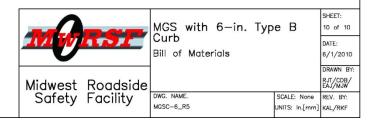


Figure 11. Bill of Materials, Test No. MGSC-6





Figure 12. Test Installation Photographs, Test No. MGSC-6





Figure 13. Test Installation Photographs, Test No. MGSC-6





Figure 14. Test Installation Photographs, Test No. MGSC-6

# 4 TEST REQUIREMENTS AND EVALUATION CRITERIA

## **4.1 Test Requirements**

Longitudinal barriers, such as W-beam guardrails with curbs, must satisfy impact safety standards in order to be accepted by the Federal Highway Administration (FHWA) for use on National Highway System (NHS) new construction projects or as a replacement for existing designs not meeting current safety standards. In recent years, these safety standards have consisted of the guidelines and procedures published in NCHRP Report 350. However, NCHRP Project 22-14(2) generated revised testing procedures and guidelines for use in the evaluation of roadside safety appurtenances and are provided in MASH. According to TL-2 of MASH, longitudinal barrier systems must be subjected to two full-scale vehicle crash tests. The two full-scale crash tests are as follows:

- 1. Test Designation 2-10 consisting of a 2,425-lb (1,100-kg) passenger car impacting the system at a nominal speed and angle of 44 mph (70 km/h) and 25 degrees, respectively.
- 2. Test Designation 2-11 consisting of a 5,000-lb (2,268-kg) pickup truck impacting the system at a nominal speed and angle of 44 mph (70 km/h) and 25 degrees, respectively.

The test conditions of TL-2 longitudinal barriers are summarized in Table 1.

Table 1. MASH TL-2 Crash Test Conditions

		Test Vehicle	Impact Conditions			
Test Article	Test Designation		Speed		Angle	Evaluation Criteria <sup>1</sup>
			mph	km/h	(deg)	
Longitudinal	2-10	1100C	44	70	25	A,D,F,H,I
Barrier	2-11	2270P	44	70	25	A,D,F,H,I

<sup>&</sup>lt;sup>1</sup> Evaluation criteria explained in Table 2.

#### 4.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the guardrail to contain and redirect impacting vehicles. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Vehicle trajectory after collision is a measure of the potential for the post-impact trajectory of the vehicle to result in secondary collisions with other vehicles or fixed objects, thereby increasing the risk of injury to the occupant of the impacting vehicle and to other vehicles. These evaluation criteria are summarized in Table 2 and defined in greater detail in MASH. The full-scale vehicle crash test was conducted and reported in accordance with the procedures provided in MASH.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported on the test summary sheet. Additional discussion on PHD, THIV and ASI is provided in Reference 9.

# **4.3 Soil Strength Requirements**

In order to limit the variation of soil strength among testing agencies, foundation soil must satisfy the recommended performance characteristics set forth in Chapter 3 and Appendix B of MASH. Testing facilities must first subject their soil to a dynamic post test to demonstrate a minimum dynamic load of 7.5 kips (33.4 kN) at deflections between 5 and 20 in. (127 and 508 mm). If satisfactory results are observed, a static test is conducted using an identical test installation. The results of this static test become the baseline requirement for soil strength in future full-scale testing. On the full-scale test day, an additional post installed near the impact point is statically tested in the same manner as the baseline test. The full-scale test can be

conducted only if the static test results show a resistance greater than or equal to 90 percent of the baseline test at deflections of 5, 10, and 15 in. (127, 254, and 381 mm). Otherwise, testing must be postponed until the soil demonstrates adequate strength.

Table 2. MASH Evaluation Criteria for Longitudinal Barrier

Structural Adequacy	A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.				
	D. Detached elements, fragments or other debris from the test artic should not penetrate or show potential for penetrating the occupa compartment, or present an undue hazard to other traffipedestrians, or personnel in a work zone. Deformations of, intrusions into, the occupant compartment should not exceed limited for the in Section 5.3 and Appendix E of MASH.					
	F.		The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.			
	Н.	Occupant Impact Velocities (OIV) (see Appendix A, Section As of MASH for calculation procedure) should satisfy the following limits:				
Occupant Impact Velocity Limits				its		
Risk	Component Preferred Maximum					
	40 ft/s (12.2 m/s)					
I. The Occupant Ridedown Acceleration (ORA) (see Apsection A5.3 of MASH for calculation procedure) should the following limits:						
	Occupant Ridedown Acceleration Limits					
	Component Preferred Maximu					
	Longitudinal and Lateral 15.0 g's 20.49 g					

#### **5 TEST CONDITIONS**

# **5.1 Test Facility**

The testing facility is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles (8.0 km) northwest of the University of Nebraska-Lincoln.

#### 5.2 Vehicle Tow and Guidance System

A reverse cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [14] was used to steer the test vehicle. A guide-flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the barrier system. The ¾-in. (9.5-mm) diameter guide cable was tensioned to approximately 3,500 lb (15.6 kN) and supported both laterally and vertically every 100 ft (30.48 m) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide-flag struck and knocked each stanchion to the ground.

#### **5.3 Test Vehicle**

For test no. MGSC-6, a 2003 Dodge Ram 1500 Quad Cab pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 5,100 lb (2,313 kg), 4,974 lb (2,256 kg), and 5,144 lb (2,333 kg), respectively. The test vehicle is shown in Figure 15, and vehicle dimensions are shown in Figure 16.







Figure 15. Test Vehicle, Test No. MGSC-6

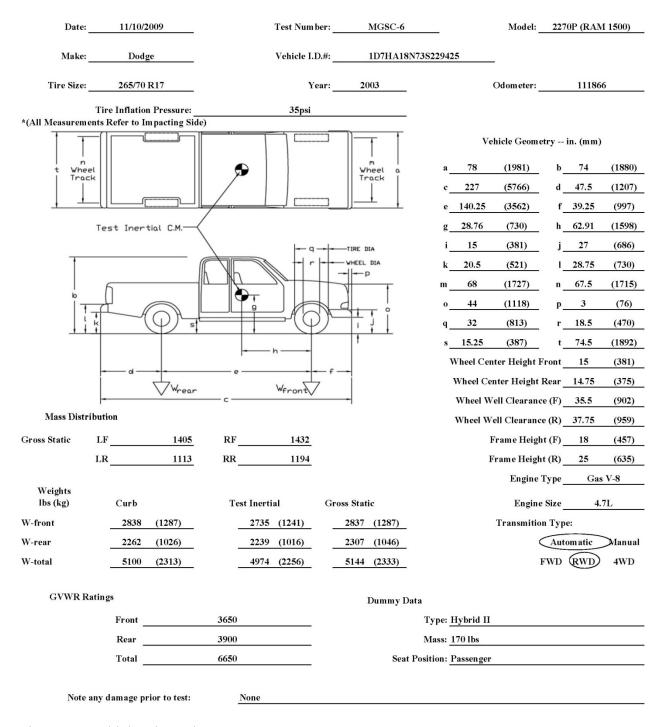


Figure 16. Vehicle Dimensions, Test No. MGSC-6

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights, while the Suspension Method [15] was used to determine the vertical component of the c.g. for the pickup truck. The latter method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The location of the final c.g. is shown in Figures 16 and 17. Data used to calculate the location of the c.g. and ballast information are shown in Appendix B.

Square, black- and white-checkered targets were placed on the vehicle to aid in the analysis of the high-speed videos, as shown in Figure 17. Round, checkered targets were placed on the center of gravity on the left-side door, the right-side door, and the roof of the vehicle. The remaining targets were located for references so that they could be viewed from the high-speed cameras for video analysis.

The front wheels of the test vehicle were aligned for camber, caster, and toe-in values of zero so that the vehicles would track properly along the guide cable. A 5B flash bulb was mounted on the right side of the vehicle's dash and was fired by a pressure tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial impact with the test article to create a visual indicator of the precise time of impact on the high-speed videos. A remote controlled brake system was installed in the test vehicle so the vehicle could be brought safely to a stop after the test.

# **5.4 Simulated Occupant**

For test no. MGSC-6, A Hybrid II 50<sup>th</sup> Percentile Adult Male Dummy, equipped with clothing and footware, was placed in the right-front seat of the test vehicle with the seat belt

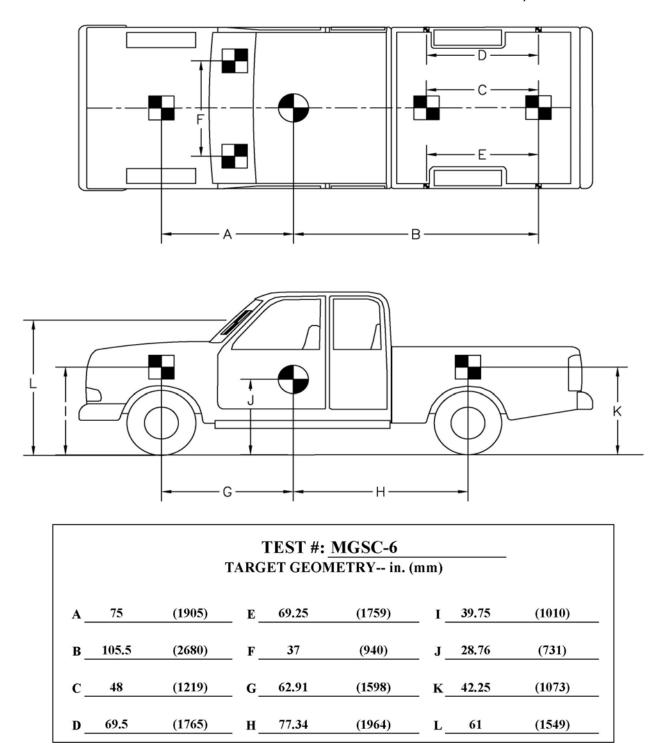


Figure 17. Target Geometry, Test No. MGSC-6

fastened. The dummy, which had a final weight of 170 lb (77 kg), was represented by model no. 572, serial no. 451, and was manufactured by Android Systems of Carson, California. As recommended by MASH, the dummy was not included in calculating the c.g location.

# **5.5 Data Acquisition Systems**

#### **5.5.1** Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. Both of the accelerometers were mounted near the center of gravity of the test vehicle.

One system was a two-arm piezoresistive accelerometer system developed by Endevco of San Juan Capistrano, California. Three accelerometers were used to measure each of the longitudinal, lateral, and vertical accelerations independently at a sample rate of 10,000 Hz. Two additional accelerometers were used to measure the longitudinal and lateral accelerations independently at the same sample rate. The accelerometers were configured and controlled using a system developed and manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. More specifically, data was collected using a DTS Sensor Input Module (SIM), Model TDAS3-SIM-16M. The SIM was configured with 16 MB SRAM memory and 8 sensor input channels with 250 kB SRAM/channel. The SIM was mounted on a TDAS3-R4 module rack. The module rack was configured with isolated power/event/communications, 10BaseT Ethernet and RS232 communication, and an internal backup battery. Both the SIM and module rack were crashworthy. The computer software program "DTS TDAS Control" and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

The second system, Model EDR-3, was a triaxial piezoresistive accelerometer system developed and manufactured by Instrumented Sensor Technology (IST) of Okemos, Michigan. The EDR-3 was configured with 256 kB of RAM memory, a range of  $\pm 200$  g's, a sample rate of

3,200 Hz, and a 1,120 Hz low-pass filter. The computer software program "DynaMax 1 (DM-1)" and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

#### **5.5.2 Rate Transducers**

An angular rate sensor, the ARS-1500, with a range of 1,500 degrees/sec in each of the three directions (roll, pitch, and yaw) was used to measure the rates of rotation of the test vehicle. The angular rate sensor was mounted on an aluminum block inside the test vehicle near the center of gravity and recorded data at 10,000 Hz to the SIM. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The computer software program "DTS TDAS Control" and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

## **5.5.3 Pressure Tape Switches**

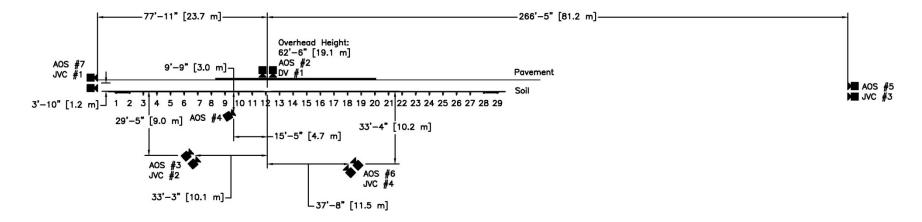
For test no. MGSC-6, five pressure-activated tape switches, spaced at approximately 6.56 ft (2 m) intervals, were used to determine the speed of the vehicle before impact. Each tape switch fired a strobe light which sent an electronic timing signal to the data acquisition system as the right-front tire of the test vehicle passed over it. Test vehicle speed was determined from electronic timing mark data recorded using TestPoint and LabVIEW computer software programs. Strobe lights and high-speed video analysis are used only as a backup in the event that vehicle speed cannot be determined from the electronic data.

# **5.5.4 High-Speed Photography**

Three AOS VITcam high-speed digital video cameras, three AOS X-PRI high-speed digital video cameras, four JVC digital video cameras, and one Canon digital video camera were used to film the crash test. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 18.

The high-speed videos were analyzed using ImageExpress MotionPlus and RedLake MotionScope software programs. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed videos. A Nikon D50 digital still camera was also used to document pre- and post-test conditions for the test.





	No.	Туре	Operating Speed (frames/sec)	Lens	Lens Setting
High-Speed Video	2	AOS Vitcam CTM	500	Cosmicar 12.5-mm Fixed	-
	3	AOS Vitcam CTM	500	TV Zoom V6x17 17-102 mm	50 mm
	4	AOS Vitcam CTM	500	Kowa 8-mm Fixed	-
	5	AOS X-PRI Gigabit	500	Telesar 135-mm Fixed	-
	6	AOS X-PRI Gigabit	500	Sigma 50-mm Fixed	-
	7	AOS X-PRI Gigabit	500	Fujinon 50-mm Fixed	-
Digital Video	1	JVC – GZ-MC500 (Everio)	29.97		
	2	JVC – GZ-MG27u (Everio)	29.97		
	3	JVC – GZ-MG27u (Everio)	29.97		
	4	JVC – GZ-MG27u (Everio)	29.97		
	1	Canon ZR90	29.97		

Figure 18. Camera Locations, Speeds, and Lens Settings, Test No. MGSC-6

#### 6 FULL-SCALE CRASH TEST NO. MGSC-6

#### **6.1 Static Soil Test**

Before full-scale test no. MGSC-6 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The static test results, as shown in Appendix C, demonstrated a soil resistance above the baseline test limits. Thus, the soil provided adequate strength, and the barrier system was approved for full-scale testing.

#### 6.2 Test No. MGSC-6

The 5,144-lb (2,333-kg) pickup truck, with a simulated occupant seated in the right-front seat, impacted the curb at a speed of 45.6 mph (73.4 km/h) and at an angle of 25.3 degrees. After mounting the curb, the vehicle impacted the guardrail at an angle of 22.5 degrees. A summary of the test results and sequential photographs are shown in Figure 19. Additional sequential photographs are shown in Figures 20 through 22. Documentary photographs of the crash test are shown in Figures 23 through 25.

#### **6.3 Weather Conditions**

Test no. MGSC-6 was conducted on November 10, 2009 at approximately 2:30 pm. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported as shown in Table 3.

Table 3. Weather Conditions, Test No. MGSC-6

Temperature	62° F
Humidity	46%
Wind Speed	11 mph
Wind Direction	120° from True North
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0 in.
Previous 7-Day Precipitation	0 in.

# **6.4 Test Description**

Initial vehicle impact with the guardrail was to occur 14 ft - 11 in. (4.6 m) upstream of the centerline of the splice between post nos. 14 and 15, as shown in Figure 26. The actual point of impact was 15 ft - 2½ in. (4.6 m) upstream of the centerline of the splice between post nos. 14 and 15. A sequential description of the impact events is contained in Table 4. The vehicle came to rest 211 ft - 8 in. (64.5 m) downstream from impact and 87 ft (26.5 m) laterally behind the front face of the guardrail. The vehicle trajectory and final position are shown in Figures 19 and 27, respectively.

Table 4. Sequential Description of Impact Events, Test No. MGSC-6

TIME	EVENT			
(sec)	D V DIVI			
-0.180	The right-front tire contacted the front face of the mountable curb.			
-0.004	The left-front tire contacted the front face of the mountable curb.			
0.000	The right-front bumper corner impacted the front face of the rail.			
0.036	The rail upstream of impact deflected downstream, and the upstream posts rotated			
	downstream.			
0.064	The vehicle began to redirect.			
0.082	The rail disengaged from post no. 13 due to bolt pullout.			
0.086	The right headlight disengaged from the vehicle.			
0.126	The right-front tire of the vehicle contacted the upstream side of post no. 13.			
0.232	The rail disengaged from post no. 14 due to bolt pullout.			
0.246	The right-front tire contacted the upstream side of post no. 14.			
0.248	The right-front tire disengaged from the vehicle.			
0.258	The right-rear tire contacted the upstream side of post no. 14.			
0.288	The right-rear quarter panel of the vehicle contacted the rail near the impact location.			
0.318	The vehicle was parallel to the system at a speed of 31.6 mph (50.9 km/h).			
0.436	The rail upstream of impact relaxed, and the upstream posts rotated upstream.			
0.582	The right taillight disengaged from the vehicle.			
	The vehicle exited the system at a speed of 30.1 mph (48.4 km/h) and at an angle of			
0.592	18.7 degrees as the right-rear quarter panel lost contact with the system at the midpoint			
	between post nos. 14 and 15.			

# **6.5 Barrier Damage**

Damage to the barrier was moderate, as shown in Figures 28 through 33. Barrier damage consisted of contact marks and deformation of the W-beam rail, deformed guardrail posts, and disengaged post-to-rail connections. The length of vehicle contact along the barrier was approximately 19 ft - 5 in. (5.92 m) which spanned from 2 in. (51 mm) downstream of post no. 12 to 10 in. (254 mm) downstream of post no. 15.

Post nos. 3 through 15 posts showed varying degrees of damage. Post nos. 3 through 11 twisted slightly downstream. Post nos. 12 and 15 rotated slightly backward and sustained minor twisting. Post nos. 13 and 14 sustained large downstream and backward rotations while twisting upstream. Tire marks were found on post no. 13.

Post nos. 13 and 14 were disengaged from the rail due to pullout of the guardrail bolt and deformation of the guardrail slot. A small tear was found in the slot at post no. 13. Gaps of ½ in. (3 mm) were present at the splices located between post nos. 2 and 3, 10 and 11, and 12 and 13.

General deformation and flattening of the W-beam rail occurred from post no. 12 to slightly downstream of post no. 15. Contact and tire marks were visible on the guardrail beginning 2 in. (51 mm) downstream of post no. 12 to 10 in. (254 mm) downstream of post no. 15. Slight buckling occurred at post no. 11 and between post nos. 11 and 12. More severe buckling occurred at post nos. 12 and 15.

A 1½-in. (32-mm) soil gap was present at the upstream edge of post no. 1, and a ½-in. (13-mm) soil gap was present on the downstream edge of post no. 2. A soil gap of ½ in. (13 mm) was present at the downstream edge of post no. 29.

The maximum permanent set rail and post deflections were 14 in. (356 mm) at the midspan between post nos. 13 and 14 and 18 in. (457 mm) at post no. 13, respectively, as measured at the test site. The maximum lateral dynamic rail and post deflections were 24.4 in.

(621 mm) at post no. 13 and 23.6 in. (600 mm) at post no. 13, respectively, as determined from high-speed digital video analysis. The working width of the system was 45.1 in. (1,146 mm), also determined from high-speed video analysis.

# **6.6 Vehicle Damage**

The damage to the vehicle was moderate, as shown in Figures 34 and 35. The maximum occupant compartment deformations are listed in Table 5 along with the deformation limits established in MASH for various areas of the occupant compartment. It should be noted that none of the MASH established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix D.

Table 5. Maximum Occupant Compartment Deformations by Location

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	<sup>3</sup> / <sub>4</sub> (19)	≤9 (229)
Floor Pan & Transmission Tunnel	1/4 (6)	≤ 12 (305)
Side Front Panel (in Front of A-Pillar)	1/4 (6)	≤ 12 (305)
Side Door (Above Seat)	1/2 (13)	≤9 (229)
Side Door (Below Seat)	1/2 (13)	≤ 12 (305)
Roof	0	≤4 (102)
Windshield	0	≤ 3 (76)

The majority of the damage was concentrated on the right-front corner and right side of the vehicle where the impact occurred. The right side of the front bumper was crushed inward and back. The right-front fender was dented and scraped. The right-front wheel was detached from the vehicle, and the right-front rim was scraped and deformed. The right-front brake lines were cut, and the right-upper control arm was bent inward. The right-side headlight and foglight

were disengaged from the vehicle. Denting and scraping were observed on the entire right side of the vehicle. The right-rear corner of the vehicle and right side of the rear bumper were slightly crushed inward. The right-side taillight was removed. The hood was ajar and slightly crushed inward. Slight deformation to the front of the vehicle frame was observed. The roof and all window glass remained undamaged.

# 6.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 6. The OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 6. The results of the occupant risk analysis, as determined from the accelerometer data, are summarized in Figure 19. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix E.

Table 6. Summary of OIV, ORA, THIV, and PHD Values, Test No. MGSC-6

Evaluation Criteria		Transducer			MASH	
		EDR-3	DTS Set 1	DTS Set 2	Limits	
OIV	Longitudinal	-11.60 (-3.54)	-13.94 (-4.25)	-14.22 (-4.34)	≤ 40 (12.2)	
ft/s (m/s)	Lateral	-13.91 (-4.24)	-13.55 (-4.13)	-14.06 (-4.29)	≤ 40 (12.2)	
ORA	Longitudinal	-10.40	-10.71	-11.02	≤ 20.49	
g's	Lateral	-6.60	-7.02	-6.84	≤ 20.49	
THIV ft/s (m/s)		NA	18.35 (5.59)	NA	not required	
PHD g's		NA	11.08	NA	not required	
ASI		0.45	0.49	NA	not required	

#### **6.8 Discussion**

The analysis of the test results for test no. MGSC-6 showed that the MGS and curb configuration adequately contained and redirected the 2270P vehicle with controlled lateral displacements of the barrier. There were no detached elements nor fragments which showed potential for penetrating the occupant compartment nor presented undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix E, were well below the limit of 75 degrees recommended by MASH. After impact, the vehicle exited the barrier at an angle of 18.7 degrees, and its trajectory did not violate the bounds of the exit box. Therefore, test no. MGSC-6 conducted on the MGS offset 6 ft (1.83 m) behind a 6-in. (152-mm) high AASHTO Type B curb was determined to be acceptable according to the MASH TL-2 safety performance criteria for test designation no. 2-11.

-0.180 sec

32'-9<sup>1</sup>/<sub>2</sub>" [10.0 m]+

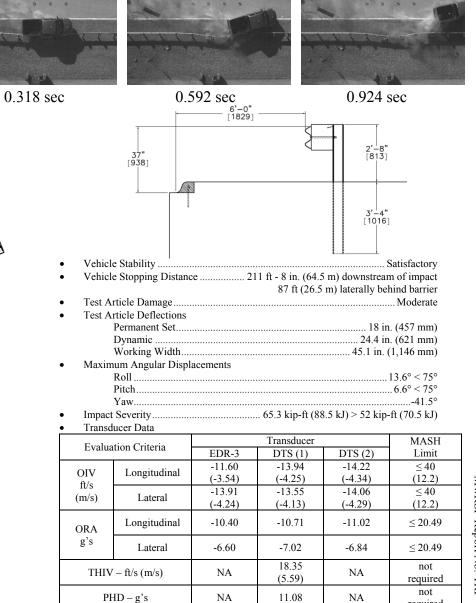
87' [26.5 m]

Key Component – Midwest Guardrail System

Key Component – AASHTO Type B Curb

Impact Conditions

Exit Conditions



0.45

0.49

NA

ASI

Figure 19. Summary of Test Results and Sequential Photographs, Test No. MGSC-6

0.000 sec

\_\_\_\_211'-8" [64.5 m]-

Test Agency MwRSF

Test Number MGSC-6

 Date
 11/10/2009

 MASH Test Designation
 2-11

Test Article ...... MGS offset 6 ft (1.83 m) behind 6-in. (152-mm) high curb

Angle (Guardrail) 22.5 deg

Location ..... 15 ft - 2½ in. (4.6 m) US of splice between posts 14 and 15

VDS<sup>[16]</sup> 1-RFQ-3

CDC<sup>[17]</sup>......1-RYEW-3

Maximum Interior Deformation...... <sup>3</sup>/<sub>4</sub> in. (19 mm)at wheel well/toe pan

Exit Box Criterion Pass

\_16'-8<sup>3</sup>/<sub>4</sub>" [5.1 m]

November 24, 2010 MwRSF Report No. TRP-03-237-10

required

not

required



Figure 20. Additional Sequential Photographs, Test No. MGSC-6

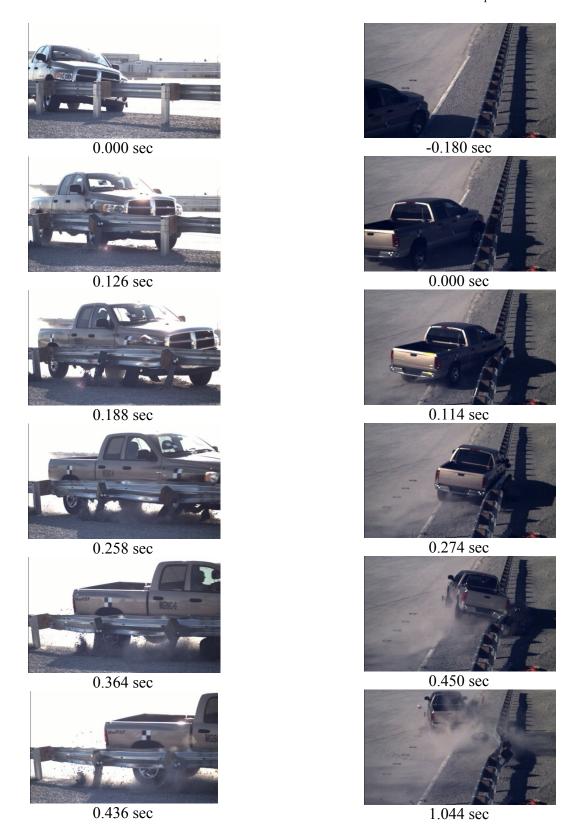


Figure 21. Additional Sequential Photographs, Test No. MGSC-6



Figure 22. Additional Sequential Photographs, Test No. MGSC-6



Figure 23. Documentary Photographs, Test No. MGSC-6













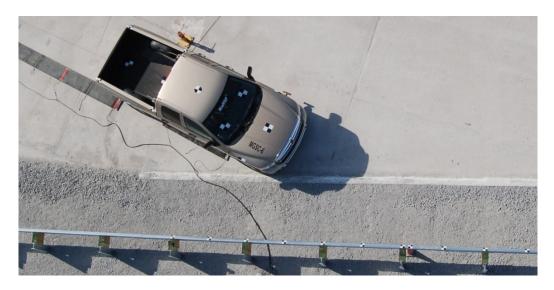




Figure 24. Documentary Photographs, Test No. MGSC-6



Figure 25. Documentary Photographs, Test No. MGSC-6





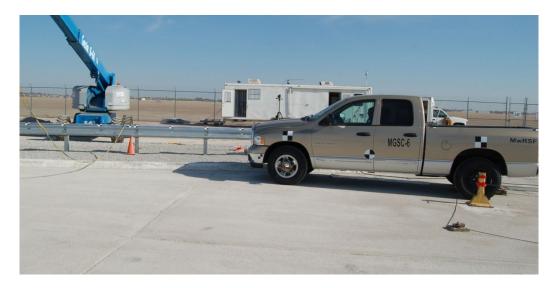


Figure 26. Impact Location, Test No. MGSC-6

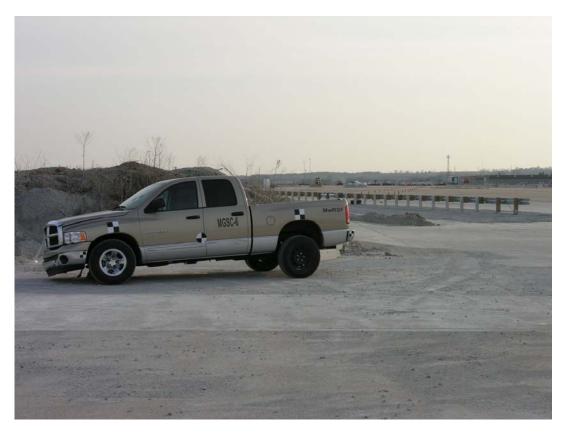




Figure 27. Vehicle Final Position and Trajectory Marks, Test No. MGSC-6





Figure 28. System Damage, Test No. MGSC-6





Figure 29. Post No. 12 Damage, Test No. MGSC-6





Figure 30. Post No. 13 Damage, Test No. MGSC-6





Figure 31. Post No. 14 Damage, Test No. MGSC-6





Figure 32. Post No. 15 Damage, Test No. MGSC-6



















Figure 34. Vehicle Damage, Test No. MGSC-6





Figure 35. Undercarriage Damage, Test No. MGSC-6

#### 7 DISCUSSION OF FINDINGS

Two items must be considered in determining the lateral placement of a 6-in. (152-mm) high curb relative to the MGS when installed with a 37-in. (940-mm) top rail height relative to the roadway at the toe of the curb.

First, if there is a zero offset (i.e., the rail face is aligned directly over the face of the curb), then a vehicle (2270P or 1100C) would impact the rail with its tires still on the roadway. The vehicle could wedge beneath the raised rail (i.e., the MGS installed at 37 in. (940 mm) relative to the roadway) with potentially severe consequences. This behavior cannot be accurately predicted and would require full-scale crash testing to fully understand the phenomena. For greater lateral offsets between the MGS and the curb, the relationship between the vehicle and the MGS becomes more like the standard 31-in. (787-mm) tall MGS placed over the curb.

Second, it is believed that vehicles cannot become wedged beneath the rail for offsets of at least 4 ft (1.22 m) from the curb, as the curb and ground geometry lower the effective rail height. Note that the small car (1100C), which becomes airborne following impact with the curb, may wedge itself under the rail due to front end suspension compression upon landing on the ground. Based on previous 25-degree angle vehicle-to-curb impact studies performed by MwRSF [10-11] and NCAC [unpublished work], it is believed that the 1100C vehicle bumper will have returned at least to its normal static equilibrium height when the vehicle has reached the 4-ft (1.22-m) lateral offset. Thus, a minimum lateral offset of 4 ft (1.22 m) is recommended for raising the MGS rail height from 31 in. (787 mm) to 37 in. (940 mm) relative to the roadway at the toe of the curb. The 37 in. (940-mm) rail height was determined by combining the heights of the 6-in. (152-mm) curb with that for the 31 in. (787 mm) MGS.

### 8 SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

The Midwest Guardrail System was installed 6 ft (1.83 m) behind a 6-in. (152-mm) high, AASHTO Type B curb and was subjected to full-scale crash testing under TL-2 conditions, as defined in MASH. The lateral offset and impact conditions were selected after the system failed to meet the TL-3 criteria with an 8-ft (2.44-m) lateral offset behind the same curb. LS-DYNA simulations demonstrated that a 6-ft (1.83-m) lateral offset produced the greatest propensity for truck override of the barrier at the TL-2 impact conditions.

Full-scale crash testing demonstrated that the MGS with a 37-in. (940-mm) top rail height relative to the roadway is valid for MASH TL-2 for lateral offsets ranging between 4 and 12 ft (1.22 and 3.66 m) behind a 6-in. (152-mm) high, AASHTO Type B curb. Note that no relevant TL-2 crash tests were available for 1100C and/or 2270P vehicles striking a curb without other barriers located behind the curb. Thus, a maximum 12-ft (3.66-m) lateral offset is recommended; since, prior TL-3 curb testing indicated potential vehicle problems beyond a 12-ft (3.66-m) lateral offset. As discussed in References 10 and 11, the Type B curb is considered the worst-case geometry for sloped curbs. Thus, this recommendation is also valid for other sloped curbs with heights of 6 in. (152 mm) or less. For lower-height curbs, the rail height should be reduced in order to maintain the 31-in. (787-mm) top rail height relative to the ground behind the curb.

The full-scale crash testing was conducted with level terrain in front of and behind the curb. However, the research sponsors have indicated that the actual terrain is rarely level in front of and behind the curb. A common roadway slope found in front of curbs consists of a 6 percent slope toward the curb. Typical slopes found behind curbs include a 2 percent slope toward the curb for adjacent sidewalks and a 4 percent slope toward or away from the curb for grass terrain.

The researchers are not concerned with a traveled way sloped downward toward the gutter region found in front of curbs. However, it is the researchers' opinion that sloped terrain

behind the curb can significantly affect a guardrail system's redirective capability. In order to address that concern, it is recommended that the top rail height relative to the top of the curb range between 31 and 32 in. (787 and 813 mm), while at the same time the rail height relative to the ground directly below the rail be no higher than 34 inches (864 mm). Thus, the desired lateral offset from the curb as well as the two criteria noted in the previous sentence must be used to determine an acceptable ground slope.

The researchers have no evidence to make any other statements regarding the use of the MGS with 6-in. (152-mm) high curbs under the TL-2 impact conditions. For example, there is no point where the rail height makes the change from 31 in. (787 mm) to 37 in. (940 mm) relative to the roadway because the valid range for the 31-in. (787-mm) rail height relative to the roadway is unknown.

Currently, there are neither plans nor budget to determine any other valid scenarios for MGS placement relative to a curb. It is believed that any such determination would require additional full-scale vehicle crash testing.

November 24, 2010 MwRSF Report No. TRP-03-237-10

Table 7. Summary of Safety Performance Evaluation Results

Evaluation Factors		Evaluation Criteria			Test No. MGSC-6	
Structural Adequacy	A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.			S	
	D.	Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH.				
	F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.				
	Н.	Occupant Impact Velocities (OIV) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:				
Occupant Risk		Occupant Impact Velocity Limits				
KISK		Component	Preferred	Maximum	S	
		Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)		
	I. The Occupant Ridedown Acceleration (ORA) (see Appendix A, Section A5.3 of MASH for calculation procedure) should satisfy the following limits:					
		Occupant Ridedown Acceleration Limits				
		Component	Preferred	Maximum		
		Longitudinal and Lateral	15.0 g's	20.49 g's		

S – Satisfactory U – Unsatisfactory NA - Not Applicable

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- 3. Polivka, K.A., Faller, R.K., Sicking, D.L., Rohde, J.R., Reid, J.D., and Holloway, J.C., *Guardrail and Guardrail Terminals Installed Over Curbs Phase II*, Final Report to the Midwest States Regional Pooled Fund, MwRSF Research Report No. TRP-03-105-00, Project No. SPR-3(017)-Year 10, Project Code RPFP-98-03, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, November 5, 2001.
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- 10. Zhu, L., <u>Critical Offset of the Midwest Guardrail System Behind a Curb</u>, Thesis, University of Nebraska-Lincoln, Lincoln, Nebraska, June 2008.
- 11. Zhu, L., Reid, J.D., Faller, R.K., Bielenberg, R.W., Sicking, D.L., Polivka, K.A., Rohde, J.R., *Installation Guidelines for MGS and 6-in. High, AASHTO Type B Curb Combination Part I: Vehicle-Curb Testing and LS-DYNA Analysis*, Final Report to the Midwest States Regional Pooled Fund Program, Transportation Research Report No. TRP-03-205-09, Project No. SPR-3(017)-Year 17, Project Code RPFP-07-03, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, May 6, 2009.
- 12. Thiele, J.C., Lechtenberg, K.A., Reid, J.D., Faller, R.K., Sicking, D.L., and Bielenberg, R.W., *Performance Limits for 6-in. (152-mm) High Curbs Placed in Advance of the MGS Using MASH Vehicles Part II: Full-Scale Crash Testing*, Final Report to the Midwest States Regional Pooled Fund Program, Transportation Research Report No. TRP-03-221-09, Project No. SPR-3(017)-Year 17, Project Code RPFP-07-03, Midwest Roadside Safety Facility, University of Nebraska-Lincoln, Lincoln, Nebraska, October 30, 2009.
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## 10 APPENDICES

## Appendix A. Material Specifications

## Certified Inalysis

Trinity Highway Products, LLC

425 E. O'Connor

Order Number: 1114174

Lima, OH

Customer PO: 2213

BOL Number: 51169

P.O. BOX 81097

Document #: 1 Shipped To: NE

LINCOLN, NE 68501-1097

Customer: MIDWEST MACH.& SUPPLY CO.

Use State: NE

Project: RESALE

	Qty	Part # Description	Spec CL	TY Heat Code/ Heat #	Yield	TS	Elg	C	Mn	P	S	Si	Cu	Cb	Cr	Vn	ACW
+	750	545G 6'0 POST/DB:DDR	A-36	J86489	50,565	68,830	26.1 0.	.090	0.950	0.010	0.040	0.200	0.290	0.00	0.160	0.003	4
	50	14662G 6'6 POST/8.5#/DB:DDR NB	A-36	J86489	50,565	68,830	26.1 0.	.090	0.950	0.010	0.040	0.200	0.290	0.00	0.160	0.003	4

Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT.

ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHERWISE STATED.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

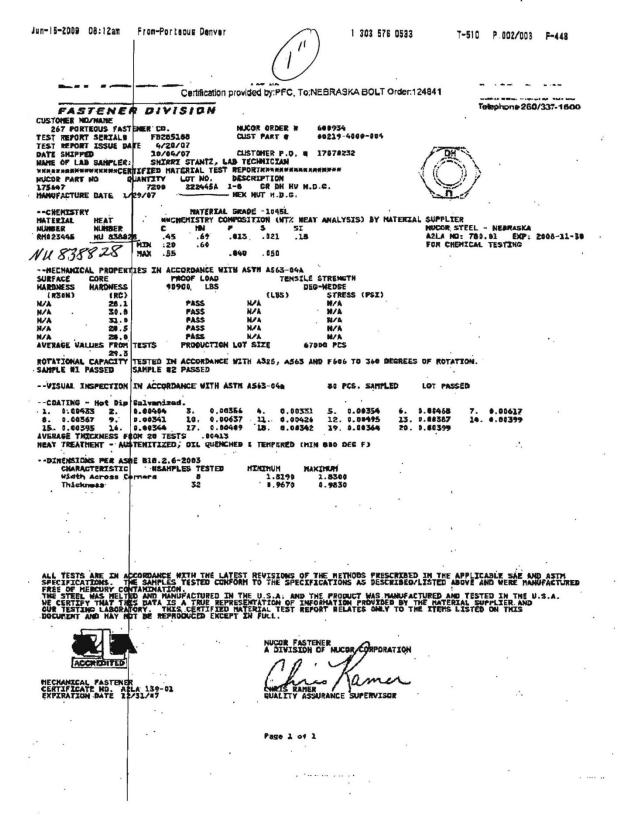
3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING STRENGTH - 49 100 LB

State of Ohio, County of Allen. Sworn and subscribed before me this 16th day of September, 2009

Commission Expires / 1,50

1 of 1

As of: 9/16/09



E'd XULL LECUES UN ALL LECUES UN CONTINUED SEES BOOZ LI UNC Figure A-2. W6x8.5 (W152x12.6) Posts Material Specification (Continued)



#### CERTIFICATE OF COMPLIANCE

1. Post

MARCH 12: 2009.

MIDWEST MACHENERY & SUPPLY POBOX 81097 LINCOLN, NE 68501

The following material delivered on 3/12/09 on bill of lading number 19216 has been inspected before and after treatment and is in full compliance with applicable Mebraska Department of Roads requirements for southern yellow pine Timber Guardrail Components, preservative treated with Chromated-Copper-Arsenate (CCA-C) to a minimum retention of .60 lbs/cu.ft. The acceptance of each piece by company quality control is indicated by a Hammer brand on the end of each piece.

MAT	ERIAL	CHARGE#	DATE	RETENTION	QUANTITY
6x8x14"	Blockout (CD)	09-26	1/29/09	0.66	70
6x8x14*	Blockout (CD)	09-67	2/19/09	0.60	70
- 6x8x14"	OCD Blockout	09-95	3/5/09	0.62	140
6x8x6'	CRT Post	09-94	3/5/09	0.69	70
6x8x6*	Line Post	09-94	3/5/08	0.69	70
51/2X71/2X421/2"	BCT Post	08-74	1/29/08	0.67	48
6x8x18"	Blockout	09-95	3/5/00	0.62	70
6x8x18"	Blockout ' 11.	: 4.09.95 · ii	3/5/09	0.62	70

THIS CERTIFICATE APPLIES TO MATERIAL OFFICED FOR YOUR OLDER TOO. 1. 2117

FOR ANY INQUIRIES, PLEASE RETAIN THIS DOCUMENT FOR FUTURE REFERENCE.

. THANK YOU FOR YOUR ORDER.

SINCEREILY,

Karen Storey

SIGNED REFORE ME THIS 12 DAY OF MARCH 2009.

Noney: And State of the State o

WIDMEST MACHINERY

402-761-3288

11/05/5003 00:23



11/02/2009 09:59

402-761-3288

MIDWEST MACHINERY

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Figure A-4. Post Blockouts Certificate of Compliance (Continued)

Dawn R. Balton Notary Public, State of Chio My Commission Expires February 24, 2008

GREGORY HIGHWAY PRODUCTS, INC.

Figure A-5. 12-ft 6-in. (3.81-m) W-Beam Guardrail Material Specification

Vice President of Sales and Marketing Gregory Highway Products, Inc. RECEIVED

03/09/2009

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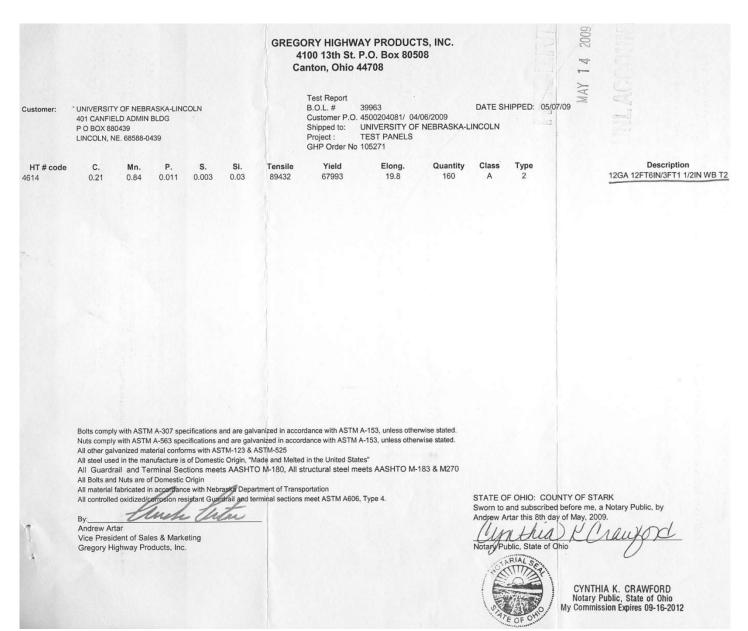


Figure A-6. Additional 12-ft 6-in. (3.81-m) W-Beam Guardrail Material Specification

# November 24, 2010 MwRSF Report No. TRP-03-237-10

## **Certified Test Report**

#### NORTH STAR BLUESCOPE STEEL LLC

6767 County Road 9 Delta, Ohio 43515 Telephone: (888) 822-2112

#### Customer:

Lawson Steel, Inc.

3238 E. 82nd St.

Order Number

171137

Ordered Width (mm/in)

1454.150 / 57.250

Cleveland, OH 44104

Line Item Number

1

Ordered Gauge (mm/in)

2.438 / 0.096

ASTM A568, 1018 CQ Modified

Customer P.O.: 021336

Cust. Ref/Part # n/a

Heat Number Coll Number 111813 842536 Material Description
Production Date/Time

Mar 1 2008 5:41PM

**Heat Chemical Analysis (wt%)** 

Γ	Туре	С	Mn	P	S	Si	Ai	Cu	Cr	Ni	Мо	Sn	N	В	٧	Nb	TI	Ca
1	Heat	0.19	0.73	0.012	0.003	0.03	0.02	0.09	0.04	0.03	0.01	0.00	0.005	0.0000	0.000	0.000	0.002	0.002

### **Mechanical Test Report**

All mechanical tests are performed on a sample from the tail of a coil.							
Yield Strength	Tensile Strength	% Elongation in 2 inches					
64,860 psi	83,230 psi	23.5%					

This material has been produced and tested in accordance with each of the following applicable standards: ASTM E 1806-86, ASTM E 415-98a, ASTM A 751-01, ASTM A 370-03a, JIS Z2201:1998, JIS Z 2241:1998. This report certifies that the above test results are representative of those contained in the records of North Star BlueScope Steel LLC for the material identified in this test report and is intended to comply with the requirements of the material description. North Star BlueScope Steel LLC is not responsible for the inability of this material to meet specific applications. Any modifications to this certificate as provided negates the validity of this test report. All reproductions must have the written approval of North Star BlueScope Steel. This product was manufactured, metted, cast, and hot-rolled (min. 3:1 reduction ratio), entirely within the U.S.A at North Star BlueScope Steel LLC, Delta, Ohio. This material was not exposed to Mercury or any alloy which is liquid at ambient temperature during processing or write in North Star BlueScope Steel LLC possession. Test equipment calibration certificates are available upon request. Uncertainty calculations are calculated in accordance with NIST standards and are maintained at a 4:1 ratio in accordance with NIST standards. Uncertainty data is available upon request.

**Tim Mitchell** 

Inthe o

Manager Quality Assurance and Technology

Date Issued: Mar 12, 2008 11:00:32

Revision#: 01

PAGE BOIDE

MIDWEST MACHINERY

06/04/2009 16:36

402-761-3288

MID WEST FABRICATING CO.

#### CERTIFICATE OF COMPLIANCE

WE CERTIFY THAT ALL BOLTS ARE MADE AND MANUFACTURED IN THE USA.

TO: TRINITY INDUSTRIES INC.

Plant #55

425 E. O'Connor

419-222-7

Lima,Ohio

SHIP DATE: 11/6/2008

MANUFACTURER: MID WEST FABRICATING CO.

ASTM: A307A

GALVANIZERS: Columbus/Piolt

TO A-153 CLASS C

QTY	PART NO.	HEAT NO.	LOT NO.	P.O.NO.
3,52	24 5/8.X 10-6"	7261134	85204	126266BR80
1,07	'6 5/8 X 10-6"	7261134	85204	126266BR78
8,90	00 5/8 X 10-6"	7261134	85204	126266BR74
YLIG 4.50	00 5/8 X 10-6"	7261611 <b>%</b>	85217	126266BR74
2,58	50 5/8 X 10W-6"	7261286	85180	126266BR84
4,50	0 5/8 X 14-6*	7366618	85199	126266BR68
6,00	0 5/8 X 18-6"	7366618	85157	126266BR84
1,53	6 5/8 X 18-6"	7366618	85157	126266BR74
130	5/8 X 18-6"	7366618	85156	126266BR74
2,96	4 5/8 X 18-6"	7366618	85149	126266BR74
4,37	0 5/8 X 18-6"	7261611	85146	126266BR74 ·
400	5/8 X 3.5°	5978691	85016	126266BR82

Signature D. Anuth

TITLE: QUALITY CONTROL

DATE:

11/6/2008

. 313 North Johns Street • Amanda, Ohio 43102 • 740/969 4411 • FAX: 740/969-4433

Figure A-8. %-in. (15.9-mm) x 10-in. (254-mm) Guardrail Bolt/Nut Material Specification

06.'04,2009 16:36 402-761-3288

MIDWEST MACHINERY

PAGE 15/52

04/14/2009 10:14 FAX 740 681 4433

MID WEST FAB: ROCKMILL

Ø002



#### **CERTIFICATE OF COMPLIANCE**

WE CERTIFY THAT ALL BOLTS ARE MADE AND MANUFACTURED IN THE USA.

45801

TO: TRINITY INDUSTRIES INC.

Plant #55

550 East Robb Ave.

419-222-7398

Lime, Ohio

SHIP DATE: 4/13/2009

MANUFACTURER: MID WEST FABRICATING CO.

**ASTM:** A307A

GALVANIZERS: Bristol/Pilot/Columbus TO A-153 CLASS C

5,250	5/8 X 10-6"	20060370	95055	130236BR25
2,625	5/8 X 10-6"	20060370	95052	130236BR25
28,500	5/8 X14-6"	7366618	85199	

Signature W. Smith. W. Sm

TITLE: QUALITY CONTROL 4/13/2009

313 North Johns Street \* Amanda, Ohio 43102 \* 740/969-4411 \* FAX: 740/969-4433

Figure A-9. 5/8-in. (15.9-mm) Dia. x 14-in. (356-mm) Long Bolt/Nut Material Specification

A25 E. O'Connor Lima, QH Print Date: 6/30/08 Costomer: MIDWEST MACH & SUPPLY CO. Sales Order: 1093497 Customer PO: 2030 Project: RESALE P.O. BOX 81097 Shipped To: NE BOL# 43073

Document# 1

LINCOLN, NE 68501-1097

#### Trinity Highway Products. LLC

Use State: KS

Certificate Of Compliance For Trinity Industries, Inc. \*\* SLOTTED RAIL TERMINAL \*\*

NCHRP Report 350 Compliant

È Pieces	Description		
32 32 32 32 32 32	12/12/6/S SRT-1		
罢 32	12/25'0/SPEC/S SRT-2		
∯ 32	3/16X12.5X16 CAB ANC BRKT		
50 64	2" X 5 1/2" PIPE (LONG) 6'0 TUBE SL/ 188X8X6		
32 32	5/8 X 6 X 8 BEARING PLATE		
153MQIW 32 32	12/BUFFER/ROLLED		
₹ 32	CBL 3/4X6/6/DBL SWG/MOHWD		
640	5/8" RD WASHER 1 3/4 OD		
1,728	5/8" GR HEX NUT		
1,152	5/8"X1,25" GR BOLT		
256	5/8"X],5" HEX BOLT A307		
F 54	5/6"X9.5" HEX BOLT A307		
ALL STBEL U ALL STBEL U ALL GUARDE ALL OTHER C BOLTS COMPI NTS COMPI NT S CAPL STRENGTH - 4	Ounty of Allen. Sworn and Subscribed before movings 30th day of June, 2008  Trinity Highway Products, LLC  Certified By:	erwise st	TATED.

Figure A-10. 5/8-in. (15.9-mm) Dia. Bolts, Washers, and Nuts Certificate of Compliance

#### TRINITY HIGHWAY PRODUCTS, LCC. Plant #55 425 E. O' CONNOR AVENUE Lima, OH 45801

419-227-1296



#### MATERIAL CERTIFICATION

	s or	ER:	STO	CK			DAT	E: Mat	ch 10, 2	009	301	H.M. Annuary (Sp. States over	The same of the same of	-	
							INVC	ICE#		and the second second	· Samuel Alfred Street Control of the Control of th	Vancour de la company de	-	of constant Market Champion and pages	
and the same	on the second	NA-LLEAN CONT.		mppp_onemonicial_on		Statement of the statem	LOT	NUMB	er: 08	11288		- to a second	and the state of t	Contract Con	
PA	RTNU	MHER	: 336	9G			QUAL	YTTY	107,4	53	Charles and the Control of the Control	eren communication gallow	- The Rose of the Real		
DE	scrip	TION:	5/8"¤ 1	( W" GI	r Bol	T	DAT	e shif	PED:						A CONTRACTOR OF THE PARTY OF TH
SPI	ECIFIC	CATIO	YS: AS	TM A3	07-A /A	153	HEA"	F#: 730	6484,72	62312	ne ne state de la companie de la co	100		The second of the second of	
			* Table de la comp	and the second	7000	Ma	TERI	al Chi	emistr	TY.	The same of the same of	A STATE OF THE PARTY OF THE PAR	and the second s		
c	MN	P	8	SI	MI	CR	мо	cu	SIN	٧	AL	N	B	Ti	NE
3	.38	.007	.002	.10	.04	.06	.02	.03	.601	.002	.037	.004	.000	.000	.000
2	7,40	********	b	Sandamine .		1	The same of the sa	1	I man	- NATE OF THE PERSON	COAT	-	6460	I success	+000

\*\*\*\* This product was manufactured in the united states of America\*\*\*

THE MATERIAL USED IN THIS PRODUCT WAS MELTED AND MANUFACTURED IN THE

WE HEREBY CERTIFY THAT TO THE BEST OF OUR KNOWLEDGE CONTAINED HEREIN IS CORRECT.

STATE OF OHIO, COUNTY OF ALLEN SWORN AND SUBSCRIBED BEFORE ME THIS 10<sup>TH</sup> DAY OF MARCH, 2009

425 E. O 'CONNOR AVENUE

LIMA, OH 45901

419-227-1296

Figure A-11. %-in. (15.9-mm) Guardrail Splice Bolts Material Specification

MIDWEST MACHINERY

PAGE 05/52

06/04/2009 16:36

402-761-3288

Trinity Industries, Inc.

No. 1357 P. 31/31

Trinity Meials Laboratory

Apr. 21. 2000 2:44PM

A CHVISION OF TRINITY INDUSTRIES 4001 RWING BLVD, 78247 - P.O. BOX 566887 DALLAS, TX 76858-2887

Phone: 214,589.7561 FAX: 214,569.7586

THE THE PARTY OF T

NACAD

rmser 214,309.7341 pps. 214,359.736

Lab No: S116344F CHERITY A. MASON TRINITY HWY PRODUCTS, LLC #55 ROLLFORM UMA, OH 49801

Receives Date: 11/21/2009
Filest Code:
Float Number: 545770
PO or Work Cider: Labr. 081031N2
Test Span: F908 ASTM METHODS
Other Information: SOR: 55-45667

Completion Date; 12/11/2008 Weld Spec: Material Type: A 563 A Material Size: 518° GR Nata

OTHER TEST:

200: 7

Type: NUT PROOF LOAD

SAMPLES PASSED PROOF LOADS OF 18,980 LBS.

Gusmity Amount: 6

Seq: 2

Type: HEAD MARKINGS TRN L

Quantity Amount: 0

We carrily the above results to be a true and occurrent representation of the samplets) submitted. Attending or period approduction of this report was void confliction. NVLAP Confliction of Accretication effective through 12-31-78. Take report may not be used to claim product carringulon, approved, or and essentiant by NVLAP. NST, or any agency of the faderal government.

Les Conscion, Shelippi St. Boulon

Page 2 of 2

Figure A-12. 5%-in. (15.9-mm) Guardrail Splice Nuts Material Specification

402-761-3288 06/04/2009 16:36

Apr. 24. 2009 1:44PM

MIDWEST MACHINERY

PAGE 04/04

Trinity Industries, Inc.

No. 1357 P. 30/31

#### Trinity Metals Laboratory

A DIVISION OF YAMITY INDUSTRIES 4001 IRVING BLVD. 75247 - P.O. BCR 562867 DALLAS, TX 75269-8887

Phone: 214.560,7591 FAX: 214,620,7594

4 19

Lab No: 8110344F

CHERITY A MASON TRINITY HWY PRODUCTS, LLC 465 **ROLLFORM** 

Reserved Doto: 11/21/5009 Heat Code: Heat Number: 545770 PO or Work Order: Lettl: 091031H2 Test Spec: FEGS ASTM METHODS

Other Information: SOM: 55-46867

Completion Date: 12/0/12(19) Weld Speci Malerial Type: A 553 A Material Size: 5/6" GR Nuts

#### HARDNESS TEST:

Sag:1

Lima, oh 45001

Hadrass Type: HARDNESS ROCKWELL SW Hordnese Lossion: SURFACE of WHENCH FLAT - A

Hordrons Average: 88

Measured Value	Messured Amt
Maonuned Value	98
Measured Value	95

PASSED

Spg:2

Herdness Type: HARDNESS ROCKWELL BW Hammasa Locobon: SURFACE of WRENCH FLAT - B

Hardnass Average; 89

Measured Value	Massured Amt
Managed Value	28
Measured Valua	80

PASSED

PASSED

PASSED

Sen:2

Hardness Type: HARONESS FLOCKWELL BW Manineso Location: SURFACE of WARNON RAT - C.

Handames Average: 89.5

Mensured Value	Messured Amt
Messured Value	98
Mesoured Value	80

Seg:4

Hardness Type: HARDNESS ROCKWELL BW Hardness Location: SURFACE of WRENCH FLAT - O Hardnoss Average: 90

Moseurod Value	Measured Amt
Messured Vickes	25

Segra

Mardness Type: HARDNESS ROCKWELL BW Hardress Location: SURFACE of WRENCH PLAT - E Mardness Average: 82

Measured Volum 90

PASSED

Mescured Value	Mossured Amt
Messured Value	81
Measured Value	\$3

We cartify the above results to be a true and acquirin representation of the sample(s) automited. Alternion or partial reproduction of this report was void confidention, MVLAP Continues of According to allering innuels 12-31-46. This report may not be used to date product confidention, approved, or endotesement by MVLAP, MST, or any agency of the federal government.

Page 1 of 2

Figure A-13. %-in. (15.9-mm) Guardrail Splice Nuts Material Specification (Continued)

402-761-3288

MIDWEST MACHINERY

PAGE BI/OZ

06/04/2009 15:36

Trinity Industries, Inc. Apr. 21. 2009 3:43PM

No. 1357 P. 27/31



#### TRINITY HIGHWAY PRODUCTS, LLC. 425 E. O'COMNOR AVENUE LIMA, OHIO 45201 419-227-1296

#### MATERIAL CERTIFICATION

CUSTOMER: STOCK	DATE: NOVEMBER 18, 2008
	INVOICE #:
	LOT 4: 081031N2
PART NUMBER: 3340G	QUANTITY: 110,000
	,
DESCRIPTION: 5/8" GR NUT SPECIFICATIONS:	DATE SHIPPED:
ASTM AS63-A/A153	REAT #: \$45770

#### MATERIAL CHEMISTY

Parameter Printers	Signature or to supply	AND DESCRIPTIONS OF THE PERSONS OF	Separation of the separation o	The second second	and handed	- ENGINE	MINE PROMISE	Secretary Secretary Sec.	processor and the second	The same of	- HELLOW THE PARTY	Mention make make make make make make make make	The same of the sa	THE REAL PROPERTY.	- The second second	Marie Comments of the	
C	MM	þ	ŝ	<b>\$1</b>	CU	M	CR	MO	AL	¥	N	CB	BN	B	"I"	NB	- Adjusted to
418	.45	.003	.013	.090	.07	.Od	,09	.01	.023	.501	.0080	.000	,905	.0001	.001	.001	

#### PLATING AND/OR PROTECTIVE COATING

1.25 AVG. hot dip galyanizing (oz per sq. ft.)

\*\*\*\*THIS PRODUCT WAS MANUFACTURED IN THE UNITED STATES OF AMERICA\*\*\*

THE MATERIAL USED IN THIS PRODUCT WAS MELTED AND MANUFACTURED IN THE U.S.A.

We hereby certify that to the best of our knowledge CONTAINED HEREIN IS CORRECT.

MINITY HIGHWAY PROPUCTS, LLC.

STATE OF OHIO, COUNTY OF ALLEN SWORN AND SUBSCRIBED BEFORE ME THIS 13 DAY OF HOWEMBER 1886

NOTARY PUBLIC

425 E. O'COMNOR AVENUE

LIMA, OHIO 45801

419-227-1296

Figure A-14. %-in. (15.9-mm) Guardrail Splice Nuts Material Specification (Continued)

PAGE 82/02

MIDWEST MACHINERY 402-751-3288 No. 1357 P. 28/31 16:36 402 2009 3:437M Trinity Industries, Inc. JUN-05-2008 THU 11:20 AM CHARTER ROLLING EVE DEPT +1 262 266 2554 . P. 05 1650 Cold Springs Road Sauladille Wisconsin 53080 CHARTER STEEL CHARTER STEEL TEST REPORT (262) 268-2400 Reverse Mas Text And Codes 1-900-437-6789 Charter Manufacturing Company, Inc. FAX (262) 268-2570 127698 1009443 Trinity Highway Fred, LLC 273108 428 E. O Conner Ave 545770 Lima, OH 45807. 357211 Attn: Attn: Aug Henline 1010 A ak for aho i hereby dertify that the metarial Generical herein has been manufactured in accordance with the appointment and change and change and the motive side, and that it calleliae these popularments, Test Beschis of Hast Load Eds770 Lab Codes 7305 Chomlessy 0,050 0.0001 0.001 0.00% CHEM. THEY ATHON EXT - CHEEN = NEW Hens Unive H of Tagin BB LAS - ORES-82 殿仓 PLOCESPOLE S IMPSWI \$2 Hookwell C (MAO) RC LAB - N/R 0 OC DEVIATION EXT. ORSEN - NIS Year Reseats of Proceeding Let # do deviation ext, processed = nin ikanpianinias pu Cimin Sind Guilly Manuel live B. 12-65-67 Maete eveletina spaditurikana with my spalinikia Civitae Sind Curtamin Decement i accomissio der the federalez customer datustenist Dated = Additional Comments: MELTED AND MARKIFACTURED IN THE USA Giveries Steel Bosekulla, W. 1484 Jenios Semilio Rom: Lesid's Mail Control Boy and Manager of Quality Assurance 08/04/2003 Pak number: (410) 222-7388

Figure A-15. 5%-in. (15.9-mm) Guardrail Splice Nuts Material Specification (Continued)

PAGE 03/52

MIDWEST MACHINERY

402-761-3288 6/04/2009 16:36

Trinity Industries, Inc. Apr. 21. 2009 3:43PM

P. 29/31 No. 1357

JUN-05-2000 TAU 11:23 AM CHARTER ROLLING CVC DEPT

The following statements are applicable to the material described on the front of it. Except as noted, the steel supplied for this order was maked, rolled and processed in 2. Mercury was not used during the manufacture of this product, not was the steet cury during processing.

Unless directed by the customer, there are no wolds in any of the colls produced for tale order. 1. The laboratory that generated the analytical or test results can be identified in test results can be identified in the results are the identified in the ident

1	Certificata	The state of the s	7 10 5 10 10 10 10	Comment of the state of the sta	Carl Safe Adventions of the Annual Control of the Article Annual C
	Number	Lab Code	annethanne and a series	yafaradas	Address
	0358-01	7388	CSMD	Charter Steel Melting Division	1659 Cold Springs Road, Saukville, Wr 53080
	0388-02	8171	CSRD/ CSPU	Charter Steel Rolling/ Processing Division	1658 Cold Springs Road, Saukville, WI 33080
	0358-03	123633	pa	Charter Steel Chilo	6255 US Highway 23, Risingson, OH 43457

033001	(380	2014T)	Melting Ohvision	1004 Com Springs Hord, Seukare, WI 23080
0388-82	8171	CSRD/ CSPD	Charter Steel Rolling/ Processing Division	1658 Cold Springs Road, Saukväle, Wi Siggo
0358-03	123633	þą		6255 US Highway 23, Risingson, OH 43457
6358-04	125544	C9C	Charter Steal Cleveland	4300 E. 46 <sup>th</sup> St., Cuyehoge Heights, OH 44125-1004
0339.05	128003	CSDT	Charter Steel Debroit	23860 Sherwood Ava. Center Line, MJ 18015
*	B <sup>0</sup>	70.2	Subconfracted hast perior	med by laboratory not in Charter Steel system

5. When run by a Charter Steel laboratory, the following tests were performed according to the latest revisions of the specifications listed below, as noted in the Charter Steel Laboratory Quality Manual:

The same of the sa	the former and stated to be found the state of the	FROM BERTON A CONTRACTOR & L. WOOD FOR EAST WENT W
Test	possible Laboratory	Specification
Chemistry Analysis	CS/4D, CSC	ASTM E415: ASTM PLOIS
X-ray Fluorescence Stainless and Alicy Steel	CSC	ASTM ES72
. Macmelch	C5MD, CSC	ASTM E361
Hardenability (Jorniny)	CSMD, CSC	LASTM A255; SAE MOS; JIS GOSGI
Grain Size	CSMD	I ASTM E112
Tensile Test	CSRO/CSPO, P4, CSC, CSDT	ASTM EB: ASTM A370
Rockwell Hardness	CSMD, CSRD/CSPD, P4, CSC,	ASTM ELO; ASTM A370
The transfer and the second se	CSDT	Constitution of the second sec
Microstructure (spheroidbation)	CSRD/CSPD, P4	i Astm Addi
Inclusion Content (Methods A. E)	! CSRD/CSPD, CSC	ASTOM E45

Charter Steel has been accredited to perform all of the above tests by the American Association for Laboratory Accreditation (A2LA). These accreditations expire 01/31/09

All other test results associated with a Charter Steel laboratory that appear on the front of this report, if any, were performed according to documented procedures developed by Charter Steel and are not accred-Red by AZLA.

- 6. The test results on the front of this report are the true values measured on the samples taken from the production lot. They do not apply to any other sample.
- 7. This test report cannot be reproduced or distributed except in full without the written permission of Charter Steel. The primary customer whose name and address appear on the front of this form may reproduce this test report, subject to the following restrictions:
  - It may be distributed only to their customers

THE TAILS TO THE WORLD SEE STREET

- Both sides of all pages must be reproduced in full
- 8. This certification is given subject to the terms and conditions of sale provided in Charter Steel's acknowledigment (designated by our Sales Order number) to the customer's purchase order. Both Order numbers appear on the front page of this.Report.
- 9. Where the customer has provided a specification, the results on the front of this test report conform to that specification unless otherwise noted on this test report.



Figure A-16. %-in. (15.9-mm) Guardrail Splice Nuts Material Specification (Continued)

MATERIAL TEST REPORT JBE COMPANY, LLC 1717 W. 115th St. VTE: 09/25/07 Chicago, IL 60643 PAGE: . The Tube People Phone: 773-239-7700 BILL OF LADING: 164358 Phone: 1-800-LEAVITT Fax: 773-239-1023 CUST: STEEL & PIPE SUPPLY - CATOOSA OK TUBING MANUFACTURED IN USA www.leavitt-tube.com 1050 FORT GIBSON ROAD QA1002-0003 Rev. 0 CATOOSA OK 74015 ATTN: \* Test Report Desk 106201 8027185 CUSTOMER QTY. ORDER CUSTOMER **ASTM** ITEM NO. PIECES SIZE, GAUGE, LENGTH SHIPPED P.O. NUMBER PART NBR SPECIFICATION GRADE 1 8.625-322HRB 252 147 4500088611 1015580 1.000 A500-03b В 2 12X2-188HRB 480 240 4500088813 1016034 1.000 A500-03b В 3. - 4 28 8.625-322HRB 504 1,176 4500091471 1025579 1.000 A500-03b В 5 8X6-188HRB 480 360 4500092386 1029189 1.000 A500-03b В ITEM NO. 2 .3 5 1 COIL NO. 395453 395532 395813 395460 391232 HEAT NO. 722562 722551 722564 722564 A13386 CORRECTED COIL CARBON .210 .210 .210 .210 .220 .860 .820 .700 MANGANESE .820 .820 .004 .004 **PHOSPHORUS** .004 .006 .006 .004 006 .006 .003 SULFUR .006 047 .050 ALUMINUM .047 .047 .024 020 .030 .020 .030 SILICON .020 FLATTEN **FLARE** WELD TESTING FLATTEN **FLATTEN FLARE** YIELD STRENGTH (PSI) 47,297 52,000 55,056 TENSILE STRENGTH (PSI) 62,162 70,666 70,787 ELONGATION IN 2" (%) 29.0 31.0 27.0

Figure A-17. Foundation Tube Material Specification

1 2 3 4 5 Are

Made and Melted

In The U.S.A.

I HEREBY CERTIFY THAT THE ABOVE IS CORRECT AS CONTAINED IN THE RECORDS OF THE COMPANY.



#### CERTIFICATE OF COMPLIANCE

AUGUST 4, 2009

MIDWEST MACHINERY & SUPPLY PO BOX 81097 LINCOLN, NE 68501

The following material delivered on 8/3/09 on bill of lading number 19477 has been inspected before and after treatment and is in full compliance with applicable Nebraska Department of Roads requirements for southern yellow pine Timber Guardrail Components, preservative treated with Chromated-Copper-Arsenate (CCA-C) to a minimum retention of .60 lbs/cu.ft. The acceptance of each piece by company quality control is indicated by a hammer brand on the end of each piece.

1	MAT	ERIAL	CHARGE #	DATE	RETENTION	QUANTITY
X	6x8x14"	Blockout (CD)	09-283	7/29/09	0.67	70
	6x8x6'	Line Post	09-283	7/29/09	0.67	175
X	51/2x71/2-46"	TB Bullnose	09-283	7/29/09	0.67	48
	6x6x8"	Blockout	09-283	7/29/09	0.67	100
	6x8x22"	Blockout	09-283	7/29/09	0.67	70

This certificate applies to material ordered for your order no.: .2191

FOR ANY INQUIRIES, PLEASE RETAIN THIS DOCUMENT FOR FUTURE REFERENCE.

THANK YOU FOR YOUR ORDER.

found St

SINCERELY,

Karen Storey

SIGNED BEFORE ME THIS 4 DAY OF AUGUST 2009.

Notary: Whole Flord Fonety Georgia
My Commission Expires Oct. 19, 2010

OTA AL

OUBLIC

OTI 19, 2010

OUBLIC

OTI 19, 2010

Phone: 706-234-1605

P.O. Box 99, Armuchee, GA 30105

Fax: 706-235-8132

Figure A-18. BCT Timber Posts Certificate of Compliance

TION A SETPIN unarge: /\*s lotal Board Ft : 6,03/ Plant No.: 1 Treatment: Irail Type 1 Total Cubic Ft: 491 Date: 7/29/09 12:42:23PM Total Treatable Cubic Ft: 491 Address S.I. Storey Lumber Co. Chemical: CCA Displaced Volume In: 285 Sike Storey Rd. Target Retention: .60 Displaced Volume Out: 535 Armuchee, GA 30105 PH: 706 234-1605 Fax:706 235-8132 Cylinder: 1 ( 9,090 ) 8,616 Volume Start : Tank: 3 7,598 Volume Finish: Operator: Richard Volume Used: 1,018 Total Time: 2:06:43 Penetration Sampled: 0 EPA Reg. No. 3008-36 Turn Around Time (min): 2,676 Penetration Failed: 0 Time/Date Off Drip Pad: Treat By Tally: True Step Retention Flow Rate **Time** Pressure Injection Volume Reason Min Max Act Min Max Act Max Act Min Max Act Ramp Start End End Initial Vacuum -23 0.00 0.00 .00 .00 .00 0.00 0.00 0.00 12:42:23 12:59:25 8,616 Time Fill 10 -23 10 0.00 0.00 0.00 .00 .00 .00 0.00 0.00 0.00 0 12:59:25 13:06:05 Full 3.281 Raise Press 75 78 0.00 0.00 0.08 .00 .00 .01 0.00 0.00 0.00 0 0 13:06:06 13:06:26 PSI 3.159 Pressure .00 45 128 0.00 3.20 .00 .32 0.00 0.00 0.01 45 75 140 13:06:26 13:51:27 2,229 Time Press Relief .00 .00 .31 25 13 0.00 0.00 1.93 0.00 0.00 0.00 PSI 0 0 13:51:27 13:52:15 2,249 Empty 0 0 0.00 0.00 2.61 .00 .00 .42 0.00 0.00 10 9 0.00 13:52:15 14:00:55 Empty 0 0 7.334 Final Vacuum 2.10 -29 -26 0.00 1.75 .00 .00 .34 0.00 0.00 0.01 0 14:00:55 0 45 45 0 14:45:57 7,588 Time Final Empty .34 0 -1 -1 -1 0.00 0.00 2.09 .00 .00 0.00 0.00 0.00 0 14:45:57 14:48:02 7,593 Empty Finish 0 0 0.00 0.00 2.07 .00 .00 .34 0.00 0.00 0.00 14:48:03 14:49:06 7,598 Time -1 Lbs. Per Gallon Total Lbs. Solution Percent Retention CCA 1.90% 1.90 % .1624 1624 .1624 165 165 .337 .337 1.90 % 1.90 % .1624 .1624 .1624 165 165 Totals: Additive List Automatic Mix Information Target Value Required Difference Water - Gals. - Gals. 1,319 Gals. 1,311 Gals. -8 Gals. CCA 1.88 % 1.90 % 25 Gals. 25 Gals. - Gals. 021.001021.60 175 Packs/Size: 5 @ 35 Desc: 6 x 8 x 6 Line Post Rough Nebraska #1 Dense BF: 4.200 Std .: Species: SYP Cust Num: Retreat?: False Chg#: Rem1: None 021.001008.60 70 Packs/Size: 70 Desc: 6 x 8 x 0-14 Blockout Rough BF: 329 27 Std.: Cust Num Retreat?: False Chg#: Species: SYP 9999 5-1/2 x 7-1/2 x 0-46 TB Bullnose Post 720 48 Packs/Size Desc: BF: CF: ANALYSIS REPORT Std .: Mill: Cust Num None Retreat?: False Chg#: Species: SYP RETENTION 9999 BF: 513 Pieces: 70 70 Desc: 6 x 8 x 0-22" Rough Blockout Std.: CR03 = 8.32 pcfRetreat?: False Species: SYP = 0.12 PCf 9999 6 x 6 x 8" Post Block CCA .60 BF: 275 Pieces: 100 Packs/Size: Std .: :40 Cust Num: Retreat?: False Species: SYP A5205 = 0.23 pcfTOTAL RETENTION 0.67 PCf Printed on: 8/4/09 9:34:53AM Plant Number: 1 Charge Number: 283

Figure A-19. BCT Timber Posts Certificate of Compliance (Continued)

905 ATLANTIC STREET, NORTH KANSAS CITY, MO 64116 1-816-474-5210 TOLL FREE 1-800-892-TUBE STEEL VERTURES, LLC don EXITUBE

#### CERTIFIED TEST REPORT

Customer:	Size:	Spec No:	Date: 05/22/2008
SPS - New Century	02.375	ASTW A500-07, A53E-07	
401 New Century Parkway	Gauge:	Grade:	Customer Order No: \$ 4500104158
New Century KS 88031	.154	A500B,C, A53BNY	
			2A No: 81162893

.Heat No Yield P.S.I. Tensile 2.S.I. Elongation % 2 Inch 280638 61,500 86,400 23.00

Heat No 280638 0.039 V 0.003

We hereby certify that the above material was manufactured in the U.S.A and that all test results shown in this report are correct as contained in the records of our company. All testing and manufacturing is in accordance to A.S.T.M. parameters encompassed within the scope of the specifications denoted in the specification and grade tiles above.

BNT=Grade B not tested - meets tensile properties ONLY.

STEEL VENTURES, LLC dba EXLTUBE

Steve Frerichs Quality Assurance Manager

Figure A-20. BCT Post Sleeves Material Specification

25 E. O'Connor

Justomer: MIDWEST MACH & SUPPLY CO.

P. O. BOX 81097

Sales Order: 1093497 Customer PO: 2030 BOL # 43073

Document# 1

Print Date: 6/30/08
Project: RESALE
Shipped To: NE
Use State: KS

LINCOLN, NE 68501-1097

Trinity Highway Products, LLC

Certificate Of Compliance For Trinity Industries, Inc. \*\* SLOTTED RAIL TERMINAL \*\*

NCHRP Report 350 Compliant

Pieces	Description.					
64	5/8"X10" GR BOLT A307	The second of th	And the second of the second o		•	
192	5/8"X18" GR BOLT A307		•			
32	1" ROUND WASHER F844					
64	1" HEX NUT A563					
; 192	WD 60 POST 6X8 CRT					
192	WD BLK 6X8X14 DR					
64	NAIL 16d SRT				*	
E4	WD 3'9 POST 5.5X7.5 BAND					
132	STRUT & YOKE ASSY					
128	SLOT GUARD '98			•		
32	3/8 X 3 X 4 PL WASHER					

Jpon delivery, all materials subject to Trinity Highway Products , LLC Storage Stain Policy No. LG-002.

LL OTHER GALVANIZED MATERIAL CONFORMS WITH ASTM-123.

CHOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

CHUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM449 AASHTO M30, TYPE II BREAKING

STRENGTH - 49100 LB

State of Ohio, County of Allen. Sworn and Subscribed before me this 39th day of June, 2008

g ctary Public: Office Office

Trinity Highway Products, LLC Certified By:

2 of 4

85

## Certified Analysis

Order Number: 1095199

Customer PO: 2041

BOL Number: 24481

Document #: 1

Shipped To: NE

Use State: KS

Project: RESALE

2548 N.E. 28th St.

Ft Worth, TX

Trinity Highway Products, LLC

Customer: MIDWEST MACH & SUPPLY CO.

LINCOLN, NE 68501-1097

P.O. BOX 81097

Qty	Part# Description	Spec CL	TY Heat Code/ Reat#	Yield	TS	Kig	C	in the same	P	\$	Si	Cu ·	Cb €	r Vo	ACW
25	8G 12/63/8	M-180 A	The state of the s	64,230	81,300	25.4	0.180	0.720 (	1.012 (	J.001 Q.	040 0.	080 0.0	60 0.0	0.000	4
20	701A .25X11.75X16 CAB ANC	A-36	4153095	44,900	60,800	34.0	0.240	0.750 (	0.012 (	0.003 0.	020 G.	020 0.1	0.0 0.0	0.002	4
10	742G GO TUBE SL/188XEX6	A-500	A8P1160	74,000	87,000	25.2	0.050	0.670 0	0.013	0.005 O.	030 O.	220 04	0.0 00	90 <b>0.02</b> 1	Ą
es 30	7820 M"X8"X8" BEAR PL/OF	A-36	6106195	46,700	69,900	23.5	0.180	0.830 (	0.010	0.005 0.	020 0.	230 04	0.0 0.0	70 0.006	4
40	907G 12/BUFFER/ROLLED	M-180 A	L0049	54,200	73,500	25,0	0.160	0.708 6	J.011 (	0.002 0.	020 0.	.200 0.0	00 0.10	000.0	4

Upon delivery, all materials subject to Trimity Highway Products, LLC Storage Stain Policy No. LG-002.

ALL STEEL USP AS MELTED AND MANUFACTURED IN USA AND COMPLES WITH THE BUY AMERICA ACT.

ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL OTHER GALVANIZED MATERIAL CONFORMS WITH ASTM-123.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

34° IAA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE E BREAKING STRENGTH -49 100 LB

State of Teres, County of Terrent. Sworn and subscribed before me this 20th day of June, 2008

Notery Public: Commission Expires



Trinity Highway Products, LLC Certified By:

Gleknie Onst. a

Asof: 6/20/08

Figure A-22. Anchor Bracket Material Specification

## Certified Inalysis

Trinity Highway Products, LLC

425 E. O'Connor

Order Number: 1114174

Lima, OH

Customer PO: 2213

Customer: MIDWEST MACH.& SUPPLY CO.

BOL Number: 51169

P. O. BOX 81097

Document #: 1

Shipped To: NE

LINCOLN, NE 68501-1097

Use State: NE

Project: RESALE

	Qty	Part # Description	Spec CL	TY Heat Code/ Heat #	Yield	TS	Elg	C	Mn	P	S	Si	Cu	Cb	Cr	Vn	ACW
+	750	545G 6'0 POST/DB:DDR	A-36	J86489	50,565	68,830	26.1 0.	.090	0.950	0.010	0.040	0.200	0.290	0.00	0.00 0.160 0.003		4
	50	14662G 6'6 POST/8.5#/DB:DDR NB	A-36	J86489	50,565	68,830	26.1 0.	.090	0.950	0.010	0.040	0.200	0.290	0.00	0.160	0.003	4

Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT.

ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHERWISE STATED.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

1

3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKING STRENGTH \_ 49 100 I R

State of Ohio, County of Allen. Sworn and subscribed before me this 16th day of September, 2009

state of onto, county of raight bworn and subgrouped bologo movins foundary of bepletinosi, 200

Commission Expires / 158 17

Trinity Highway Products , LLC

Certified By:

od By: National Ouality Assurance

1 of 1

As of: 9/16/09

Figure A-23. BCT Cable Anchor Assembly Certificate of Compliance

87

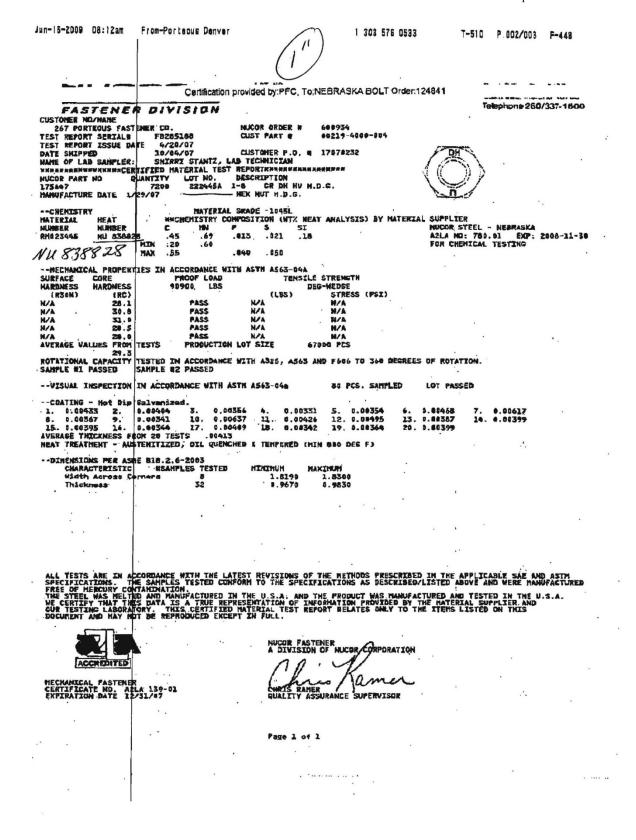


Figure A-24. BCT Cable Anchor Assembly Certificate of Compliance (Continued)

HP LASERJET FAX

Jun 17 2009 9:22

## Trinity Highway Products, LLC 2548 N.E. 28th St.

Certified Analysis

Order Number: 1095199

Oustomer PO: 2041

BOL Number: 24481 Customer: MIDWEST MACH & SUPPLY CO.

Document #: 1

Shipped To: NE

Use State: KS LINCOLN, NE 68501-1097

Project: RESALE

P.O. BOX 81097

Ft Worth, TX

Notary Public:

Commission Expires Figure A-25. Anchor Bearing Plate Certificate of Compliance

Trinity Highway Products, LLC Certified By:

Asof: 6/20/08

Qty	Part# Dascription	Spec CL	TY He	est Code/ Heat #	Yeld	TS	Rig	C	in the	128	\$	S		Cb	Cr		ACW
25	6G 12/63/8	M-180 A	849	964	64,230	81,300	25.4	0.180	0.720	0.012	0.001	0.040	0.080	0.000	0.060	0.000	4
- 20 -	701A .25X11.75X16(	CAB ANC A-36	415	53095	44,900	60,800	34.0	0.240	0.750	0.012	0.003	0.020	0.020	0.000	0.040	0.002	4
10	742G 60 TUBE SL/.10	SEXEX6 A-500	A8	P1160	74,000	87,000	25,2	0.050	0.670	0.083	0.005	0.030	0.220	0.000	0.060	0.021	A.
eser 20	7823 5/8"X8"X8" BE	ARPLIOF A-36	бЦ	06195	46,700	69,900	23.5	0.130	0.830	010.0	0.005	0.020	0.230	0.000	0.070	0.006	4
40	907G 12/BUFFER/RO	LLED M-180 A	L	1649	54,200	73,500	25.0	0.160	0.709	0.011	0.008	0.020	0.200	9.000	0.100	0.000	4

Upon delivery, all materials subject to Trinity Highway Products , LLC Storage Stein Policy No. LG-002.

ALL STEEL USP AS MELTED AND MANUFACTURED IN USA AND COMPLES WITH THE BUY AMERICA ACT.

ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL OTHER GALVANIZED MATERIAL CONFORMS WITH ASTM-123.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

34" DIA CABLE 6X19 ZINC COATED SWAGED BND AISI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BREAKUNG STRENGTH -49100 LB

State of Texas, County of Terrant. Swom and subscribed before me this 20th day of June, 2008







#### CAUTION FRESH CONCRETE

Body and or eye contact with fresh (moist) concrete should be avoided because it contains alkali and is caustic.

#### Ready Mixed Concrete Company

6200 Comhusker Highway, P.O. Box 29288 Lincoln, Nebraska 68529 Telephone 402-434-1844

						-			
ANT	MIX CODE	YARDS	TRUCK	DRIVER	DESTINATION	CLASS	TIME	DATE	TICKET
01	13013000	1.25	0135	056	NO1		b1:27P	MO3/05/09	1117450
ISTOMER	JOB	CUSTOM	ER NAME			TAX CODE	PARTIAL	NIGHT R.	LOADS
00003			-MIDWES	ROADSID	E				1
LIVERY ADD	RESS			SPECIAL INS				P.O. NUMBER	
4800 N	W 35TH			N/ OF INSIDE	THE NO. GC FENCE	ODYEAR H	ANGER	450-6250	
LOAD QUANTITY	CUMULAT		RDERED	PRODUCT CODE	PRODI	JCT DESCRIPTION		UNIT PRICE	AMOUNT
1.25	1.25	5 1	.25 13		SG 3000 MINIMUM HA WINTER SEF	UL	2.00	86.50	108.13 57.50 5.00
TER ADDED	ON JOB 'S REQUEST	GAL	R	ECEIVED BY	A gu		-	TOTAL	170.63 11.94 182.57 182.57



Figure A-26. Concrete Material Specification

1115		
A CANADA SA		Service Annual Property
Ri	II To:	

#### CONCRETE INDUSTRIES, INC.

6300 Cornhusker Highway, Lincoln, NE 6 402-434-1800 Fax: 402-434-1899 www.ConcreteIndustries.com

**Customer Receipt** 

Driver:	
Truck #:	
Ordered By:	CALL

5 CASH SALES-CONCRETE INDUSTRIES

Ship To: UNL MIDWEST ROADSIDE SAFETY CURT MEYER

1-0529

Ship From:
CONCRETE INDUSTRIES 6300 CORNHUSKER HWY LINCOLN NE 68507

Delivery Directions:	
	1

09:28	Order Number: SP 1102642	0	Delivery Date:	02/10/09	Cus	tomer F	O Number:		
Line	Item Description		Picked	Ordered	Back Order	Units	Unit Price	Discount	Extension
1	#4 STOCK REBAR GRADE 60 20'-0" R46020	4 4	TO HAZALITON	7.00		EA	6.0200	× .	42.14
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MACO	on the state of th	A	45H 3 Mar - 45, 54A	ele el colo colo				30 . A	50 g15/2 54 5

Received by Print Name/Company Sub Total: No returns w/o invoice. No returns on unusable material, seconds. Tax Code:CINTE Nebraska Tax Exempt Sales Tax: architectural, decorative, all special order materials, and fractional units. All 42.14 Total Amount: returnable materials subject to 50% restocking charge. No returns accepted Total Weight: 93.52 Down Payment: Balance Due: after 30 days from date of purchase. 42.14 Total Cubic: All invoices must be paid within 30 days of invoice. Past due accounts will be charged an interest rate of 1.33% per month which is 16% per year. 0 Print Date: 02/10/09 Print Time: 09:28 bobb Document: Page: 1

Figure A-27. Reinforcing Steel Material Specification

MwRSF R	
MwRSF Report No. TRP-03-237-10	INOACIII
P-03-237-10	INOVERTION 24, 2010

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	60	M644041	.15	.86	.010	.020	.18	.38	.14	.13	.027	.002	.001	.0104	.013	.602	-	.00000		.008		-	+	+	+	-	-	-
	Ph: 1(800)237-0230	Mechanical Test: Customer Requirement Commont Stort not of	s SOUR	mercury	STP CA	STING:	STRAN mont de	ID CAST	Melt si	5.4 MPA rop had	#81491i	₩	, 25.0/2	09.2mm	Bend	: OK	Red R	155.69	Std Dev	:0 ld	Oiam: .	482	ANTES CARRO					nes.
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	6	HEAT LD. M684042	C	.64	.012	.030	Si .19	Cu .31	.13		A60 .027	.002	.003	N .0183	.016	At .002	11	Ca .00020	Zn .00700	.008		ļ	-			<u> </u>	-	1
CONCRETE INDUSTRIES	Name: Gerdeu Amerieteel AutoFax System		Vield 49 ts SOUR sposed to	500 PSI CE: GA-	, 341.29 STP CA	MPA STING: d repair	Tensile STRAA med pe	: 68000   ID CAST Informed.	PSI, 46	B.04 MP/	<b>%</b> E	28,8/8	n, 28.8	203.2mg	Sen	d: OK	RedF	155.69	Sed De	ev:0 kd								
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Figure A-28. Reinforcing Steel Material Specification (Continued)

## Appendix B. Vehicle Center of Gravity Determination

Test	:: MGSC-6		Vehicle:	2270P (RA	M 1500)			
			Vehicle C	G Determin	ation			
		Weight	Long CG	Lat CG	Vert CG	Long M	Lat M	Vert M
<b>VEHICLE</b>	Equipment	(lb)	(in.)	(in.)	(in.)	(lb-in.)	(lb-in.)	(lb-in.)
+	Unbalasted Truck(Curb)	5100	62.2047	-0.03985	28.74069	317244	-203.25	146577.5
+	Brake receivers/wires	6	108	0	53	648	0	318
+	Brake Frame	5	40	-19	25	200	-95	125
+	Brake Cylinder (Nitrogen)	28	73	17	28	2044	784	784
+	Strobe/Brake Battery	6	78	3	32	468	192	192
+	Hub	27	0	-41	15.125	0	-1107	408.375
+	CG Plate (EDRs)	8	54	0	31	432	0	248
-	Battery	-47	-7.5	-25	39	352.5	1175	-1833
-	Oil	-10	8.5	0	17	-85	0	-170
-	Interior	-60	52	0	22	-3120	0	-1320
-	Fuel	-161	112	-11	20	-18032	1771	-3220
-	Coolant	-21	-26	0	36	546	0	-756
-	Washer fluid	-9	-26	17	33	234	-153	-297
BALLAST	Water	110	112	-11	20	12320	-1210	2200
	DTS Rack	18	71	0	29	1278	0	522
	Misc.					0	0	0
						314529.5	1153.75	143778.9
	TOTAL WEIGHT	5000	lb	CG lo	cation (in.)	62.90589	0.23075	28.75578

wheel base	140.25	Calculated Test Ine	rtial Weight	
	MASH Targets	Targets	CURRENT	Difference
	Test Inertial Weight (lb)	5000 ± 110	5000	0.0
	Long CG (in.)	63 ± 4	62.91	-0.09411
	Lat CG (in.)	NA	0.23	NA
	Vert CG (in.)	28 min.	28.76	0.75578

Note: Long. CG is measured from front axle of test vehicle

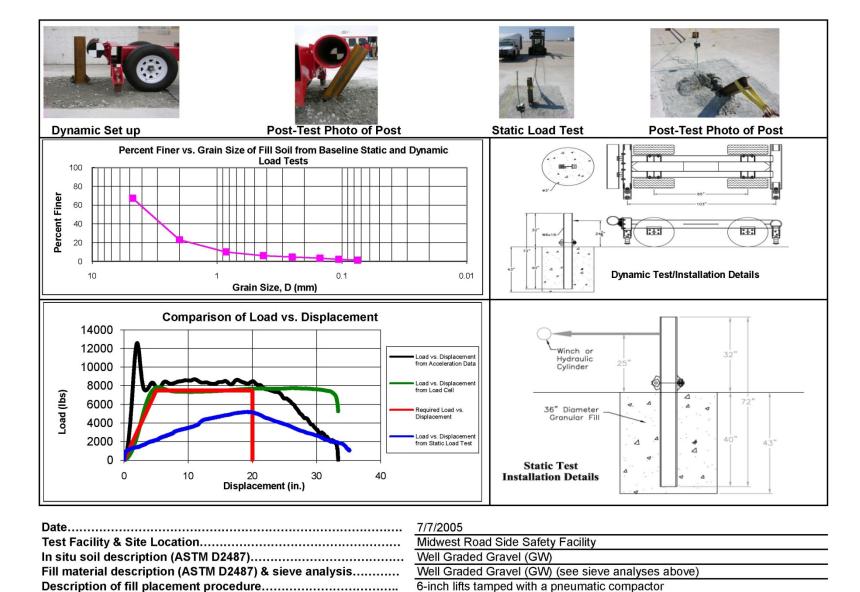
Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

Curb Weight (lb)			
	Left	R	ight
Front		1416	1422
Rear		1137	1125
FRONT		2838 lb	1
REAR		2262 lb	(
TOTAL		5100 lb	r.

Actual test inertial weight (lb)									
(from scales)									
	Left		Right						
Front		1402		1333					
Rear		1084		1155					
FRONT		2735	lb						
REAR		2239	lb						
TOTAL		4974	lb						

Figure B-1. Vehicle Mass Distribution, Test No. MGSC-6

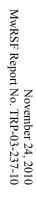
## Appendix C. Static Soil Tests



19.08 mph

Figure C-1. Soil Strength, Initial Calibration Tests

Impact Velocity.....



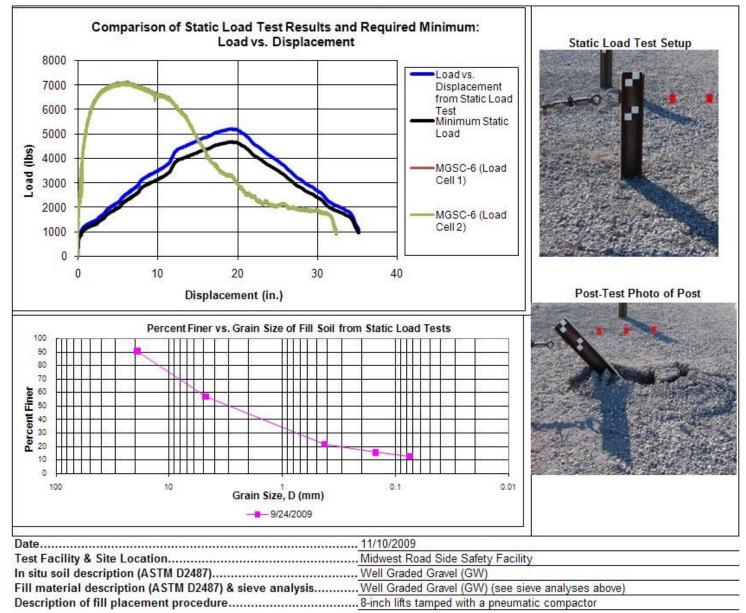


Figure C-2. Static Soil Test, Test No. MGSC-6

## Appendix D. Vehicle Deformation Records

#### VEHICLE PRE/POST CRUSH FLOORPAN - SET 1

TEST: MGSC-6 VEHICLE: 2270P (RAM 1500) Note: If impact is on driver side need to enter negative number for Y

	Х	Υ	Z	X'	Y'	Z'	ΔΧ	ΔΥ	ΔZ
POINT	(in.)								
1	26.25	10.5	0	26.5	11	0	0.25	0.5	0
2	29.5	15.25	-1	29.5	15.75	-1	0	0.5	0
3	32	20.75	-1.5	31.75	21	-1.5	-0.25	0.25	0
4	30.75	27.75	0	30.5	28	0	-0.25	0.25	0
5	24.75	12.25	-1.25	25	12.25	-1	0.25	0	0.25
6	26.5	18.75	-6.25	26.25	18	-6.25	-0.25	-0.75	0
7	26.5	24.75	-6.25	26.5	24.25	-6	0	-0.5	0.25
8	26.5	30	-5.5	26.5	29.5	-5.5	0	-0.5	0
9	19	7.5	-2	19.25	7.75	-2.25	0.25	0.25	-0.25
10	20.5	13.25	-5.25	20.75	13.75	-5.25	0.25	0.5	0
11	22	19.75	-9	22	20.25	-8.75	0	0.5	0.25
12	22.25	28.25	-8.75	22	28.25	-8.5	-0.25	0	0.25
13	14	3.75	-2.75	14	3.75	-3	0	0	-0.25
14	14	7.25	-2.75	13.75	7.25	-2.75	-0.25	0	0
15	16.5	13	-9.25	16.5	13.75	-9.25	0	0.75	0
16	16.75	21.25	-9.25	16.75	22	-9.25	0	0.75	0
17	16.75	28.5	-9	16.75	28.75	-9	0	0.25	0
18	8.75	3.75	-3.25	8.75	3.75	-3.25	0	0	0
19	12.5	11.5	-9.5	12.5	12	-9.5	0	0.5	0
20	12.5	17.5	-9.25	12.5	18.25	-9.25	0	0.75	0
21	12.75	25	-9.25	12.75	25.75	-9.25	0	0.75	0
22	5.25	7	-3.5	5.25	7	-3.5	0	0	0
23	7	17.25	-9.25	6.75	17.75	-9.5	-0.25	0.5	-0.25
24	7.25	27.25	-9	7	27.75	-9	-0.25	0.5	0
25	0.75	4	-2.75	0.75	4	-2.75	0	0	0
26	0.75	11.5	-5	0.75	11.5	-5	0	0	0
27	1	19.5	-5	1	19.25	-4.75	0	-0.25	0.25
28	1	26.75	-4.75	1	26.5	-4.75	0	-0.25	0
29							0	0	0
30							0	0	0
31					j j		0	0	0

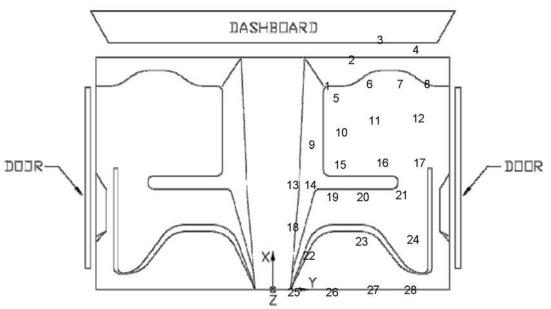


Figure D-1. Floor Pan Deformation Data – Set 1, Test No. MGSC-6

#### VEHICLE PRE/POST CRUSH FLOORPAN - SET 2

TEST: MGSC-6
VEHICLE: 2270P (RAM 1500)

Note: If impact is on driver side need to enter negative number for Y

	Х	Υ	Z	X'	Y'	Z'	ΔΧ	ΔΥ	ΔZ
POINT	(in.)								
1	49	17	0	48.75	17.75	0	-0.25	0.75	0
2	52	22	-1.25	52	22.5	-1	0	0.5	0.25
3	54.75	28.25	-1.5	54.75	28.25	-1.5	0	0	0
4	53.25	34.75	0	53.25	35	0	0	0.25	0
5	47.5	18.5	-1.25	47.5	19	-1	0	0.5	0.25
6	49.25	24.75	-6.25	49.25	25	-6.25	0	0.25	0
7	49.5	30.5	-6.25	49.5	31	-6.25	0	0.5	0
8	49.25	37	-5.5	49.5	36.25	-5.5	0.25	-0.75	0
9	42	14	-2.25	42	14.25	-2.25	0	0.25	0
10	43.5	20.25	-5.25	43.5	20.5	-5.25	0	0.25	0
11	45	26.25	-9	45	27	-9	0	0.75	0
12	45	35.5	-8.75	45	35	-8.75	0	-0.5	0
13	36.75	10.5	-3	37	10.5	-3	0.25	0	0
14	37	14.25	-3	36.75	14.25	-3	-0.25	0	0
15	39.5	20	-9.5	39.5	20.5	-9.25	0	0.5	0.25
16	39.75	28.25	-9.25	39.75	28.75	-9.25	0	0.5	0
17	39.75	36	-9.25	39.75	36	-9.25	0	0	0
18	32	10.5	-3.5	31.75	10.75	-3.5	-0.25	0.25	0
19	34.75	18.5	-9.75	34.5	18.75	-9.75	-0.25	0.25	0
20	35	24.75	-9.5	34.75	25.25	-9.5	-0.25	0.5	0
21	35	32	-9.25	34.75	32.75	-9.25	-0.25	0.75	0
22	28.25	13.75	-3.25	28.5	13.75	-3.75	0.25	0	-0.5
23	30	24.25	-9.25	29.5	24.5	-9.25	-0.5	0.25	0
24	30.75	34	-9	30	34.5	9	-0.75	0.5	0
25	23.75	11	-3	23.75	10.75	-3	0	-0.25	0
26	23.5	18.5	-5.25	23.5	18.5	-5.25	0	0	0
27	24	26.25	-5	24	26.25	-5	0	0	0
28	24	33.75	-4.75	24	33.5	-4.75	0	-0.25	0
29							0	0	0
30							0	0	0
31							0	0	0

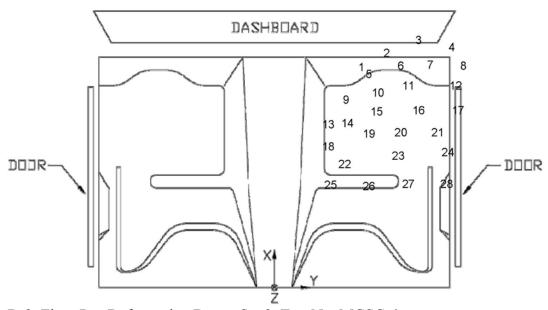


Figure D-2. Floor Pan Deformation Data – Set 2, Test No. MGSC-6

#### VEHICLE PRE/POST CRUSH INTERIOR CRUSH - SET 1

TEST: MGSC-6
VEHICLE: 2270P (RAM 1500)

Note: If impact is on driver side need to enter negative number for Y

		Х	Υ	Z	X'	Y'	Z'	ΔX	ΔΥ	ΔZ
	POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)
Î	A1	12	1.5	21.5	11.75	1.5	21.75	-0.25	0	0.25
-5000	A2	12	11.5	21.75	11.75	11.5	21.5	-0.25	0	-0.25
LS.	А3	12	21	21	12	20.25	21	0	-0.75	0
DASH	A4	9.5	1.5	15	9.75	1.5	15	0.25	0	0
	A5	9.75	11.5	15.5	9.75	11	15.25	0	-0.5	-0.25
	A6	10.25	21	15.5	10.25	20.75	15.5	0	-0.25	0
	B1	23	23.25	0.25	23	23.25	0.5	0	0	0.25
SIDE PANEL	B2	19.25	23.25	-3.5	19	23.25	-3.5	-0.25	0	0
S PA	B3	17.5	23.25	1	17.5	23.25	1	0	0	0
	C1	1	25.5	17.25		26	17.25	0	0.5	0
IMPACT SIDE DOOR	C2		25.5	17.75		26	17.75	0	0.5	0
S T	C3		25.5	18.25		26	18.25	0	0.5	0
SO	C4		24.75	0.5		25	0.5	0	0.25	0
AP,	C5		25	3.75		25.25	3.75	0	0.25	0
=	C6	L.	25	3.75		25.25	3.75	0	0.25	0
	D1							0	0	0
	D2							0	0	0
	D3							0	0	0
	D4	Not needed	due to low	probability	of damge			#VALUE!	0	0
	D5							0	0	0
	D6							0	0	0
ш	D7							0	0	0
ROOF	D8							0	0	0
ŭ	D9		j					0	0	0
	D10							0	0	0
	D11							0	0	0
	D12							0	0	0
	D13							0	0	0
	D14							0	0	0
	D15							0	0	0

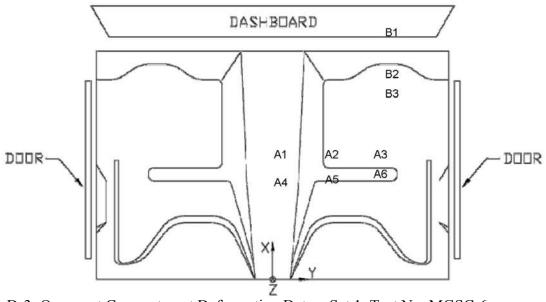


Figure D-3. Occupant Compartment Deformation Data – Set 1, Test No. MGSC-6

### VEHICLE PRE/POST CRUSH INTERIOR CRUSH - SET 2

TEST:	MGSC-6	Note: If impact is on driver side need to
VEHICLE:	2270P (RAM 1500)	enter negative number for Y

		Х	Υ	Z	X'	Y'	Z'	ΔΧ	ΔΥ	ΔZ
	POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)
	A1	29.5	18.5	21.25	30	18.5	21.5	0.5	0	0.25
	A2	29.5	28.5	21.5	29.5	28.75	21.25	0	0.25	-0.25
SH	A3	29.5	37.5	21	29.5	38	21	0	0.5	0
DASH	A4	27.25	19	15	27.5	18.75	14.75	0.25	-0.25	-0.25
	A5	27.5	27.75	15.25	27.5	28.5	15	0	0.75	-0.25
	A6	27.5	37.75	15.5	27.75	38.5	15.5	0.25	0.75	0
	B1	40	41.75	0.25	40	41.5	0.5	0	-0.25	0.25
SIDE PANEL	B2	36.25	41.75	-3.75	36	41.5	-3.75	-0.25	-0.25	0
S PA	B3	34.75	41.75	1	34.75	41.5	1	0	-0.25	0
101	C1	24.25	43	17.25	24.25	43.5	17	0	0.5	-0.25
SIDE R	C2	12.5	43.25	17.5	12.25	43.75	17.5	-0.25	0.5	0
	C3	1.25	43.25	18	1	43.75	18	-0.25	0.5	0
IMPACT SI DOOR	C4	25.75	43.25	0.25	25.25	43.25	0.5	-0.5	0	0.25
MP,	C5	15.5	43.25	3.5	15.25	43.25	3.5	-0.25	0	0
=	C6	3	43.5	3.5	3	43.25	3.5	0	-0.25	0
	D1							0	0	0
	D2							0	0	0
	D3							0	0	0
	D4	Not needed	d due to low	probability	of damge			#VALUE!	0	0
	D5							0	0	0
	D6							0	0	0
ш	D7							0	0	0
ROOF	D8							0	0	0
č	D9							0	0	0
	D10							0	0	0
	D11							0	0	0
	D12							0	0	0
	D13							0	0	0
	D14							0	0	0
	D15							0	0	0

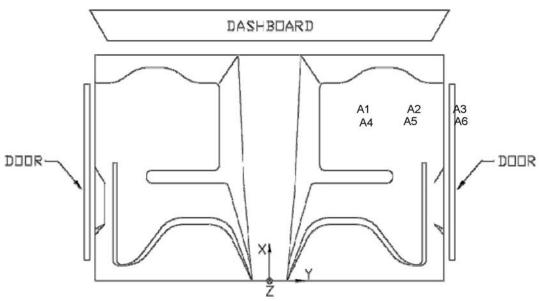
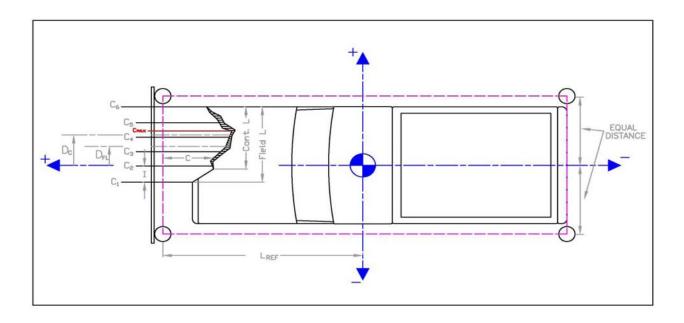


Figure D-4. Occupant Compartment Deformation Data – Set 2, Test No. MGSC-6

 Date:
 11/23/2009
 Test Number:
 MGSC-6

 Make:
 Dodge
 Model:
 2270P (RAM 1500)
 Year:
 2003



	in.	(mm)
Distance from C.G. to reference line - $L_{\mbox{\scriptsize REF}}$ :	110	(2794)
Width of contact and induced crush - Field L:	21.5	(546)
Crush measurement spacing interval (L/5) - I:	4.3	(109)
Distance from center of vehicle to center of Field L - DFL:	28.25	(718)
Width of Contact Damage:	21.5	(546)
Distance from center of vehicle to center of contect damage - D c:	28.25	(718)

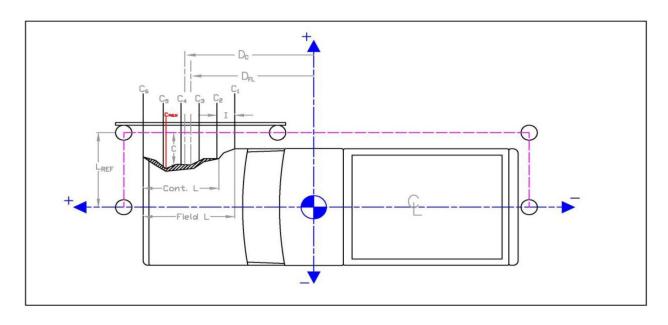
NOTE: Enter "NA" for crush measurement if distance can not be measured (i.e., side of vehicle has been pushed inward)

	Crush Measurement		Lateral Location			Original Profile Measurement		Dist. Between Ref. Lines		Crush
	in.	(mm)	in.	(mm)	in.	(mm)	in.	(mm)	in.	(mm)
$C_1$	8.75	(222)	17.5	(445)	12.0313	(306)	-2.655892	-(67)	-0.625358	-(16)
C <sub>2</sub>	11	(279)	21.8	(554)	12.9375	(329)			0.718392	(18)
C <sub>3</sub>	16	(406)	26.1	(663)	14.5	(368)			4.155892	(106)
C <sub>4</sub>	23.5	(597)	30.4	(772)	16.2969	(414)			9.859017	(250)
C <sub>5</sub>	NA	#VALUE!	34.7	(881)	19.9375	(506)			<b>#VALUE!</b>	#VALUE!
C <sub>6</sub>	NA	#VALUE!	39	(991)	29	(737)			#VALUE!	#VALUE!
$\mathbf{C}_{\mathbf{MAX}}$	28.25	(718)	35	(889)	20.625	(524)			10.28089	(261)

Figure D-5. Exterior Vehicle Crush (NASS) - Front, Test No. MGSC-6

 Date:
 11/23/2009
 Test Number:
 MGSC-6

 Make:
 Dodge
 Model:
 2270P (RAM 1500)
 Year:
 2003



	in.	(mm)
Distance from centerline to reference line - $\boldsymbol{L}_{REF}$ :	46.25	(1175)
Width of contact and induced crush - Field L:	227	(5766)
Crush measurement spacing interval (L/5) - I:	45.4	(1153)
Distance from vehicle c.g. to center of Field $L$ - $D_{FL}$ :	-11.34	-(288)
Width of Contact Damage:	227	(5766)
Distance from vehicle c.g. to center of contect damage - $D_C$ :	11.34	(288)

NOTE: Enter "NA" for crush measurement if distance can not be measured (i.e., front of vehicle has been pushed inward or tire has been remeoved)

	Crush Measurement				Longitudi	nal Location	Original Measur			etween Ref. Lines	Actual	Crush
	in.	(mm)	in.	(mm)	in.	(mm)	in.	(mm)	in.	(mm)		
$C_1$	NA	<b>#VALUE!</b>	-124.84	-(3171)	14.75	(375)	-3.75	-(95)	#VALUE!	<b>#VALUE!</b>		
$C_2$	10	(254)	-79.44	-(2018)	10.5	(267)			3.25	(83)		
$C_3$	7.75	(197)	-34.04	-(865)	11.60417	(295)			-0.10417	-(3)		
$C_4$	7.5	(191)	11.36	(289)	11.25	(286)			0	0		
$C_5$	NA	#VALUE!	56.76	(1442)	10.5	(267)			#VALUE!	#VALUE!		
$C_6$	NA	#VALUE!	102.16	(2595)	37	(940)			#VALUE!	#VALUE!		
$\mathbf{C}_{\mathbf{MAX}}$	16	(406)	76.75	(1949)	10.875	(276)			8.875	(225)		

Figure D-6. Exterior Vehicle Crush (NASS) - Side, Test No. MGSC-6

## Appendix E. Accelerometer and Rate Transducer Data Plots, Test No. MGSC-6

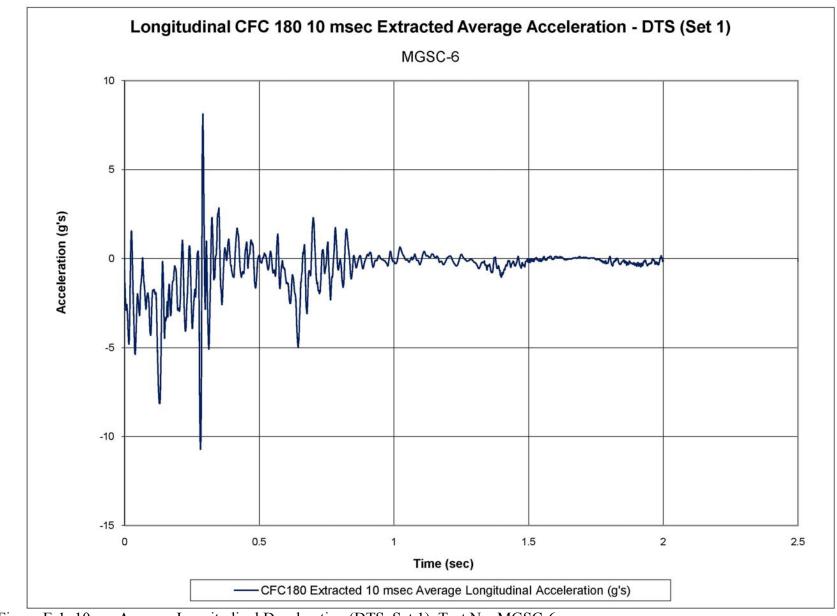


Figure E-1. 10-ms Average Longitudinal Deceleration (DTS, Set 1), Test No. MGSC-6

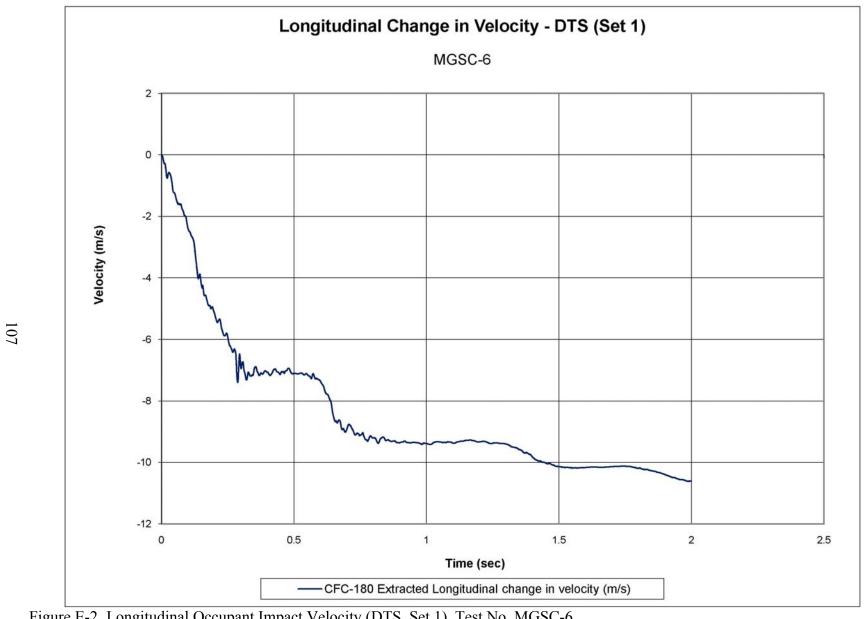


Figure E-2. Longitudinal Occupant Impact Velocity (DTS, Set 1), Test No. MGSC-6

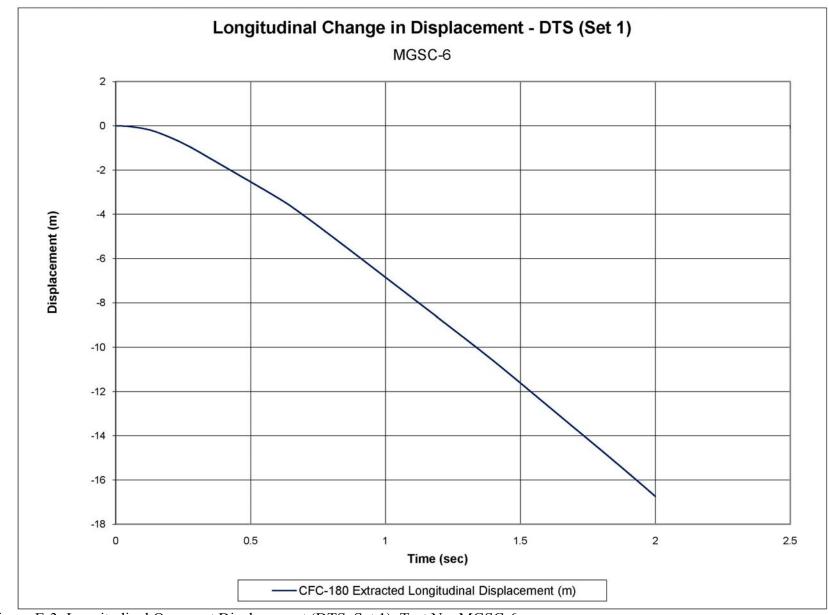


Figure E-3. Longitudinal Occupant Displacement (DTS, Set 1), Test No. MGSC-6

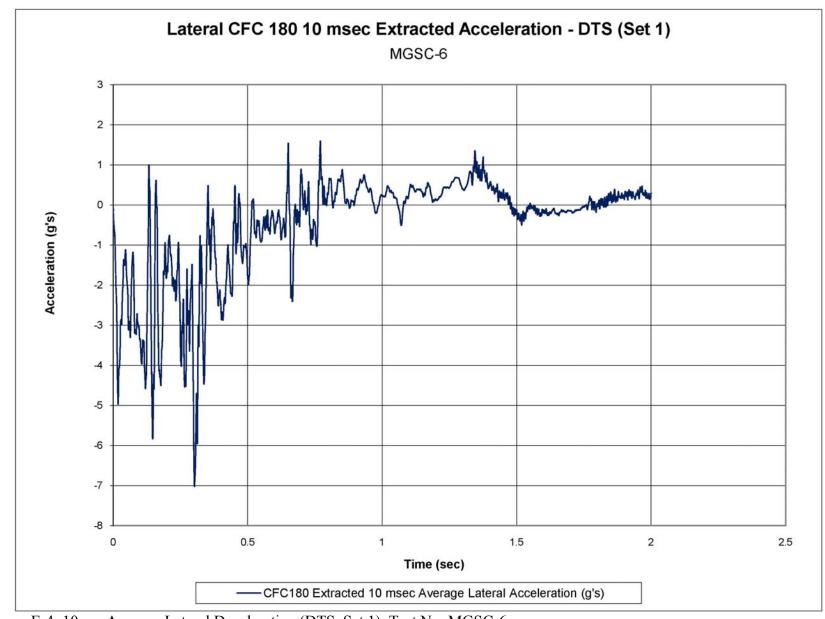


Figure E-4. 10-ms Average Lateral Deceleration (DTS, Set 1), Test No. MGSC-6

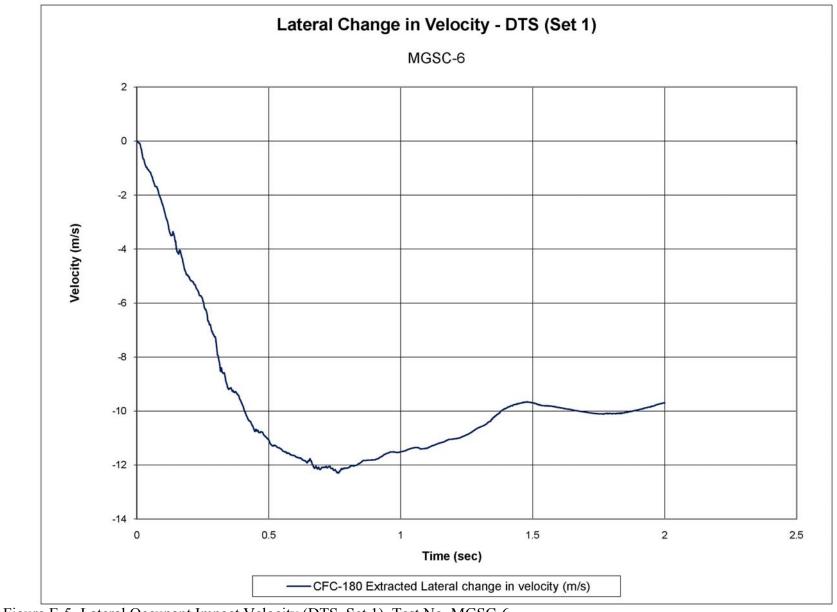


Figure E-5. Lateral Occupant Impact Velocity (DTS, Set 1), Test No. MGSC-6

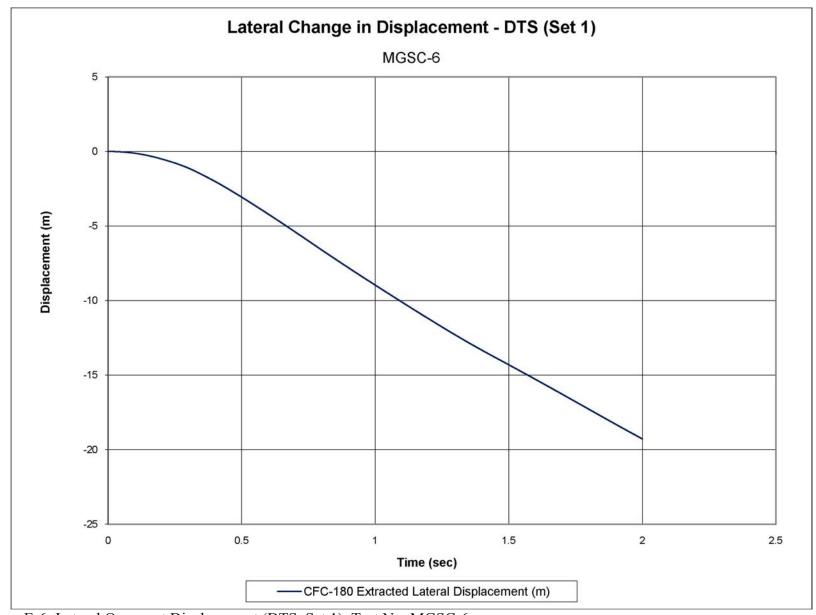


Figure E-6. Lateral Occupant Displacement (DTS, Set 1), Test No. MGSC-6

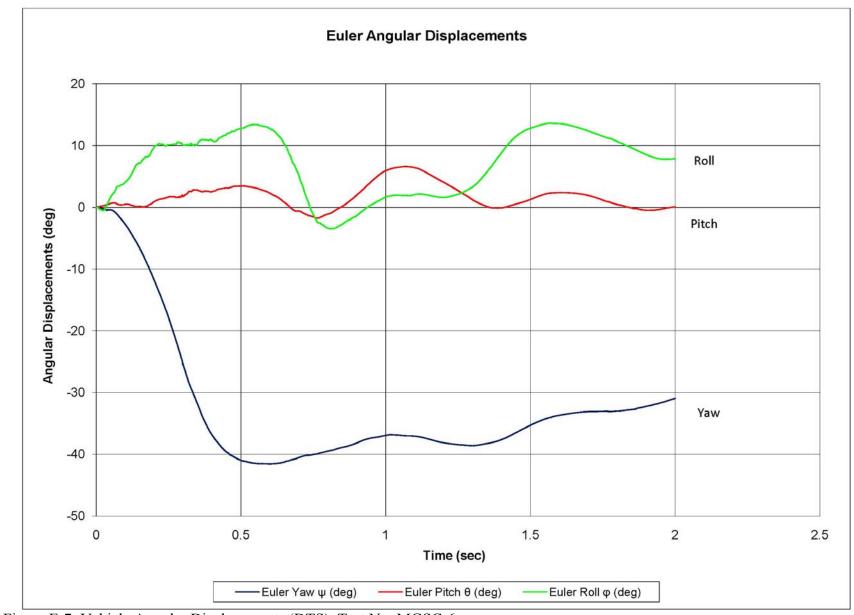


Figure E-7. Vehicle Angular Displacements (DTS), Test No. MGSC-6

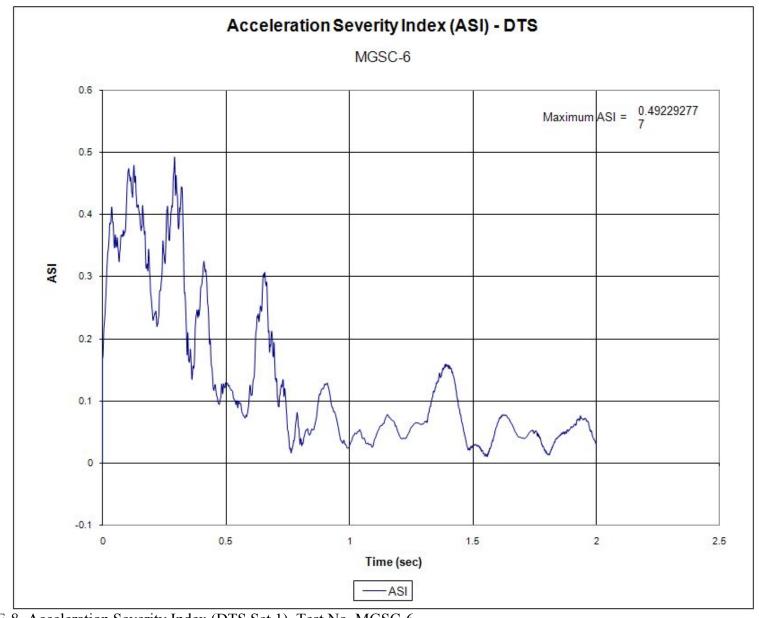


Figure E-8. Acceleration Severity Index (DTS Set 1), Test No. MGSC-6

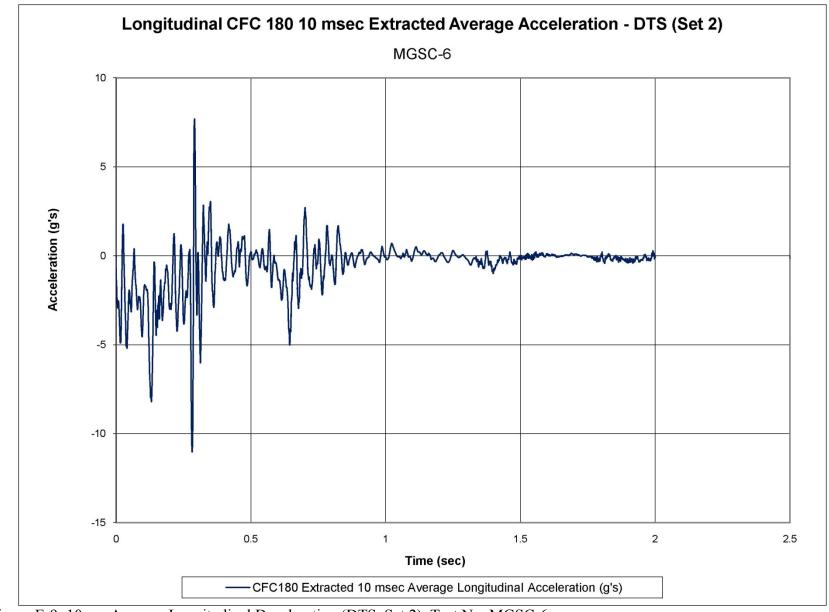


Figure E-9. 10-ms Average Longitudinal Deceleration (DTS, Set 2), Test No. MGSC-6

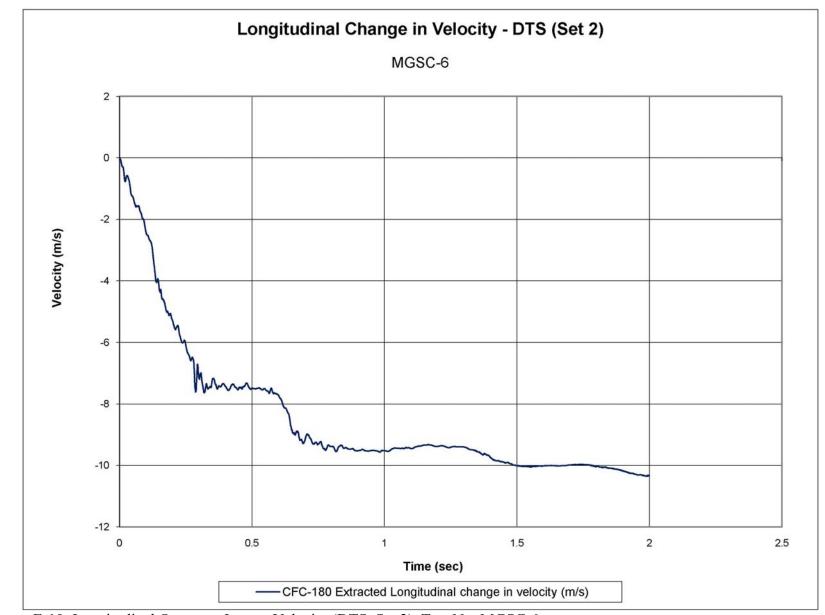


Figure E-10. Longitudinal Occupant Impact Velocity (DTS, Set 2), Test No. MGSC-6

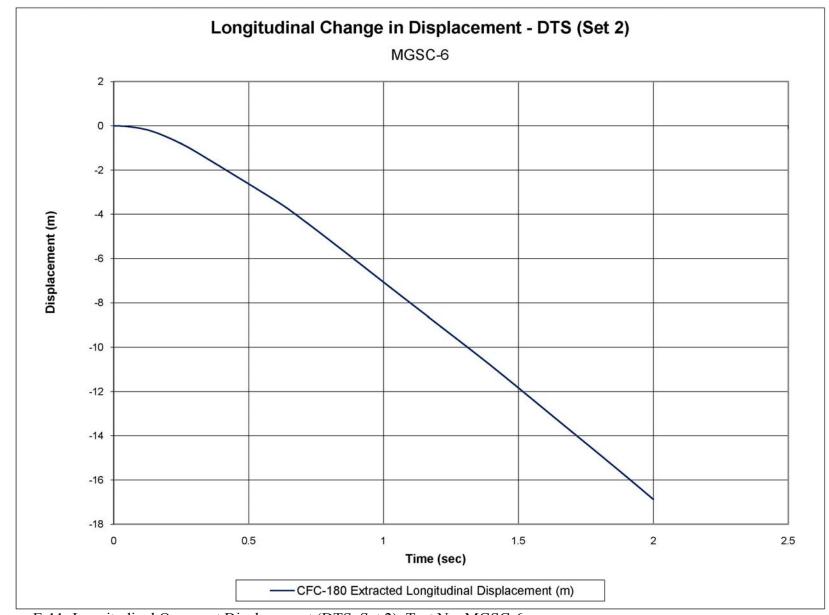


Figure E-11. Longitudinal Occupant Displacement (DTS, Set 2), Test No. MGSC-6

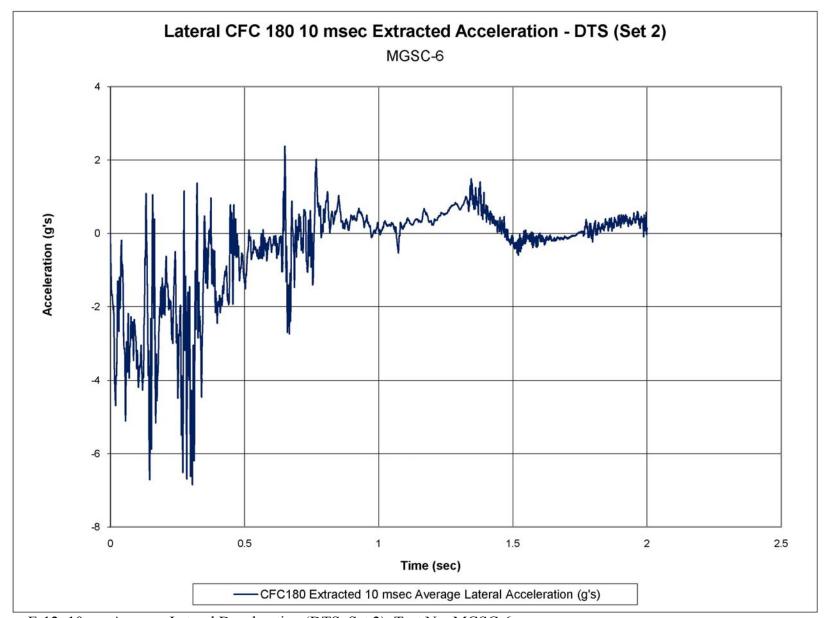


Figure E-12. 10-ms Average Lateral Deceleration (DTS, Set 2), Test No. MGSC-6

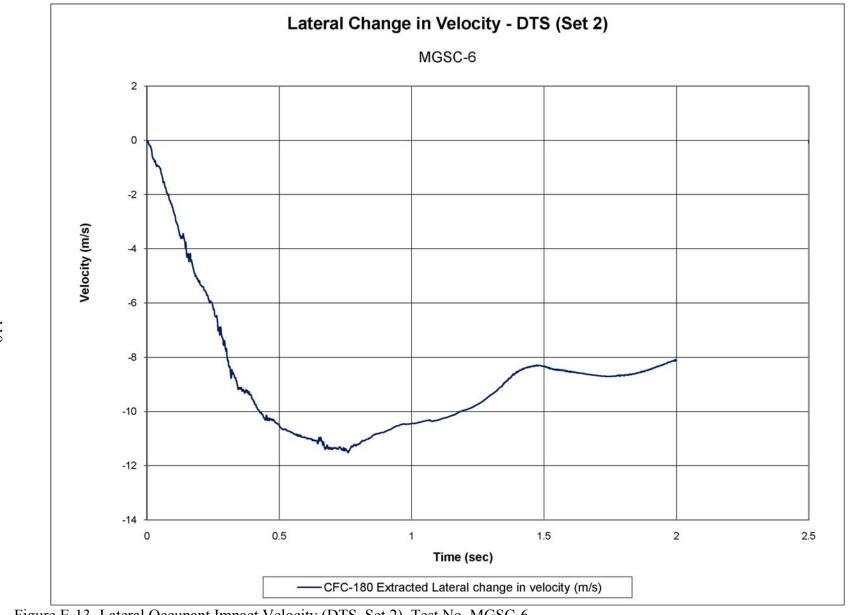


Figure E-13. Lateral Occupant Impact Velocity (DTS, Set 2), Test No. MGSC-6

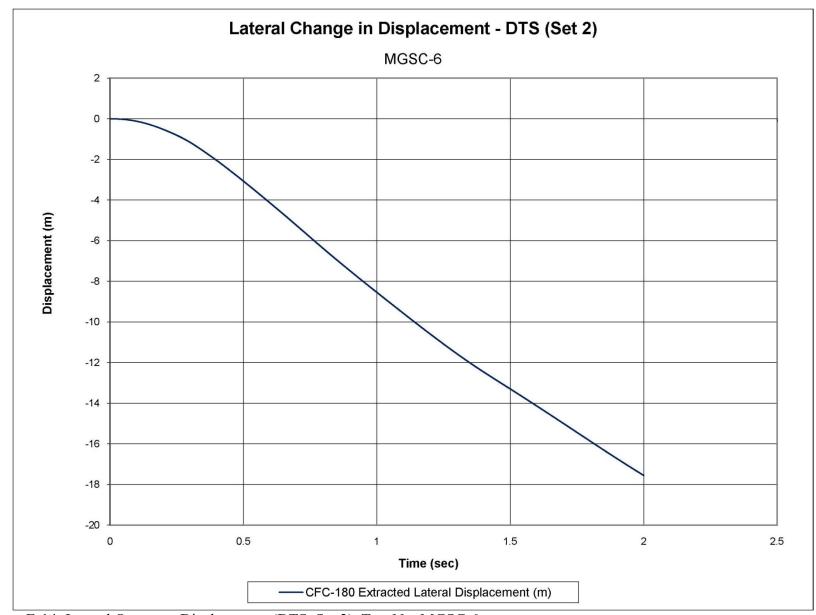


Figure E-14. Lateral Occupant Displacement (DTS, Set 2), Test No. MGSC-6

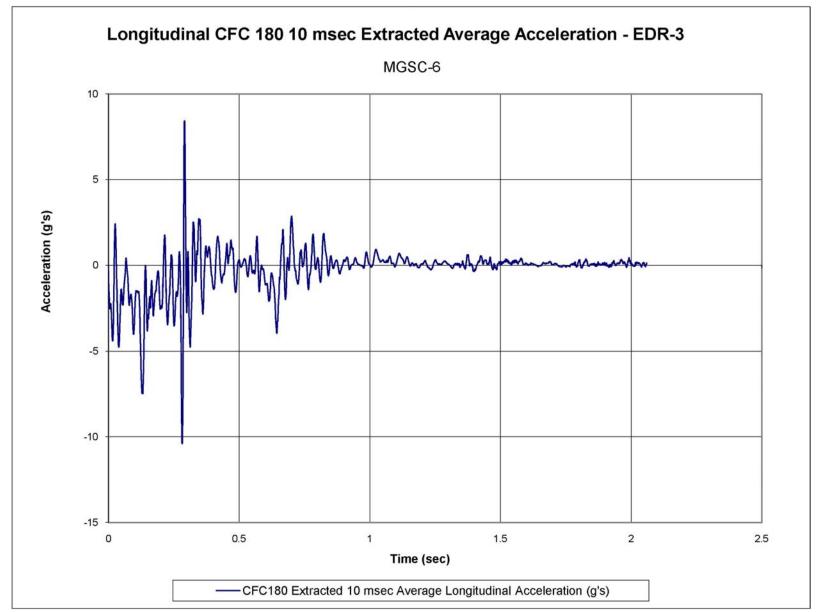


Figure E-15. 10-ms Average Longitudinal Deceleration (EDR-3), Test No. MGSC-6

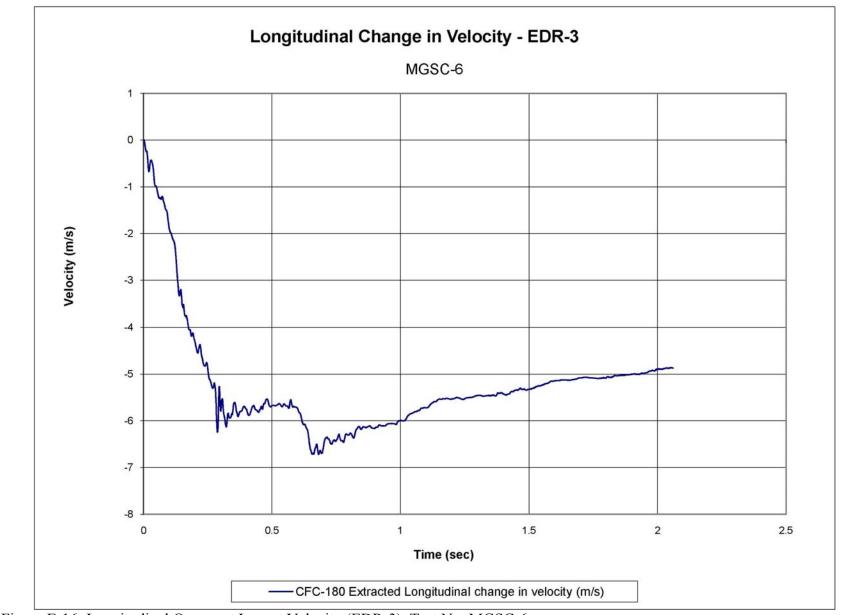


Figure E-16. Longitudinal Occupant Impact Velocity (EDR-3), Test No. MGSC-6



Figure E-17. Longitudinal Occupant Displacement (EDR-3), Test No. MGSC-6

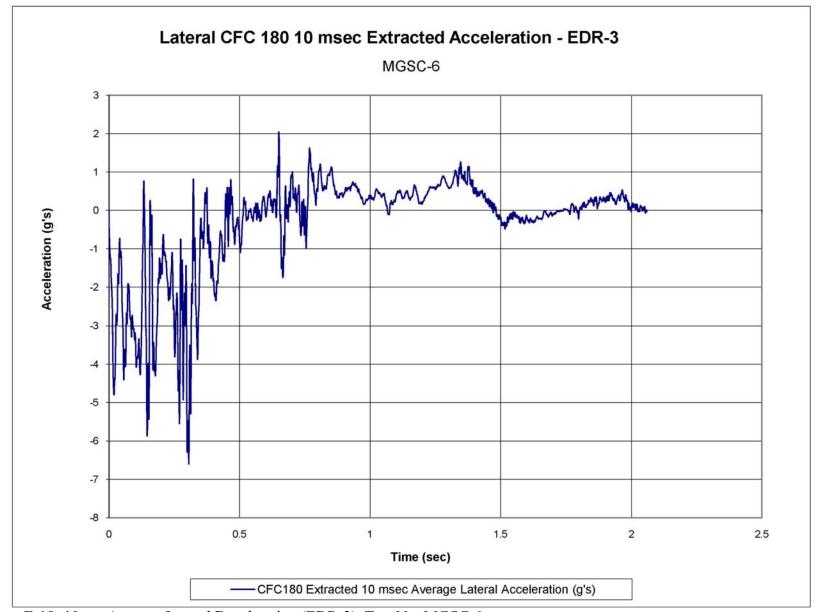


Figure E-18. 10-ms Average Lateral Deceleration (EDR-3), Test No. MGSC-6

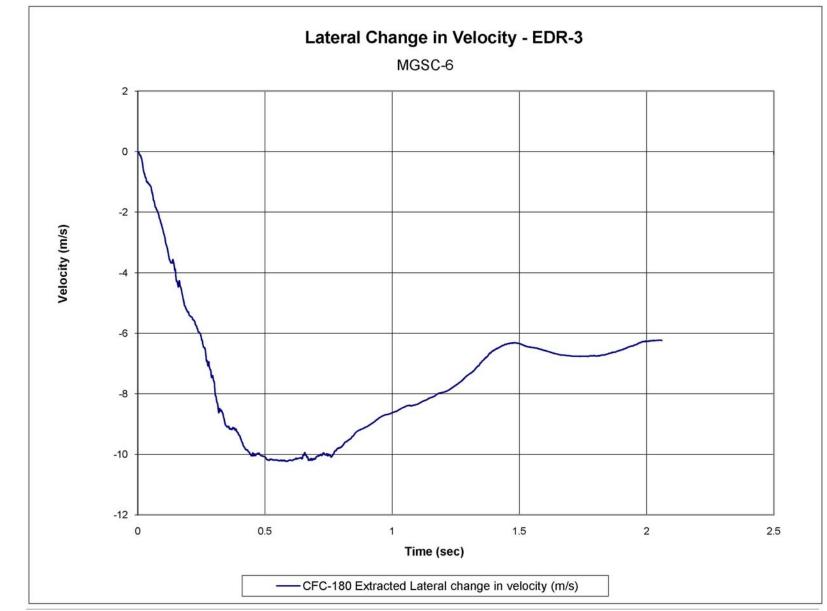


Figure E-19. Lateral Occupant Impact Velocity (EDR-3), Test No. MGSC-6



Figure E-20. Lateral Occupant Displacement (EDR-3), Test No. MGSC-6

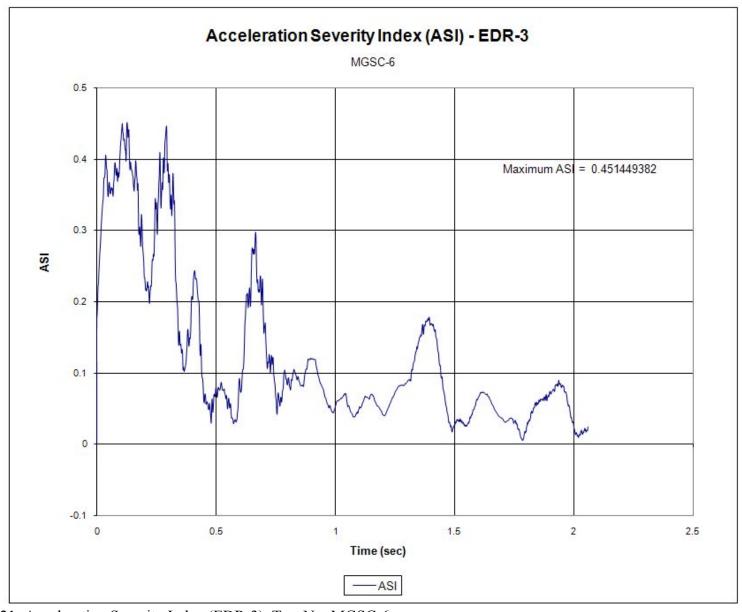


Figure E-21. Acceleration Severity Index (EDR-3), Test No. MGSC-6

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