TTI: 9-1002-12



# MASH TL-3 TESTING AND EVALUATION OF THE TXDOT T131RC BRIDGE RAIL TRANSITION



Crash testing performed at: TTI Proving Ground 3100 SH 47, Building 7091 Bryan, TX 77807

**Test Report 9-1002-12-4** 

**Cooperative Research Program** 

TEXAS A&M TRANSPORTATION INSTITUTE
THE TEXAS A&M UNIVERSITY SYSTEM
COLLEGE STATION, TEXAS

TEXAS DEPARTMENT OF TRANSPORTATION

in cooperation with the Federal Highway Administration and the Texas Department of Transportation http://tti.tamu.edu/documents/9-1002-12-4.pdf

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16. Abstract

This project designed and crash tested a transition design for the Texas Department of Transportation (TxDOT) T131RC Bridge Rail that would meet the strength and safety performance criteria for Test Level 3 of American Association of State Highway Official's (AASHTO) Manual for Assessing Safety Hardware (*MASH*).

The TxDOT T131RC Bridge Rail Transition contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic rail deflection was 7.4 inches. No detached elements, fragments, or other debris were present to penetrate or to show potential for penetrating the occupant compartment, or to present hazard to others. Maximum occupant compartment deformation was 2.5 inches in the left door at occupant hip height. The 1100C vehicle remained upright during and after the collision event. Occupant risk factors were within the limits specified in *MASH*. The 1100C crossed the exit box within the limits specified in *MASH*.

The TxDOT T131RC Bridge Rail Transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8.4 inches. No detached elements, fragments, or other debris were present to penetrate or to show potential for penetrating the occupant compartment, or to present hazard to others. Maximum occupant compartment deformation was 0.25 inch in the left door at occupant hip height. The 2270P vehicle remained upright during and after the collision event. Occupant risk factors were within the limits specified in *MASH*. The 22270P vehicle crossed the exit box within the limits specified in *MASH*. The TxDOT T131RC Bridge Rail Transition performed acceptably as a *MASH* TL-3 transition.

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### MASH TL-3 TESTING AND EVALUATION OF THE TXDOT T131RC BRIDGE RAIL TRANSITION

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#### **DISCLAIMER**

This research was performed in cooperation with the Texas Department of Transportation (TxDOT) and the Federal Highway Administration (FHWA). The contents of this report reflect the views of the authors, who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official view or policies of the FHWA or TxDOT. This report does not constitute a standard, specification, or regulation, and its contents are not intended for construction, bidding, or permit purposes. In addition, the above listed agencies assume no liability for its contents or use thereof. The United States Government and the State of Texas do not endorse products or manufacturers. Trade or manufacturers' names appear herein solely because they are considered essential to the object of this report. The engineer in charge of the project was Roger P. Bligh, P.E. (Texas, #78550).

#### TTI PROVING GROUND DISCLAIMER

The results of the crash testing reported herein apply only to the article being tested.

ACCREDITED ISO 17025 Laboratory

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#### CHAPTER 1. INTRODUCTION

#### 1.1 INTRODUCTION

This project was set up to provide the Texas Department of Transportation (TxDOT) with a mechanism to quickly and effectively evaluate high-priority issues related to roadside safety devices. Roadside safety devices shield motorists from roadside hazards such as non-traversable terrain and fixed objects. To maintain the desired level of safety for the motoring public, these safety devices must be designed to accommodate a variety of site conditions, placement locations, and a changing vehicle fleet. Periodically, there is a need to assess the compliance of existing safety devices with current vehicle testing criteria and develop new devices that address identified needs.

Under this project, roadside safety issues are identified and prioritized for investigation. Each roadside safety issue is addressed with a separate work plan, and the results are summarized in individual test reports.

#### 1.2 BACKGROUND

The TxDOT Type T101RC Bridge Rail has been widely used as a retrofit for obsolete bridge rails mounted on a deck curb. The T101RC was 27 inches in height and anchored to the curb using four adhesive anchors. The height of the posts and the number of bridge rail elements varied depending on the height of the concrete curb. Based on unsatisfactory crash test performance of rail designs of similar height, TxDOT decided to develop a new retrofit bridge rail system that meets the American Association of State Highway and Transportation Officials (AASHTO) *Manual for Assessing Safety Hardware (MASH)* (1). This new bridge rail system, known as the TxDOT T131RC Bridge Rail, was successfully crash tested in according with *MASH* Test Level 3 (TL-3) and was recommended for implementation on new or retrofit railing applications (2). The implementation of this new bridge rail created a need to develop a transition from standard guardrail to the TxDOT T131RC Bridge Rail.

#### 1.3 OBJECTIVES/SCOPE OF RESEARCH

This project developed a transition for connecting a 31-inch tall W-beam guardrail to the TxDOT T131RC Bridge Rail. The transition was required to meet the impact performance criteria for *MASH* TL-3

#### **CHAPTER 2. SYSTEM DETAILS**

#### 2.1 TEST ARTICLE DESIGN AND CONSTRUCTION

The TxDOT T131RC Bridge Rail Transition consists of a two nested 12 gage thrie beam sections supported by six W6×8.5 posts spaced at 37½ inches on centers. The nested thrie beams connect to a 10 gage asymmetric transition piece on the upstream end. This asymmetric transition section was connected to approximately 56 ft-3 inches of W-beam guardrail with an ET anchor terminal. The nested thrie beam transition was connected to a 10 gage end shoe on the downstream end. This end shoe was anchored to the end of the T131RC Bridge Rail. The overall length of the test installation was approximately 79 ft-6¾ inches.

The height to the top of the W-beam guardrail and transition was 31 inches above finished grade. The end shoe rail of the nested thrie beam sections were attached to the traffic face of the  $HSS6\times6\times1/4$  tubes used for the T131RC Bridge Rail. Two steel fill blocks were located between the  $HSS6\times6\times1/4$  tubes and were attached to the T131RC Bridge Rail tubes using two  $^3$ /4-inch diameter  $\times$  20 inches long bolts. These fill blocks were mounted flush to the  $HSS6\times6\times1/4$  tubes in the bridge rail. The fill blocks were fabricated using  $HSS6\times6\times1/4$  tubes and were tapered on the exposed end in the installation. The thrie beam transition end shoe was attached to the end of the T131RC Bridge Rail using three 78-inch diameter A325 bolts. The thrie beam end shoe was anchored to the end of the rail and fill blocks near the  $W6\times15$  anchor post in the concrete curb. This anchor post was anchored within a 12-inch diameter by 30-inch deep concrete footing. This post and footing was constructed within an 80-inch long concrete curb constructed on the end of the T131RC Bridge Rail test installation.

Texas A&M Transportation Institute (TTI) Proving Ground personnel constructed 80 inches of concrete curb for this project. This concrete curb was 12 inches wide and 11 inches high and closely matched the traffic side face of the concrete curb used for the T131RC Bridge Rail. The concrete curb extended approximately 62 inches from the end of the T131RC Bridge Rail curb and tapered 6 inches back from the traffic side over a distance of 18 inches. The width of the curb was 6 inches at the end. The curb was 11 inches in height above grade and 12 inches below grade. A W6×15 end anchor post was located 60 inches from the centerline of the last T131RC Bridge Rail post located on the bridge rail test installation. This anchor post was cast within a 12-inch diameter by 30-inch deep unreinforced concrete footing. This footing was cast monolithically with the concrete curb. The concrete transition curb was not anchored to the concrete curb or deck for the T131RC Bridge Rail installation. Reinforcement in the concrete curb and footing consisted of #3 "U" shaped stirrups spaced approximately 10 inches on centers. Six #3 longitudinal bars were located within these stirrups. Concrete for the concrete curb and footing was specified to be 3600 psi.

Figure 2.1 gives overall details of the TxDOT T131RC Bridge Rail Transition, and a complete set of drawings can be found in Appendix A. Figure 2.2 shows photographs of the completed installation prior to testing.

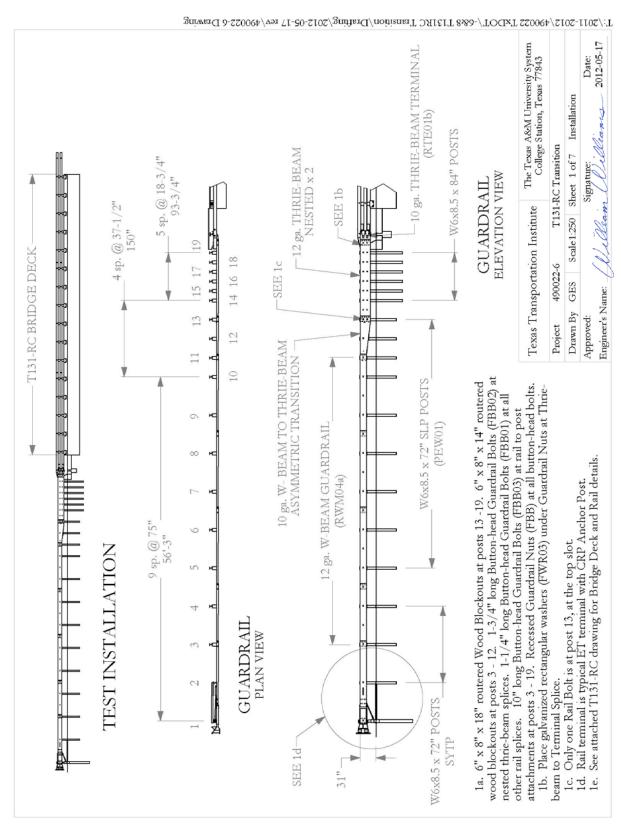


Figure 2.1. Details of the TxDOT T131RC Bridge Rail Transition Installation.







#### 2.2 MATERIAL SPECIFICATIONS

The fill blocks were fabricated using HSS6×6×¼ A500 Grade B material with welded A36 plate. All tubular rail elements were fabricated using HSS6×6×¼ A500 Grade B material. All reinforcing steel was specified to be ASTM A615 grade 60 material. All hex head bolts connecting the end shoe to the T131RC bridge rail were specified to be A325 structural bolts. All other bolts (button head bolts) used in the installation were A307 grade. Appendix B provides the material certification documents.

Concrete for the concrete curb and footing was specified to be 3600 psi. Compressive strength on the concrete used to construct the curb was measured at 4038 psi on the day of test no. 490022-6 (7 days of age). Compressive strength of the concrete on the day of test no. 490022-8 (11 days of age) was measured at 4436 psi.

#### 2.3 SOIL CONDITIONS

In accordance with Appendix B of *MASH*, soil strength was measured on the day of each crash test. During installation of the TxDOT T131RC Bridge Rail Transition, two standard W6×16 posts were installed in the immediate vicinity of the transition, utilizing the same fill materials and installation procedures followed for the guardrail system and used in the reference tests (see Appendix C, Figure C1).

As the reference tests in Appendix C, Figure C1 show, the minimum post loads required for deflections at 5 inches, 10 inches, and 15 inches, measured at a height of 25 inches, are 3940 lb, 5500 lb, and 6540 lb, respectively (90 percent of static load for the initial standard installation).

On the day of test 490022-6, May 25, 2012, load on the test post at deflections of 5 inches, 10 inches, and 15 inches was 8969 lbf, 9575 lbf, and 9181 lbf, respectively. The strength of the backfill material met minimum requirements (see Appendix C, Figure C2).

On the day of test 490022-8, June 29, 2012, load on the test post at deflections of 5 inches, 10 inches, and 15 inches was 7667 lbf, 7636 lbf, and 7333 lbf, respectively. The strength of the backfill material met minimum requirements.

### CHAPTER 3. TEST REQUIREMENTS AND EVALUATION CRITERIA

#### 3.1 CRASH TEST MATRIX

According to *MASH*, two tests are recommended to evaluate bridge rail transitions to test level three (TL-3).

**MASH** Test Designation 3-20: A 2425-lb vehicle impacting the critical impact point (CIP) of the transition at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect a small passenger vehicle.

**MASH** Test Designation 3-21: A 5000-lb pickup truck impacting the CIP of the transition at a nominal impact speed and angle of 62 mi/h and 25 degrees, respectively. This test investigates a barrier's ability to successfully contain and redirect light trucks and sport utility vehicles.

MASH test 3-20 for a transition section is an optional test to evaluate the occupant risk and post-impact trajectory criteria for all test levels. This test should be conducted if there is reasonable uncertainty regarding the impact performance of the system for impacts with small passenger vehicle. Due to the geometry of the transition design and certain structural components in the transition area, namely the curb, the research team decided that this test was necessary to evaluate the crash performance of the new transition design.

Procedures in *MASH* section 2.3.2.1 were used by the research team to calculate the CIP for each test. The target CIP for *MASH* test 3-20 with the small car was 5.0 ft upstream of centerline of anchor post in concrete curb (post 20). The target CIP for *MASH* test 3-21 with the pickup was 6.8 ft upstream of centerline of anchor post in concrete curb (post 20).

The crash test and data analysis procedures were in accordance with guidelines presented in *MASH*. Chapter 4 presents brief descriptions of these procedures.

#### 3.2 EVALUATION CRITERIA

The crash test was evaluated in accordance with the criteria presented in *MASH*. The performance of the TxDOT T131RC Bridge Rail Transition is judged on the basis of three factors: structural adequacy, occupant risk, and post impact vehicle trajectory. Structural adequacy is judged upon the ability of the TxDOT T131RC Bridge Rail Transition to contain and redirect the vehicle, or bring the vehicle to a controlled stop in a predictable manner. Occupant risk criteria evaluate the potential risk of hazard to occupants in the impacting vehicle, and, to some extent, other traffic, pedestrians, or workers in construction zones, if applicable. Post-impact vehicle trajectory is assessed to determine potential for secondary impact with other vehicles or fixed objects, creating further risk of injury to occupants of the impacting vehicle and/or risk of injury to occupants in other vehicles. The appropriate safety evaluation criteria

from Table 5-1 of MASH were used to evaluate the crash test reported here and are listed in further detail under the assessment of the crash test.

#### **CHAPTER 4. CRASH TEST PROCEDURES**

#### 4.1 TEST FACILITY

The full-scale crash tests reported herein were performed at Texas A&M Transportation Institute (TTI) Proving Ground, an International Standards Organization (ISO) 17025 accredited laboratory with American Association for Laboratory Accreditation (A2LA) Mechanical Testing certificate 2821.01. The full-scale crash test was performed according to TTI Proving Ground quality procedures and according to the *MASH* guidelines and standards.

The TTI Proving Ground is a 2000-acre complex of research and training facilities located 10 miles northwest of the main campus of Texas A&M University. The site, formerly an Air Force base, has large expanses of concrete runways and parking aprons well-suited for experimental research and testing in the areas of vehicle performance and handling, vehicle-roadway interaction, durability and efficacy of highway pavements, and safety evaluation of roadside safety hardware. The site selected for construction and testing of the TxDOT T131RC Bridge Rail Transition evaluated under this project was along the edge of an out-of-service apron. The apron consists of an unreinforced jointed-concrete pavement in 12.5 ft  $\times$  15 ft blocks nominally 6 inches deep. The apron is over 60 years old, and the joints have some displacement, but are otherwise flat and level.

#### 4.2 VEHICLE TOW AND GUIDANCE PROCEDURES

Each test vehicle was towed into the test installation using a steel cable guidance and reverse tow system. A steel cable for guiding the test vehicle was tensioned along the path, anchored at each end, and threaded through an attachment to the front wheel of the test vehicle. An additional steel cable was connected to the test vehicle, passed around a pulley near the impact point, through a pulley on the tow vehicle, and then anchored to the ground such that the tow vehicle moved away from the test site. A two-to-one speed ratio between the test and tow vehicle existed with this system. Just prior to impact with the installation, the test vehicle was released to be unrestrained. The vehicle remained free-wheeling (i.e., no steering or braking inputs) until it cleared the immediate area of the test site, after which the brakes were activated to bring it to a safe and controlled stop.

#### 4.3 DATA ACQUISITION SYSTEMS

#### 4.3.1 Vehicle Instrumentation and Data Processing

Each test vehicle was instrumented with a self-contained, on-board data acquisition system. The signal conditioning and acquisition system is a 16-channel, Tiny Data Acquisition System (TDAS) Pro produced by Diversified Technical Systems, Inc. The accelerometers, that measure the x, y, and z axis of vehicle acceleration, are strain gauge type with linear millivolt output proportional to acceleration. Angular rate sensors, measuring vehicle roll, pitch, and yaw rates, are ultra-small size, solid state units designs for crash test service. The TDAS Pro hardware and software conform to the latest SAE J211, Instrumentation for Impact Test. Each of

the 16 channels is capable of providing precision amplification, scaling, and filtering based on transducer specifications and calibrations. During the test, data are recorded from each channel at a rate of 10,000 values per second with a resolution of one part in 65,536. Once recorded, the data are backed up inside the unit by internal batteries should the primary battery cable be severed. Initial contact of the pressure switch on the vehicle bumper provides a time zero mark as well as initiating the recording process. After each test, the data are downloaded from the TDAS Pro unit into a laptop computer at the test site. The raw data are then processed by the Test Risk Assessment Program (TRAP) software to produce detailed reports of the test results. Each of the TDAS Pro units are returned to the factory annually for complete recalibration. Accelerometers and rate transducers are also calibrated annually with traceability to the National Institute for Standards and Technology. Acceleration data are measured with an expanded uncertainty of ±1.7 percent at a confidence factor of 95 percent (k=2).

TRAP uses the data from the TDAS Pro to compute occupant/compartment impact velocities, time of occupant/compartment impact after vehicle impact, and the highest 10-millisecond (ms) average ridedown acceleration. TRAP calculates change in vehicle velocity at the end of a given impulse period. In addition, maximum average accelerations over 50-ms intervals in each of the three directions are computed. For reporting purposes, the data from the vehicle-mounted accelerometers are filtered with a 60-Hz digital filter, and acceleration versus time curves for the longitudinal, lateral, and vertical directions are plotted using TRAP.

TRAP uses the data from the yaw, pitch, and roll rate transducers to compute angular displacement in degrees at 0.0001-s intervals and then plots yaw, pitch, and roll versus time. These displacements are in reference to the vehicle-fixed coordinate system with the initial position and orientation of the vehicle-fixed coordinate systems being initial impact. Rate of rotation data is measured with an expanded uncertainty of  $\pm 0.7$  percent at a confidence factor of 95 percent (k=2).

#### 4.3.2 Anthropomorphic Dummy Instrumentation

An Alderson Research Laboratories Hybrid II, 50<sup>th</sup> percentile male anthropomorphic dummy, restrained with lap and shoulder belts, was placed in the driver's position of the 1100C vehicle. The dummy was uninstrumented. According to *MASH*, the use of a dummy in the 2270P vehicle is optional. Researchers did not use a dummy in the test with the 2270P vehicle.

#### 4.3.3 Photographic Instrumentation and Data Processing

Photographic coverage of the tests included three high-speed cameras: one overhead with a field of view perpendicular to the ground and directly over the impact point; one placed behind the installation at an angle; and a third placed to have a field of view parallel to and aligned with the installation at the downstream end. A flashbulb activated by pressure-sensitive tape switches was positioned on the impacting vehicle to indicate the instant of contact with the installation and was visible from each camera. The films from these high-speed cameras were analyzed on a computer-linked motion analyzer to observe phenomena occurring during the collision and to obtain time-event, displacement, and angular data. A mini-DV camera and still cameras recorded and documented conditions of the test vehicle and installation before and after the test.

### CHAPTER 5. CRASH TEST NO. 490022-6 (*MASH* 3-20)

#### 5.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

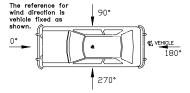
MASH test 3-20 involves an 1100C vehicle weighing 2425 lb  $\pm 55$  lb and impacting the test article at an impact speed of 62.2 mi/h  $\pm 2.5$  mi/h and an angle of 25 degrees  $\pm 1.5$  degrees. The target impact point was 5.0 ft upstream of centerline of anchor post in concrete curb (post 20). The 2006 Kia Rio used in the test weighed 2423 lb and the actual impact speed and angle were 61.5 mi/h and 25.6 degrees, respectively. The actual impact point was 5.0 ft (60.5 inches) upstream of post 20. Target impact severity (IS) was 55.7 kip-ft, and the actual IS was 57.2 kip-ft.

#### 5.2 **TEST VEHICLE**

A 2006 Kia Rio, shown in Figures 5.1 and 5.2, was used for the crash test. Test inertia weight of the vehicle was 2423 lb, and its gross static weight was 2602 lb. The height to the lower edge of the vehicle bumper was 7.12 inches, and it was 21.00 inches to the upper edge of the bumper. Table D1 in Appendix D give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be free-wheeling just prior to impact.

#### 5.3 WEATHER CONDITIONS

The test was performed on the morning of May 25, 2012. Weather conditions at the time of testing were as follows: wind speed: 14 mi/h; wind direction: 168 degrees with respect to the vehicle (vehicle was traveling in a northwesterly direction), temperature: 86°F, relative humidity: 65 percent.



#### 5.4 **TEST DESCRIPTION**

The 2006 Kia Rio, traveling at an impact speed of 61.5 mi/h, impacted the TxDOT T131RC Bridge Rail Transition 60.5 inches upstream of post 20 at an impact angle of 25.6 degrees. At approximately 0.012 s after impact, the thrie beam guardrail began to deflect toward the field side, and at 0.024 s, the vehicle began to redirect. The concrete transition curb began to deflect toward the field side at 0.029 s, and a crack formed in the concrete bridge rail curb downstream of post 21 at 0.053 s. The concrete bridge rail curb under post 21 began to crack at 0.057 s with some of the pieces of concrete spalling off at 0.220 s. At 0.307 s, the vehicle lost contact with the bridge rail traveling at an exit speed and angle of 44.8 mi/h and 4.4 degrees, respectively. Brakes on the vehicle were not applied, and the vehicle came to rest 180 ft downstream of impact and 21 ft toward traffic lanes. Figures D1 and D2 in Appendix D show sequential photographs of the test period.





Figure 5.1. Vehicle/TxDOT T131RC Bridge Rail Transition Geometrics for Test No. 490022-6.





Figure 5.2. Vehicle before Test No. 490022-6.

#### 5.5 DAMAGE TO TEST INSTALLATION

Figures 5.3 and 5.4 show damage to the T131RC Transition and bridge rail. The transition curb deflected toward the field side 0.5 inch. No cracking of the transition curb was noted. The concrete curb around post 21 was cracked significantly, and there was minor cracking around post 22. The vehicle was in contact with the installation 13.3 ft. Vehicle intrusion (formerly working width) was 7.4 inches. Maximum deflection of the thrie beam guardrail during the test was 7.4 inches, and maximum residual deformation after the test was 1.25 inches.

#### **5.6 VEHICLE DAMAGE**

Figure 5.5 presents damage to the 1100C vehicle. The left strut and strut tower were deformed. The front bumper, grill, hood, radiator, radiator support, left front fender, left front tire and wheel rim, left front door, left rear door, left rear quarter panel were deformed. The windshield sustained stress cracks from the left lower corner. Maximum crush to the exterior of the vehicle was 12.0 inches in the front plane in the left front corner at bumper height. Maximum occupant compartment deformation was 2.5 inches in the left front door near occupant hip height. The floor pan and firewall were also deformed. Tables D2 and D3 in Appendix D present the exterior crush profile and occupant compartment deformations.

#### 5.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was 21.0 ft/s at 0.080 s, the highest 0.010-s occupant ridedown acceleration was 6.1 Gs from 0.083 to 0.093 s, and the maximum 0.050-s average acceleration was –10.8 Gs between 0.023 and 0.073 s. In the lateral direction, the occupant impact velocity was 27.6 ft/s at 0.080 s, the highest 0.010-s occupant ridedown acceleration was 6.3 Gs from 0.118 to 0.128 s, and the maximum 0.050-s average was 15.3 Gs between 0.025 and 0.075 s. Theoretical Head Impact Velocity (THIV) was 37.7 km/h or 10.5 m/s at 0.078 s; Post-Impact Head Decelerations (PHD) was 6.9 Gs between 0.117 and 0.127 s; and Acceleration Severity Index (ASI) was 1.92 between 0.025 and 0.075 s. Figure 5.6 summarizes these data and other pertinent information from the test. Vehicle angular displacements and accelerations versus time traces are presented in Appendix D, Figures D3 through D9.



Figure 5.3. Vehicle/TxDOT T131RC Bridge Rail Transition Positions after Test No. 490022-6.





Figure 5.4. TxDOT T131RC Bridge Rail Transition after Test No. 490022-6.





Figure 5.5. Vehicle after Test No. 490022-6.

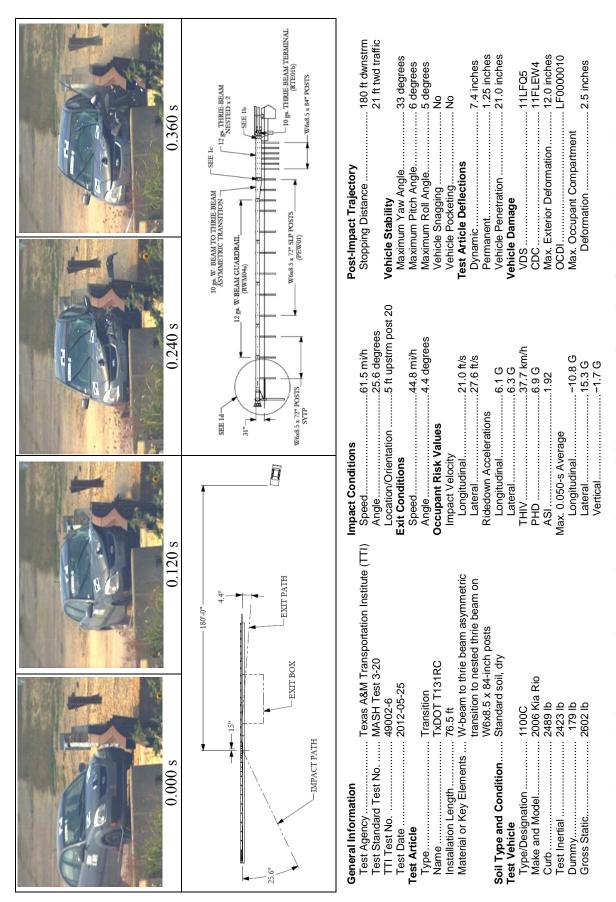


Figure 5.6. Summary of Results for MASH Test 3-20 on the TxDOT T131RC Bridge Rail Transition.

#### 5.8 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable *MASH* safety evaluation criteria is provided below.

#### 5.8.1 Structural Adequacy

A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.

Results: The TxDOT T131RC Bridge Rail Transition contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 7.4 inches. (PASS)

#### 5.8.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.

Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH. (roof  $\leq 4.0$  inches; windshield =  $\leq 3.0$  inches; side windows = no shattering by test article structural member; wheel/foot well/toe pan  $\leq 9.0$  inches; forward of A-pillar  $\leq 12.0$  inches; front side door area above seat  $\leq 9.0$  inches; front side door below seat  $\leq 12.0$  inches; floor pan/transmission tunnel area  $\leq 12.0$  inches).

Results: No detached elements, fragments, or other debris were present to penetrate or to show potential for penetrating the occupant compartment, or to present hazard to others. (PASS)

Maximum occupant compartment deformation was 2.5 inches in the left door at occupant hip height. (PASS)

F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.

Results: The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 5 degrees and 6 degrees, respectively. (PASS)

H. Occupant impact velocities should satisfy the following:

<u>Longitudinal and Lateral Occupant Impact Velocity</u>

<u>Preferred</u>

30 ft/s

Maximum

40 ft/s

Results: Longitudinal occupant impact velocity was 21.0 ft/s, and lateral occupant impact velocity was 27.6 ft/s. (PASS)

I. Occupant ridedown accelerations should satisfy the following:

Longitudinal and Lateral Occupant Ridedown Accelerations

 Preferred
 Maximum

 15.0 Gs
 20.49 Gs

Results: Longitudinal occupant ridedown acceleration was 6.1 G, and lateral occupant ridedown acceleration was 6.3 G. (PASS)

### **5.8.3** Vehicle Trajectory

For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).

Result: The 1100C crossed the exit box 80.1 ft downstream of loss of contact with the installation. (PASS)

#### CHAPTER 6. CRASH TEST 490022-8 (*MASH* 3-21)

#### 6.1 TEST DESIGNATION AND ACTUAL IMPACT CONDITIONS

*MASH* test 3-11 involves a 2270P vehicle weighing 5000 lb  $\pm$ 100 lb and impacting the test article at an impact speed of 62.2 mi/h  $\pm$ 2.5 mi/h and an angle of 25 degrees  $\pm$ 1.5 degrees. The target impact point was 6.8 ft upstream of centerline of anchor post in concrete curb (post 20). The 2008 Dodge Ram 1500 pickup truck used in the test weighed 5015 lb and the actual impact speed and angle were 62.7 mi/h and 25.1 degrees, respectively. The actual impact point was 7.2 ft upstream of post 20. Target IS was 115.1 kip-ft, and actual IS was 118.6 kip-ft.

#### 6.2 TEST VEHICLE

A 2008 Dodge Ram 1500 pickup truck, shown in Figures 6.1 and 6.2, was used for the crash test. Test inertia weight of the vehicle was 5015 lb, and its gross static weight was 5015 lb. The height to the lower edge of the vehicle bumper was 13.75 inches, and it was 25.38 inches to the upper edge of the bumper. The height to the vehicle's center of gravity was 29.0 inches. Tables E1 and E2 in Appendix E give additional dimensions and information on the vehicle. The vehicle was directed into the installation using the cable reverse tow and guidance system, and was released to be unrestrained just prior to impact.

#### 6.3 WEATHER CONDITIONS

The test was performed on the morning of June 29, 2012. Weather conditions at the time of testing were as follows: wind speed: 6 mi/h; wind direction: 180 degrees with respect to the vehicle (vehicle was traveling in a northwesterly direction); temperature: 90°F, relative humidity: 63 percent.

270°

#### 6.4 TEST DESCRIPTION

The 2008 Dodge Ram 1500 pickup truck, traveling at an impact speed of 62.7 mi/h, impacted the TxDOT T131RC Bridge Rail Transition 7.2 ft upstream of post 20 at an impact angle of 25.1 degrees. At approximately 0.024 s, the thrie beam guardrail began to deflect toward the field side, and at 0.050 s, the vehicle began to redirect. The transition curb began to deflect toward the field side at 0.127 s, and the rear of the vehicle contacted the transition at 0.209 s. At 0.363 s, the vehicle lost contact with the installation traveling at an exit speed and angle of 47.1 mi/h and 5.6 degrees, respectively. Brakes on the vehicle were applied 1.8 s after impact, and the vehicle subsequently came to rest 202 ft downstream of impact with the left side of the vehicle aligned with the traffic face of the bridge rail. Figures E1 and E2 in Appendix E show sequential photographs of the test period.





Figure 6.1. Vehicle/TxDOT T131RC Bridge Rail Transition Geometrics for Test No. 490022-8.





Figure 6.2. Vehicle before Test No. 490022-8.

### 6.5 DAMAGE TO TEST INSTALLATION

Figure 6.3 and 6.4 show damage to the T131RC Transition and the bridge rail. Post 14 was deflected toward the field side 0.25 inch, and post 15 was deflected toward the field side 0.5 inch. The soil around post 16 and 17 was disturbed. Post 18 was deflected toward the field side 1.38 inches, and maximum residual deformation at post 18 was 1.0 inch. The soil around post 19 was disturbed. The transition curb deflected toward the field side 1.5 inches. The transition curb was not cracked, but was marred with tire marks. Significant cracking of the bridge rail curb occurred at post 21 with slight damage at post 22. Length of contact of the vehicle with the installation was 15.3 ft. Vehicle intrusion (formerly working width) was 15.9 inches. Maximum dynamic deflection during the test was 8.37 inches, and maximum permanent residual deformation was 1.0 inch.

### 6.6 VEHICLE DAMAGE

Figure 6.5 presents damage to the 2270P vehicle. The left upper ball joint and left front upper and lower A-arms were deformed and the rear axle was broken. The front bumper, grill, hood, radiator, fan, water pump, left front fender, left front tire and wheel rim, left front door, left rear door, left rear exterior bed, left rear tire and wheel rim and rear bumper were deformed. The windshield sustained stress cracks from the right lower corner due to impact with a secondary barrier. Maximum crush to the exterior of the vehicle was not attainable due to the secondary impact. Maximum occupant compartment deformation was 0.25 inch in the left front door near occupant hip height. The floor pan and firewall were also deformed. Figure 6.6 shows photographs of the interior of the vehicle. Tables E3 and E4 in Appendix E present the exterior crush profile and occupant compartment deformations.

### 6.7 OCCUPANT RISK FACTORS

Data from the accelerometer, located at the vehicle center of gravity, were digitized for evaluation of occupant risk. In the longitudinal direction, the occupant impact velocity was 18.4 ft/s at 0.092 s, the highest 0.010-s occupant ridedown acceleration was 6.6 Gs from 0.120 to 0.130 s, and the maximum 0.050-s average acceleration was -8.0 Gs between 0.040 and 0.090 s. In the lateral direction, the occupant impact velocity was 23.6 ft/s at 0.092 s, the highest 0.010-s occupant ridedown acceleration was 9.4 Gs from 0.221 to 0.231 s, and the maximum 0.050-s average was 12.4 Gs between 0.030 and 0.080 s. Theoretical Head Impact Velocity (THIV) was 32.4 km/h or 9.0 m/s at 0.090 s; Post-Impact Head Decelerations (PHD) was 9.5 Gs between 0.221 and 0.231 s; and Acceleration Severity Index (ASI) was 1.52 between 0.030 and 0.080 s. Figure 6.7 summarizes these data and other pertinent information from the test. Vehicle angular displacements and accelerations versus time traces are presented in Appendix E, Figures E2 through E8.





Figure 6.3. Vehicle/TxDOT T131RC Bridge Rail Transition Positions after Test No. 490022-8.



Figure 6.4. TxDOT T131RC Bridge Rail Transition after Test No. 490022-8.

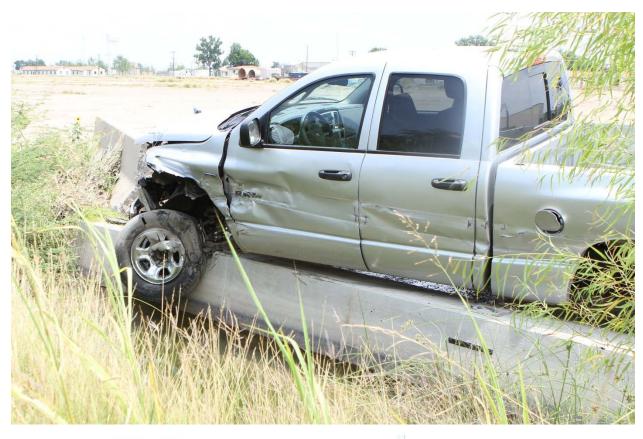




Figure 6.5. Vehicle after Test No. 490022-8.



Before Test





Figure 6.6. Interior of Vehicle for Test No. 490022-8.

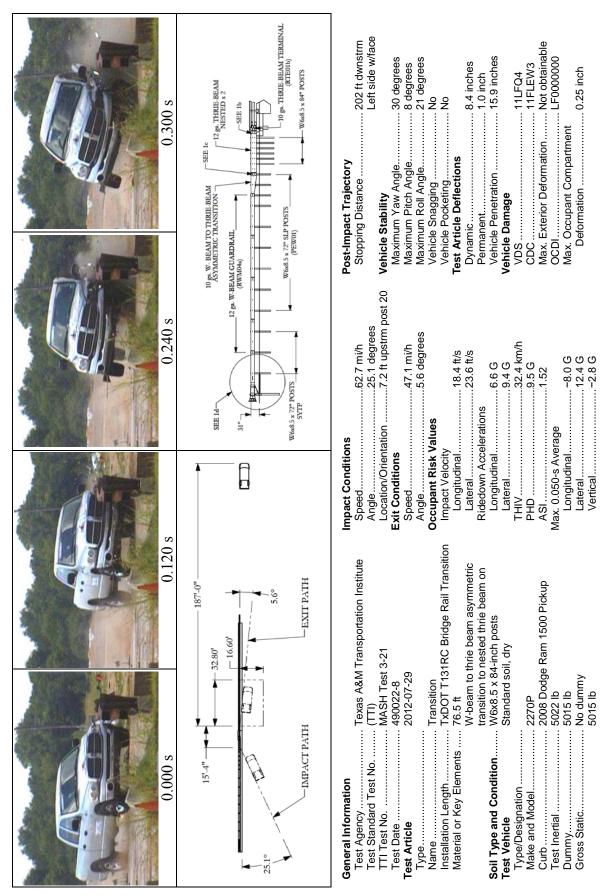


Figure 6.7. Summary of Results for MASH Test 3-21 on the TxDOT T131RC Bridge Rail Transition.

### 6.8 ASSESSMENT OF TEST RESULTS

An assessment of the test based on the applicable *MASH* safety evaluation criteria is provided below.

## 6.8.1 Structural Adequacy

A. Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.

Results: The TxDOT T131RC Bridge Rail Transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8.4 inches. (PASS)

## 6.8.2 Occupant Risk

D. Detached elements, fragments, or other debris from the test article should not penetrate or show potential for penetrating the occupant compartment, or present an undue hazard to other traffic, pedestrians, or personnel in a work zone.

Deformation of, or intrusions into, the occupant compartment should not exceed limits set forth in Section 5.3 and Appendix E of MASH (roof  $\leq 4.0$  inches; windshield =  $\leq 3.0$  inches; side windows = no shattering by test article structural member; wheel/foot well/toe pan  $\leq 9.0$  inches; forward of A-pillar  $\leq 12.0$  inches; front side door area above seat  $\leq 9.0$  inches; front side door below seat  $\leq 12.0$  inches; floor pan/transmission tunnel area  $\leq 12.0$  inches).

Results: No detached elements, fragments, or other debris were present to penetrate of to show potential for penetrating the occupant compartment, or to present hazard to others. (PASS)

Maximum occupant compartment deformation was 0.25 inch in the left door at occupant hip height. (PASS)

F. The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.

Results: The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 21 degrees and 8 degrees, respectively. (PASS)

I. Occupant impact velocities should satisfy the following:

Longitudinal and Lateral Occupant Impact Velocity

Preferred
30 ft/s
40 ft/s

Results: Longitudinal occupant impact velocity was 18.4 ft/s, and lateral occupant impact velocity was 23.6 ft/s. (PASS)

I. Occupant ridedown accelerations should satisfy the following:

<u>Longitudinal and Lateral Occupant Ridedown Accelerations</u>

 Preferred
 Maximum

 15.0 Gs
 20.49 Gs

Results: Longitudinal ridedown acceleration was 6.6 G, and lateral

ridedown acceleration was 9.4 G. (PASS)

## **6.8.3** Vehicle Trajectory

For redirective devices, the vehicle shall exit the barrier within the exit box (not less than 32.8 ft).

Result: The 22270P vehicle crossed the exit box within the limits specified in

MASH. (PASS)

## **CHAPTER 7. SUMMARY AND CONCLUSIONS**

### 7.1 SUMMARY OF CRASH TEST RESULTS

## 7.1.1 Crash Test No. 490022-6 (MASH Test 3-20)

The TxDOT T131RC Bridge Rail Transition contained and redirected the 1100C vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 7.4 inches. No detached elements, fragments, or other debris were present to penetrate of to show potential for penetrating the occupant compartment, or to present hazard to others. Maximum occupant compartment deformation was 2.5 inches in the left door at occupant hip height. The 1100C vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 5 degrees and 6 degrees, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 1100C crossed the exit box 80.1 ft downstream of loss of contact with the installation, which was within the *MASH* recommendation

## 7.1.2 Crash Test No. 490022-8 (*MASH* Test 3-21)

The TxDOT T131RC Bridge Rail Transition contained and redirected the 2270P vehicle. The vehicle did not penetrate, underride, or override the installation. Maximum dynamic deflection during the test was 8.4 inches. No detached elements, fragments, or other debris were present to penetrate of to show potential for penetrating the occupant compartment, or to present hazard to others. Maximum occupant compartment deformation was 0.25 inch in the left door at occupant hip height. The 2270P vehicle remained upright during and after the collision event. Maximum roll and pitch angles were 21 degrees and 8 degrees, respectively. Occupant risk factors were within the preferred limits specified in *MASH*. The 22270P vehicle crossed the exit box within the limits specified in *MASH*.

## 7.2 CONCLUSIONS

The TxDOT T131RC Bridge Rail Transition performed acceptably as a *MASH* TL-3 transitions, as shown in Tables 7.1 and 7.2.

Table 7.1. Performance Evaluation Summary for MASH Test 3-20 on the TxDOT T131RC Bridge Rail Transition.

	Test Agen	Test Agency: Texas A&M Transportation Institute	Test No.: 490022-6	Test Date: 201205-25
		MASH Test 3-20 Evaluation Criteria	Test Results	Assessment
<u> </u>	Structural	Structural Adequacy		
,	A. Test	Test article should contain and redirect the vehicle or	The TxDOT T131RC Bridge Rail Transition	
	brins	bring the vehicle to a controlled stop; the vehicle	contained and redirected the 1100C vehicle. The	
	shon	should not penetrate, underride, or override the	vehicle did not penetrate, underride, or override	Pass
	insta	installation although controlled lateral deflection of	the installation. Maximum dynamic deflection	
	the to	the test article is acceptable.	during the test was 7.4 inches.	
<u> </u>	Occupant Risk	Risk		
•	D. Deta	Detached elements, fragments, or other debris from	No detached elements, fragments, or other debris	
	the to	the test article should not penetrate or show potential	were present to penetrate of to show potential for	
	for p	for penetrating the occupant compartment, or present	penetrating the occupant compartment, or to	Pass
	an m	an undue hazard to other traffic, pedestrians, or	present hazard to others.	
	persa	personnel in a work zone.		
	Defo	Deformations of, or intrusions into, the occupant	Maximum occupant compartment deformation	
	com t	compartment should not exceed limits set forth in	was 2.5 inches in the left door at occupant hip	Pass
	Secti	Section 5.3 and Appendix E of MASH.	height.	
•	$F.$ The $\iota$	The vehicle should remain upright during and after	The 1100C vehicle remained upright during and	
	colli	collision. The maximum roll and pitch angles are not	after the collision event. Maximum roll and	Pass
	to ex	to exceed 75 degrees.	pitch angles were 5 and 6 degrees, respectively.	
-	H. Long	Longitudinal and lateral occupant impact velocities	Longitudinal occupant impact velocity was	
	shon	should fall below the preferred value of 30 ft/s, or at	21.0 ft/s, and lateral occupant impact velocity	Pass
	least	least below the maximum allowable value of 40 ft/s.	was 27.6 ft/s	
	l. Long	Longitudinal and lateral occupant ridedown	Longitudinal occupant ridedown acceleration	
	acce'	accelerations should fall below the preferred value of	was 6.1 G, and lateral occupant ridedown	Dace
	15.0	15.0 Gs, or at least below the maximum allowable	acceleration was 6.3 G.	1 433
	value	value of 20.49 Gs.		
	Vehicle Trajectory	rajectory		
	For	For redirective devices, the vehicle shall exit the	The 1100C crossed the exit box 80.1 ft	ı
	barr	barrier within the exit box (not less than 32.8 ft).	downstream of loss of contact with the installation.	Pass

Table 7.2. Performance Evaluation Summary for MASH Test 3-21 on the TxDOT T131RC Bridge Rail Transition.

Te	Test Agency: Texas A&M Transportation Institute	Test No.: 490022-8	Test Date: 2012-06-29
	MASH Test 3-21 Evaluation Criteria	Test Results	Assessment
Str	Structural Adequacy		
H.	Test article should contain and redirect the vehicle or	The TxDOT T131RC Bridge Rail Transition	
	bring the vehicle to a controlled stop; the vehicle	contained and redirected the 2270P vehicle. The	
	should not penetrate, underride, or override the	vehicle did not penetrate, underride, or override	Pass
	installation although controlled lateral deflection of	the installation. Maximum dynamic deflection	
	the test article is acceptable.	during the test was 8.4 inches.	
Oc	Occupant Risk		
D.	Detached elements, fragments, or other debris from	No detached elements, fragments, or other debris	
	the test article should not penetrate or show potential	were present to penetrate of to show potential for	
	for penetrating the occupant compartment, or present	penetrating the occupant compartment, or to	Pass
	an undue hazard to other traffic, pedestrians, or	present hazard to others.	
	personnel in a work zone.		
	Deformations of, or intrusions into, the occupant	Maximum occupant compartment deformation	
	compartment should not exceed limits set forth in	was 0.25 inch in the left door at occupant hip	Pass
	Section 5.3 and Appendix E of MASH.	height.	
<i>F</i> .	The vehicle should remain upright during and after	The 2270P vehicle remained upright during and	
	collision. The maximum roll and pitch angles are not	after the collision event. Maximum roll and	Pass
	to exceed 75 degrees.	pitch angles were 21 and 8 degrees, respectively.	
Н.	Longitudinal and lateral occupant impact velocities	Longitudinal occupant impact velocity was	
	should fall below the preferred value of 30 ft/s, or at	18.4 ft/s, and lateral occupant impact velocity	Pass
	least below the maximum allowable value of 40 ft/s.	was 23.6 ft/s.	
I.	Longitudinal and lateral occupant ridedown	Longitudinal ridedown acceleration was 6.6 G,	
	accelerations should fall below the preferred value of	and lateral ridedown acceleration was 9.4 G.	Dace
	15.0 Gs, or at least below the maximum allowable		1 455
	value of 20.49 Gs.		
Ve	Vehicle Trajectory		
	For redirective devices, the vehicle shall exit the	The 22270P vehicle crossed the exit box within	Pass
	barrier within the exit box (not less than $32.8  \text{ft}$ ).	the limits specified in MASH.	

## **CHAPTER 8. IMPLEMENTATION STATEMENT**

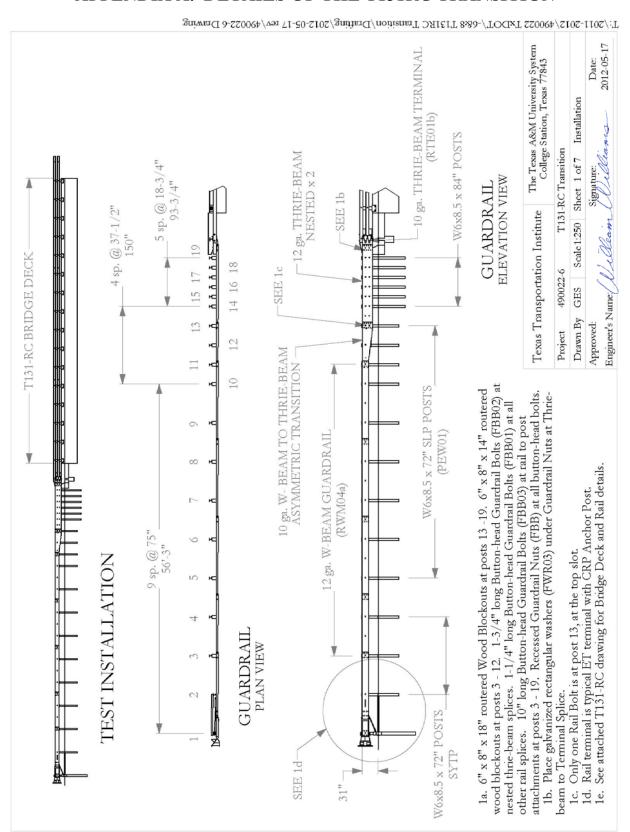
TTI researchers recently designed and successfully crash tested the TxDOT Type 131RC Bridge Rail. The T131RC Bridge Rail consists of two HSS6×6×½ steel tubes supported by W6×15 steel posts spaced on 5 ft on centers. The posts were anchored to an 11-inch high concrete curb. The curb was 10 inches wide at the base and 8 inches wide at the top. The posts were anchored to the concrete curb using ¾-inch diameter adhesive anchors. The base plate for the T131RC post design was bent to conform to the shape of the concrete curb. The TxDOT T131RC Bridge Rail tested previously met all the strength and safety performance criteria of *MASH*.

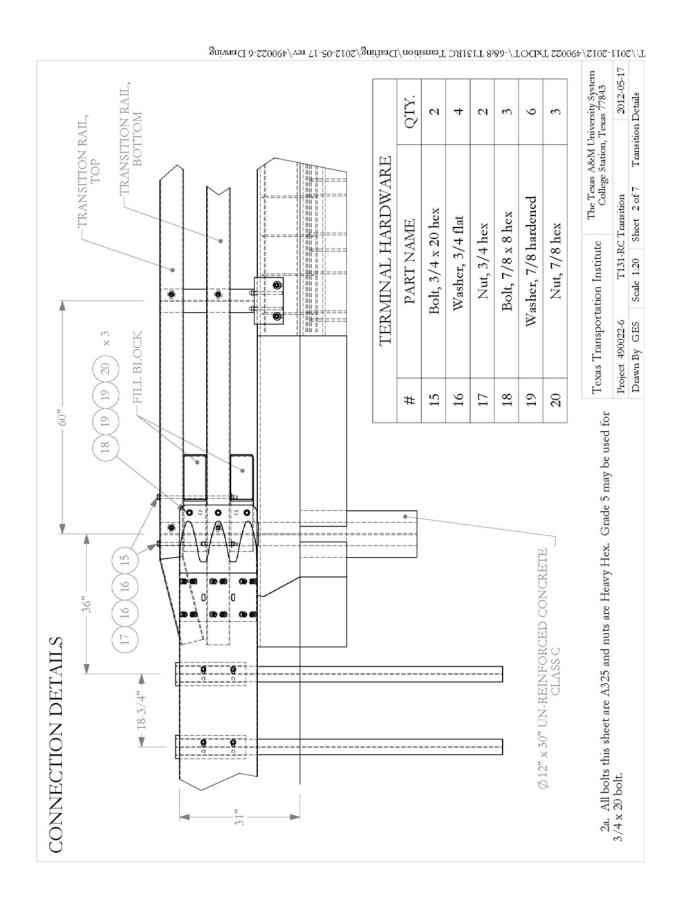
The purpose of this portion of the project was to develop a transition for connecting a 31-inch tall W-beam approach guardrail to the new T131RC Bridge Rail. The transition designed and tested for this project met all *MASH* safety performance criteria for a TL-3 transition. The transition is recommended for implementation on all projects using the new T131RC Bridge Rail design.

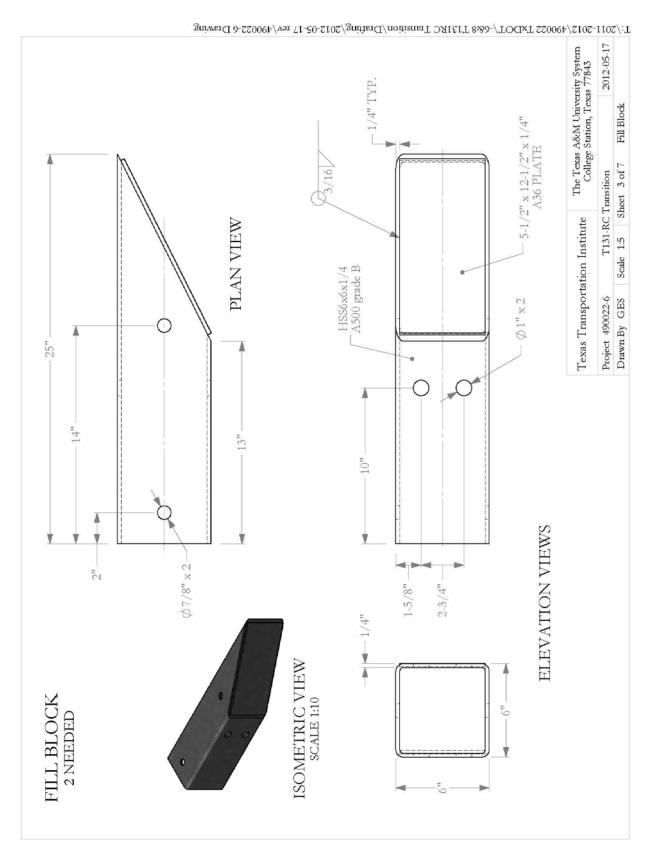
## REFERENCES

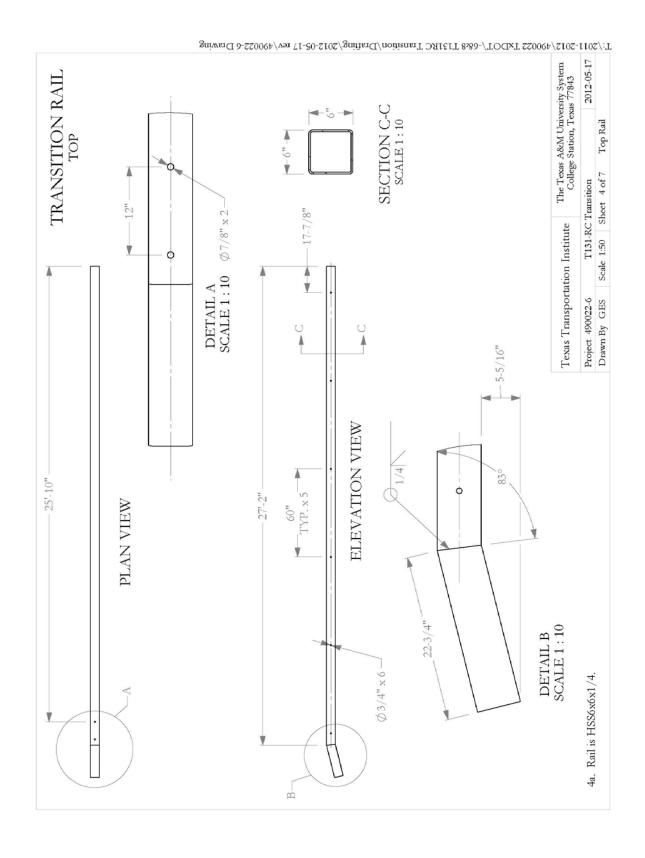
- 1. AASHTO, *Manual for Assessing Safety Hardware*, American Association of State Highway and Transportation Officials, Washington, D.C., 2009.
- W. F. Williams, R. P. Bligh, and W. L. Menges, *MASH Test 3-11 on the T131RC Bridge Rail*, Test Report No. 9-1002-1, Texas Transportation Institute, The Texas A&M University System, College Station, TX, June 2012.

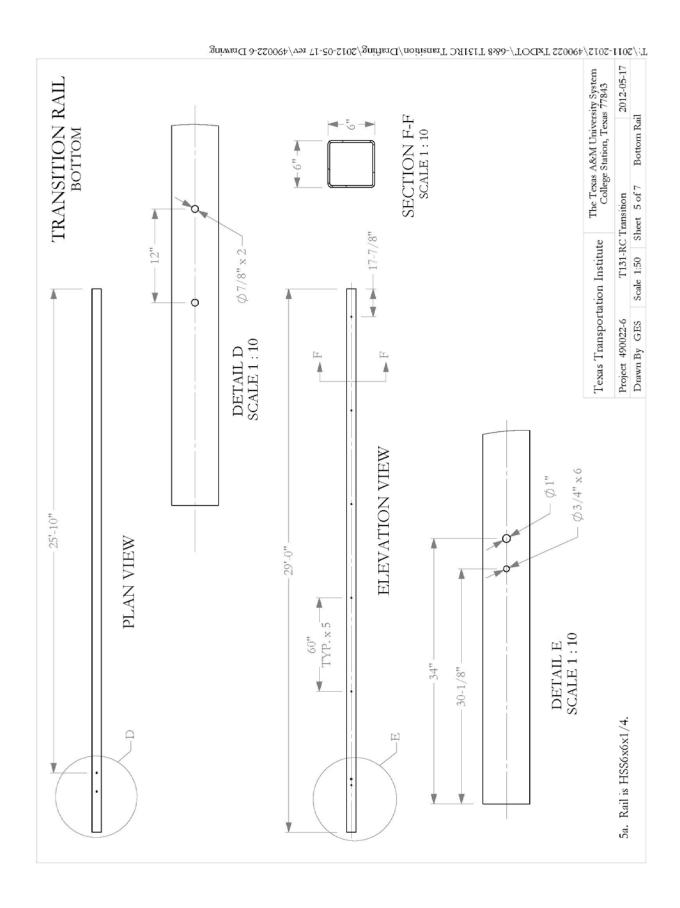
## APPENDIX A. DETAILS OF THE T131RC TRANSITION

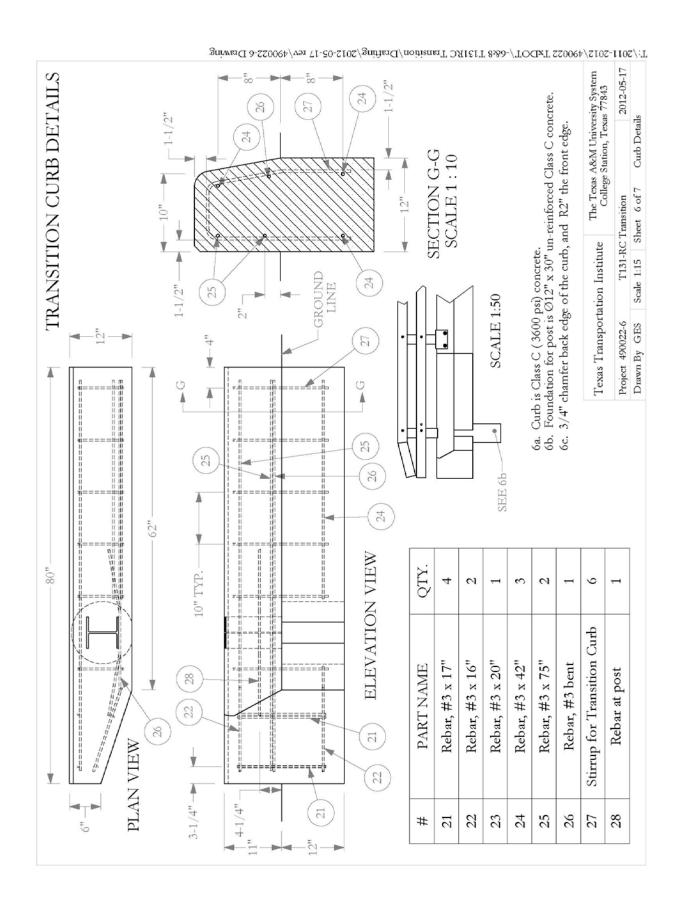


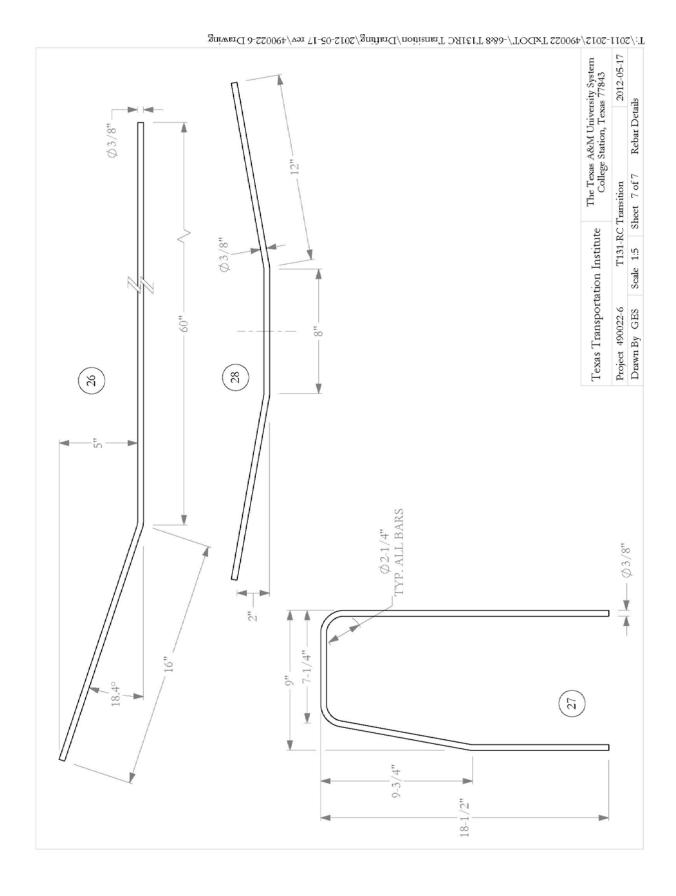












## APPENDIX B. CERTIFICATION DOCUMENTATION

MATERIAL USED

TEST NUMBER 490022-6

TEST NAME T131RC Transition

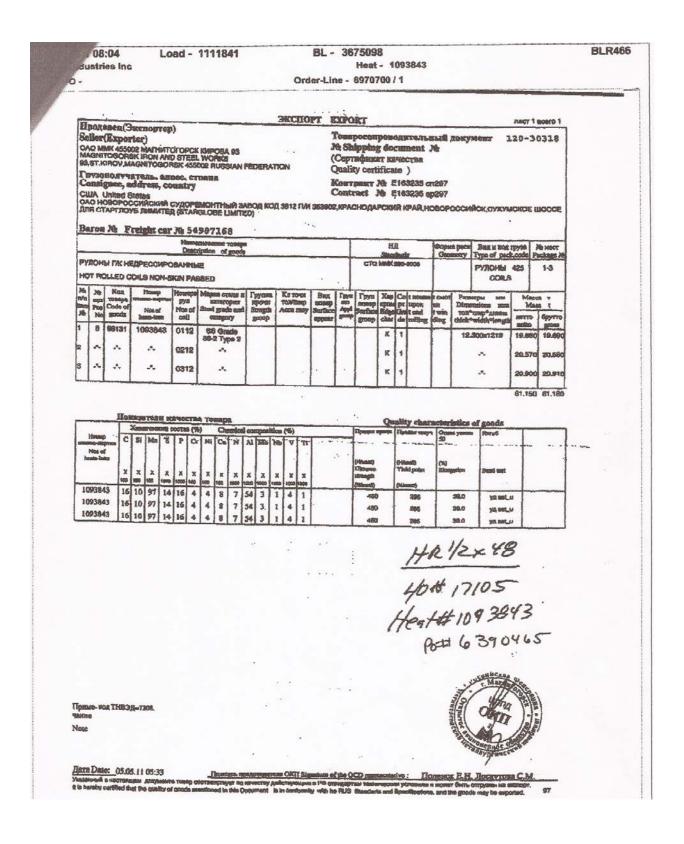
DATE 2012-05-25

DATE RECEIVED	ITEM NUMBER	DESCRIPTION	SUPPLIER	HEAT#	NOTE
2012-01-26*	Parts-15	Guardrail Parts	Brazos Industries	see file	1
2012-01-12	Rebar 03-06	3/8" x 20' grd 60	CMC-Sheplers	3028608	1
2012-01-12	Rebar 04-25	1/2" x 20' gr 60	CMC-Sheplers	see file	1
2012-05-02	Parts-20	Guardrail Parts	Trinity	see file	2

These parts were used on the Bridge Deck for test 490022-1. These parts were used for the Transition for this test.

<sup>2</sup> 

BLR466			375	9111 - 1412	SY78 -	70		01000	11 - bsod		Se-2011 12:0
		-		1 / 9888	TOT - əni.	Order-L					- Od 79
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COR SIECE D. Box 2259	101 bio2		ription	13 0429.3 2.1920#	5 10.00' 2822.5 2.1920#	828 060' 30.33' 2233861.7 012.1926#	10.33' 3845.1 2.1320m	7475 30 DASS = 25.01044 = 01(51/39)	caby certification and the design and design		
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01-02-2012 04:10 Load - 1132336 BLR466 BL - 3677708 Heat - 762367 Brazos Industries Inc Order-Line - 7073336 / 5 Cust. PO -Ø1004/005 12/22/2011 THU 18:59 FAX 519 738 5061 atlastube shipping Artes Tube Canada ULC 200 Clark St. Harrow, Omsrie, Canada NOR 100 Tel: 519-738-3541 Fox: 519-738-3537 DDD JMC STEEL GROUP MATERIAL TEST REPORT Sold to Shipped to NAMASCO CORPORATION Steel Warehousing Corporati 500 COLONIAL CENTER PR ROSWELL GA 30076 USA NAMASCO SOUTH WEST SOUTH LOOP 4, P.O. BOX BUDA TX 78715-0367 USA Material: 5.0x5.0x250x48'0"0(4x2). Material No: 500502504800 Melted in: Canada Purchase Order: 6408907 Quat Material #: T514SQA5000576 Salas order: 688743 Mn P S Si Al Cu Co Mo Ni Cr V TE B N Bundle No PCs Yield Tensile Etn.2in Certification CE: 0.36 M101100675 8 063850 Pai 078200 Pai 32.6 % ASTM A500-10A GRADE B&C Material Note: Sales Or.Note: Material: 6.0x6.0x250x40\*0\*0(3x3). Material No: 600602504000 Mado in: Canada Welted in: Canada Punchase Order: 6409841 Cust Material #: T814SQA5000480 Sales order: 689536 Sì Al Cu Ch Mo Ni Cr V Ti B 
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 Eln.2in Certification ASTM A500-10A GRADE B&C Material: 8.0x4.0x250x40\*0\*0(2x4). Material No: 800402504000 Made in: Canada Melted In: Canada Purchase Order: 6409841 Cust Material #: T8414RECTA5000480 Sales order: 889538 Heat No C Ma P S SI Al Cu Ch Me Na 762777 0.180 0.790 0.008 0.008 0.013 0.066 0.049 0.005 0.005 0.015 0.035 0.002 0.000 0.000 0.000 Bundio No PCs Yield Tonsils Ein.2In 8101096343 8 060430 Psi 075020 Psi 35.5 % Certification CE: 0.33 ASTM A500-10A GRADE 8&C Sales Or. Note: Authorized by Quasity Ansurance: M. Whell.
The results reported an about The results reported on this report represent the actual attributes of the meterial furnished and indicate full compliance with all applicable specification and contract requirements. Pago : 2 Of 3 Metals Service Center institute Institute

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	NUDDR STEEL TUBOALOOSA, IND.	ber Tally	TO CONCINCT	Order Bescription: A36, 9.5550 IN x 96.000 IN x 240.000 IN Quality Plan Description: A36NDWAN-TRIPLE: A5TM A36-08 NUD NW.ASME	Heat/Stab Runder	-	81U7759-03	1 -		+	-		STADOGRAFI	-	-	-		Harner 3 P.CS: 10 Weight:	Manuay has not come in connact with this product disting the manufacturing process not have say mercury been used by the manufacturing process. Confilted in accordance with EM 10204.3.1. No wold regist has been performed on this material. Manufactured to a trily afford the grain practice. "Produced from Coil " Nannisobured to a trily afford the grain practice." Produced from Coil " ISO 97101.2018 Registered, PED Carafied	*** ind kales Heats malked wid	
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#	1	10			CEV CEV	0.37	0.37	Test	Temp									Si Si			

# **Porteous Fastener Company**

# **Product Information Sheet**

# Carriage Bolt, Inch Series, Grade A



- > PFC Product Category: 00100
- Typical Material: Low Carbon Steel
- Material and Mechanical Properties: Purchased to meet ASTM A307 Grade A.
- > Dimensions: ASME B18.5, Round Head Square Neck Bolt, Rolled Threads
  - > Full thread to 6 inches in length.
  - Undersize body and 6 inches of threads on lengths over 6 to 12 inches.
     6 inches threads and full size body on lengths over 12 inches.
- > Zinc Plating: Purchased to meet ASTW-1941 FeZna
- discount of the second second > Hot-Dip Galvanized: Purchase
- > Typical Hardress:
- > Tensile Strength 60,000 PSI Minimum FIRST CLASS SCRUBTE

Tensile Strength - NC Threads ASTM A307 Grade A									
Size	PSI	Pounds							
1/4-20	60,000	1900							
5/16-18	60,000	3100							
3/8-16	60,000	4650							
7/16-14	60,000	6,350							
1/2-13	60,000	8,500							
9/16-12	60,000	11,000							
5/8-11	60,000	13,550							
3/4-10	60,000	20,050							
7/8-9	60,000	27,700							
1-8	60,000	36,350							

Len	gth Toler	ances - C	arriage B	olts							
	Nominal Size										
Nominal Length	#10 to 3/8	7/16 & 1/2	9/16 to 3/4	7/8 to 1							
		Tolerance	on Length								
Up to & Incl 1"	+0.02/-0.03	+0.02/-0.03	+0.02/-0.03								
Over 1" to 2 1/2", incl.	+0.02/-0.04	+0.04/-0.05	+0.06/-0.08	+0.08/-0.10							
Over 2 1/2" to 4", incl.	+0.04/-0.06	+0.06/-0.08	+0.08/-0.10	+0.10/-0.14							
Over 4" to 6", incl.	+0.06/-0.10	+0.08/-0.10	+0.10/-0.10	+0.12/-0.16							
Over 5"	+0.10/-0.18	+0.12/-0.18	+0.14/-0.18	+0.16/-0.20							

Porteous Fastener Company

Page 1 of 1

The information presented is believed to be accurate at the time of document creation. However, Porteous Fastener Company is not responsible for any claim traceable to any errors (typographical or otherwise) as contained herein. Porteous Fastener Company makes no warranties as to the accuracy of this information.

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Page:

PORT CERTIFIE

> NUCOR CORPORATION NUCOR STEEL TEXAS

SOLD ADELPHIA METALS I LLC 411 MAIN ST E TO: NEW PRAGUE, MN 56071-

なロいコス

Date: 26-Oct-2011 B.L. Number: 586989

Load Number: 195932

8812 Hwy 79 W JEWETT, TX 75846 800-527-6445 Nucor Steel - Texas Ship from:

Material Safety Data Sheets are available at www.nucorbar.com or by contacting your inside sales representative.

C.E. .62 61 33 32 4. 10. . 12. 12. 13. CHEMICAL TESTS .04 .03 024 .039 .019 1.02 .15 .98 4.5 4 4 떮 %±% BEND PHYSICAL TESTS ELONG % IN 8" 70,700 108,900 12.0% 487MPa 751MPa 70,000 110,500 13.0% 483MPa 762MPa TENSILE P.S.I. YIELD P.S.I. A615M Gr 420 (Gr60) ASTM A615/A615M-09b GR 60[420] ASTM A615/A615M-09b GR 60[420] DESCRIPTION A615M Gr 420 (Gr60) AASHTO M31-07 Nucor Steel - Texas AASHTO M31-07 Nucor Steel - Texas 13/#4 Rebar 20' 13/#4 Rebar 20' 801746 JW1110880301 JW1110880201 HEAT NUM. \* PO# => PO# ₽

QUALITY ASSURANCE:

Nathan Stewart

TR No. 9-1002-12-4

ADELPHIA METALS-CUST PU N/A JEWETT, TX 75846-

SE 5

55

2012-10-25

CMC STEEL TEXAS 1 STEEL MILL DRIVE SEGUIN TX 78155-7510

CERTIFIED MILL TEST REPORT

For additional copies call 830-372-8771

are accurate and conform to the reported grade specification We hereby certify that the test results presented here

Daniel & Arthurte Daniel J. Schacht

Quality Assurance Manager

HEAT NO.:3028608 SECTION: REBAR 10MM (#3) 20'0" 420/60 GRADE: ASTM A615-09b Gr 420/60 ROLL DATE: 11/20/2011 MELT DATE: 11/19/2011	0 - D - O	CMC Construction Svcs College Stati 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900	e Stati S H H P P P P O O O	CMC Construction Svcs College Stati 10650 State Hwy 30 College Station TX US 77845-7950 979 774 5900	ge Stati	Delivery#: 80634703 BOL#: 70224264 CUST PO#: 5390AB CUST P/N: DLVRY LBS / HEAT: 16848.000 LB DLVRY PCS / HEAT: 2240 EA
Characteristic V.	Value		Characteristic	stic Value		Characteristic Value
0 0	0.45%					
Mn 0.	0.81%					
О В	0.012%	,				
0 s	0.037%					
O IS	0.17%					
O 10	0.34%					
O 10	0.17%					
O	0.16%					
Mo 0.	0.059%					
o >	0.002%	-0				
o 85	0.001%					
Sn 0.	0.013%				**************************************	
AI 0.	0.002%					
					4	
_	/ U.DKSI					
_	108.3ksi	is			Character Sales and Associated Spiriters and	$1.3^{\circ} \circ \phi = 0.000000000000000000000000000000000$
	13%					
Elongation Gage Lgth test 1 81	8IN					
	Passed					
	5				-	

THIS MATERIAL IS FULLY KILLED, 100% MELTED AND MANUFACTURED IN THE USA, WITH NO WELD REPAIR OR MERCURY CONTAMINATION IN THE PROCESS. REMARKS:

the property diet, her helm to exploye the contract as or within the lensing at a cognition and as to each relating the conditions undi-	Phone: 934 ier: 12/87 7 7 7 6 Delivery:and remit to:	of jecopie informal maled state clock agrees a jump bit data in clock agrees a jump bit data in the clock agree and the clock agreement and the clock agreement and the clock agreement ag	rgres and centres as deen below are close of sharing and dependent. The close of sharing add dependent. The close of sharing add dependent. The close of sharing and control of sharing dependent and	and temper of the acts company and state that is to be an index of the first partial read or course, and a party over all it are countries and all and of the state of the acts of the act	Shipper's No.  S/O No.  Subject to Section 7 of Copioshes Bill of Lading, if this sidelivered to the consignes with the consignes with the camer shall not make shipment without peyment of other lawful charges.  TRINITY HIGHW PRODUCTS, LL  Per (Signature of Center III thanges are to be preparation of the property of the property of the property of the property described he control that property desc	delivery of this freight, and all AY C
No. Piece Pkgs. Count	Description of Articles	*Wi. Class or Flate	V No. Piece Cal. Piegs. Court	Description of Ar		Diess or V Rate Col.
10 10 10 10 10 44	110 12/12/6/51.5/8. 320 12/12/6/51.5/8. 320 12/12/6/5/12/8/12/8/12/8/12/8/12/8/12/8/12/8/12		3-PA	Notes		
18 2 16 10 4 6 12 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	4076B WD BLK RTD 6.78 X.14 6019B REPL SHT 13 X.27.5 Y/B LT 6149B WD BLK RTD 6.X 8 X.18 6900G 7/8" X.15.5" HXBLT A.449 5"I 12227G T12/126/3" 1.5.6@16.75/5 14578G 60 PST/8.58/3 XH TX 14785G 60 POST/8.58/3 KH TX 14785G 60 POST/8.58/1 KANB TX 33725A ET+CAM-50, 12% HBA/SYTY 33795G SYT-3" AN STRT 3-HL 66 352474 CONN PL 40" X20" RT MO		GUARDR NMFC CI	AL HWY STEEL ITEM 105460 ASS 50		
18 2 16 10 4 6 12 2 2 2 2 3 FECIAL INSTRUCT SHIPPE 1' the st prient in NOTE - Wheel in NOTE - Wheel in the area of doc.	4076B WD BLK RTD 6.78 X.14 6019B REPL SHT 13 X.27.5 Y/B LT 6149B WD BLK RTD 6.X 8 X.18 6900G 7/8" X.15.5" HXBLT A.449 5"I 12227G T12/126/3" 1.5.6@16.75/5 14578G 60 PST/8.58/3 XH TX 14785G 60 POST/8.58/3 KH TX 14785G 60 POST/8.58/1 KANB TX 33725A ET+CAM-50, 12% HBA/SYTY 33795G SYT-3" AN STRT 3-HL 66 352474 CONN PL 40" X20" RT MO	Quires that the bill of ledings are specifically in writing aretion of values (1 any) of.	GUARDR NMFC CI  16-41901  In agreed or dadared value  Pet CONSIGNEE ON AGENT  SIGN HERE DRIVER	Received the above described prope the back hereof and agree to the fore	Total Weig	7 3

Popular Annia			As of 5/1/12						*	Si Cu Cb Cr Vn ACW	29.0 0.190 0.770 0.007 0.001 0.020 0.150 0.00 0.040 0.002 4	26.0 0.200 0.810 0.013 0.004 0.020 0.090 0.000 0.050 0.000 4	25.0 0.200 0.780 0.009 0.003 0.020 0.130 0.000 0.040 0.002 4	
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alysis		172458	Customer PO: TTI-TEST 490022-	1901		×	×			TS	78,400	82,800	79,100	
Certified Analysis		Order Number: 1172458	Customer PO: T	BOL Number: 41901	Document #: 1	Shipped To: TX	Use State: TX			TY Heat Code/ Heat # Yield	5 58,600	137784 64,330	203516 54,900	
J								022-6		CL TY Heat	A 2 103056	A 2 1	A 2 2	
				,TRAINING MTRLS	RWY			TING PROJECT 490		Spec	M-180 A	M-180	M-180	
	Trinity Highway Products, LLC	8th St.	11191	Customer: SAMPLES, TESTING, TRAINING MTRLS	2525 STEMMONS FRWY		DALLAS, TX 75207	SAMPLES AND TESTING PROJECT 490022-6	-	Qty Part# Description	6 11G 12/12/6/31.5/S			
	Trinity Hig	2548 N.E. 28th St.	Ft Worth, TX 76111	Customer:				Project:		Qty	9			

CW	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	
Vn ACW	0.007	0.000	0.002	0.002	0.002	0.002	0.001	0.001	0.001	0.001	0.001	0.000	0.001	0.001	0.001	0.001	0.001	0.003	0.004	0.000	0.002	0.003	of 3
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Elg	29.0	26.0	25.0	29.0	25.0	23.0	27.1	21.2	27.0	25.0	23.6	26.0	31.4	29.5	26.0	28.0	28.5	28.2	30.5	31.9	26.0	27.6	
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TS	78,400	82,800	79,100	78,400	79,600	80,100	85,300	83,700	82,800	84,500	88,300	75,300	70,830	72,990	79,070	77,600	76,830	71,963	73,194	66,100	77,470	78,876	
												_						_		0	0	61	
Yield	58,600	64,330	54,900	58,600	60,600	60,100	53,600	61,600	61,600	62,700	66,200	57,310	54,310	55,520	60,750	59,780	59,460	54,730	56,593	58,100	58,680	59,962	
at #																							
Heat Code/ Heat#		137784	203516	203516	203517	204446	a54903	A54907	A56188	C53442	C54778		149773	150044	150046	150058	150060	4	4		150000	∞	
Heat C	103056	13	20	20	30	20	28	¥.	A;	Ü	Ü	150045	17	15	1,4	17	1.5	1017684	1017674	125745	151877	1018448	
TY	7	2	2	7	2	2	2	7	2	2	7	7	7	2	2	2	7				5		
C	A	<	A	A	A	V	<	٧	V	A	A	V	A	A	A	A	A				¥		
	M-180	80	80	80	80	80	80	80	80	80	80	M-180	081	081	08	08	08	A-36	A-36	A-36	M-180	A-36	
Spec	X	M-180	M-180	M-180	M-180	M-180	M-180	M-180	M-180	M-180	M-180	X	M-180	M-180	M-180	M-180	M-180	<	<.	∢	M	V.	
												ANC								INI	8.75/S		
												12/12'6/6'3/S ET2000 ANC						DDR		T10/END SHOE/SLANT	T12/12′6/3′1.5:6@1′6.75/S	SYTP	
otion	/3.1.5/											S/E,9/9						ST/8.5/		ND SH	2.6/3.1.5	1/8.5#/	
Description	12/12'6/3'1.5/S											12/12'6						6'0 POST/8.5/DDR		T10/E	T12/12	6'0 PST/8.5#/SYTP	
	G											32G						533G	533G	5086	12227G	78G	
Qty Part#	5 11G											2 32							53	2 98	4 122	6 14578G	
Qty	9											.4						14		, ,	1		
	1																						

Frinity Highway Products, LLC 2548 N.E. 28th St.

Customer: SAMPLES, TESTING, TRAINING MTRLS Ft Worth, TX 76111

2525 STEMMONS FRWY

Customer PO: TTI-TEST 490022-Order Number: 1172458

BOL Number: 41901

Shipped To: TX

Document #:

As of: 5/1/12

**DALLAS, TX 75207** 

SAMPLES AND TESTING PROJECT 490022-6

Project:

Ϋ́ Use State: Vn ACW 4 0.00 0.090 0.014 0.00 0.120 0.017 0.00 0.140 0.003 0.00 0.220 0.004 0.030 0.001 0.00 0.140 0.003 ڻ 0.00 c 25.7 0.120 0.930 0.012 0.040 0.180 0.360 27.5 0.110 0.980 0.023 0.044 0.180 0.320 28.0 0.150 0.910 0.015 0.040 0.190 0.370 29.5 0.220 0.790 0.010 0.005 0.022 0.029 33.0 0.160 0.910 0.014 0.023 0.190 0.300 Č 0.180 S 0.012 0.040 C Mn Elg 75,900 79,900 TS 72,244 73,902 71,300 Yield 53,613 53,600 56,700 58,000 56,271 53,613 TY Heat Code/ Heat # 813U66380 1017007 1016659 3031507 3029682 CL A-500 A-36 A-36 A-36 A-36 Spec ET+CAN-50',12'6 HBA/SYTP SYT-3"AN STRT 3-HL 6'6 6'0 POST/8.5#/TRANS TX KT IHE/#S.8/1SOJ 0.9 7'0 POST/8.5#/3HI TX Description 2 14785G 2 33795G Part # 2 14786G 33726A 14784G 33726A Qt/

TL -3 or TL-4 COMPLIANT when installed according to manufactures specifications

4

0.00 0.050 0.000

34.0 0.190 0.750 0.010 0.013 0.011 0.040

69,500

44,200

37482C

A-36

CONN PL 40"X20" RT MO

2 35247A

Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.

ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT.

ALL GUARDRAIL MEETS AASIITO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36

ALL COATINGS PROCESSES OF THE STEEL OR IRON ARE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHERWISE STATED.

BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.

3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD I!" DIA ASTM 449 AASHTO M30, TYPE II BREAKING STRENGTIT 49100 LB

2 of 3

TR No. 9-1002-12-4



# Certified Analysis

Trinity Highway Products, LLC

2548 N.E. 28th St.

Ft Worth, TX 76111

Customer: SAMPLES, TESTING, TRAINING MTRLS

2525 STEMMONS FRWY

DALLAS, TX 75207

Order Number: 1172458

Customer PO: TTI-TEST 490022-

Shipped To: TX

As of: 5/1/12

BOL Number: 41901 Document #: 1

Use State: TX

Trinity

Certified By:

State of Texas, County of Tarrant. Sworn and subscribed before methis 1st day of May, 2012

SAMPLES AND TESTING PROJECT 490022-6

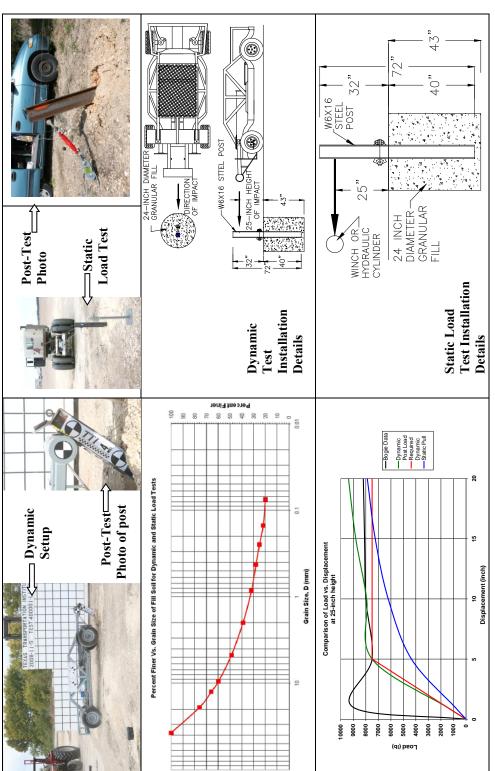
Project:

Notary Public:

Commission Expires:

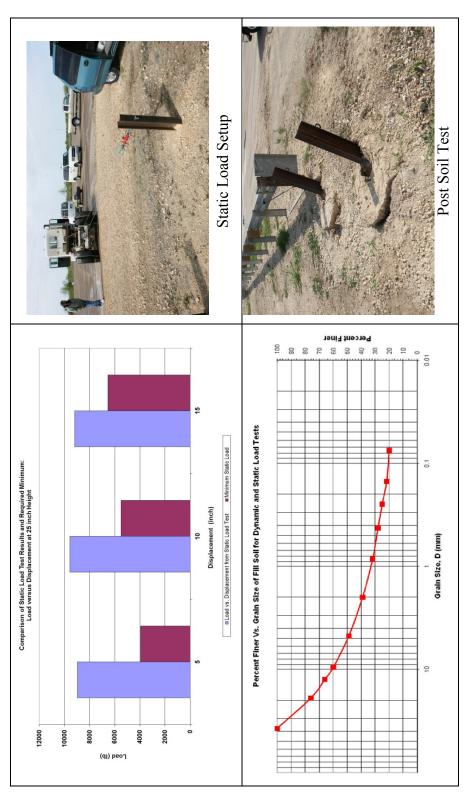


### APPENDIX C. SOIL PROPERTIES



Date Test Facility and Site Location In Situ Soil Description (ASTM D2487	2008-11-05 TTI Proving Ground, 3100 SH 47, Bryan, TX 77807 Sandy gravel with silty fines
Fill Material Description (ASTM D2487) and sieve analysis  Description of Fill Placement Procedure  Bogie Weight  Impact Velocity	AASHTO Grade B Soil-Aggregate (see sieve analysis above) 6-inch lifts tamped with a pneumatic compactor 5009 lb 20.5 mph

Figure C1. Summary of Strong Soil Test Results for Establishing Installation Procedure.



AASHTO Grade B Soil-Aggregate (see sieve analysis) 6-inch lifts tamped with a pneumatic compactor TTI Proving Ground, 3100 SH 47, Bryan, TX Sandy gravel with silty fines May 25, 2012 In Situ Soil Description (ASTM D2487) Description of Fill Placement Procedure ...... Test Facility and Site Location Fill Material Description (ASTM D2487) and sieve analysis ..... Date.....

Figure C2. Test Day Static Soil Strength Documentation for Test No. 490022-6.

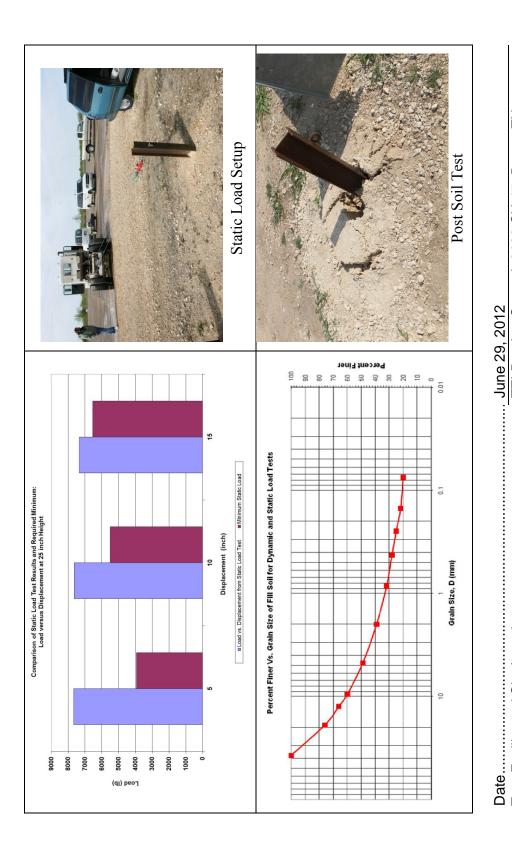


Figure C3. Test Day Static Soil Strength Documentation for Test No. 490022-8.

Description of Fill Placement Procedure ......

Test Facility and Site Location

AASHTO Grade B Soil-Aggregate (see sieve analysis) 6-inch lifts tamped with a pneumatic compactor

TTI Proving Ground, 3100 SH 47, Bryan, TX

Sandy gravel with silty fines

### APPENDIX D. CRASH TEST NO. 490022-6 (MASH TEST 3-20)

### D1. TEST VEHICLE PROPERTIES AND INFORMATION

Table D1. Vehicle Properties for Test No. 490022-6.

Date: 2012	-05-25	Test No.:	490022-6	_	VIN No.:	KNADE1	23366068232	
Year: 2006		Make:	Kia		Model:	Rio		
Tire Inflation P	ressure: 32	: psi	Odometer:	119617		Tire Size:	P185/65R14	<u>.                                    </u>
Describe any o	damage to the	vehicle prio	r to test:					
Denotes according	celerometer lo	cation.					ACCELEROMETERS note:	
NOTES:			. A WHEEL TRACK			Œ.		WHEEL N T
Engine Type: Engine CID:	4 cylinder 1.6 liter		M TRACK	=		VEHIC	SLE	TRACK
Transmission Auto  X Auto X FWD Optional Equip	or RWD	_ Manual 4WD	TIRE WHEEL		-	TEST	NERTIAL C.M.	
Dummy Data: Type: Mass: Seat Position	179 lb	entile male		F	W H	G S S	M <sub>rear</sub> D	
•	inches		ļ <u>.                                    </u>			_ C		
A 66.38	F_	33.00	-	11.00	Р_	4.12	_ U	15.75
B 57.75	G_	0.4.70	-	24.12	Q _	22.19	_ V	21.50
C 165.75	H _	34.72		57.75	R _	15.38	_ W	39.50
D 34.00 E 98.75	l _ J	7.12		57.12 30.62	S _ T	7.62 66.12	_ X	108.50
Wheel Center		11.00	Wheel Cent		_	11.00	_	
GVWR Ratin	qs:	Mass: lb	<u>Curb</u>		Test	<u>Inertial</u>	Gross	Static
Front	1918	$M_{front}$		598		1577		1670
Back	1874	$M_{rear}$		891		852		932
Total	3638	$M_{Total}$	2	489		2423		2602
Mass Distribu	tion: LF:	763	RF:	808	LR:	460	RR:39	2

### Table D2. Exterior Crush Measurements for Test No. 490022-6.

 $\geq$  4 inches \_\_

Date:	2012-05-25	Test No.:	490022-6		VIN No.:	KNADE123366068232
Year:	2006	Make:	Kia		Model:	Rio
	7	VEHICLE (	CRUSH MEA	ASUREM	MENT SHE	EET <sup>1</sup>
			Complete Who	en Applical	ole	
	End Da	mage			S	lide Damage
	Undeformed	d end width _			Bowing: B1	1 X1
	Corne	er shift: A1 _			B2	2 X2
		A2 _				
	End shift at fran	ne (CDC)		Во	wing constar	nt
	(check or	ne)			X1 + X2	_
		< 4 inches				

Note: Measure C<sub>1</sub> to C<sub>6</sub> from Driver to Passenger side in Front or Rear impacts – Rear to Front in Side Impacts.

G : W		Direct I	Damage								
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	$C_1$	$C_2$	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>	±D
1	Front plane at bumper ht	12	12	18	12	8	6	5.5	3	0	-9
2	Side plane at bumper ht	20	11	48	0	1.5	6.75	8.5	9	11	152
	Measurements recorded										
	in inches										

<sup>&</sup>lt;sup>1</sup>Table taken from National Accident Sampling System (NASS).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

<sup>\*</sup>Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

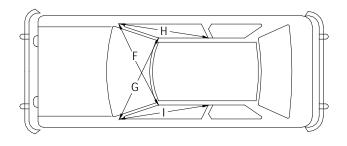
<sup>\*\*</sup>Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

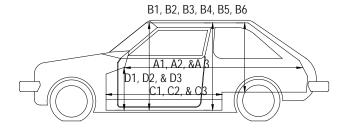
<sup>\*\*\*</sup>Measure and document on the vehicle diagram the location of the maximum crush.

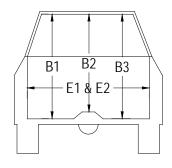
Table D3. Occupant Compartment Measurements for Test No. 490022-6.

Date: 2012-05-25 Test No.: 490022-6 VIN No.: KNADE123366068232

Year: 2006 Make: Kia Model: Rio







### OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

	Before (inches)	After (inches)
A1	67.50	67.38
A2	67.50	67.50
A3	67.50	67.50
B1	40.75	40.75
B2	36.75	36.75
В3	40.75	40.75
B4	36.25	36.25
B5	35.75	35.75
B6	36.25	36.25
C1	26.00	26.00
C2		
C3	27.5	27.5
D1	9.75	9.75
D2		
D3	9.50	9.50
E1	51.00	48.50
E2	51.00	52.25
F	51.00	51.00
G	51.00	50.00
Н	37.00	37.00
I	37.00	37.00
J*	50.75	50.50

2012-10-25

<sup>\*</sup>Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.



Figure D1. Sequential Photographs for Test No. 490022-6 (Overhead and Frontal Views).

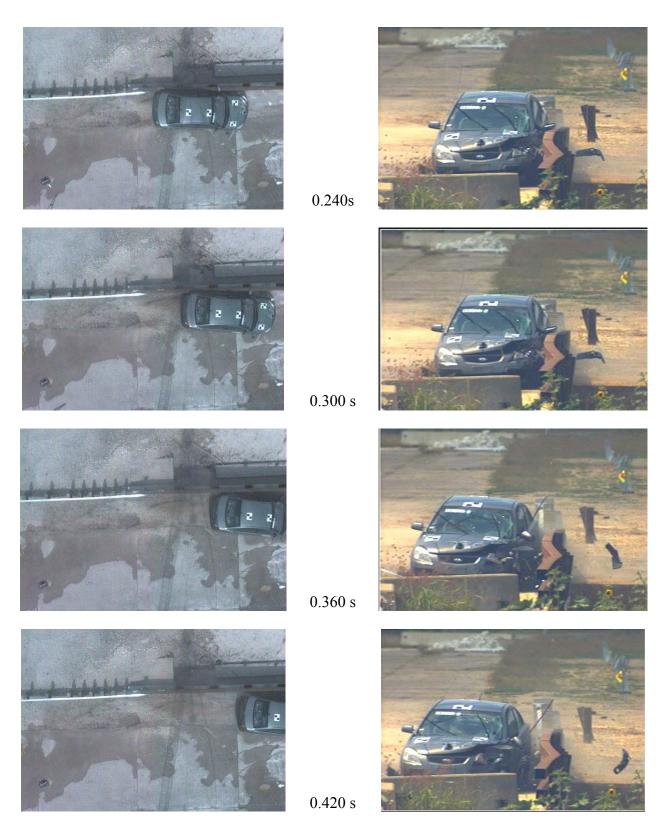


Figure D1. Sequential Photographs for Test No. 490022-6 (Overhead and Frontal Views) (continued).

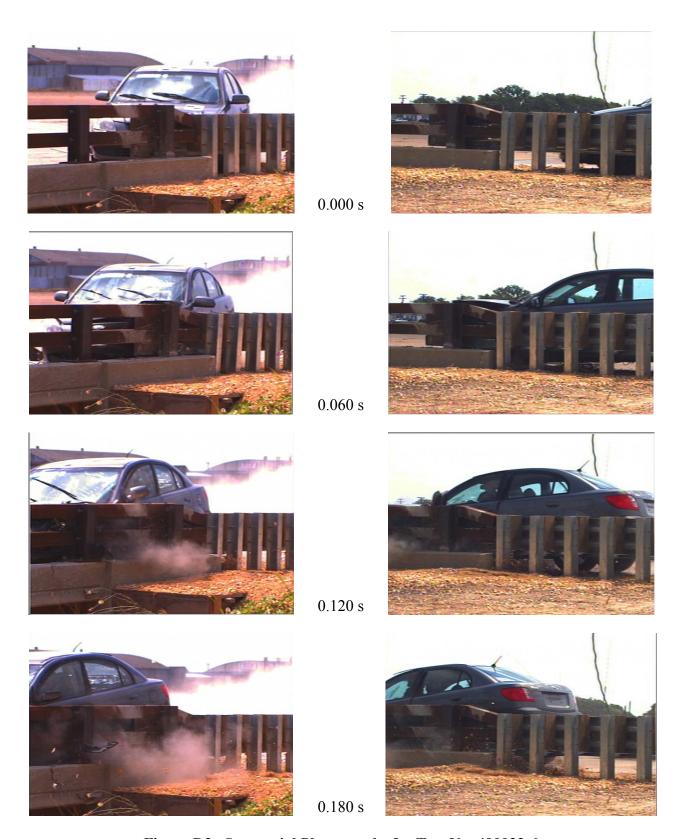


Figure D2. Sequential Photographs for Test No. 490022-6 (Field Side Transition Views).

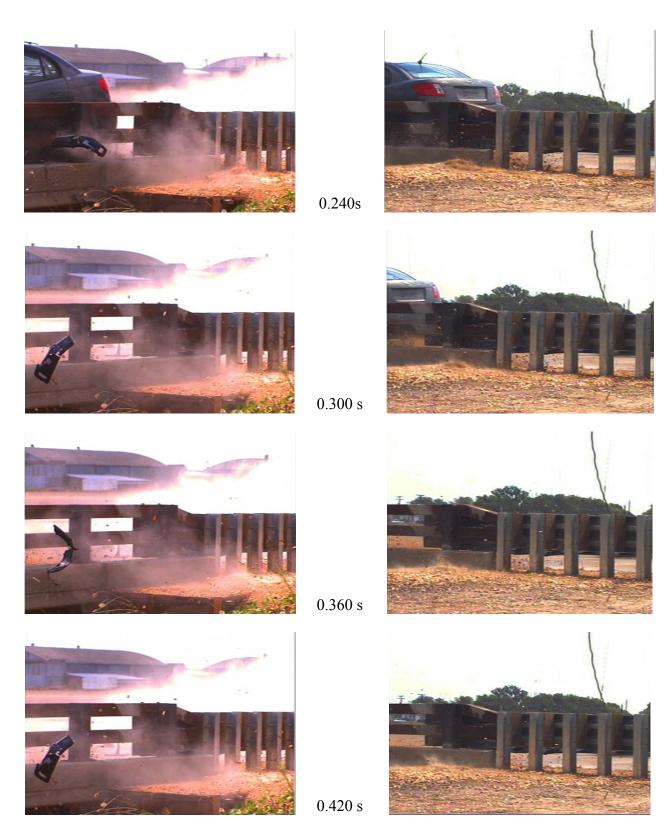


Figure D2. Sequential Photographs for Test No. 490022-6 (Field Side Transition Views) (continued).

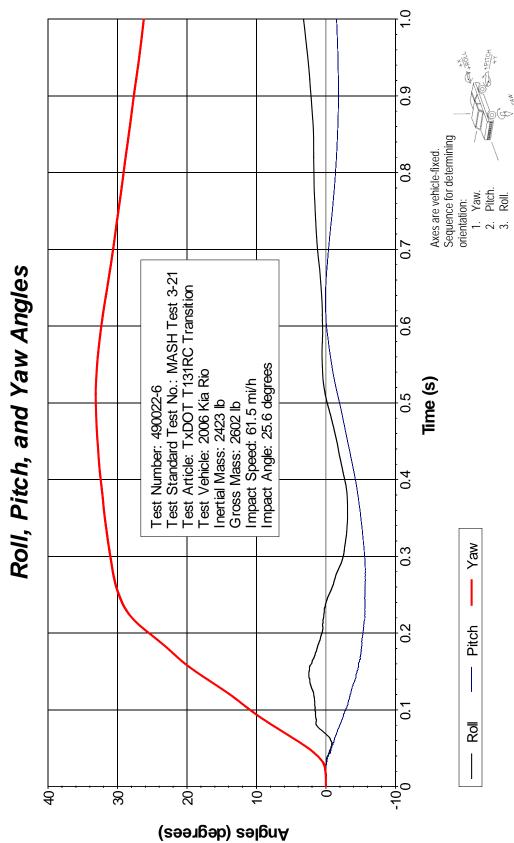


Figure D3. Vehicle Angular Displacements for Test No. 490022-6.

# 0.0 Gross Mass: 2602 lb Impact Speed: 61.5 mi/h Impact Angle: 25.6 degrees 0.7 X Acceleration at CG 0.6 Time (s) 0.4 0.3 0.7 -15 5 ιĊ

Longitudinal Acceleration (G)

Figure D4. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-6 (Accelerometer Located at Center of Gravity).

50-msec average

SAE Class 60 Filter

Time of OIV (0.0802 sec)

1.0

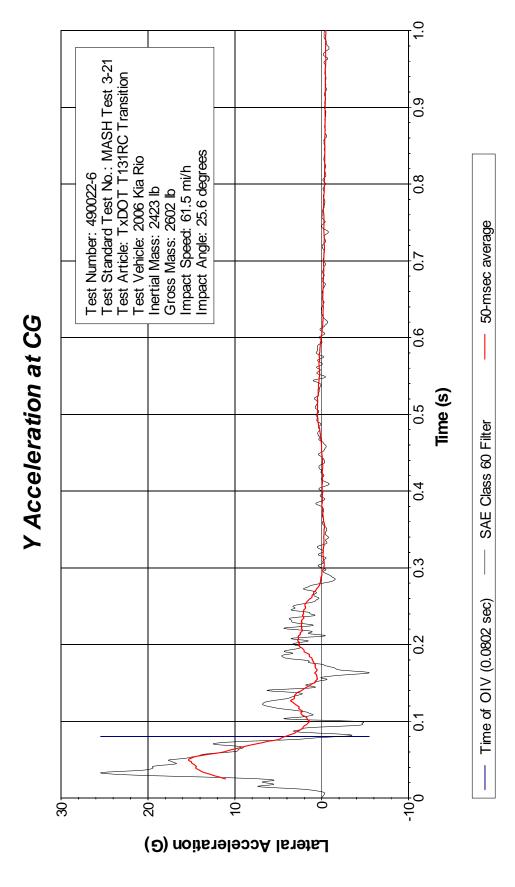


Figure D5. Vehicle Lateral Accelerometer Trace for Test No. 490022-6 (Accelerometer Located at Center of Gravity).

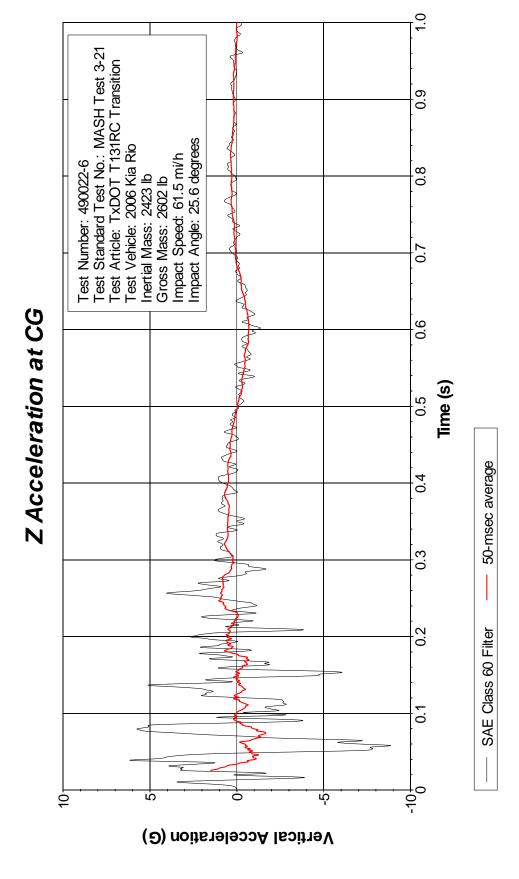


Figure D6. Vehicle Vertical Accelerometer Trace for Test No. 490022-6 (Accelerometer Located at Center of Gravity).

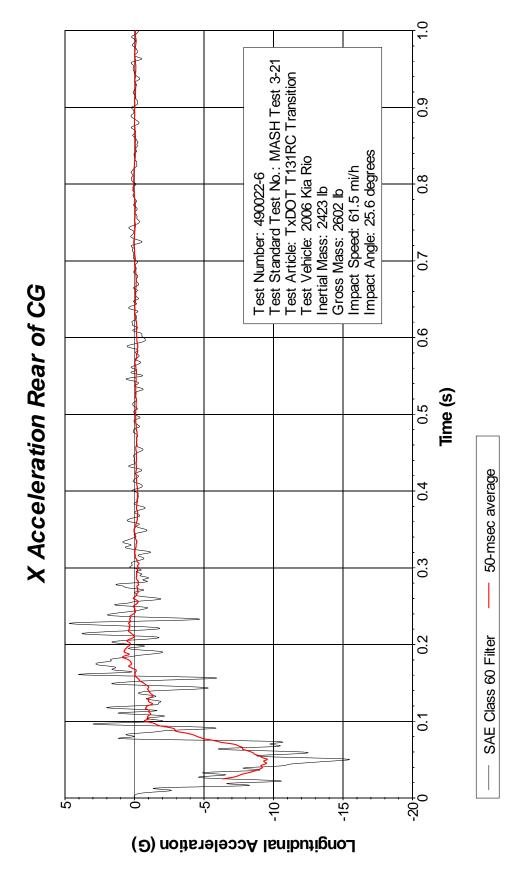


Figure D7. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-6 (Accelerometer Located Rear of Center of Gravity).

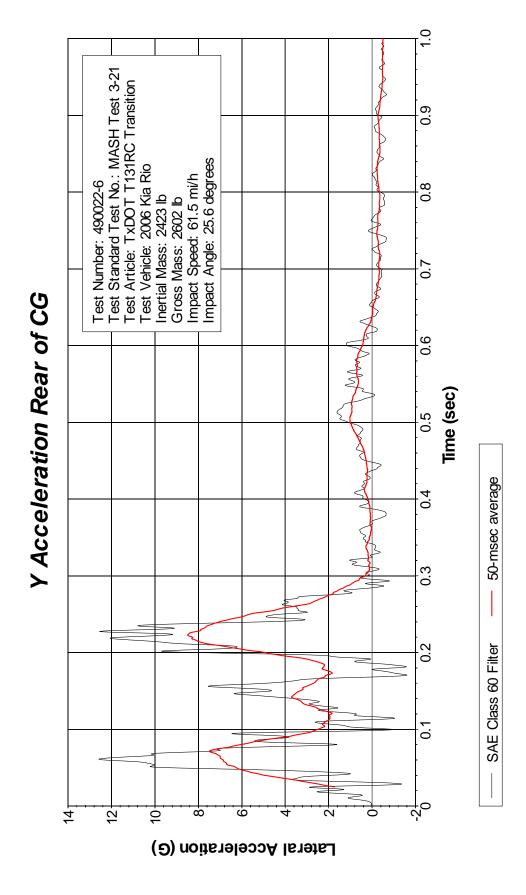


Figure D8. Vehicle Lateral Accelerometer Trace for Test No. 490022-6 (Accelerometer Located Rear of Center of Gravity).

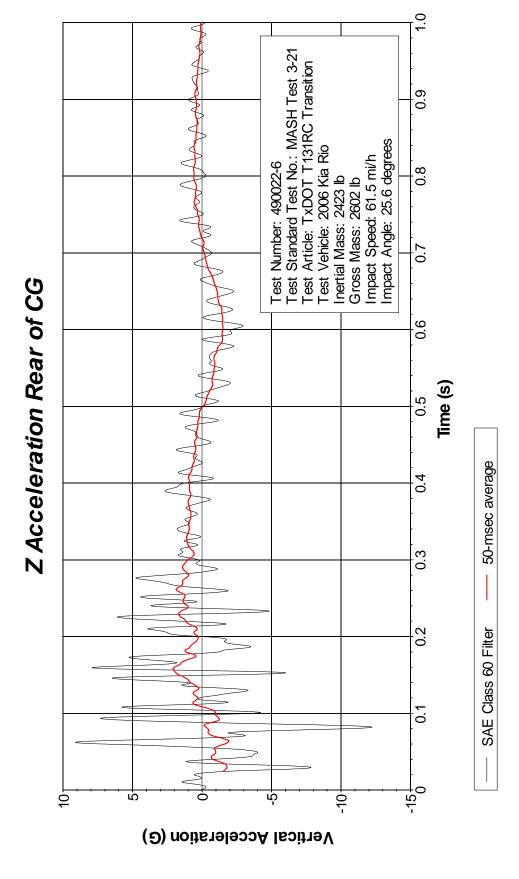


Figure D9. Vehicle Vertical Accelerometer Trace for Test No. 490022-6 (Accelerometer Located Rear of Center of Gravity).

### APPENDIX E. CRASH TEST NO. 490022-8 (MASH TEST 3-21)

### E1. TEST VEHICLE PROPERTIES AND INFORMATION

Table E1. Vehicle Properties for Test No. 490022-8.

Date:	2012-06-2	29	Test No.:	490022-8	8	_ VIN No.:	1DTHA182	18J0415	0
Year:	2008		Make:	Dodge		Model:	Ram 1500		
Tire Siz	e: <u>265</u>	5/70R17			Tire	Inflation Pre	essure: 35 ps	si	
Tread T	ype: Hig	hway				Odd	meter: <u>1398</u>	49	
Note ar	ny damage t	to the vel	nicle prior to	test:					
• Deno	otes acceler	ometer lo	ocation.			X - W	-		
NOTES	S:			_ 1		*7//			1
				- ] ],					
Engine Engine		V-8 5.7 liter		-   M   V   V   V   V   V   V   V   V   V	WHEEL TRACK				WHEEL TRACK
Transm	ission Type	<b>)</b> :		<u> </u>			TES	T' INERTIAL C. M.	
	Auto or FWD x		_ Manual 4WD		R	Q →			
		_	4₩₽		P -				
Optiona	al Equipmer	11.		<b>†</b>	5				Ē
Dummy	/ Data:			_ j j-	I T			$(\bigcirc)_{f}$	$\mathcal{L}_{K}$
Type:	<u></u>	No dumm	ny	-		U	LvLs		
Mass: Seat F	osition:			_	<b>-</b>	H	E 	<b>→</b> D-	-
Geome	try: inch	00		_		V M FRONT		▼ M REAR	
A	78.25	F	36.00	K	20.50	P	c 2.88	U	<b>→</b> 28.50
^ B	75.00	 G	29.00	- '` _ L	29.12	_ '	31.25	V _	29.50
	223.75	н _	61.21		68.50	R	18.38	W	59.50
D	47.25	Ι _	13.75	N	68.00	S	12.00	X	78.00
	140.50	J _	25.38	0	44.50	_ T _	77.50	_	
	eel Center eight Front		14.75 Cle	Wheel Wo earance (Fror		5.00	Bottom Fram Height - Fror		17.125
	eel Center eight Rear		14.75 CI	Wheel We earance (Rea		10.25	Bottom Fram Height - Rea		24.75
GVWF	R Ratings:		Mass: Ib	) (	<u>Curb</u>	Tes	t Inertial	Gro	ss Static
Front	•	700	$M_{front}$		2870		2830		
Back	3	900	$M_{rear}$		2152		2185		
Total	6	700_	$M_{\text{Total}}$		5022		5015		
	istribution								
lb		LF:	1426	RF:	1404	LR:	1069	RR:	1116

### Table E2. Vehicle Parametric Measurements for Vertical CG.

Date: <u>2012-06</u>	5-29 Te	st No.: _4	90022-8	\	/IN: <u>1DT</u>	HA18218	J0415	0	
Year: 2008		Make: D	odge		Model: _F	Ram 1500	0		
Body Style: Q	uad Cab			N	/lileage: _1	139849			
Engine: 5.7 lit	er V-8			Transr	nission: _ <i>F</i>	Automatio	<u> </u>		
Fuel Level: <u>E</u>	mpty	Balla	ıst: <u>80 l</u>	bs in front	of bed			(440 lb	max)
Tire Pressure:	Front: 3	8 <u>5</u> psi	Rear	35	psi Siz	e: <u>265/</u>	70R17		
Measured Ve	hicle Wei	ghts: (l	b)						
LF:	1426		RF:	1404		Front	Axle:	2830	
LR:	1069		RR:	1116		Rear	Axle:	2185	
Left:	2495		Right:	2520			Total:		
						5	000 ±110	0 lb allow ed	
Wh	eel Base:	140.5	inches	Track: F:	68.5	inches	R:	68	inche
	148 ±12 inch	es allow ed			Track = (F+R	$R)/2 = 67 \pm 1.$	.5 inches	allow ed	
Center of Gra	avity, SAE	J874 Sus	spension N	/lethod					
X:	61.21	in	Rear of F	ront Axle	(63 ±4 inche	s allow ed)			
Y:	0.17	in	Left -	Right +	of Vehicle	e Centerli	ine		
Z:	29	in	Above Gre	ound	(minumum 28	3.0 inches a	llow ed)		
الممطالمنصلا	.1.	44.50	in ah a a	Frant D		a la t	0.5	5 0 7 F in a	مما
Hood Heigh		thes allowed	IIICH <del>e</del> S	FIORE	umper nei	grit.		<u>).373</u> IIIC	nes
Front Overhan	g:	36.00	inches	Rear B	umper Hei	ght:	29	9.125 inc	ches
	39 ±3 inc	ches allowed							
Overall Lengt									
	237 +13	inches allowe	d						

### Table E3. Exterior Crush Measurements for Test No. 490022-8.

Date:	2012-06-29	_ Test No.:	490022-8		VIN No.:	1DTHA18218J04150		
Year:	2008	_ Make:	Dodge		Model:	Ram 1500		
	,	VEHICLE C				EET <sup>1</sup>		
			Complete Whe	en Applicat	ole			
	End Da	ımage		Side Damage				
	Undeformed	d end width			Bowing: B1	X1		
	Corn	er shift: A1 _			B2	X2		
		A2						
	End shift at fran	me (CDC)		Bowing constant				
	(check or	ne)		X1 + X2 =				
		< 4 inches						
		$\geq$ 4 inches						
Note: M	Ieasure $C_1$ to $C_6$ from	Driver to Passe	nger side in Fi	ont or Rea	r impacts – F	Rear to Front in Side Impacts.		

	1 0	Direct I									
Specific Impact Number	Plane* of C-Measurements	Width** (CDC)	Max*** Crush	Field L**	$C_1$	$C_2$	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>	±D
							_				
Meas	urements not taken d										
			<u> </u>								

Table taken from National Accident Sampling System (NASS).

Free space value is defined as the distance between the baseline and the original body contour taken at the individual C locations. This may include the following: bumper lead, bumper taper, side protrusion, side taper, etc. Record the value for each C-measurement and maximum crush.

Note: Use as many lines/columns as necessary to describe each damage profile.

<sup>\*</sup>Identify the plane at which the C-measurements are taken (e.g., at bumper, above bumper, at sill, above sill, at beltline, etc.) or label adjustments (e.g., free space).

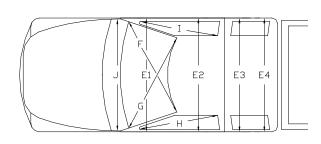
<sup>\*\*</sup>Measure and document on the vehicle diagram the beginning or end of the direct damage width and field L (e.g., side damage with respect to undamaged axle).

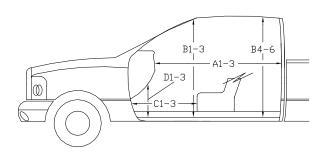
<sup>\*\*\*</sup>Measure and document on the vehicle diagram the location of the maximum crush.

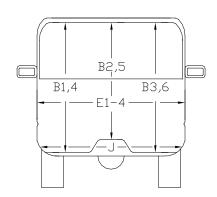
Table E4. Occupant Compartment Measurements for Test No. 490022-8.

Date: 2012-06-29 Test No.: 490022-8 VIN No.: 1DTHA18218J04150

Year: <u>2008</u> Make: <u>Dodge</u> Model: <u>Ram 1500</u>







\*Lateral area across the cab from driver's side kickpanel to passenger's side kickpanel.

### OCCUPANT COMPARTMENT DEFORMATION MEASUREMENT

A1       65.00       65.00         A2       64.50       64.50         A3       65.00       65.00         B1       45.50       45.50         B2       39.12       39.12         B3       45.50       45.50         B4       42.12       42.12         B5       42.62       42.62         B6       42.12       42.12         C1       29.00       29.00
A3       65.00       65.00         B1       45.50       45.50         B2       39.12       39.12         B3       45.50       45.50         B4       42.12       42.12         B5       42.62       42.62         B6       42.12       42.12
B1       45.50       45.50         B2       39.12       39.12         B3       45.50       45.50         B4       42.12       42.12         B5       42.62       42.62         B6       42.12       42.12
B2       39.12       39.12         B3       45.50       45.50         B4       42.12       42.12         B5       42.62       42.62         B6       42.12       42.12
B3       45.50       45.50         B4       42.12       42.12         B5       42.62       42.62         B6       42.12       42.12
B4       42.12       42.12         B5       42.62       42.62         B6       42.12       42.12
B5       42.62       42.62         B6       42.12       42.12
B6 42.12 42.12
<del></del>
C1 <u>29.00</u> <u>29.00</u>
C2
C3 <u>27.00</u> <u>27.00</u>
D1 12.88 12.88
D2
D3 <u>11.75</u> <u>11.75</u>
E1 62.75 62.50
E2 <u>64.50</u> <u>64.50</u>
E3 64.12 64.12
E4 64.12 64.12
F 60.00 60.00
G 60.00 60.00
H <u>39.00</u> <u>39.00</u>
I <u>39.00</u> <u>39.00</u>
J* 62.00 61.88

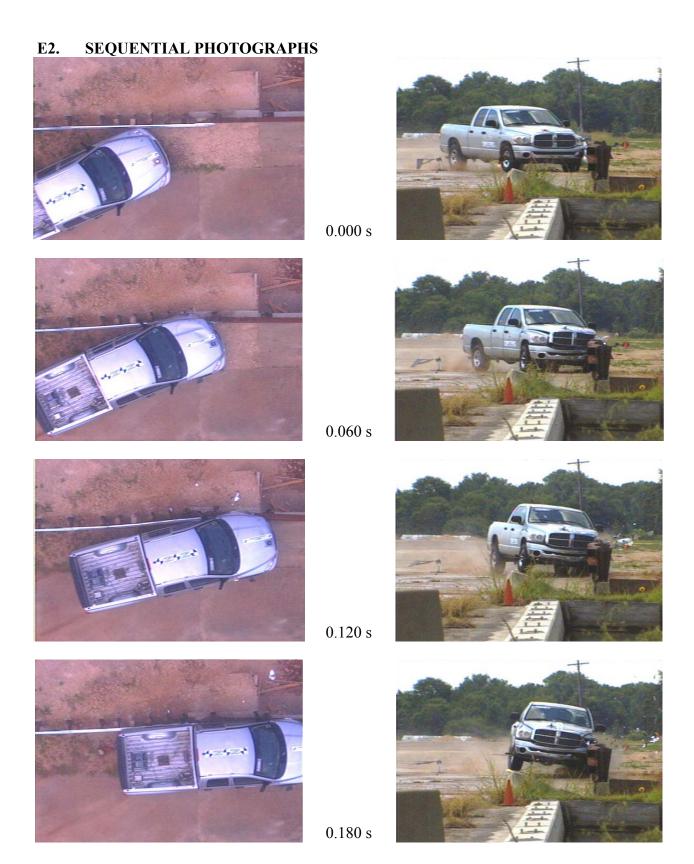


Figure E1. Sequential Photographs for Test No. 490022-8 (Overhead and Frontal Views).

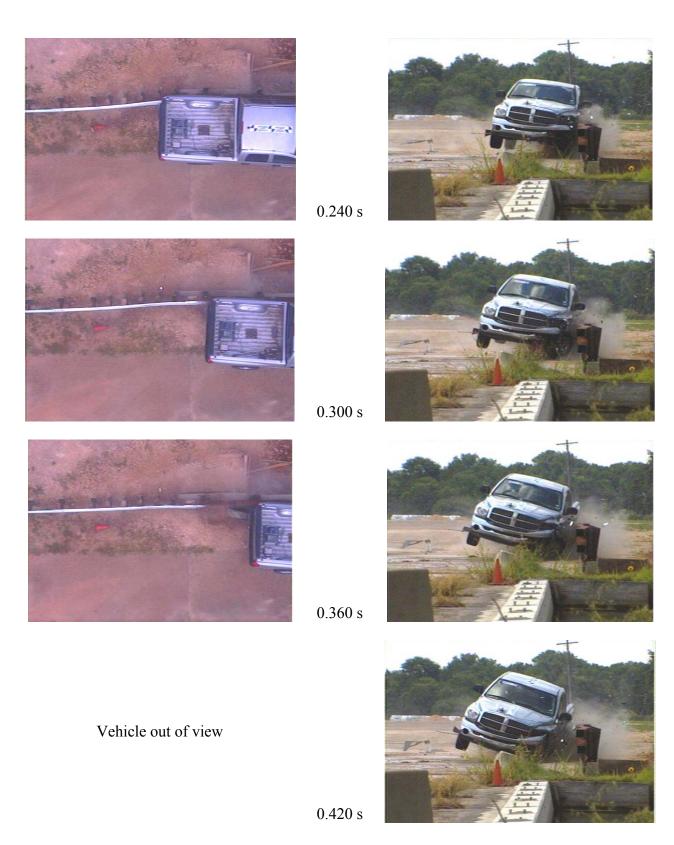


Figure E1. Sequential Photographs for Test No. 490022-8 (Overhead and Frontal Views) (continued).

## Axes are vehicle-fixed. Sequence for determining orientation: Yaw Pitch 0.1 8 -30 0 0 9 -10 4 8 8 20 Angles (degrees)

Figure E2. Vehicle Angular Displacements for Test No. 490022-8.

Yaw. Pitch. Roll.

Longitudinal Acceleration (G)

**VEHICLE ACCELERATIONS** 

E4.

# Figure E3. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-8 (Accelerometer Located at Center of Gravity).

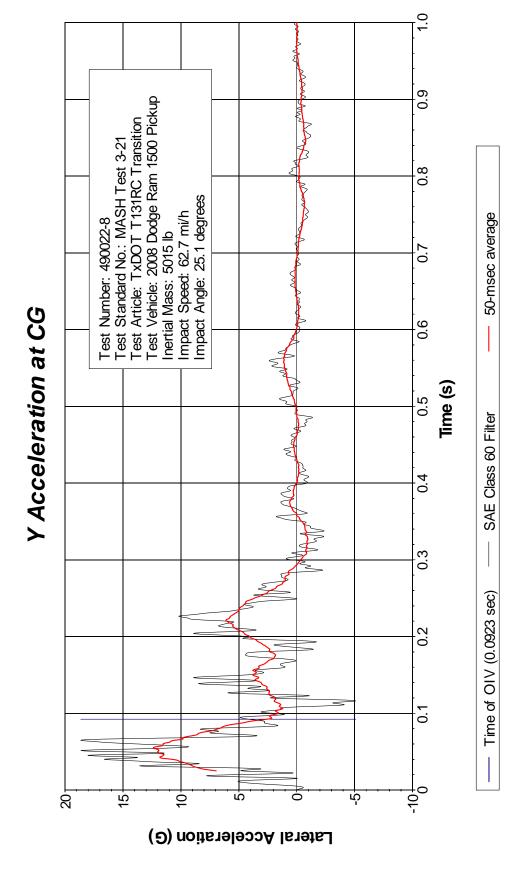


Figure E4. Vehicle Lateral Accelerometer Trace for Test No. 490022-8 (Accelerometer Located at Center of Gravity).

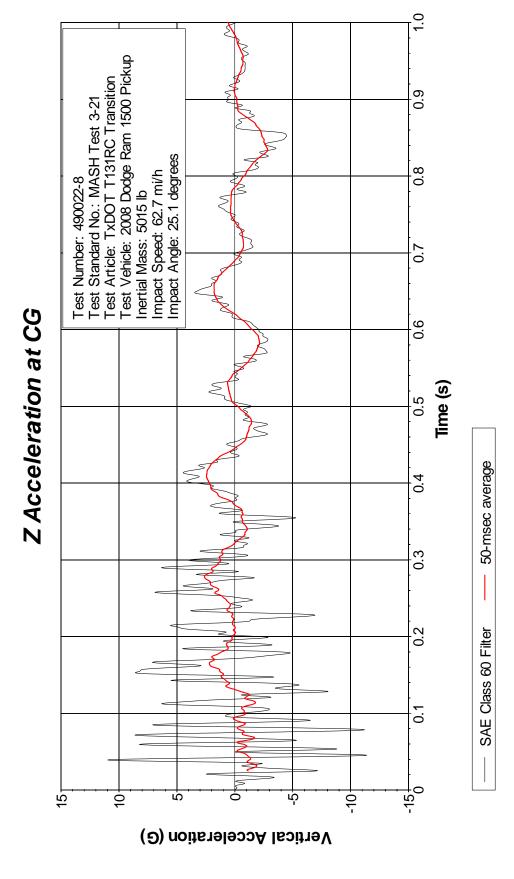


Figure E5. Vehicle Vertical Accelerometer Trace for Test No. 490022-8 (Accelerometer Located at Center of Gravity).

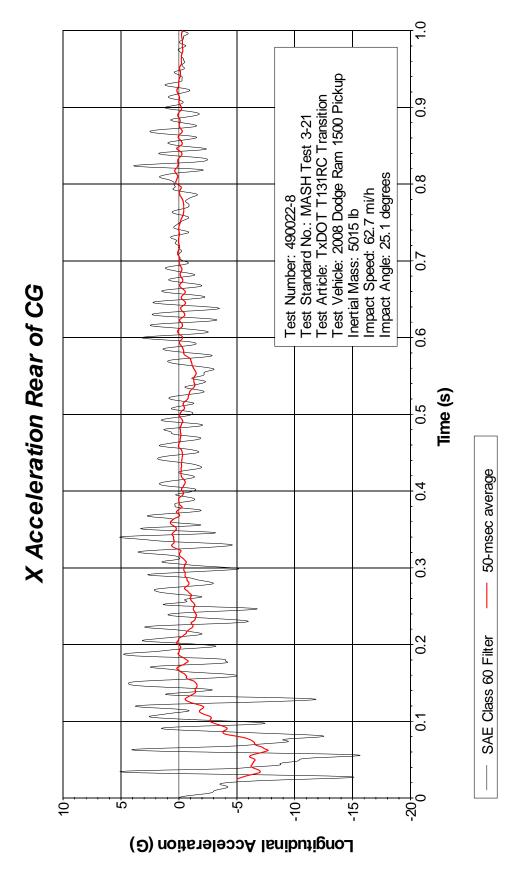


Figure E6. Vehicle Longitudinal Accelerometer Trace for Test No. 490022-8 (Accelerometer Located Rear of Center of Gravity).

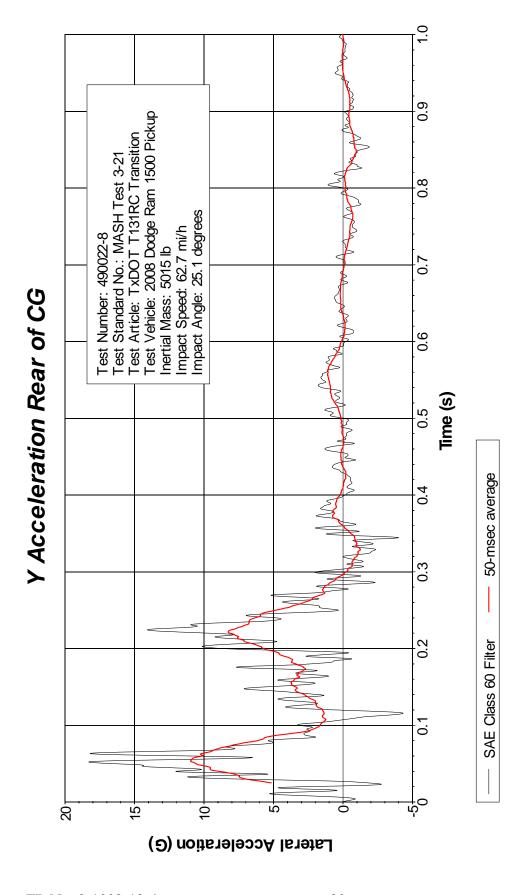


Figure E7. Vehicle Lateral Accelerometer Trace for Test No. 490022-8 (Accelerometer Located Rear of Center of Gravity).

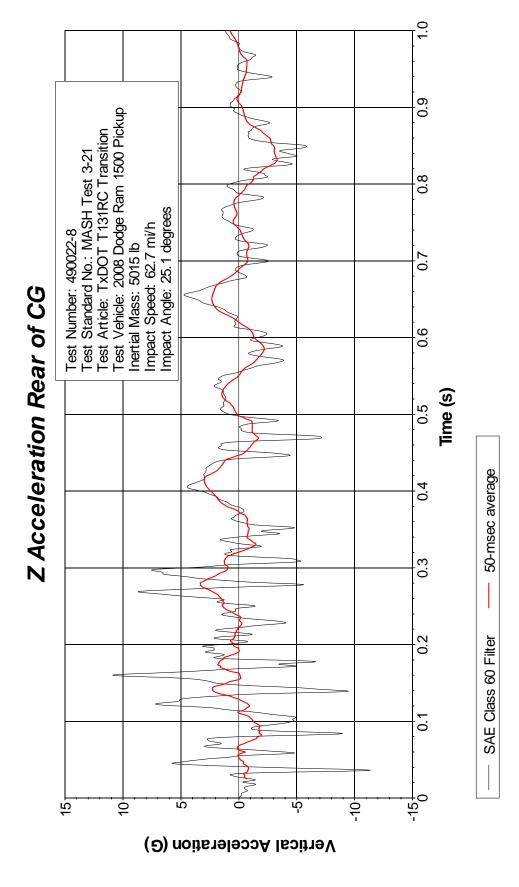


Figure E8. Vehicle Vertical Accelerometer Trace for Test No. 490022-8 (Accelerometer Located Rear of Center of Gravity).