PERFORMANCE EVALUATION OF THE MODIFIED G4(1S) GUARDRAIL – UPDATE TO NCHRP 350 TEST NO. 3-11 WITH 28" C.G. HEIGHT (2214WB-2)

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16. Abstract (Limit: 200 words)

Based on the proposed changes to the National Cooperative Highway Research Program (NCHRP) Report No. 350 guidelines, NCHRP Project 22-14(2) researchers deemed it appropriate to evaluate a strong-post W-beam guardrail systems prior to finalizing the new crash testing procedures and guidelines. For this effort, the modified G4(1S) W-beam guardrail system was selected for evaluation. One full-scale vehicle crash test was performed on the longitudinal barrier system in accordance with the Test Level 3 (TL-3) requirements presented in the Update to NCHRP Report No. 350. For the modified G4(1S) testing program, a 2270P pickup truck vehicle, which was a ½-ton, four-door vehicle with a 711 mm (28 in.) c.g. height, was used.

The modified G4(1S) W-beam guardrail system, mounted at the metric top rail height of 706 mm (27.75 in.), provided an acceptable safety performance when impacted by the ½-ton, four-door pickup truck, thus meeting the proposed TL-3 requirements presented in the Update to NCHRP Report No. 350.

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TABLE OF CONTENTS

Page

List of Figures

Page

List of Tables

Page

1 INTRODUCTION

1.1 Problem Statement

In the late 1990s, roadside safety experts, State DOT representatives, Federal government officials, and industry personnel began discussions and preparations for updating the National Cooperative Highway Research Program (NCHRP) Report No. 350 safety performance guidelines (1). The new guidelines would improve upon existing test procedures, consider changes in the vehicle fleet, provide criteria for new roadside hardware categories and re-evaluate the appropriateness of the impact conditions.

In 1997, NCHRP Project 22-14, entitled *Improvement of the Procedures for the Safety Performance Evaluation of Roadside Features*, was initiated with the intent to: (1) evaluate the relevance and efficacy of the crash testing procedures, (2) assess the needs for updating NCHRP Report No. 350, and (3) provide recommended strategies for their implementation. Following the completion of this NCHRP study at the Texas Transportation Institute (TTI) in 2001, a follow-on research study was begun in 2002. NCHRP Project 22-14(2), entitled *Improved Procedures for Safety Performance Evaluation of Roadside Features*, was undertaken by Midwest Roadside Safety Facility (MwRSF) researchers with the objectives to: (1) prepare the revised crash testing guidelines, (2) assess the effects of any proposed guidelines, and (3) identify research needs for future improvements to the procedures.

Consequently, it was anticipated that a number of revisions would be incorporated into the Update of NCHRP Report No. 350 guidelines (2). For example, changes in the vehicle fleet have resulted in the need to reassess the small car and pickup truck test vehicles. Accordingly, new, heavier test vehicles have been selected for both the small car and light truck classes of vehicles.

Additionally, during the second study, researchers determined that the 100 km/h (62.1 mph) impact speed and 25 degree impact angle would remain the same as used in NCHRP Report No. 350 for the large passenger vehicle class impacting longitudinal barriers. However, the impact angle for the small car impact condition would increase from 20 to 25 degrees for evaluating longitudinal barriers and the length-of-need for guardrail terminals. The effects of any changes to vehicle specifications or impact conditions must be understood before the safety performance evaluation guidelines are finalized. Therefore, a series of full-scale crash tests on NCHRP Report No. 350 approved systems were to be conducted with the new test vehicles and impact conditions.

1.2 Objective

The objective of this research project was to evaluate the safety performance of the modified G4(1S) guardrail system when full-scale vehicle crash tested according to the test designation no. 3-11 criteria presented in the Update of NCHRP Report No. 350 guidelines (2).

1.3 Scope

The research objective was achieved through the completion of several tasks. First, a full-scale vehicle crash test was performed on the modified G4(1S) guardrail system. The crash test utilized a pickup truck, weighing approximately 2,268 kg (5,000 lbs) with a center of gravity (c.g.) height of 711 mm (28 in.). The target impact conditions for the test were an impact speed of 100.0 km/h (62.1 mph) and an impact angle of 25 degrees. Next, the test results were analyzed, evaluated, and documented. Finally, conclusions and recommendations were made that pertain to the safety performance of the modified G4(1S) guardrail system relative to the test performed.

2 TEST REQUIREMENTS AND EVALUATION CRITERIA

2.1 Test Requirements

Historically, longitudinal barriers, such as W-beam guardrail systems, have been required to satisfy impact safety standards in order to be accepted by the Federal Highway Administration (FHWA) for use on National Highway System (NHS) construction projects or as a replacement for existing designs not meeting current safety standards. In recent years, these safety standards have consisted of the guidelines and procedures published in NCHRP Report No. 350 (1). However, NCHRP Project 22-14(2) generated revised testing procedures and guidelines for use in the evaluation of roadside safety appurtenances and were presented in the draft report entitled, *NCHRP Report 350 Update* (2). Therefore, according to Test Level 3 (TL-3) of the Update to NCHRP Report No. 350, longitudinal barrier systems must be subjected to two full-scale vehicle crash tests. The two full-scale crash tests are as follows:

1. Test Designation 3-10. An 1,100-kg (2,425-lb) passenger car impacting at a nominal speed and angle of 100.0 km/h (62.1 mph) and 25 degrees, respectively.

2. Test Designation 3-11. A 2,270-kg (5,004-lb) pickup truck impacting at a nominal speed and angle of 100.0 km/h (62.1 mph) and 25 degrees, respectively.

The test conditions for TL-3 longitudinal barriers are summarized in Table 1. Test Designation 3-11 was conducted for the modified G4(1S) guardrail system described herein.

2.2 Evaluation Criteria

According to the Update to NCHRP Report No. 350, the evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the barrier to contain, redirect, or allow controlled vehicle penetration in a predictable manner. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Vehicle trajectory after collision is a measure of the potential for the post-impact trajectory of the vehicle to cause subsequent multi-vehicle accidents. This criterion also indicates the potential safety hazard for the occupants of other vehicles or the occupants of the impacting vehicle when subjected secondary collisions with other fixed objects. These three evaluation criteria are summarized in Table 2 and defined in greater detail in the Update to NCHRP Report No. 350 report (2). The full-scale vehicle crash tests were conducted and reported in accordance with the procedures provided in the Update to NCHRP Report No. 350.

Table 1. Update to NCHRP Report No. 350 Test Level 3 Crash Test Conditions

Test Article	Test Designation	Test Vehicle	Impact Conditions			Evaluation Criteria [1]
			Speed		Angle (degrees)	
			(km/h)	(mph)		
Longitudinal Barrier	3-10	1100C	100	62.1	25	A,D,F,H,I,M
	3-11	2270P	100	62.1	25	A,D,F,H,I,M

[1] Evaluation criteria explained in Table 2.

Table 2. Update to NCHRP Report No. 350 Evaluation Criteria for Crash Tests

Structural Adequacy	A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.
Occupant Risk	D. Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of the Update to NCHRP Report No. 350.
	F. The vehicle should remain upright during and after collision.
	H. Longitudinal and lateral occupant impact velocities should fall below the preferred value of 9.0 m/s (29.5 ft/s), or at least below the maximum allowable value of 12.0 m/s (39.4 ft/s).
	I. Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15 Gs, or at least below the maximum allowable value of 20.0 Gs.
Vehicle Trajectory	M. After impact, the vehicle shall exit the barrier within the exit box.

3 TEST CONDITIONS

3.1 Test Facility

The testing facility is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 8.0 km (5 mi.) northwest of the University of Nebraska-Lincoln.

3.2 Vehicle Tow and Guidance System

A reverse cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer was located on the tow vehicle to increase the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch (3) was used to steer the test vehicle. A guide-flag, attached to the front-right wheel and the guide cable, was sheared off before impact with the barrier system. The 9.5-mm (0.375-in.) diameter guide cable was tensioned to approximately 15.6 kN (3,500 lbf), and supported laterally and vertically every 30.48 m (100 ft) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide-flag struck and knocked each stanchion to the ground. For test 2214WB-2, the vehicle guidance system was 324 m (1,062 ft) long.

3.3 Test Vehicles

For test 2214WB-2, a 2002 Dodge Ram 1500 Quad Cab pickup truck was used as the test vehicle. The test inertial and gross static weights were 2,268 kg (5,000 lbs). The test vehicle is shown in Figure 1, and vehicle dimensions are shown in Figure 2.

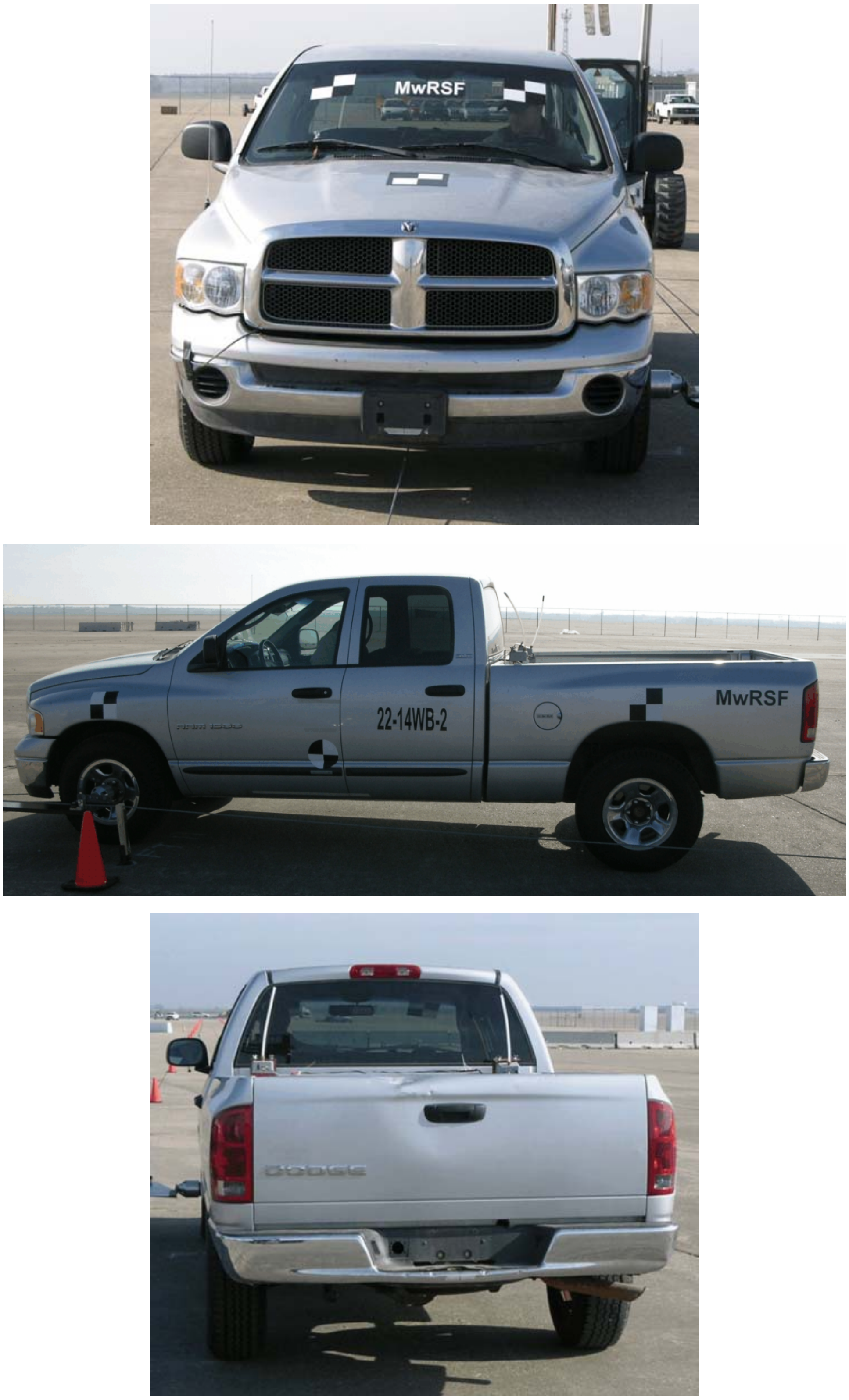


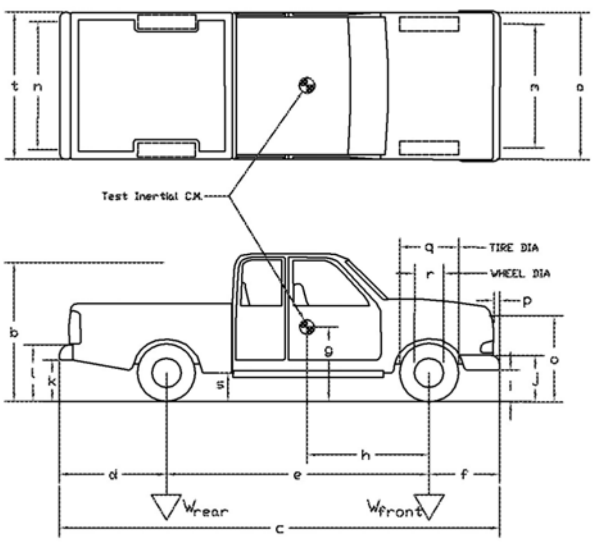
Figure 1. Test Vehicle, Test 2214WB-2

Date: 04/08/2005 Test Number: 2214WB-2 Model: RAM 1500 QUAD CAD 4x2

Make: DODGE Vehicle I.D.#: 1d7ha18z925520817

Tire Size: LT 265/70 R17 Year: 2002 Odometer: 97127

*(All Measurements Refer to Impacting Side)



Vehicle Geometry – mm (in.)

a	1981 (78.0)	b	1911 (75.25)
c	5779 (227.5)	d	1213 (47.75)
e	3562 (140.25)	f	1003 (39.5)
g	716 (28.2)	h	1537 (60.5)
i	375 (14.75)	j	679 (26.75)
k	546 (21.5)	l	756 (29.75)
m	1718 (67.625)	n	1718 (67.625)
o	1099 (43.25)	p	89 (3.5)
q	800 (31.5)	r	445 (17.5)
s	400 (15.75)	t	1911 (75.25)

Wheel Center Height Front 381 (15.0)

Wheel Center Height Rear 387 (15.25)

Wheel Well Clearance (FR) 895 (35.25)

Wheel Well Clearance (RR) 978 (38.50)

Frame Height (FR) 444 (17.5)

Frame Height (RR) 648 (25.5)

Weights kg (lbs)	Curb	Test Inertial	Gross Static
W_{front}	1325 (2921)	1290 (2844)	1290 (2844)
W_{rear}	997 (2197)	978 (2156)	978 (2156)
W_{total}	2321 (5118)	2268 (5000)	2268 (5000)

GVWR Ratings
Front 1656 (3650)
Rear 1769 (3900)
Total 3016 (6650)

Engine Type 8 CYL. GAS

Engine Size 5.9 L 360c.i.

Transmission Type:

(Automatic) or Manual

FWD or (RWD) or 4WD

Note any damage prior to test: None

Figure 2. Vehicle Dimensions, Test 2214WB-2

The Suspension Method (4) was used to determine the vertical component of the c.g. for the pickup truck. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the location of the center of gravity. The longitudinal component of the c.g. was determined using the measured axle weights. The location of the final center of gravity is shown in Figures 1 and 2.

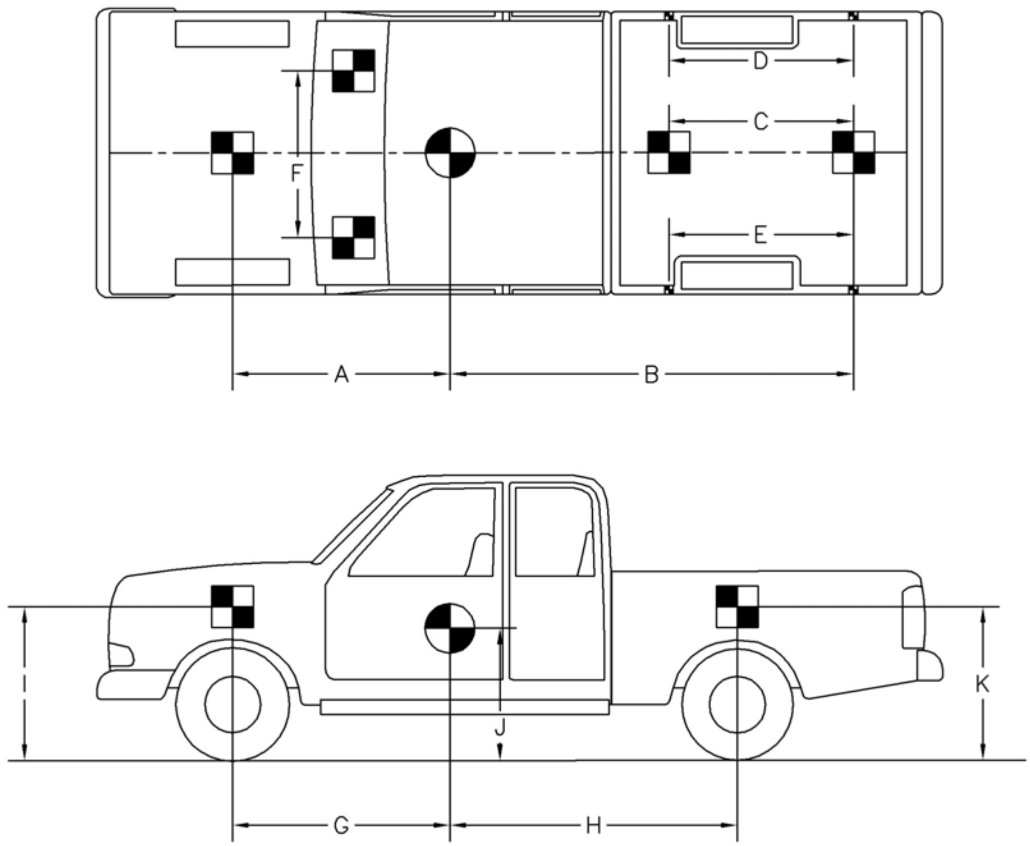
Square black and white-checkered targets were placed on the vehicle to aid in the analysis of the high-speed film and E/cam and Photron video, as shown in Figure 3. Checkered targets were placed on the center of gravity, on the driver's side door, on the passenger's side door, and on the roof of the vehicle. The remaining targets were located for reference so that they could be viewed from the high-speed cameras for film analysis.

The front wheels of the test vehicle were aligned for camber, caster, and toe-in values of zero so that the vehicle would track properly along the guide cable. Two 5B flash bulbs were mounted on both the hood and roof of the vehicle to pinpoint the time of impact with the barrier on the high-speed film, E/cam video, and Photron video. The flash bulbs were fired by a pressure tape switch mounted on the front face of the bumper. A remote-controlled brake system was installed in the test vehicle so the vehicle could be brought safely to a stop after the test.

3.4 Data Acquisition Systems

3.4.1 Accelerometers

One triaxial piezoresistive accelerometer system with a range of ±200 Gs was used to measure the acceleration in the longitudinal, lateral, and vertical directions at a sample rate of 10,000



TEST #: 2214WB-2

TARGET GEOMETRY -- mm (in.)

A 2486 (97.875)	D 1622 (63.875)	G 1537 (60.5)	J 1099 (43.25)
B 2324 (91.5)	E 1626 (64.0)	H 2026 (79.75)	K 716 (28.2)
C 1699 (66.875)	F 918 (36.125)	I 1013 (39.875)	

Figure 3. Vehicle Target Locations, Test 2214WB-2

Hz. The environmental shock and vibration sensor/recorder system, Model EDR-4M6, was developed by Instrumented Sensor Technology (IST) of Okemos, Michigan and includes three differential channels as well as three single-ended channels. The EDR-4 was configured with 6 MB of RAM memory and a 1,500 Hz lowpass filter. Computer software, “DynaMax 1 (DM-1)” and “DADiSP”, was used to analyze and plot the accelerometer data.

Another triaxial piezoresistive accelerometer system with a range of ±200 Gs was also used to measure the acceleration in the longitudinal, lateral, and vertical directions at a sample rate of 3,200 Hz. The environmental shock and vibration sensor/recorder system, Model EDR-3, was developed by Instrumental Sensor Technology (IST) of Okemos, Michigan. The EDR-3 was configured with 256 kB of RAM memory and a 1,120 Hz lowpass filter. Computer software, “DynaMax 1 (DM-1)” and “DADiSP”, was used to analyze and plot the accelerometer data.

3.4.2 Rate Transducers

An Analog Systems 3-axis rate transducer with a range of 1,200 degrees/sec in each of the three directions (pitch, roll, and yaw) was used to measure the rates of motion of the test vehicle. The rate transducer was mounted inside the body of the EDR-4M6 and recorded data at 10,000 Hz to a second data acquisition board inside the EDR-4M6 housing. The raw data measurements were then downloaded, converted to the appropriate Euler angles for analysis, and plotted. Computer software, “DynaMax 1 (DM-1)” and “DADiSP”, was used to analyze and plot the rate transducer data.

3.4.3 High-Speed Photography

For test 2214WB-2, two high-speed Photron video cameras, two high-speed AOS VITcam video cameras, and one high-speed Red Lake E/cam video cameras, all with operating speeds of 500 frames/sec, were used to film the crash test. Seven Canon digital video cameras, with a standard operating speed of 29.97 frames/sec, were also used to film the crash test. Camera details and a schematic of all twelve camera locations for test 2214WB-2 is shown in Figure 4. The Photron and AOS videos and E/cam videos were analyzed using the ImageExpress MotionPlus software and Redlake Motion Scope software, respectively. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed film.

3.4.4 Pressure Tape Switches

For test 2214WB-2, five pressure-activated tape switches, spaced at 2-m (6.56-ft) intervals, were used to determine the speed of the vehicle before impact. Each tape switch fired a strobe light which sent an electronic timing signal to the data acquisition system as the right-front tire of the test vehicle passed over it. Test vehicle speed was determined from electronic timing mark data recorded using TestPoint software. Strobe lights and high-speed film analysis are used only as a backup in the event that vehicle speed cannot be determined from the electronic data.

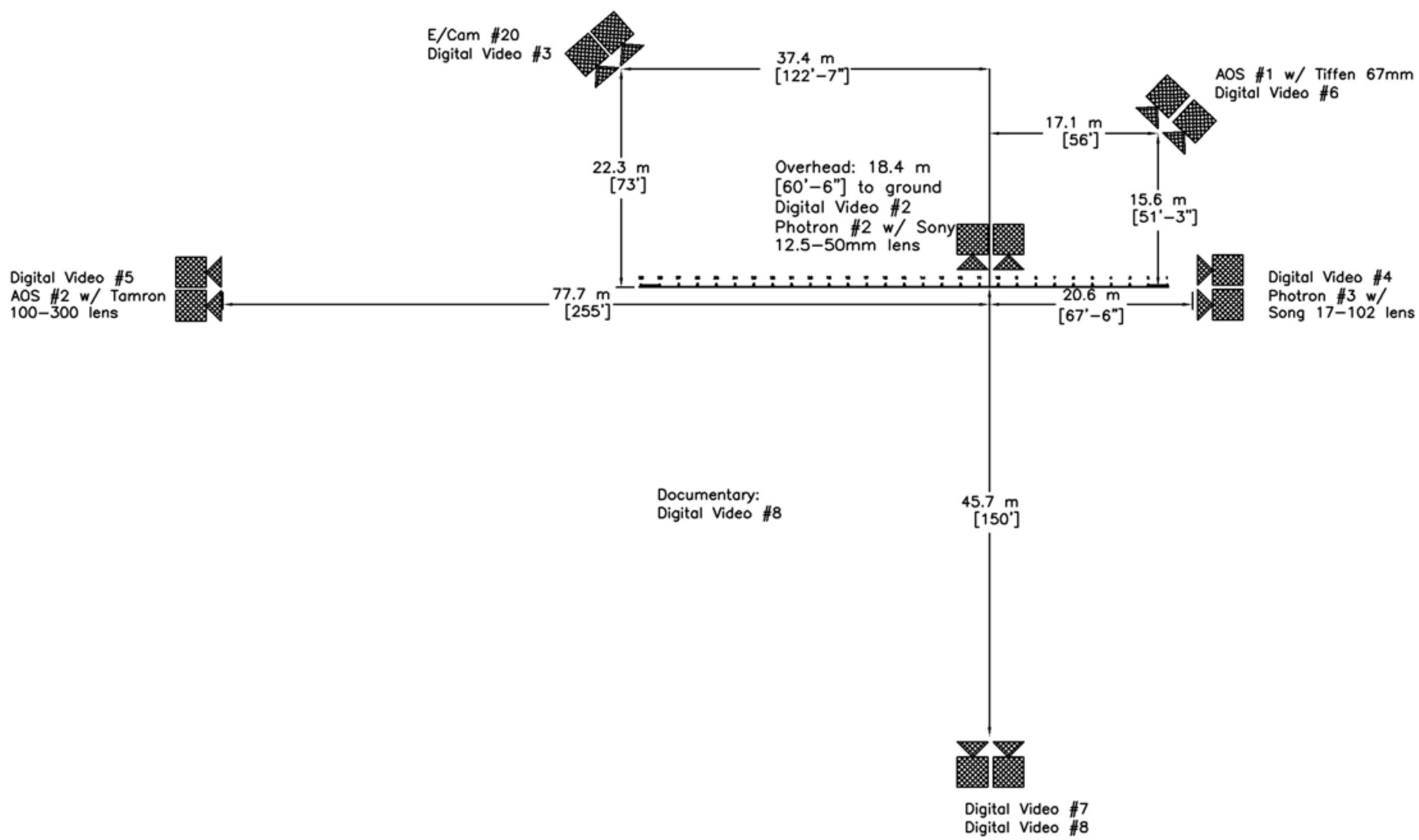


Figure 4. Location of High-Speed Cameras, Test 2214WB-2

4 DESIGN DETAILS

The test installation consisted of 53.34 m (175 ft) of standard 2.66-mm (12-gauge) thick W-beam guardrail supported by steel posts, as shown in Figure 5. Anchorage systems similar to those used on tangent guardrail terminals were utilized on both the upstream and downstream ends of the guardrail system. Design details are shown in as shown in Figures 5 through 10. The corresponding English-unit drawings are shown in Appendix A. Photographs of the test installation are shown in Figures 11 through 14.

The entire system was constructed with twenty-nine guardrail posts. Post nos. 3 through 27 were galvanized ASTM A36 steel W152x13.4 (W6x9) sections measuring 1,829 mm (6 ft) long. Post nos. 1, 2, 28, and 29 were timber posts measuring 140 mm wide x 190 mm deep x 1,080 mm long (5.5 in. x 7.5 in. x 42.5 in.) and were placed in 1,524-mm (5-ft) long steel foundation tubes with 457-mm wide x 610-mm long x 6-mm thick (18-in. x 24-in. x 0.25-in.)soil plates. The timber posts and foundation tubes were part of anchor systems designed to replicate the capacity of a tangent guardrail terminal.

Post nos. 3 through 27 were spaced 1,905 mm (75 in.) on center with a soil embedment depth of 1,098 mm (43.25 in.), as shown in Figures 5 and 7. The posts were placed in a compacted coarse, crushed limestone material that met Grading B of AASHTO M147-65 (1990) as found in the Update to NCHRP Report No. 350. For post nos. 3 through 27, 152-mm wide x 203-mm deep x 362-mm long (6-in. x 8-in. x 14.25-in.) routed wood spacer blockouts were used to block the rail away from the front face of the steel posts.

Standard 2.66-mm (12-gauge) thick W-beam rails were placed between post nos. 1 and 29, as shown in Figures 5 and 11. The W-beam's top rail height was 706 mm (27.75 in.) with a 550-mm

(21.625-in.) center mounting height. All lap-splice connections between the rail sections were configured to reduce vehicle snag at the splice during the crash test.

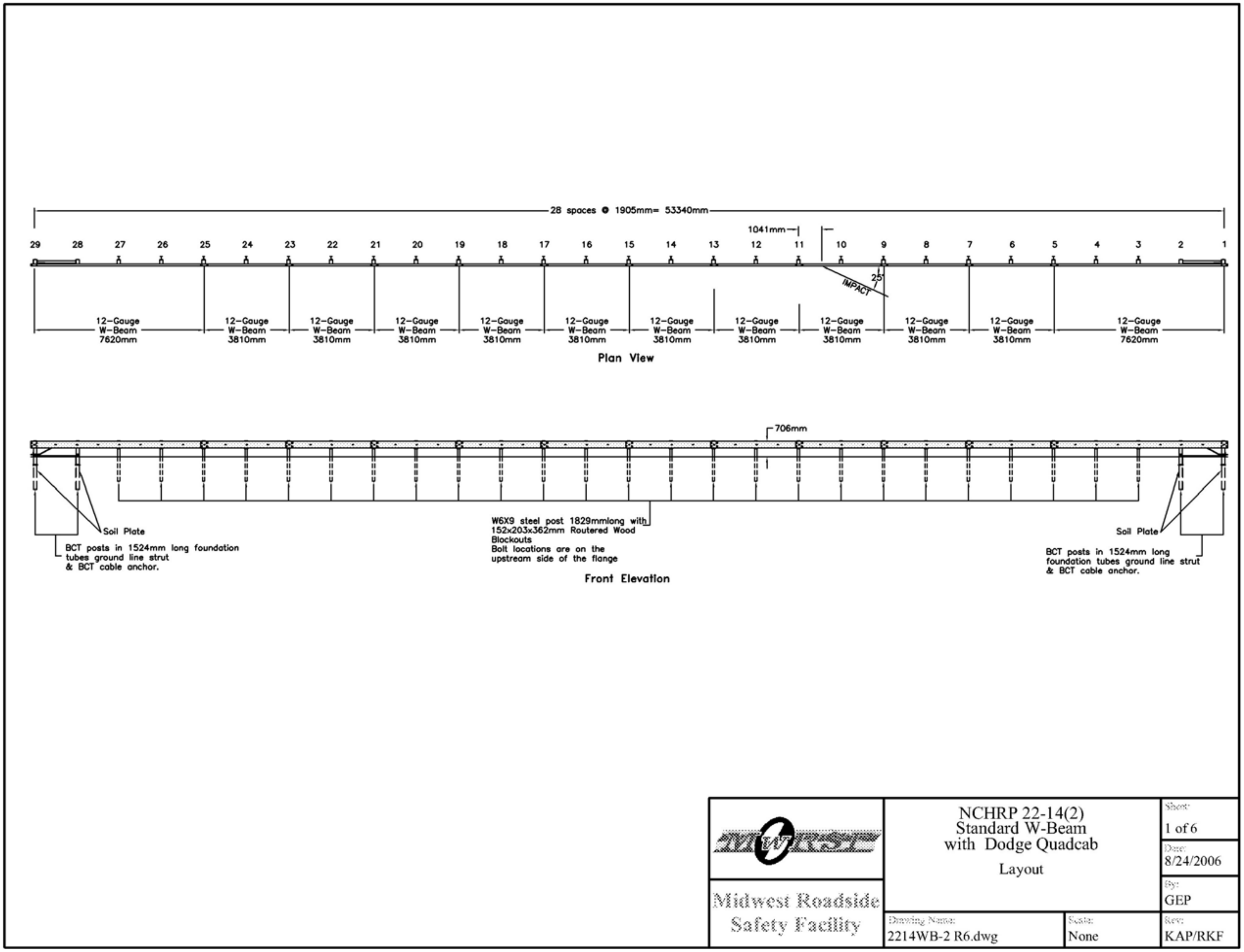


Figure 5. Layout of Standard Height, Strong Post, Wood Blockout W-beam Guardrail Design

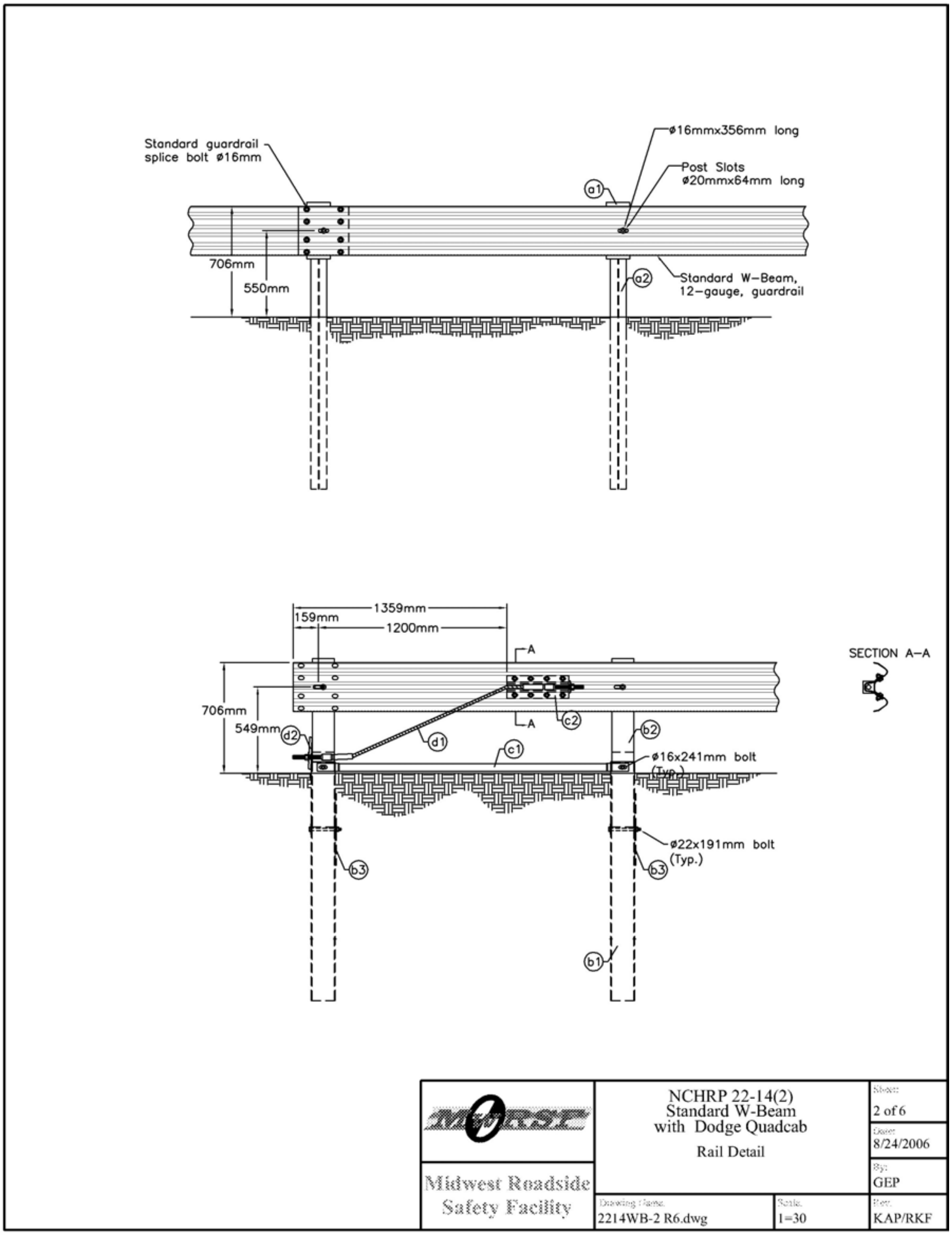


Figure 6. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail Rail Details

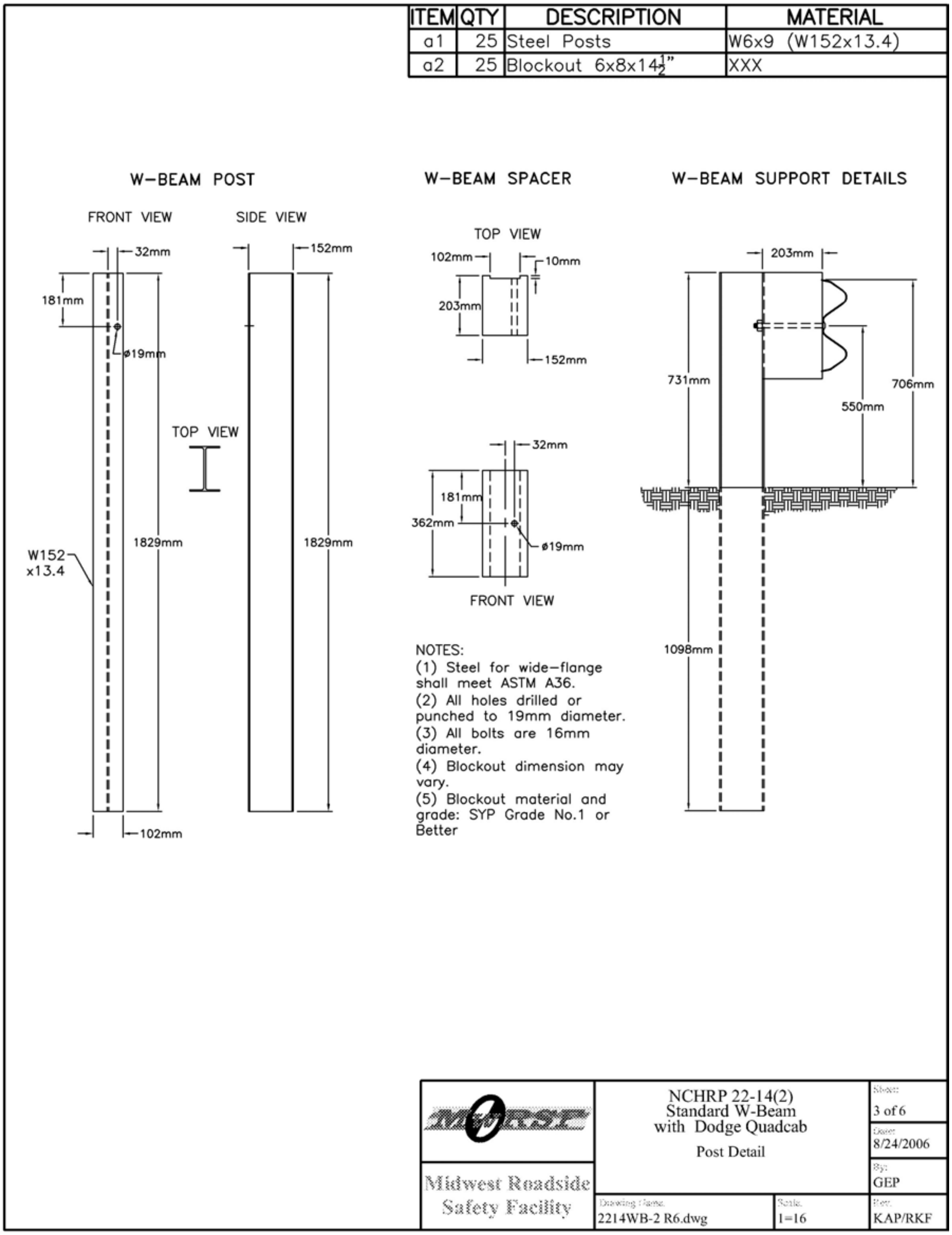


Figure 7. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail Post Details

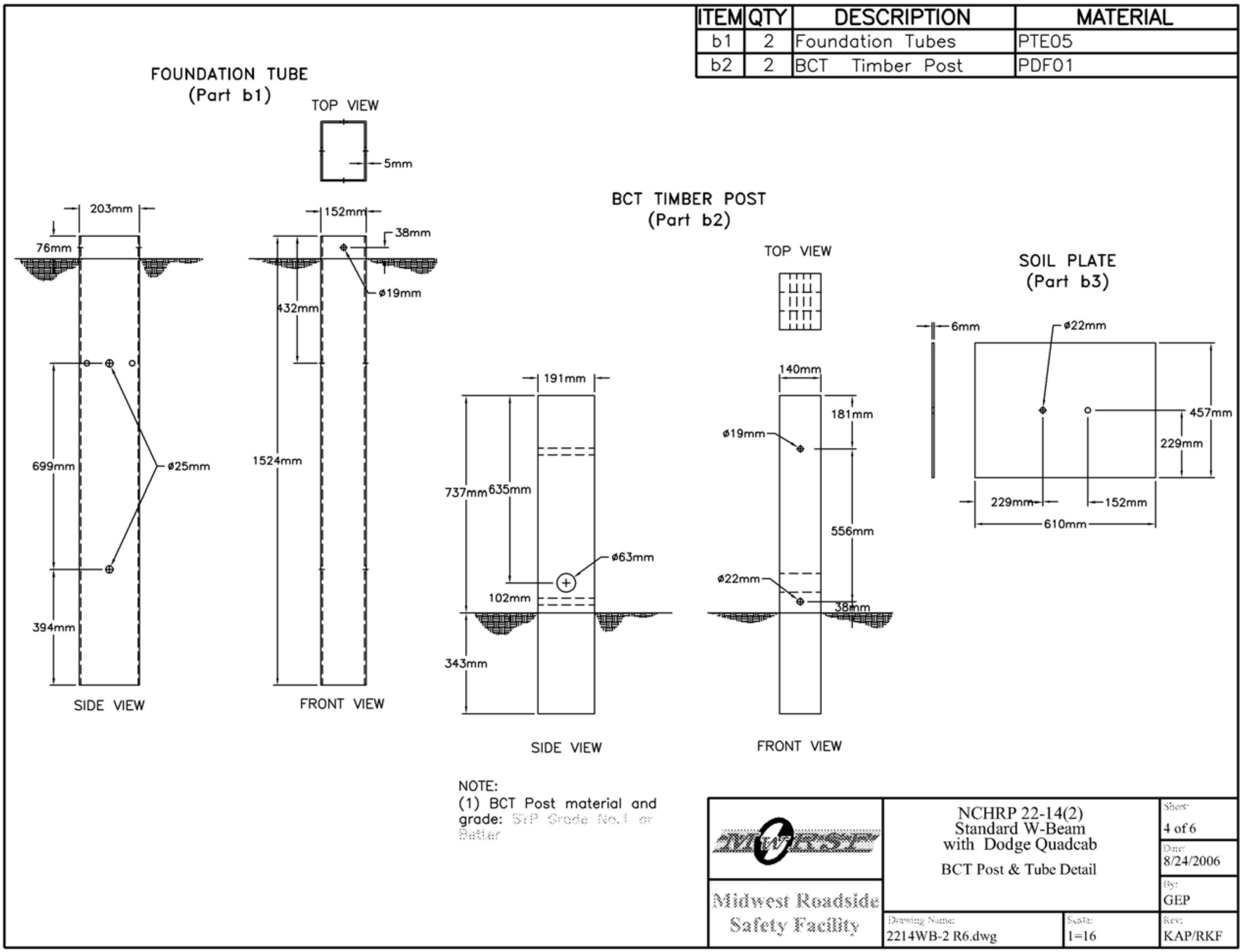


Figure 8. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail Design Anchorage Details

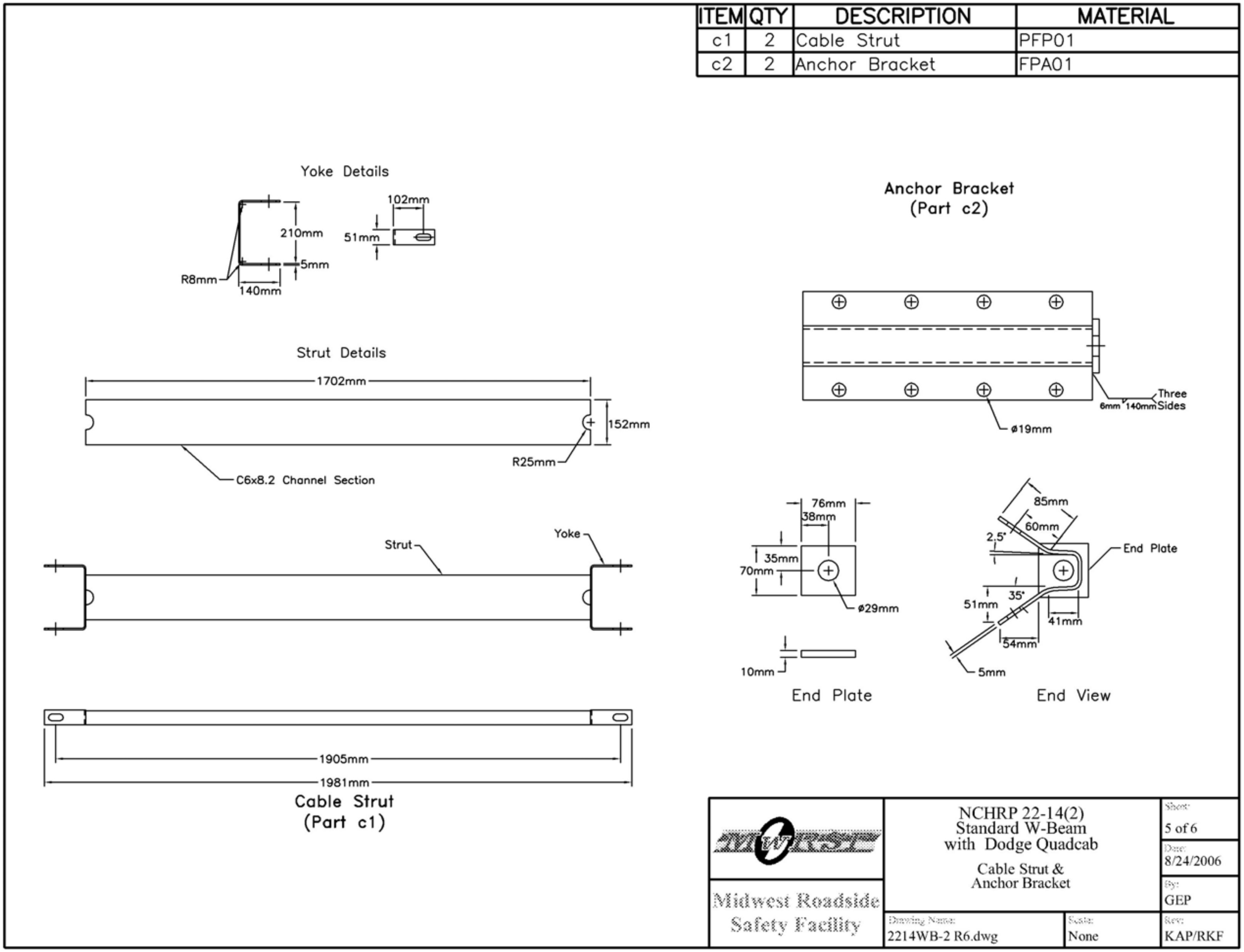


Figure 9. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail Design Anchorage Details

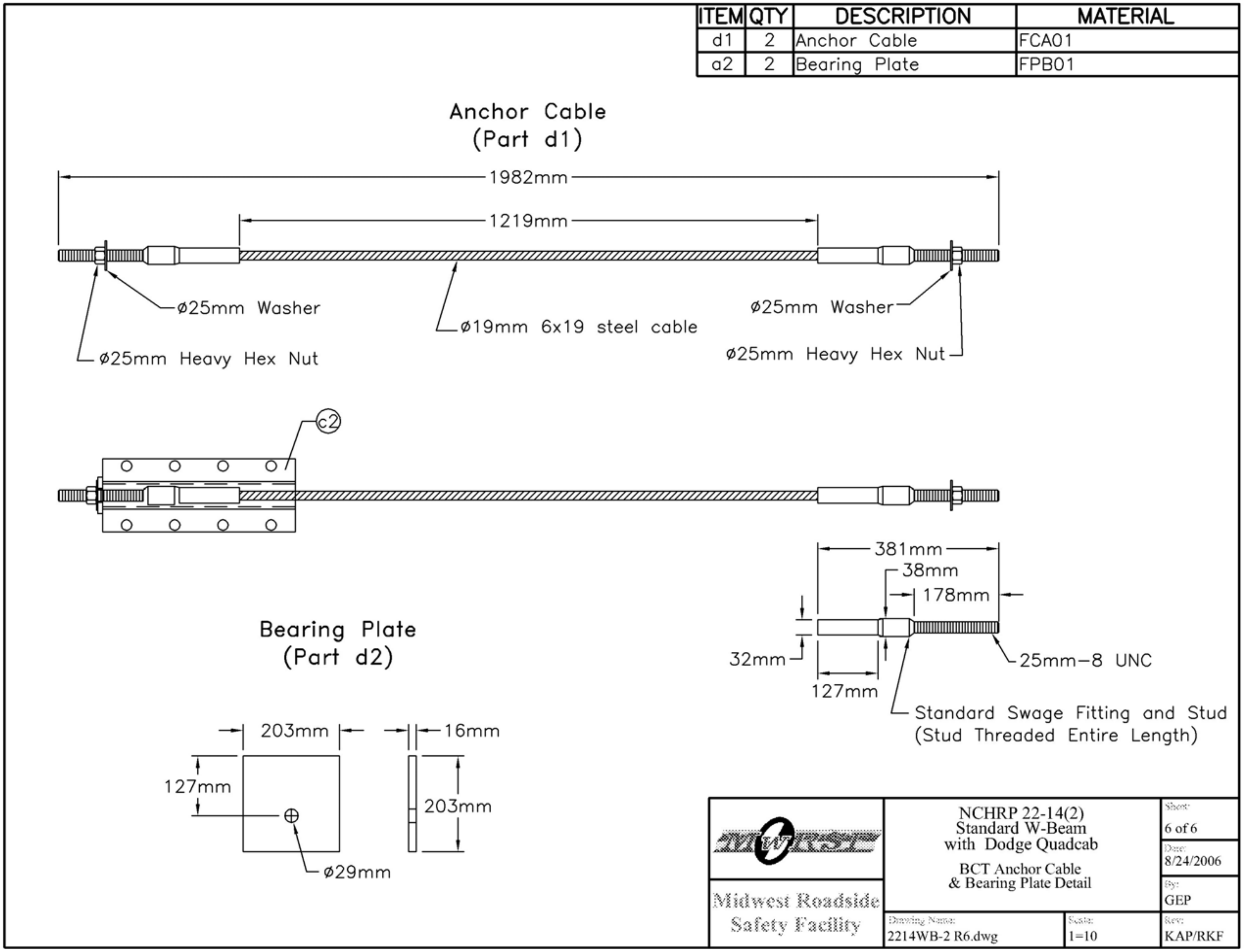


Figure 10. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail Design Anchorage Details

Figure 11. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail System

Figure 12. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail System

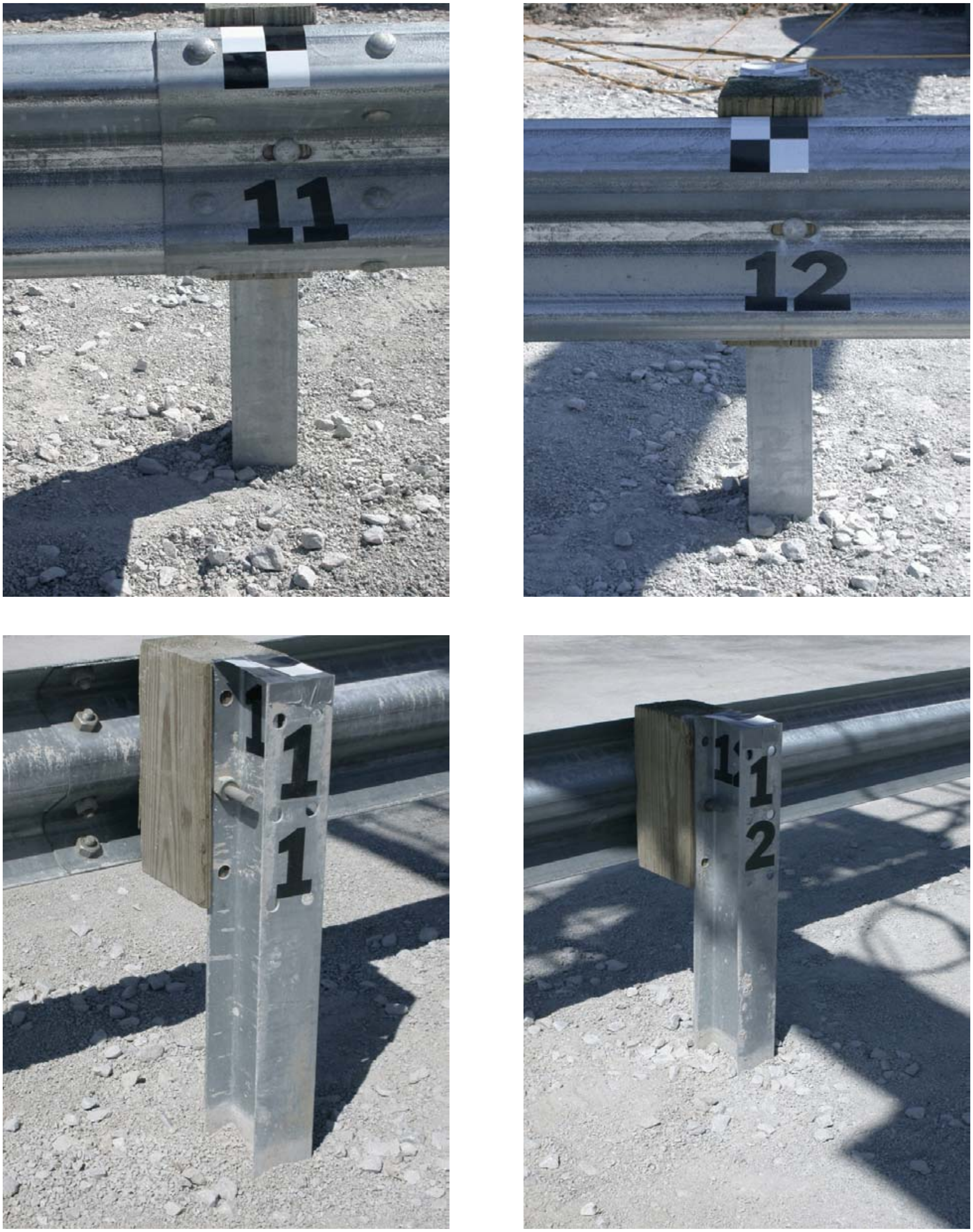


Figure 13. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail System

Figure 14. Standard Height, Strong Post, Wood Blockout W-Beam Guardrail System

5 CRASH TEST

5.1 Test 2214WB-2

The 2,268-kg (5,000-lb) pickup truck impacted the standard height, strong post, wood blockout W-beam guardrail system at a speed of 100.4 km/h (62.4 mph) and at an angle of 25.8 degrees. A summary of the test results and sequential photographs are shown in Figure 15. The summary of the test results and sequential photographs in English units are shown in Appendix B. Additional sequential photographs are shown in Figures 16 through 18. Documentary photographs of the crash test are shown in Figures 19 and 20.

5.2 Test Description

Initial vehicle impact was to occur between post nos. 10 and 11, or 1,041 mm (41 in.) upstream from the centerline of post no. 11, as shown in Figure 21. Actual vehicle impact occurred 940 mm (37 in.) upstream from the centerline of post no. 11. At 0.004 sec after impact, post no. 11 deflected. At 0.020 sec, post nos. 10 and 12 deflected. At 0.036 sec, the right-front corner of the vehicle was located at post no. 11. At 0.056 sec, the rail released from post no. 11, and the right-front headlight disengaged from the vehicle. At 0.080 sec, the vehicle began to redirect. At 0.092 sec, post nos. 6 through 12 exhibited twisting movement downstream. At 0.136 sec, the right-front corner of the vehicle was located at post no. 12. At 0.144 sec, the lower portion of the rail encountered a tear downstream of post no. 12. At 0.152 sec, the blockout disengaged from post no. 12. At 0.190 sec, the vehicle rolled CW toward the system. At 0.204 sec, post no. 15 deflected as the right-front corner of the vehicle was located at post no. 13. At this same time, the blockout disengaged from post no. 13. At 0.278 sec, the rear of the vehicle protruded over the deformed rail. At 0.292 sec, the right-front corner of the vehicle was located at post no. 14. At 0.300 sec, post no.

16 deflected. At 0.316, the vehicle became parallel to the barrier with a resultant velocity of 63.9 km/h (39.7 mph). At 0.336 sec, the blockout disengaged from post no. 14. At this same time, the CW roll of the vehicle increased. At 0.356 sec, the blockout at post no. 15 fractured and part of it disengaged from the post. At 0.382 sec, the right-front corner of the vehicle was located at post no. 15. At 0.426 sec, the left-rear tire was airborne. At 0.580 sec, the rear of the vehicle pitched downward. At 0.760 sec, the vehicle began to roll CCW away from the system. At 0.790 sec, the rear end of the vehicle yawed away from the system as the front of the vehicle pitched downward. At 0.888 sec, the vehicle exited the system at an angle of 20.7 degrees and a velocity of 50.2 km/h (31.2 mph). At 0.940 sec, the rear of the vehicle descended toward the ground. At 1.350 sec, the vehicle continued to roll CCW away from the system. At 1.490 sec, the vehicle redirected toward the system. At 1.690 sec, the vehicle rolled CW toward the system. At 1.880 sec, the front of the vehicle pitched downward. The vehicle came to rest 36.84 m (120 ft - 10.5 in.) downstream from impact and against the traffic-side face of the guardrail system. The trajectory and final position of the pickup truck are shown in Figures 15 and 22.

5.3 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 23 through 27. Barrier damage consisted of deformed guardrail posts, disengaged wooden blockouts, contact marks on a guardrail section, and deformed and torn W-beam rail. The length of vehicle contact along the W-beam guardrail system was approximately 10.5 m (34.5 ft), which spanned from 940 mm (39 in.) upstream from the centerline of post no. 11 through the centerline of post no. 16.

Moderated deformation and flattening of the impacted section of W-beam rail occurred between post nos. 10 and 16. The bottom of the rail deformed under around post no. 14. Contact marks were found on the guardrail between post nos. 10 and 16. The guardrail buckled 279 mm (11 in.) upstream of post no. 15 and at post no. 16. A 495-mm (19.5-in.) long tear was found in the lower corrugation beginning 76 mm (3 in.) downstream of post no. 12. The W-beam was pulled off of post nos. 3, 6, and 12 through 15. Due to the secondary impact after vehicle exit and redirection, the W-beam rail was flattened between post nos. 26 and 29.

Steel post nos. 3 through 9 encountered minor twisting. Post nos. 10 and 11 rotated backward and twisted. Post no. 12 through 15 encountered significant twisting and were bent longitudinally downstream to the ground. Tire contact marks were found on the front flange of post no. 12, the upstream edge of both the front and back flanges of post no. 13, and the upstream edge of the back flange of post no. 14. Post no. 14 also encountered severe chipping in the galvanization on the upstream edge of the front flange of the post. The upstream edge of the front flange of post no. 15 buckled 305 mm (12 in.) from the top. The post bolt for post no. 15 tore through the hole in the post's flange. Post no. 16 rotated backward slightly. The upstream anchorage system slightly moved longitudinally, however the posts in the anchorage system were not damaged. Due to the secondary impact after vehicle exit and redirection, post no. 27 deflected back ward and the downstream anchorage system shifted backward slightly with post no. 28 partially fractured at the breakaway hole. The wooden blockout at post nos. 12 through 15 were fractured and disengaged from the posts.

The permanent set of the barrier system is shown in Figure 24. The upstream and downstream cable anchor ends encountered slight permanent set deformations. The maximum lateral permanent set rail and post deflections were 829 mm (32.625 in.) at the midspan between post nos. 13 and 14 and 845 mm (33.25 in.) at the centerline of post no. 12, respectively, as measured in the field. The maximum lateral dynamic rail and post deflections were 1,196 mm (47.0 in.) at the midspan between post nos. 14 and 15 and 962 mm (37.87 in.) at the centerline of post no. 12, respectively, as determined from high-speed digital video analysis. The working width of the system was found to be 1,395 mm (54.9 in.).

5.4 Vehicle Damage

Exterior vehicle damage was moderate, as shown in Figures 28 and 29. Occupant compartment deformations to the right side and center of the floorboard were judged insufficient to cause serious injury to the vehicle occupants. Maximum longitudinal deflections of 13 mm (0.5 in.) were located near the left side of the right side of the floorboard. Maximum lateral deflections of 13 mm (0.5 in.) were located near the right-front corner of the right-side floor pan and the center of the right side of the floorboard. Maximum vertical deflections of 6 mm (0.25 in.) were located throughout the right side of the floorboard. Complete occupant compartment deformations and the corresponding locations are provided in Appendix C.

Damage was concentrated on the right-front corner of the vehicle. The right-front quarter panel was deformed inward and upward toward the engine compartment. The right side of the front bumper was bent back toward the engine compartment. The both right-side doors encountered deformations and flattening of sheet metal. Contact marks from vehicle-rail interlock were observed along the entire right side of the vehicle. The right-rear quarter panel was deformed inward and away from the bumper. The right side of the rear bumper was dented. The top of the right-front door was ajar. The right side of the grill was fractured. The right-side tail light cover was deformed away from the vehicle. The exhaust pipe was dented and deformed. The right-front wheel assembly deformed and crushed inward toward the engine compartment. The right-side sway bar and lower control arm connection along with the right-front tire disengaged from the rest of the wheel assembly. The right-rear steel rim was deformed and dented. The roof, the hood, the left side, and the rear of the vehicle, and all the window glass remained undamaged.

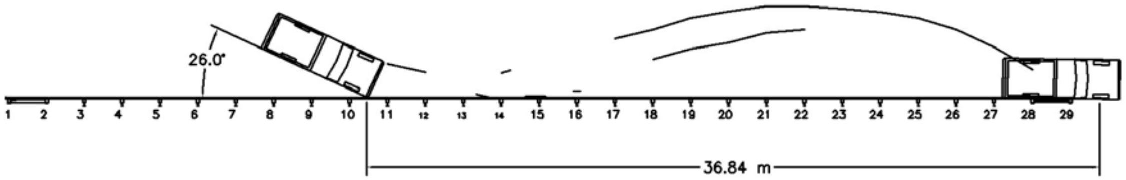
5.5 Occupant Risk Values

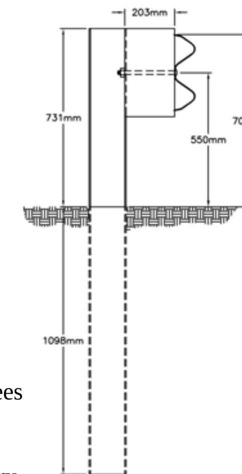
The longitudinal and lateral occupant impact velocities were determined to be 5.38 m/s (17.66 ft/s) and 3.99 m/s (13.10 ft/s), respectively. The maximum 0.010-sec average occupant ridedown decelerations in the longitudinal and lateral directions were -6.92 Gs and 6.61 Gs, respectively. It is noted that the occupant impact velocities (OIVs) and occupant ridedown decelerations (ORDs) were within the suggested limits provided in NCHRP Report No. 350. The THIV and PHD values were determined to be 6.91 m/s (22.67 ft/s) and 8.19 Gs, respectively. The results of the occupant risk, as determined from the accelerometer data, are summarized in Figure 15. Results are shown graphically in Appendix D. The results from the rate transducer are shown graphically in Appendix D.

5.6 Discussion

The analysis of the test results for test no. 2214WB-2 showed that the standard height, strong post, wood blockout W-beam guardrail system impacted with the new 2270P vehicle of the Update to NCHRP Report No. 350 adequately contained and redirected the vehicle with controlled lateral displacements of the barrier system. There were no detached elements nor fragments which showed potential for penetrating the occupant compartment nor presented undue hazard to other traffic. However, it should be noted that the rail did begin to tear in the impact region. Deformations of, or intrusion into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier system and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements were noted, but they were deemed acceptable because they did not adversely influence occupant risk safety criteria nor cause rollover. After collision, the vehicle's trajectory revealed minimum intrusion into adjacent traffic lanes. In addition, the vehicle exited the barrier within the exit box. Therefore, test no. 2214WB-2 conducted on the standard height, strong post, wood blockout W-beam guardrail system was determined to be acceptable according to the TL-3 safety performance criteria found in the Update to NCHRP Report No. 350.

0.000 sec | 0.136 sec | 0.292 sec | 0.416 sec | 0.828 sec





- Test Agency . . . . MwRSF
- Test Number 2214WB-2
- Date 4/8/05
- NCHRP 350 Update Test Designation . . 3-11
- Appurtenance . . . . Modified G4(1S) Guardrail
- Total Length . . . . 53.34 m
- Key Elements - Steel W-Beam
  - Thickness . . . . 2.66 mm
  - Top Mounting Height . . . . 706 mm
- Key Elements - Steel Posts
  - Post Nos. 3 - 27 . . . . W152x13.4 by 1,829 mm long
  - Spacing . . . . 1,905 mm
- Key Elements - Wood Posts
  - Post Nos. 1 - 2, 28 - 29 (BCT) . . . . 140 mm x 190 mm by 1,080 mm long
- Key Elements - Steel Foundation Tube . 1,524 mm long with soil plate
- Key Elements - Wood Spacer Blocks
  - Post Nos. 3 - 27 . . . . 152 mm x 203 mm by 362 mm long
- Type of Soil . . . . Grading B - AASHTO M 147-65 (1990)
- Test Vehicle
  - Type/Designation 2270P
  - Make and Model . . . . 2002 Dodge Ram 1500 Quad Cab Pickup
  - Curb . . . . 2,321 kg
  - Test Inertial . . . . 2,268 kg
  - Gross Static . . . . 2,268 kg
- Impact Conditions
  - Speed . . . . 100.4 km/h
  - Angle . . . . 25.8 degrees
  - Impact Location . . . . 940 mm upstream centerline post no. 11
- Exit Conditions
  - Speed . . . . 50.2 km/h
  - Angle . . . . 20.7 degrees
  - Exit Box Criterion . . . . Pass
- Post-Impact Trajectory
  - Vehicle Stability . . . . Satisfactory
  - Stopping Distance . . . . 36.84 m downstream Against traffic-side face
- Occupant Impact Velocity (350 Update)
  - Longitudinal . . . . $5.38 m/s < 12 m/s$
  - Lateral . . . . $3.99 m/s < 12 m/s$
- Occupant Ridedown Deceleration (350 Update)
  - Longitudinal . . . . $-6.92 Gs < 20 Gs$
  - Lateral . . . . $6.61 Gs < 20 Gs$
- THIV (not required) . . . . 6.91 m/s
- PHD (not required) . . . . 8.19 Gs
- Test Article Damage . . . . Moderate
- Test Article Deflections
  - Permanent Set . . . . 845 mm
  - Dynamic . . . . 1,196 mm
  - Working Width . . . . 1,395 mm
- Vehicle Damage . . . . Moderate
  - VDS[5] 1-RFQ-4
  - CDC[6] 1-RFEN3
  - Maximum Deformation . . . . 13 mm at front floorpan

Figure 15. Summary of Test Results and Sequential Photographs, Test 2214WB-2

0.000 sec

0.128 sec

0.278 sec

0.362 sec

0.458 sec

0.538 sec

0.778 sec

0.882 sec

1.002 sec

1.210 sec

Figure 16. Additional Sequential Photographs, Test 2214WB-2

0.000 sec

0.000 sec

0.190 sec

0.196 sec

0.330 sec

0.352 sec

0.580 sec

0.416 sec

0.940 sec

0696 sec

Figure 17. Additional Sequential Photographs, Test 2214WB-2

0.000 sec

0.000 sec

0.130 sec

0.634 sec

0.214 sec

0.934 sec

0.352 sec

1.668 sec

0.482 sec

2.236 sec

Figure 18. Additional Sequential Photographs, Test 2214WB-2

Figure 19. Documentary Photographs, Test 2214WB-2

Figure 20. Documentary Photographs, Test 2214WB-2

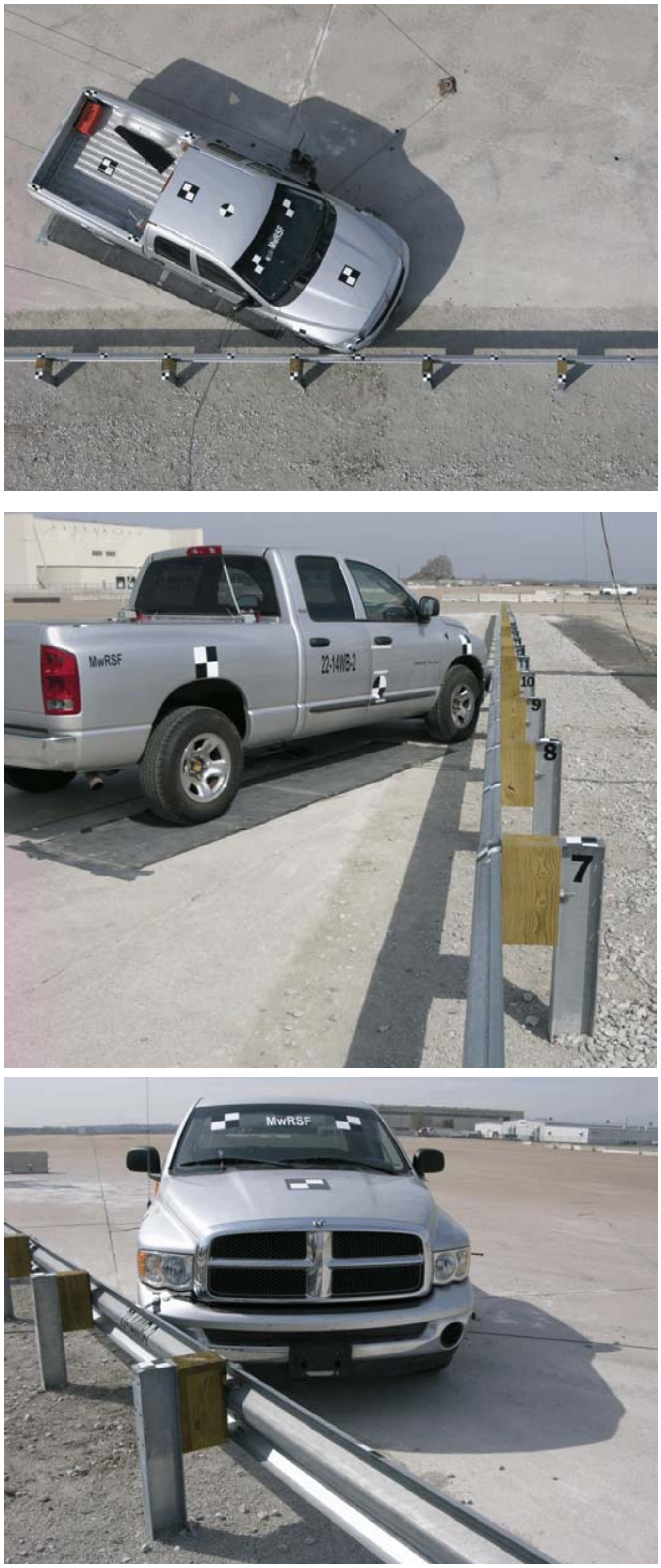


Figure 21. Impact Location, Test 2214WB-2

Figure 22. Vehicle Final Position and Trajectory Marks, Test 2214WB-2

Figure 23. Standard Strong-Post, WoodBlockout, W-beam Guardrail System Damage, Test 2214WB-2

Figure 24. Standard Strong-Post, Wood-Blockout, W-beam Guardrail System Damage, Test 2214WB-2

Figure 25. Post Nos. 9 through 12 Damage, Test 2214WB-2

Figure 26. Post Nos. 13 through 16 Damage, Test 2214WB-2

Figure 27. Rail Damage Between Post Nos. 10 through 15 Damage, Test 2214WB-2

Figure 28. Vehicle Damage, Test 2214WB-2

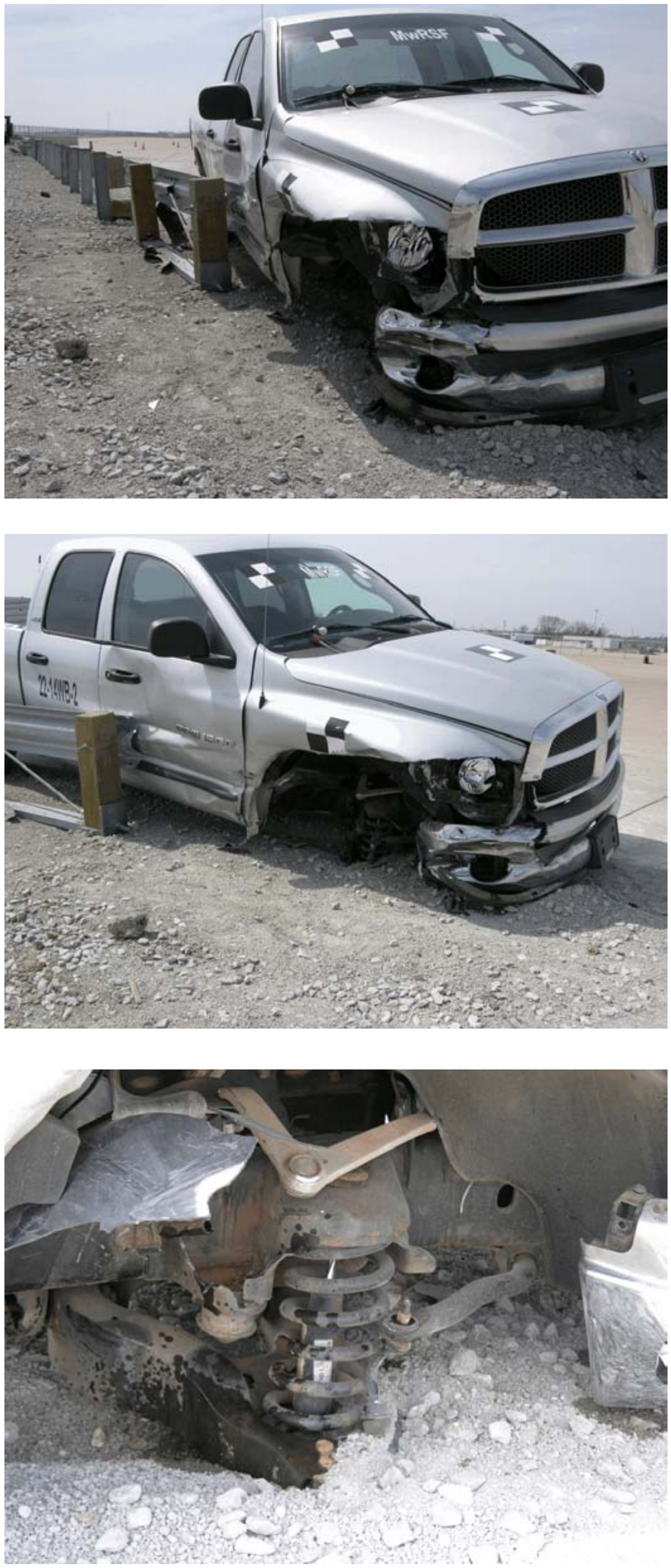


Figure 29. Vehicle Damage, Test 2214WB-2

6 SUMMARY AND CONCLUSIONS

A strong-post, W-beam guardrail system, the modified G4(1S) guardrail, was constructed and full-scale vehicle crash tested. One full-scale vehicle crash test, using a pickup truck vehicle, was performed on the longitudinal barrier system and was determined to be acceptable according to the TL-3 safety performance criteria presented in the Update to NCHRP Report No. 350. A summary of the safety performance evaluation is provided in Table 3.

Table 3. Summary of Safety Performance Evaluation Results

Evaluation Factors	Evaluation Criteria		Test 2214WB-2
Structural Adequacy	A.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.	S
Occupant Risk	D.	Detached elements, fragments or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone. Deformations of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of the Update to NCHRP Report No. 350.	S
	F.	The vehicle should remain upright during and after collision.	S
	H.	Longitudinal and lateral occupant impact velocities should fall below the preferred value of 9.0 m/s (29.5 ft/s), or at least below the maximum allowable value of 12.0 m/s (39.4 ft/s).	S
	I.	Longitudinal and lateral occupant ridedown accelerations should fall below the preferred value of 15 Gs, or at least below the maximum allowable value of 20.0 Gs.	S
Vehicle Trajectory	M.	After impact, the vehicle shall exit the barrier within the exit box.	S

S - Satisfactory
U - Unsatisfactory
NA - Not Available

7 REFERENCES

1. Ross, H.E., Sicking, D.L., Zimmer, R.A., and Michie, J.D., *Recommended Procedures for the Safety Performance Evaluation of Highway Features*, National Cooperative Research Program (NCHRP) Report No. 350, Transportation Research Board, Washington, D.C., 1993.

2. Sicking, D.L., Mak, K.K., and Rohde, J.R., *NCHRP Report No. 350 Update - Chapters 1 through 7, Draft Report*, Presented to the Transportation Research Board, Prepared by the Midwest Roadside Safety Facility, University of Nebraska-Lincoln, July 2005 [Privileged Document].

3. Hinch, J., Yang, T.L., and Owings, R., *Guidance Systems for Vehicle Testing*, ENSCO, Inc., Springfield, VA, 1986.

4. *Center of Gravity Test Code - SAE J874 March 1981*, SAE Handbook Vol. 4, Society of Automotive Engineers, Inc., Warrendale, Pennsylvania, 1986.

5. *Vehicle Damage Scale for Traffic Investigators*, Second Edition, Technical Bulletin No. 1, Traffic Accident Data (TAD) Project, National Safety Council, Chicago, Illinois, 1971.

6. *Collision Deformation Classification - Recommended Practice J224 March 1980*, Handbook Volume 4, Society of Automotive Engineers (SAE), Warrendale, Pennsylvania, 1985.

8 APPENDICES

APPENDIX A

English-Unit System Drawings

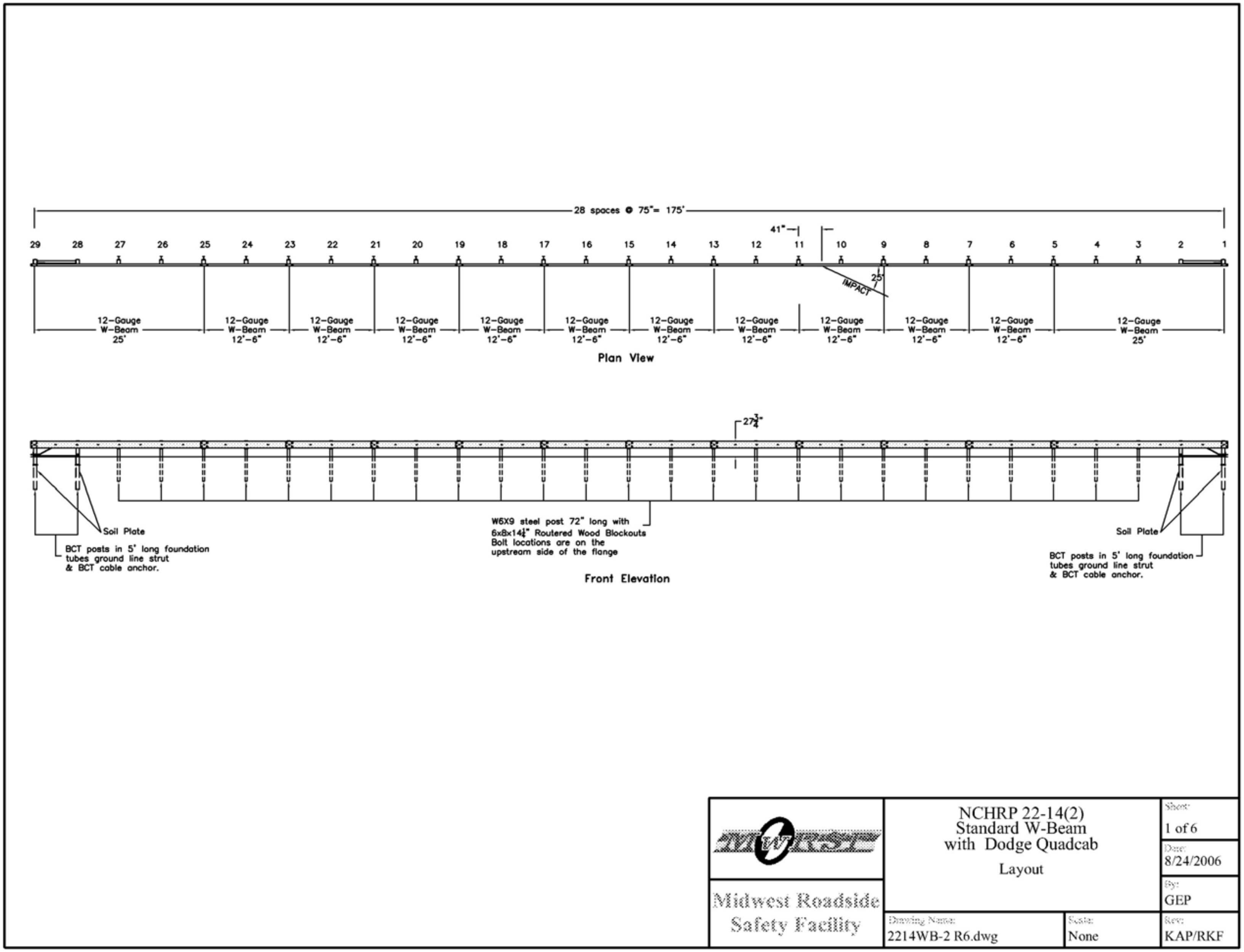


Figure A-1. Layout of Standard Height, Strong Post, Wood Blockout W-beam Guardrail Design (English)

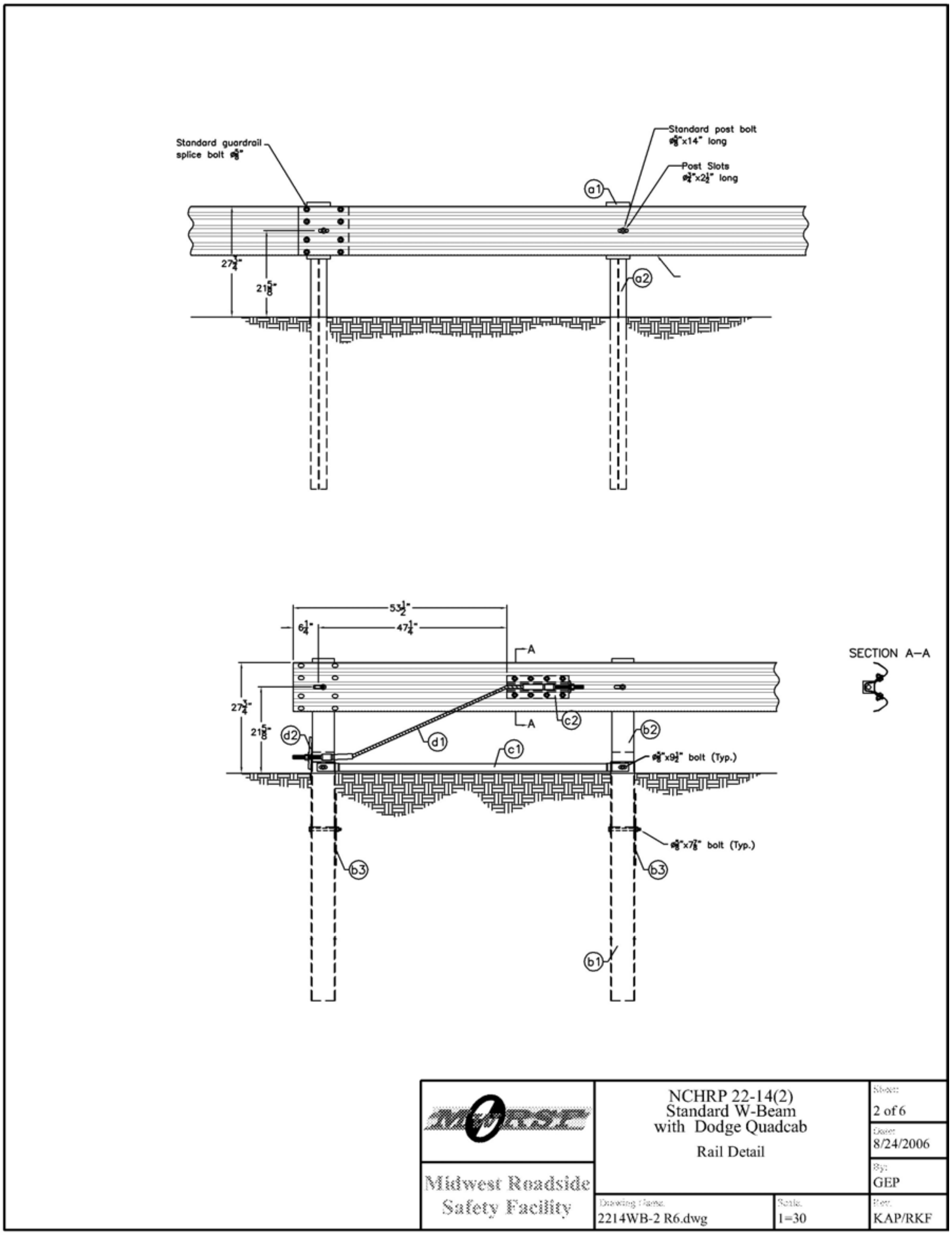
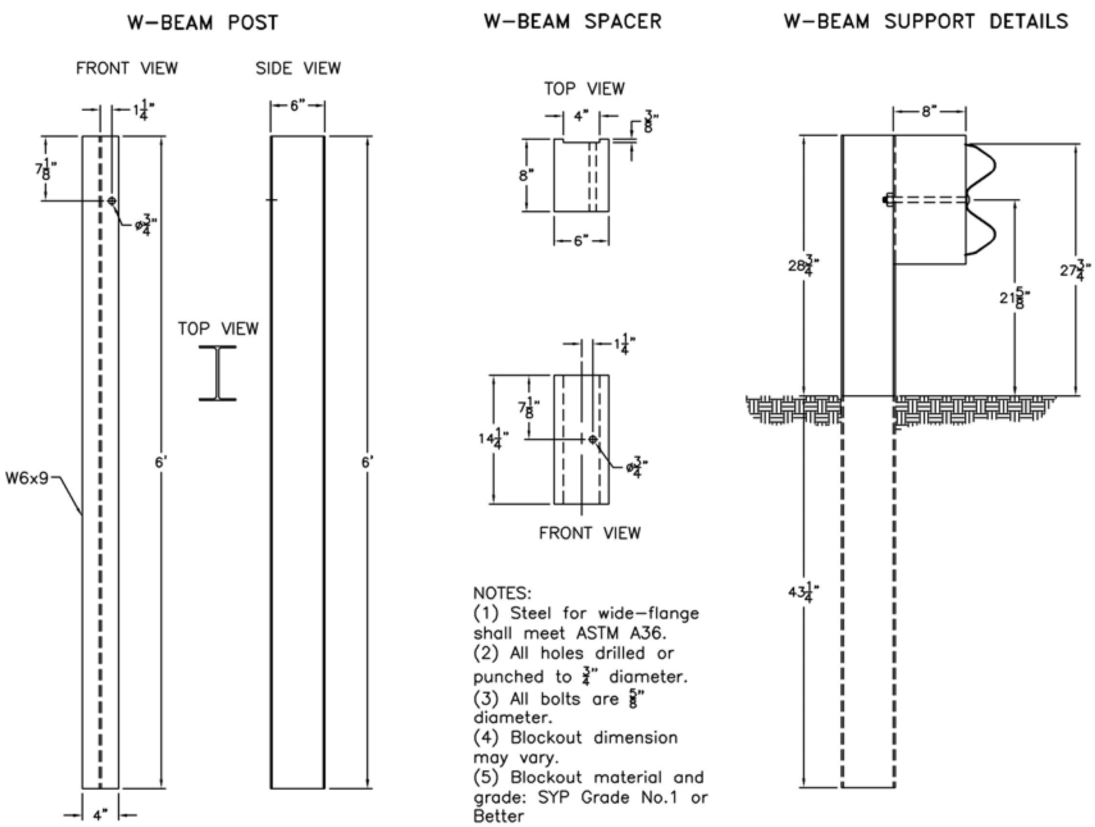


Figure A-2. Standard Height, Strong Post, Wood Blockout W-beam Guardrail Rail Details (English)

ITEM	QTY	DESCRIPTION	MATERIAL
a1	25	Steel Posts	W6x9 (W152x13.4)
a2	25	Blockout 6x8x14½"	XXX



Midwest Roadside Safety Facility

NCHRP 22-14(2)
Standard W-Beam
with Dodge Quadcab

Post Detail

Sheet: 3 of 6
Date: 8/24/2006
By: GEP
Drawing Name: 2214WB-2 R6.dwg
Scale: 1=16
Rev: KAP/RKF

Figure A-3. Standard Height, Strong Post, Wood Blockout W-beam Guardrail Post Details (English)

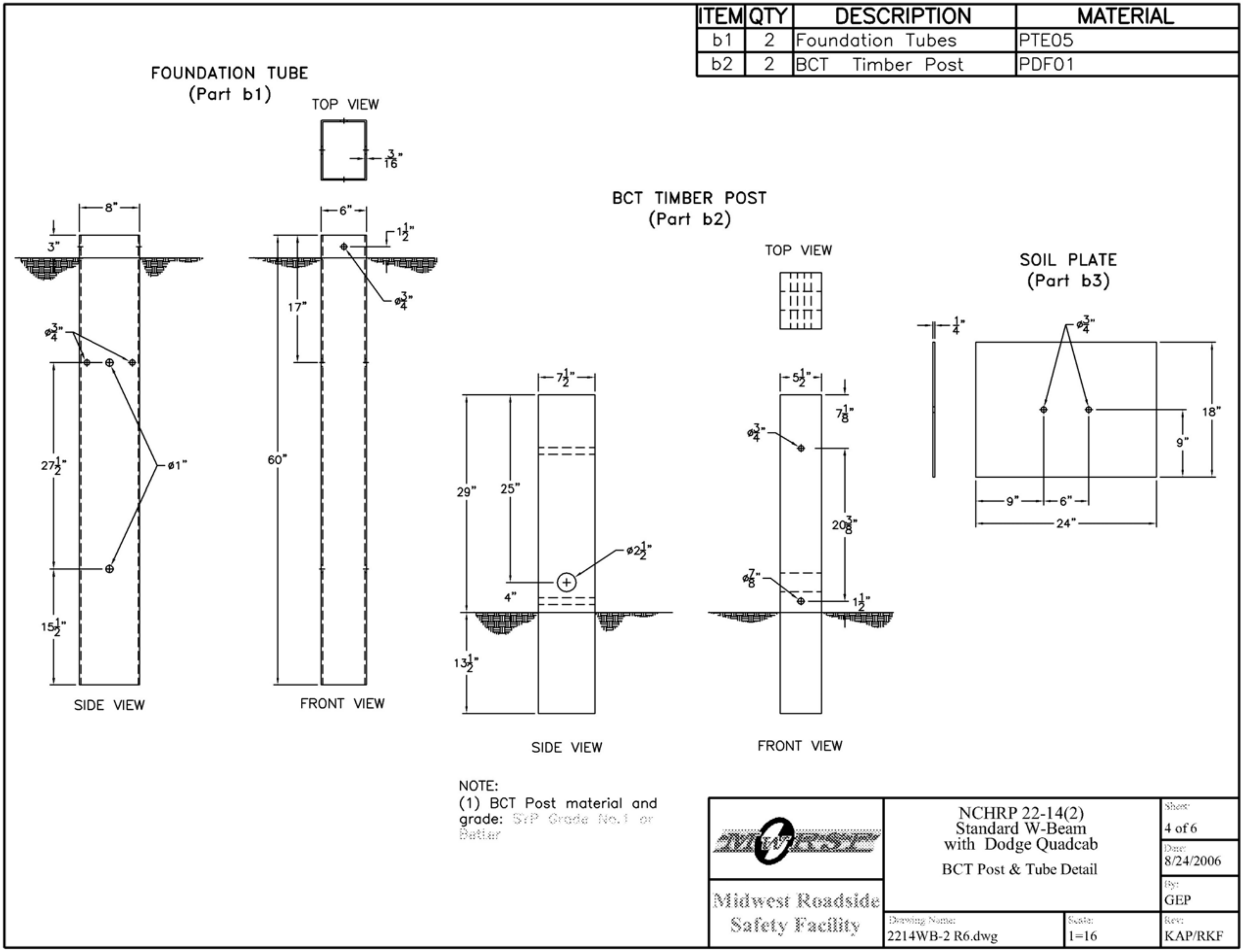


Figure A-4. Standard Height, Strong Post, Wood Blockout W-beam Guardrail Design Anchorage Details (English)

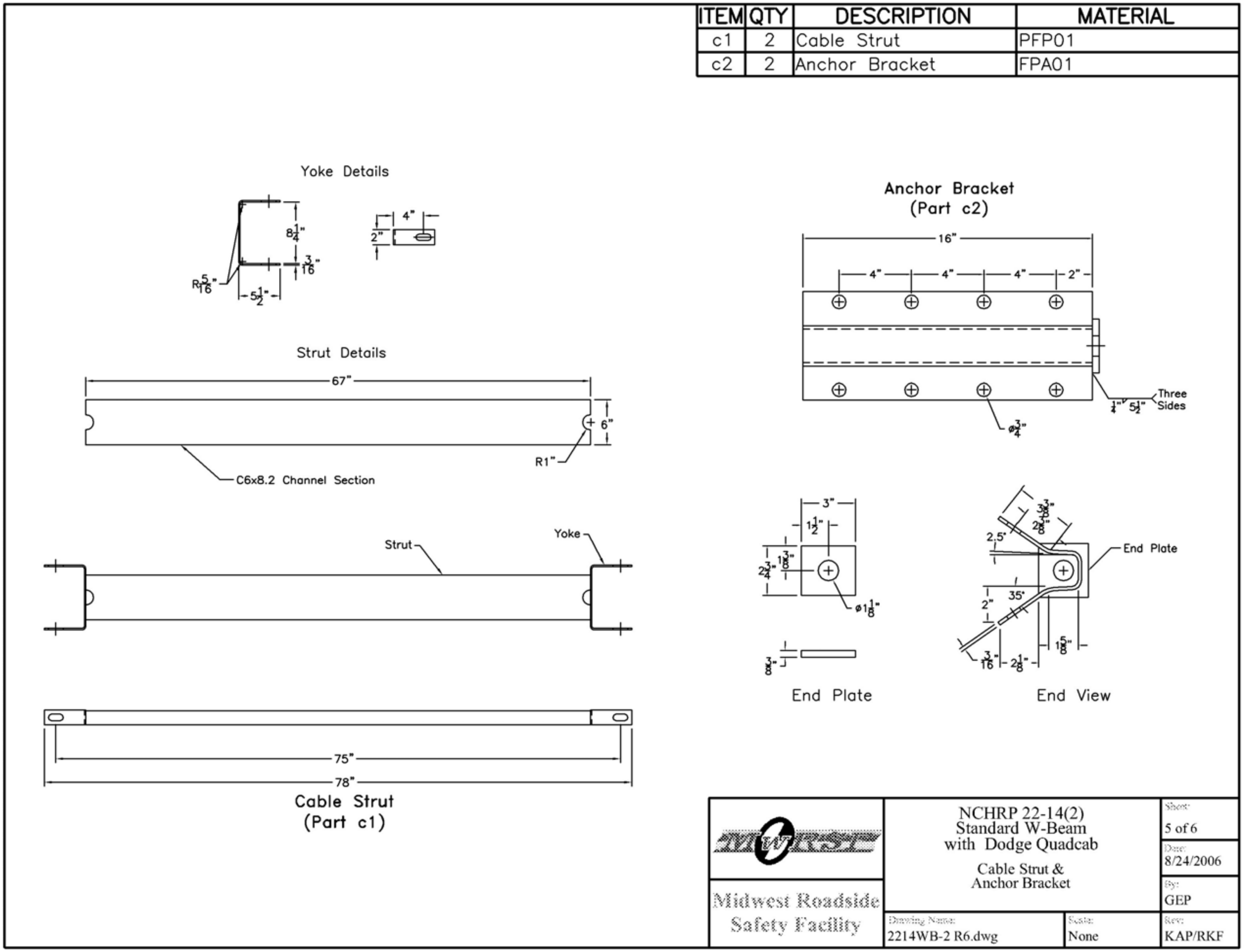


Figure A-5. Standard Height, Strong Post, Wood Blockout W-beam Guardrail Design Anchorage Details (English)

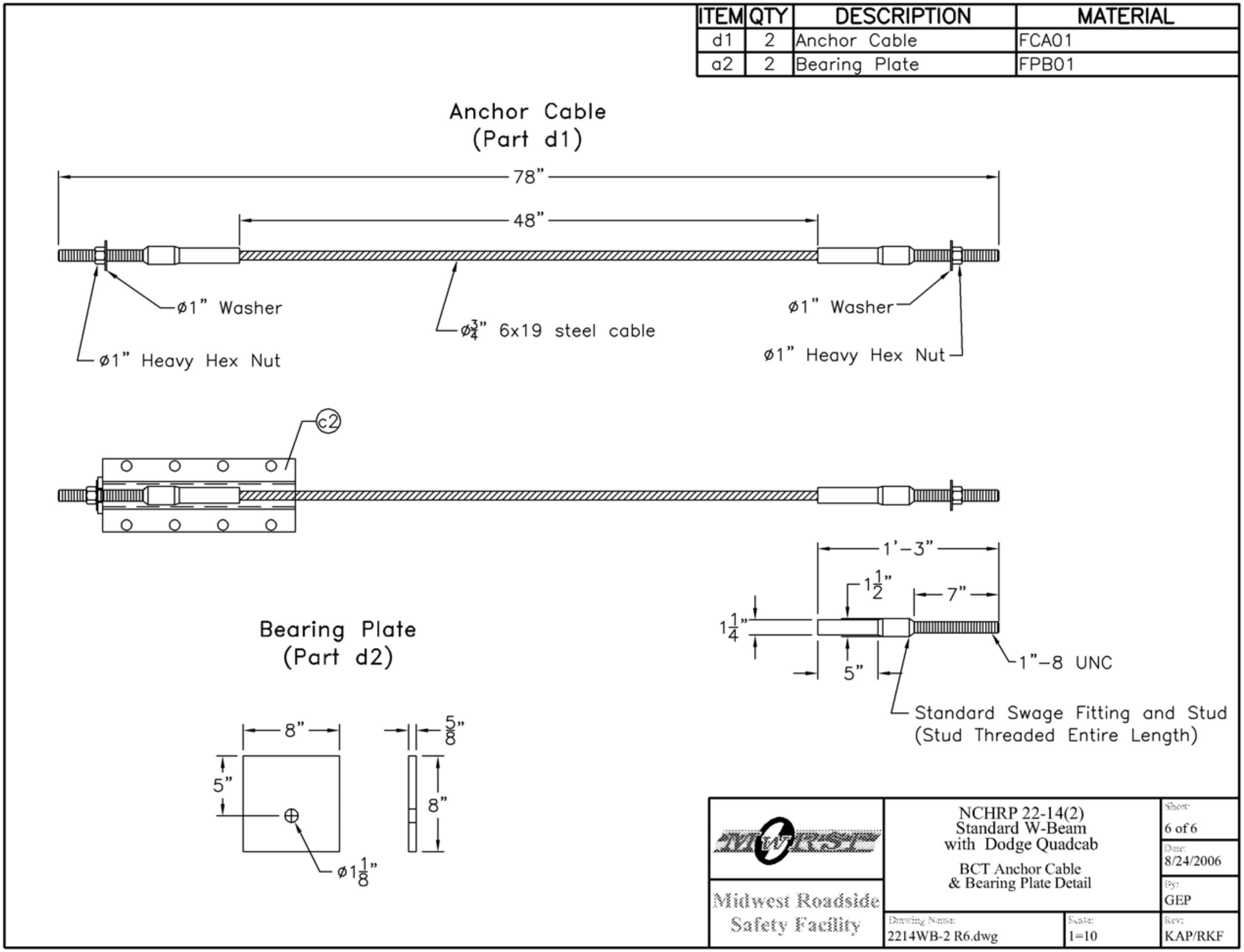


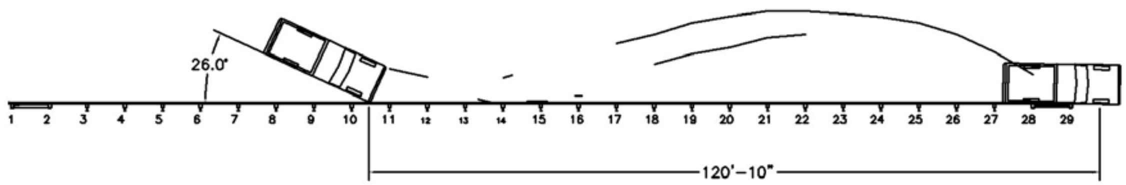
Figure A-6. Standard Height, Strong Post, Wood Blockout W-beam Guardrail Design Anchorage Details (English)

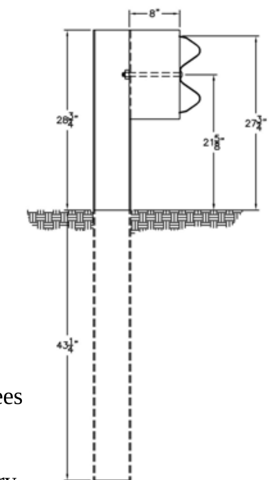
APPENDIX B

Test Summary Sheet in English Units

Figure B-1. Summary of Test Results and Sequential Photographs (English), Test 2214WB-2

0.000 sec | 0.136 sec | 0.292 sec | 0.416 sec | 0.828 sec





- Test Agency . . . . MwRSF
- Test Number 2214WB-2
- Date 4/8/05
- NCHRP 350 Update Test Designation . . 3-11
- Appurtenance . . . . Modified G4(1S) Guardrail
- Total Length . . . . 175 ft
- Key Elements - Steel W-Beam
  - Thickness . . . . 12 gauge
  - Top Mounting Height . . . . 27.75 in.
- Key Elements - Steel Posts
  - Post Nos. 3 - 27 . . . . W6x9 by 6 ft long
  - Spacing . . . . 75 in.
- Key Elements - Wood Posts
  - Post Nos. 1 - 2, 28 - 29 (BCT) . . . . 5.5 in. x 7.5 in. by 42.5 in. long
- Key Elements - Steel Foundation Tube . 5-ft long with soil plate
- Key Elements - Wood Spacer Blocks
  - Post Nos. 3 - 27 . . . . 6 in. x 8 in. by 14.25 in. long
- Type of Soil . . . . Grading B - AASHTO M 147-65 (1990)
- Test Vehicle
  - Type/Designation 2270P
  - Make and Model . . . . 2002 Dodge Ram 1500 Quad Cab Pickup
  - Curb . . . . 5,118 lbs
  - Test Inertial . . . . 5,000 lbs
  - Gross Static . . . . 5,000 lbs
- Impact Conditions
  - Speed . . . . 62.4 mph
  - Angle . . . . 25.8 degrees
  - Impact Location . . . . 37 in. upstream centerline post no. 11
- Exit Conditions
  - Speed . . . . 31.2 mph
  - Angle . . . . 20.7 degrees
  - Exit Box Criterion . . . . Pass
- Post-Impact Trajectory
  - Vehicle Stability . . . . Satisfactory
  - Stopping Distance . . . . 120 ft - 10.5 in. downstream Against traffic-side face
- Occupant Impact Velocity (350 Update)
  - Longitudinal . . . . 17.66 ft/s < 39.4 ft/s
  - Lateral . . . . 13.10 ft/s < 39.4 ft/s
- Occupant Ridedown Deceleration (350 Update)
  - Longitudinal . . . . -6.92 Gs < 20 Gs
  - Lateral . . . . 6.61 Gs < 20 Gs
- THIV (not required) . . . . 22.67 ft/s
- PHD (not required) . . . . 8.19 Gs
- Test Article Damage . . . . Moderate
- Test Article Deflections
  - Permanent Set . . . . 33.25 in.
  - Dynamic . . . . 47.0 in.
  - Working Width . . . . 54.9 in.
- Vehicle Damage . . . . Moderate
  - VDS[5] 1-RFQ-4
  - CDC[6] 1-RFEN3
  - Maximum Deformation . . . . 0.5 in. at front floorpan

Figure B-1. Summary of Test Results and Sequential Photographs (English), Test 2214WB-2

APPENDIX C

Occupant Compartment Deformation Data, Test 2214WB-2

VEHICLE PRE/POST CRUSH INFO
Set-1

TEST: 2214WB-2
VEHICLE: 02 Dodge Ram 1500 Quad Cab 4x2

Note: If impact is on driver side need to enter negative number for Y

POINT	X	Y	Z	X'	Y'	Z'	DEL X	DEL Y	DEL Z
1	54.75	8.25	1	54.5	8.25	1	-0.25	0	0
2	55.25	12.25	2.5	55	12	2.5	-0.25	-0.25	0
3	56.5	16.25	5.25	56.25	16.25	5	-0.25	0	-0.25
4	57.5	21.25	7.5	57.5	20.75	7.5	0	-0.5	0
5	60.75	27.5	7.5	60.75	27.5	7.5	0	0	0
6	46	2.25	2.5	45.75	2.25	2.5	-0.25	0	0
7	48.75	8.25	3.25	49	8.25	3	0.25	0	-0.25
8	50	12	6.75	50	11.75	6.5	0	-0.25	-0.25
9	51.25	16	9.5	51.25	15.75	9.5	0	-0.25	0
10	51.25	21	9.75	51.25	21	9.75	0	0	0
11	54	27.75	9.5	54.25	28	9.5	0.25	0.25	0
12	41	2.5	3	41	2.5	3	0	0	0
13	44.5	9	5.75	44.5	9	5.75	0	0	0
14	54.75	14.25	9.5	45.5	14.25	9.5	-9.25	0	0
15	46	22.25	9.5	45.75	22.25	9.25	-0.25	0	-0.25
16	48.5	28.25	9.25	48.75	28.75	9.25	0.25	0.5	0
17	35	3	3.25	34.5	3	3.25	-0.5	0	0
18	37.75	9.5	7	38	9.25	6.75	0.25	-0.25	-0.25
19	38.25	15	8.75	38.25	14.5	9	0	-0.5	0.25
20	38.75	22	8.75	38.75	21.75	9	0	-0.25	0.25
21	42	28.5	8.75	42	28.25	8.75	0	-0.25	0
22	30.75	3	2.5	30.5	3	2.5	-0.25	0	0
23	32.75	11.5	5	33	11.5	5	0.25	0	0
24	33	20.75	4.5	33.25	20.75	4.75	0.25	0	0.25
25	36.25	27	4.25	36.25	27	4.5	0	0	0.25
26	22.25	4	3	22	4	3	-0.25	0	0
27	25	17	7.25	25	16.75	7.5	0	-0.25	0.25
28	27	27.75	7.25	27	27.5	7.25	0	-0.25	0
29									
30									

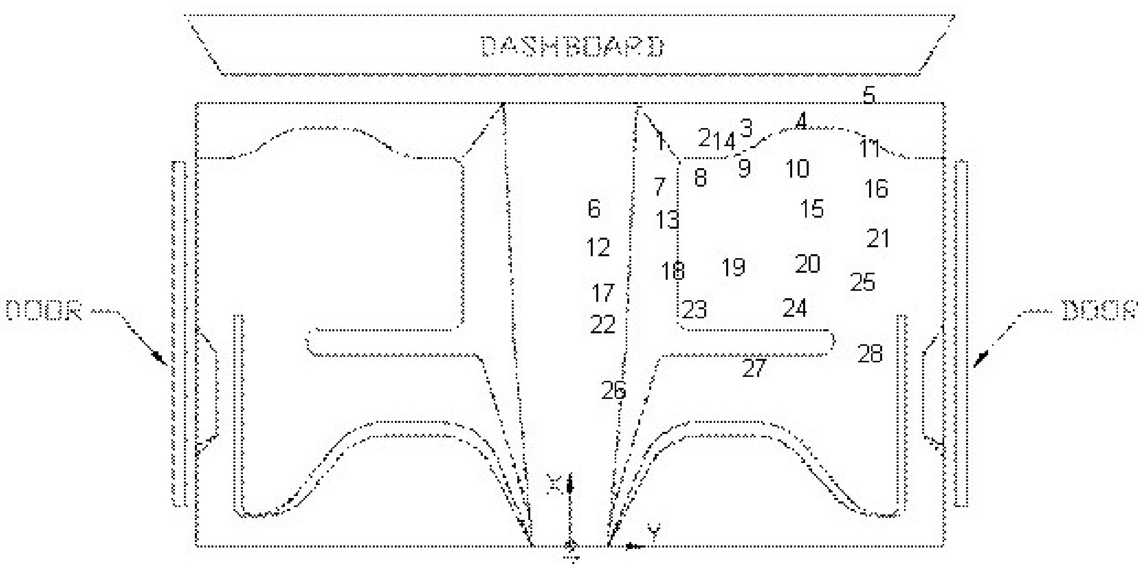


Figure C-1. Occupant Compartment Deformation Data - Set 1, Test 2214WB-2

VEHICLE PRE/POST CRUSH INFO
Set-2

TEST: 2214WB-2
VEHICLE: 02 Dodge Ram 1500 Quad Cab 4x2

Note: If impact is on driver side need to enter negative number for Y

POINT	X	Y	Z	X'	Y'	Z'	DEL X	DEL Y	DEL Z
1	43.5	11.75	1	43.5	11.75	1	0	0	0
2	44.25	15.75	2.5	44.25	15.5	2.5	0	-0.25	0
3	45.5	19.75	5.25	45.5	19.75	5.25	0	0	0
4	47	24.75	7.75	47	24.25	7.5	0	-0.5	-0.25
5	47	31	7.5	47	31	7.5	0	0	0
6	37	5.75	2.5	37	5.75	2.5	0	0	0
7	38	11.75	3.25	38	11.75	3.25	0	0	0
8	39.5	15.5	6.75	39.5	15.25	6.75	0	-0.25	0
9	41	19.5	9.75	41	19.25	9.75	0	-0.25	0
10	41	24.5	10	41	24.5	9.75	0	0	-0.25
11	41	31.25	9.75	41	31.5	9.75	0	0.25	0
12	32.5	6	3	32.25	6	3	-0.25	0	0
13	34	12.5	6	34	12.5	5.75	0	0	-0.25
14	36	17.75	9.75	35.75	17.75	9.75	-0.25	0	0
15	36	25.75	9.5	36	25.75	9.5	0	0	0
16	36	31.75	9.5	36	32.25	9.25	0	0.5	-0.25
17	26.25	6.5	3.25	26.25	6.5	3.25	0	0	0
18	27.75	13	7	27.75	12.75	7	0	-0.25	0
19	27.75	18.5	9	27.75	18	9	0	-0.5	0
20	28.5	25.5	9	28.5	25.25	9	0	-0.25	0
21	28.5	32	9	28.5	31.75	9	0	-0.25	0
22	22	6.5	2.25	22	6.5	2.5	0	0	0.25
23	22.5	15	5	22.75	15	5	0.25	0	0
24	22.75	24.25	4.75	23	24.25	4.75	0.25	0	0
25	23	30.5	4.5	23	30.5	4.5	0	0	0
26	14	7.5	3	14	7.5	3	0	0	0
27	16.25	20.5	7.5	16.25	20.25	7.5	0	-0.25	0
28	16	31.25	7.5	16	31	7.5	0	-0.25	0
29									
30									

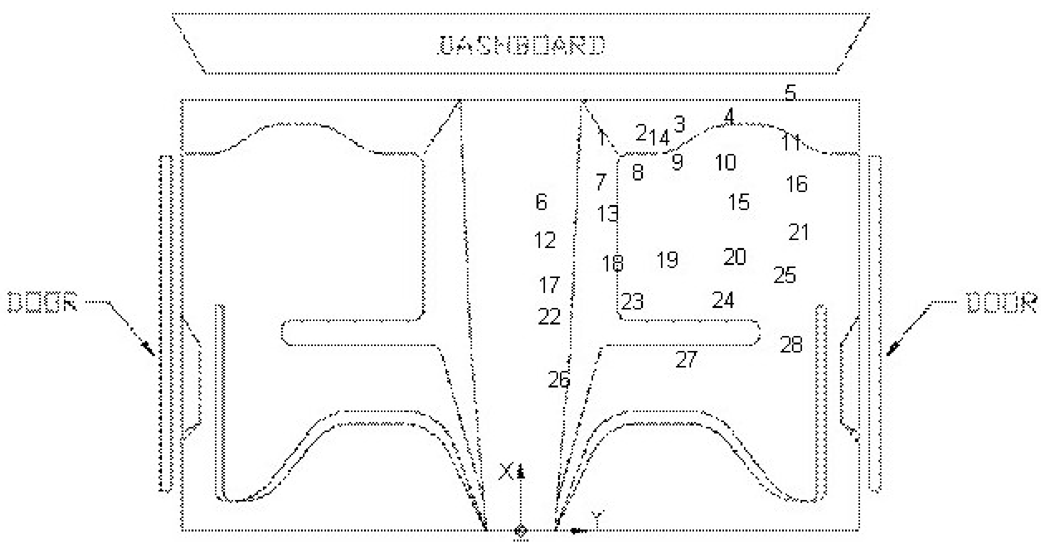


Figure C-2. Occupant Compartment Deformation Data - Set 2, Test 2214WB-2

Occupant Compartment Deformation Index (OCDI)

Test No. 2214WB-2
Vehicle Type: 02 Dodge Ram 1500 Quad Cab 4X2

OCDI = XXABCDEFGHI

XX = location of occupant compartment deformation

A = distance between the dashboard and a reference point at the rear of the occupant compartment, such as the top of the rear seat or the rear of the cab on a pickup

B = distance between the roof and the floor panel

C = distance between a reference point at the rear of the occupant compartment and the motor panel

D = distance between the lower dashboard and the floor panel

E = interior width

F = distance between the lower edge of right window and the upper edge of left window

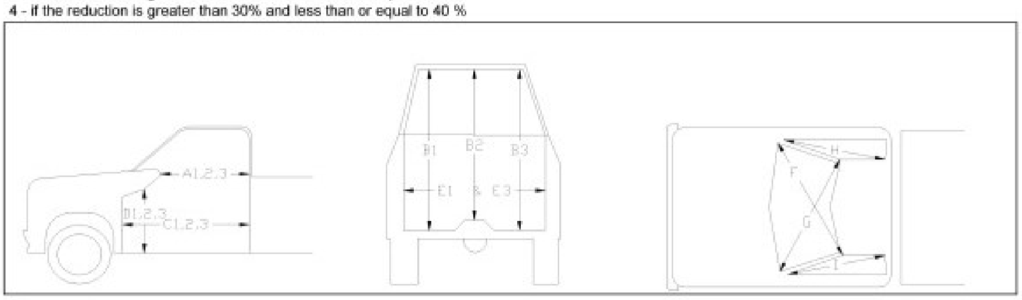
G = distance between the lower edge of left window and the upper edge of right window

H= distance between bottom front corner and top rear corner of the passenger side window

I= distance between bottom front corner and top rear corner of the driver side window

Severity Indices

0 - if the reduction is less than 3%
1 - if the reduction is greater than 3% and less than or equal to 10 %
2 - if the reduction is greater than 10% and less than or equal to 20 %
3 - if the reduction is greater than 20% and less than or equal to 30 %
4 - if the reduction is greater than 30% and less than or equal to 40 %



where,
1 = Passenger Side
2 = Middle
3 = Driver Side

Location:

Measurement	Pre-Test (in.)	Post-Test (in.)	Change (in.)	% Difference	Severity Index
A1	68.75	68.75	0.00	0.00	0
A2	69.75	69.75	0.00	0.00	0
A3	71.00	71.00	0.00	0.00	0
B1	45.50	45.50	0.00	0.00	0
B2	42.00	42.00	0.00	0.00	0
B3	47.25	47.25	0.00	0.00	0
C1	63.25	63.25	0.00	0.00	0
C2	46.25	46.25	0.00	0.00	0
C3	63.75	63.50	-0.25	-0.39	0
D1	18.25	18.25	0.00	0.00	0
D2	7.00	7.00	0.00	0.00	0
D3	14.75	14.75	0.00	0.00	0
E1	66.25	66.00	-0.25	-0.38	0
E3	64.75	64.75	0.00	0.00	0
F	59.25	59.25	0.00	0.00	0
G	59.25	59.25	0.00	0.00	0
H	36.50	36.25	-0.25	-0.68	0
I	37.25	37.25	0.00	0.00	0

Note: Maximum sevrity index for each variable (A-I) is used for determination of final OCDI value

	XX	A	B	C	D	E	F	G	H	I
Final OCDI:	RF	0	0	0	0	0	0	0	0	0

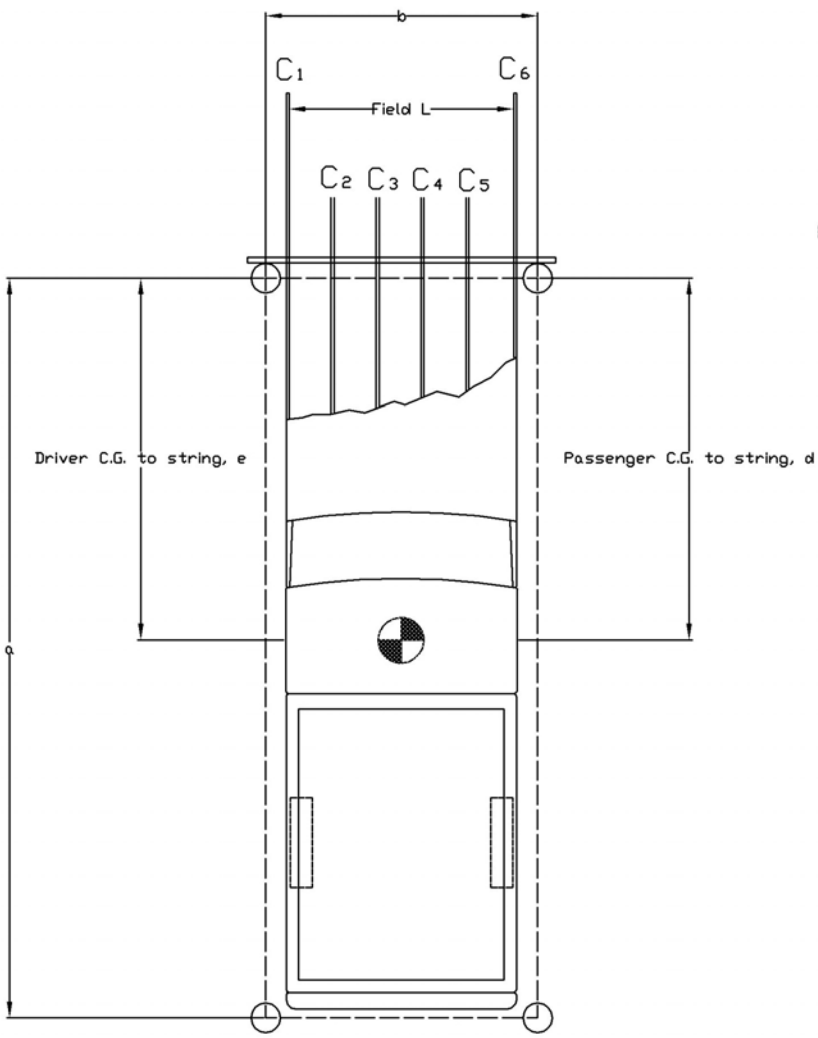
Figure C-3. Occupant Compartment Deformation Index (OCDI), Test 2214WB-2

Date: 5/26/05 Test Number: 2214WB-2 Model: Ram 1500 Quad Cab 4x2

Make: Dodge Vehicle I.D.#: 1D7HA18Z925520817

Tire Size: 265/70 R17 Year: 2002 Odometer: 97127

*(All Measurements Refer to Impacting Side) Vehicle Geometry -- mm (in.)



a 6160 (242.5)

b 2283 (89.875)

Field L 1708 (67.25)

Bumper Height 495 (19.5)

d 3016 (118.75)

e 3004 (118.25)

C_1 886 (34.875)

C_2 524 (20.625)

C_3 464 (18.25)

C_4 451 (17.75)

C_5 540 (21.25)

C_6 1022 (40.25)

Figure C-4. NASS Crush Data, Test 2214WB-2

APPENDIX D

Accelerometer and Rate Transducer Data Analysis, Test 2214WB-2

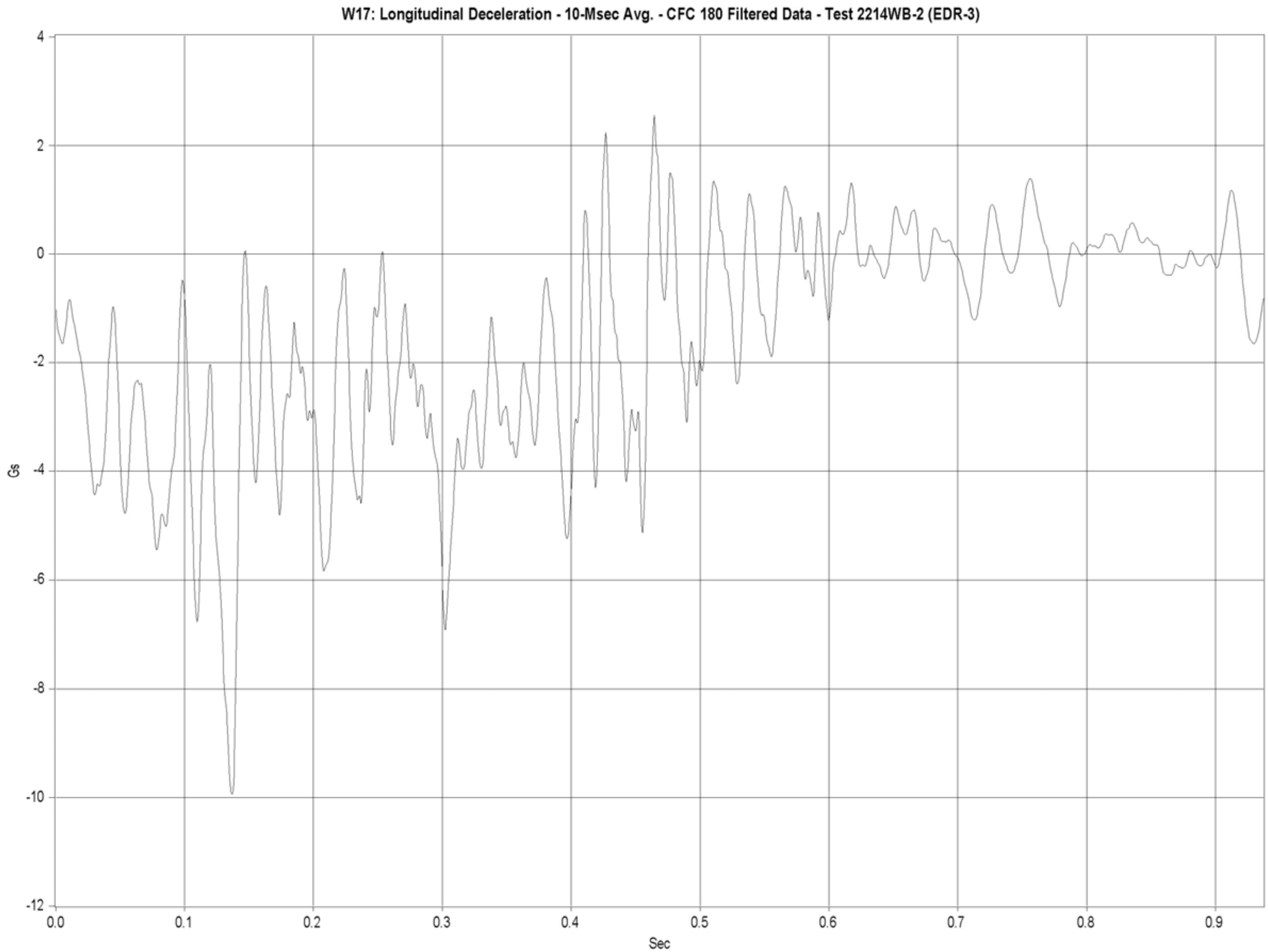


Figure D-1. Graph of Longitudinal Deceleration, Test 2214WB-2

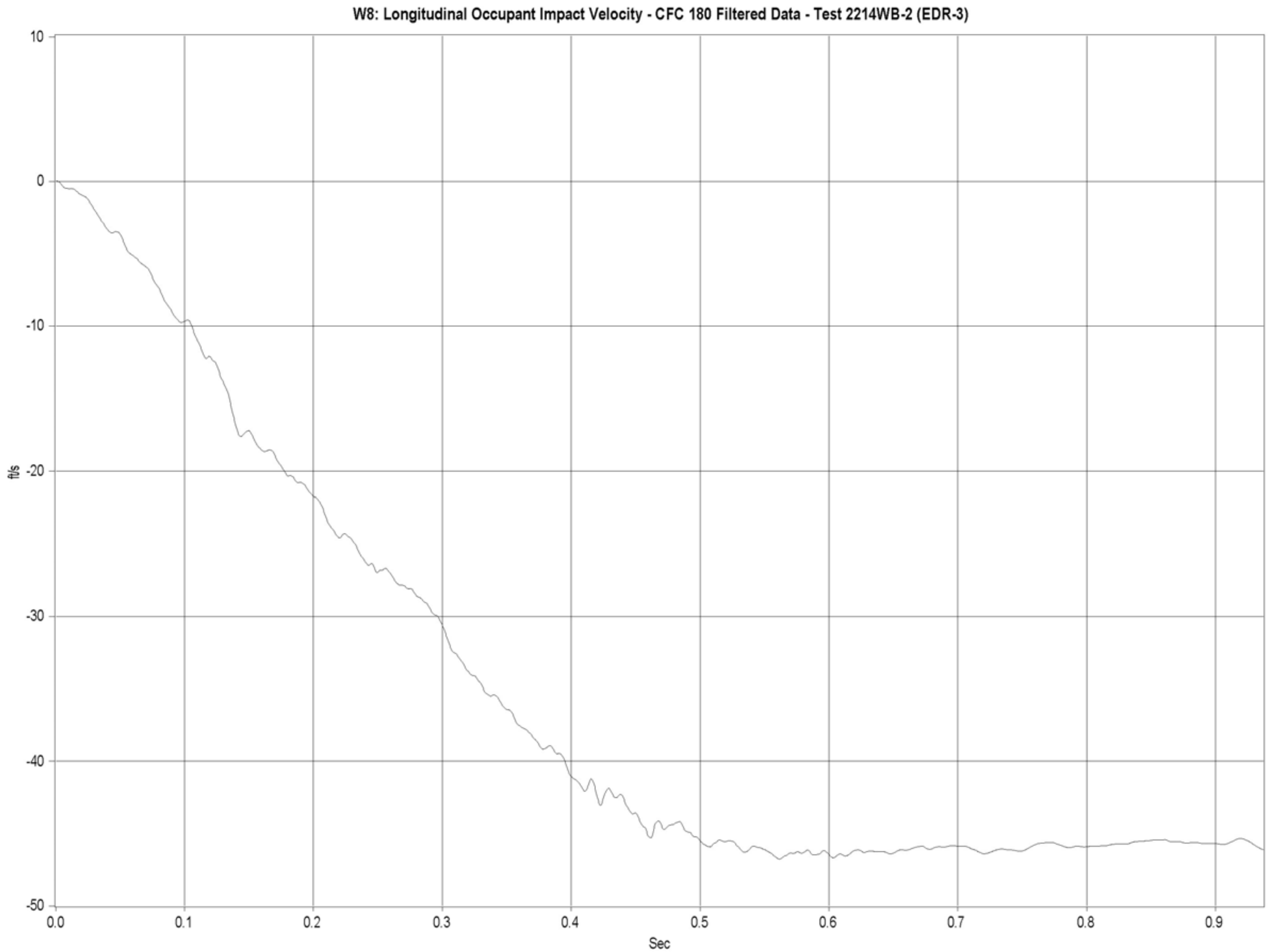


Figure D-2. Graph of Longitudinal Occupant Impact Velocity, Test 2214WB-2

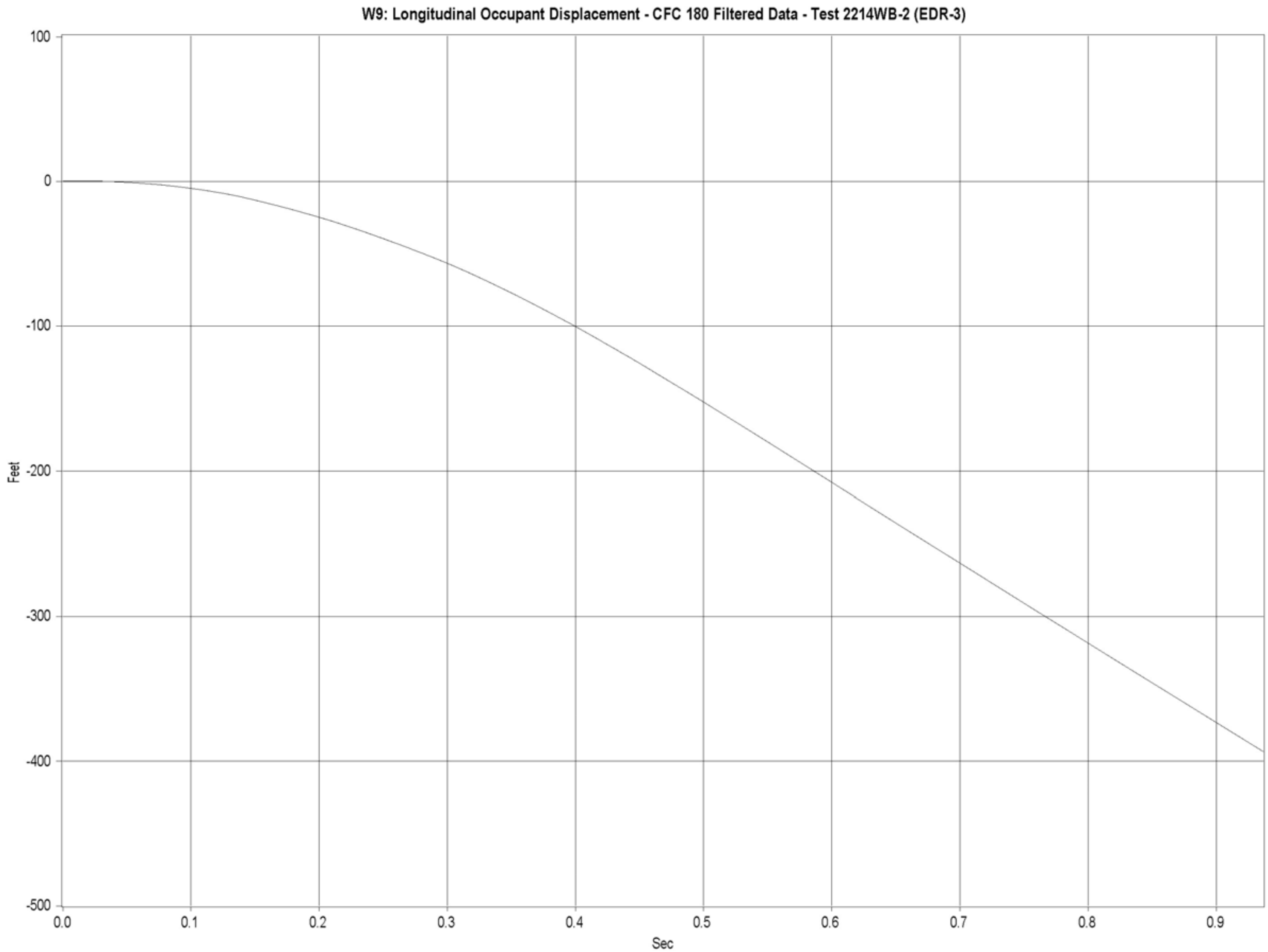


Figure D-3. Graph of Longitudinal Occupant Displacement, Test 2214WB-2

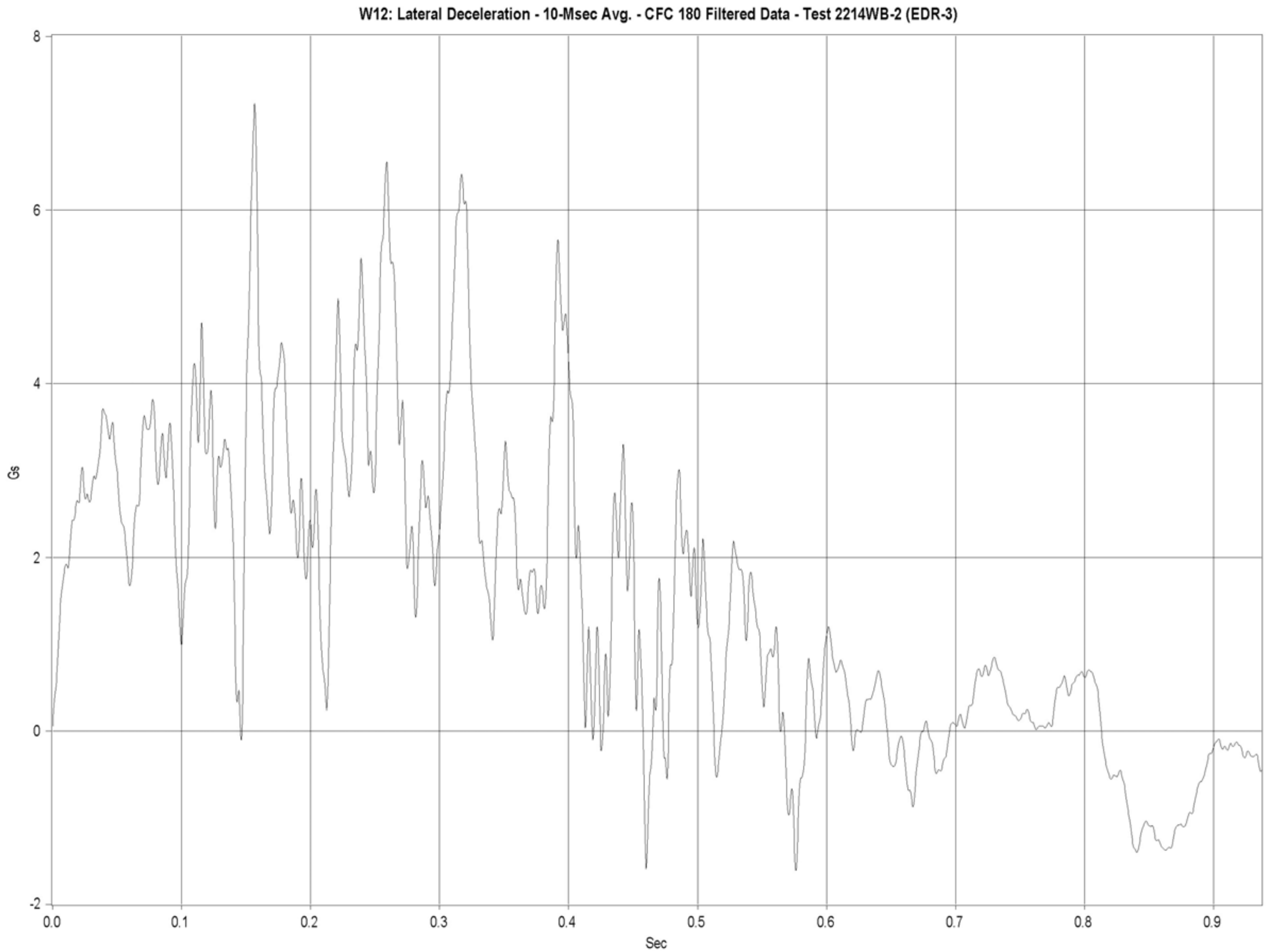


Figure D-4. Graph of Lateral Deceleration, Test 2214WB-2

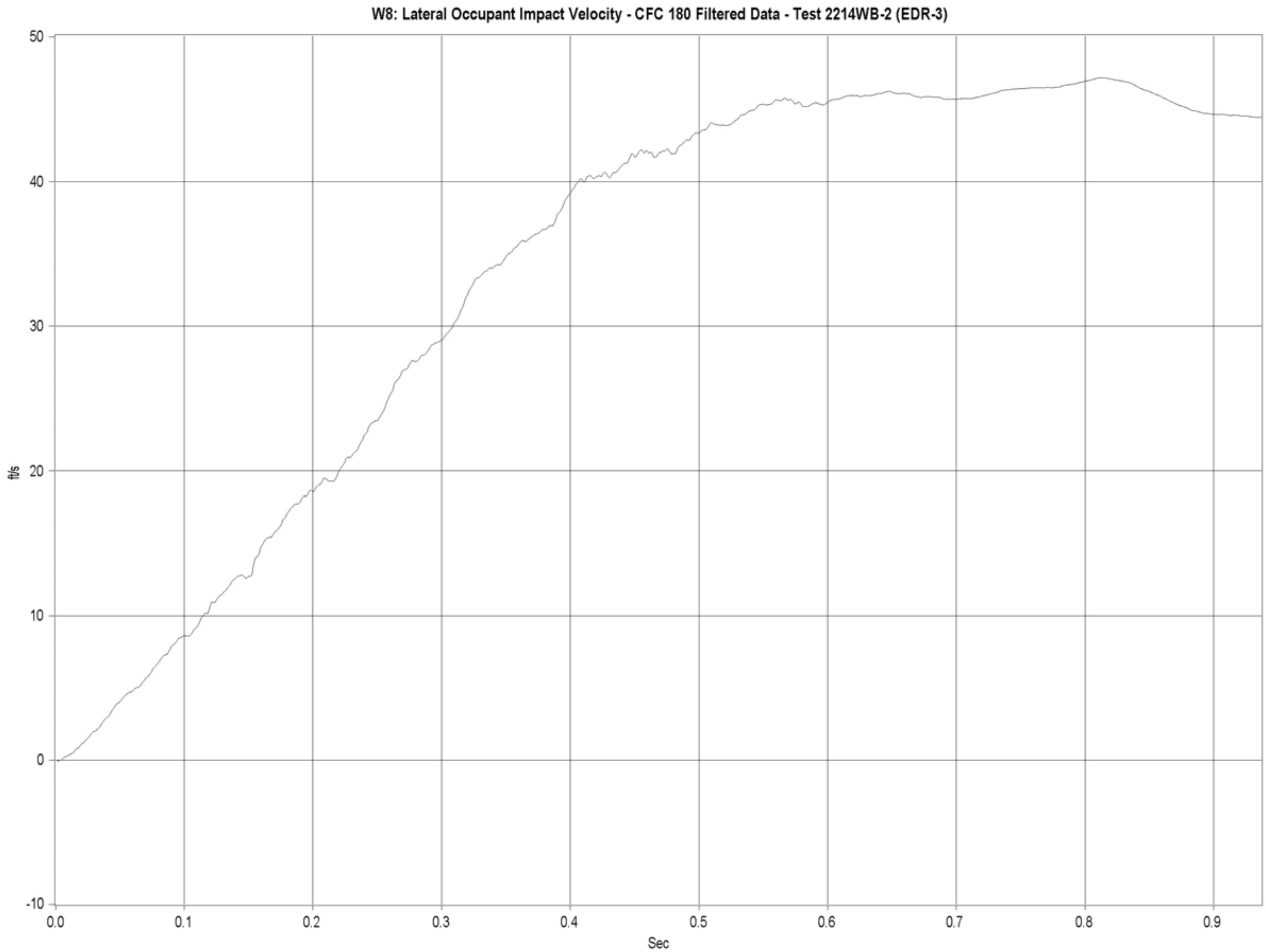


Figure D-5. Graph of Lateral Occupant Impact Velocity, Test 2214WB-2

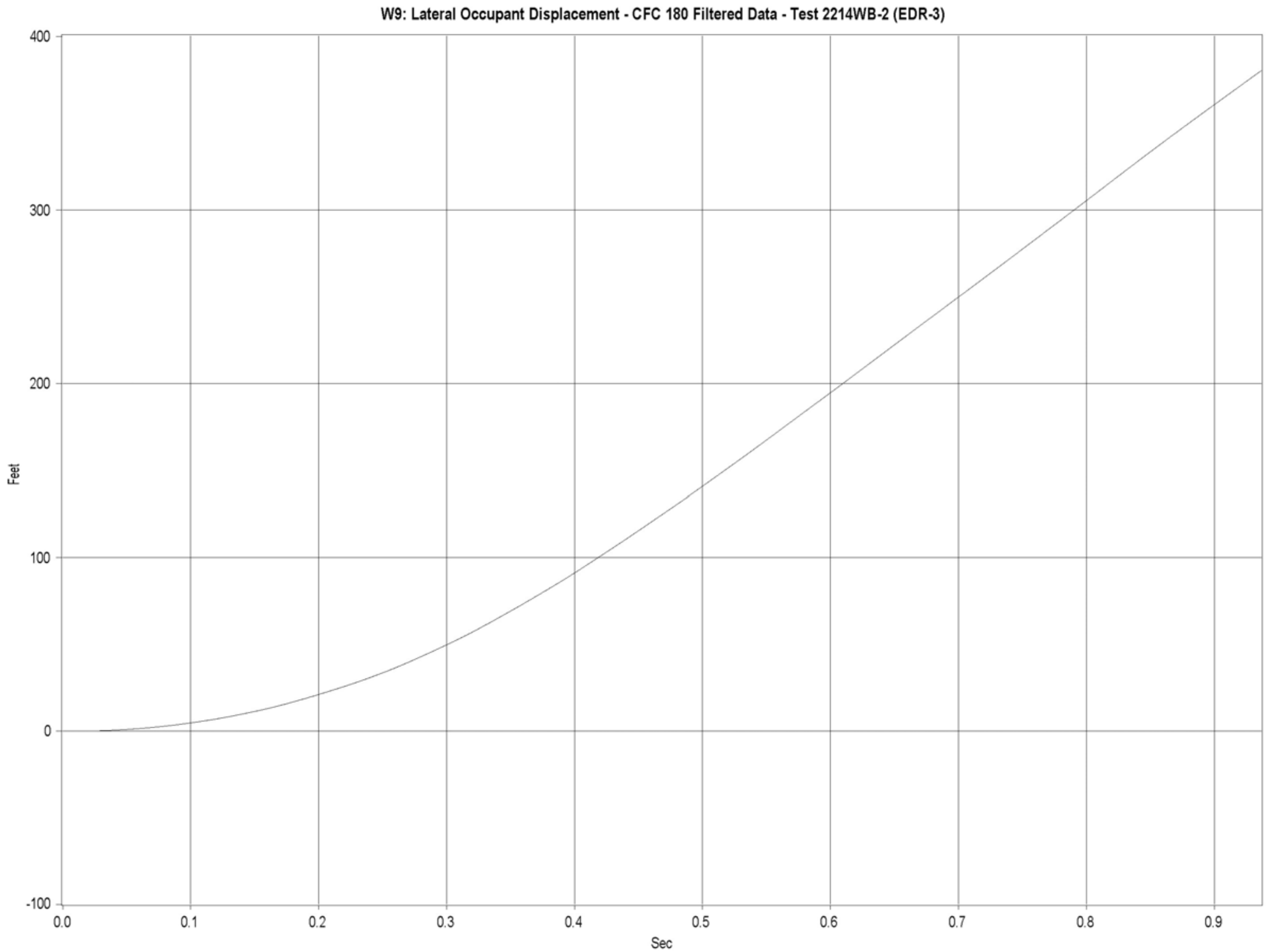


Figure D-6. Graph of Lateral Occupant Displacement, Test 2214WB-2

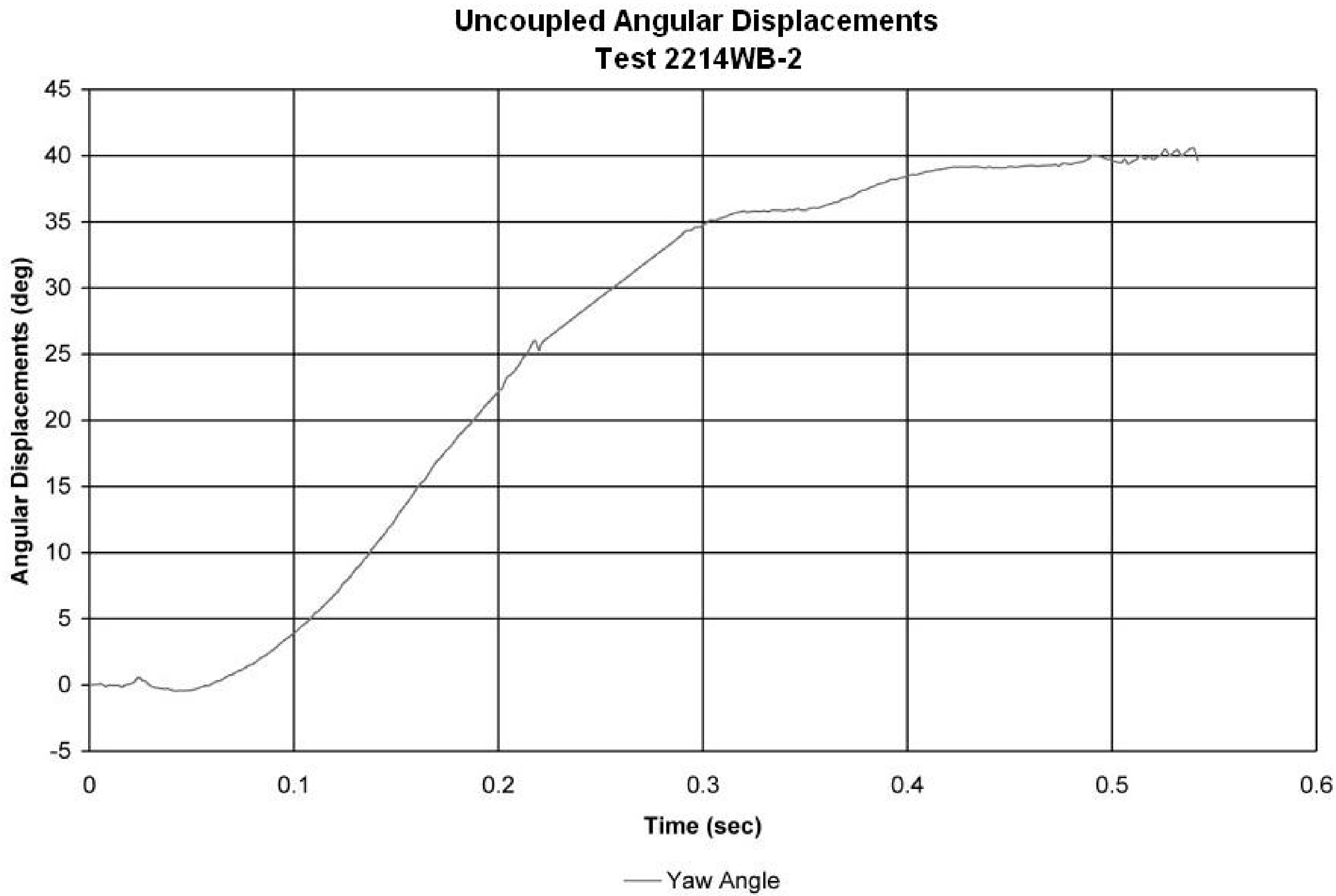


Figure D-7. Graph of Yaw Angular Displacements, Test 2214WB-2